

Spontaneous fracture of a titanium mesh cranioplasty implant in a child: A case report

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Abstract

BACKGROUND

Titanium mesh cranioplasty is often performed after decompressive craniectomy. Spontaneous fracture of the titanium prosthesis is an extremely rare postoperative complication. Here, we report a 10-year-old boy who presented with a spontaneous fracture of titanium mesh without antecedent head trauma.

CASE SUMMARY

A 10-year-old boy presented with a 1-wk history of a tender bulge over the left temporo-parieto-occipital scalp. He had undergone a temporo-parieto-occipital titanium mesh cranioplasty 26 mo previously. He denied antecedent head trauma. Computerized tomography disclosed a perpendicular fissure in the titanium mesh, suggesting a diagnosis of spontaneous titanium mesh fracture. He underwent a second temporo-parieto-occipital cranioplasty and made an uneventful recovery. Three-dimensional modeling and finite element analyses were used to explore potential risk factors of titanium mesh fracture.

CONCLUSION

We report a case of spontaneous fracture of a titanium mesh cranioplasty implant. The current case and literature review indicate that titanium mesh implants should be well-anchored to the base of bony defects to prevent fatigue-induced fractures.

Key Words: Cranioplasty; Prosthesis fracture; Spontaneous fracture; Titanium; Case report

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Core Tip: Titanium mesh cranioplasty is often indicated after decompressive craniectomy. We present a rare case of a spontaneous fracture of a titanium mesh cranioplasty implant in a 10-year-old boy. By conducting a literature review and finite element analysis, we learned that titanium mesh prosthetic implants should be well-anchored to the base of bony defects to prevent fatigue-induced fractures.

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INTRODUCTION

Titanium mesh is considered safe for implantation during cranioplasties in both adults and children[1-5], and is among the most commonly used biocompatible materials for calvarial fixation and reconstruction. Although titanium mesh cranioplasty is usually a straightforward surgical procedure, complication rates may reach 34% [6-10]. However, spontaneous fractures of titanium mesh cranioplasty implants are extremely rare. To our knowledge, only one case has been reported previously[11]. Here, we report a spontaneous fracture of titanium mesh without antecedent head trauma in a 10-year-old boy, and provide a literature review to investigate underlying mechanisms and risk factors.

CASE PRESENTATION

Chief complaints

A 10-year-old boy was admitted to our department with complaint of a tender bulge of the left temporo-parieto-occipital scalp of 1 wk duration.

History of present illness

The patient had undergone a temporo-parieto-occipital cranioplasty 26 mo previously. The patient denied antecedent trauma or intensive force to the head.

History of past illness

Three years previously, the patient fell from a height of 3 meters and sustained a closed head injury. He was brought immediately to an emergency department, where he was diagnosed with a left temporo-parieto-occipital laceration, skull fracture, epidural hematoma, and cerebral contusion. He underwent an emergent craniotomy to evacuate the epidural hematoma, followed by a large decompressive craniectomy of the temporo-parieto-occipital skull flap. He made marked clinical improvement and was readmitted to our department 12 mo later for cranioplasty. Computerized tomography (CT) showed a 10 cm × 8 cm bone defect of the left temporo-parieto-occipital skull with a local encephalocele (Figure 1A and B).

Personal and family history

The patient denied any significant personal or family medical histories.

Physical examination

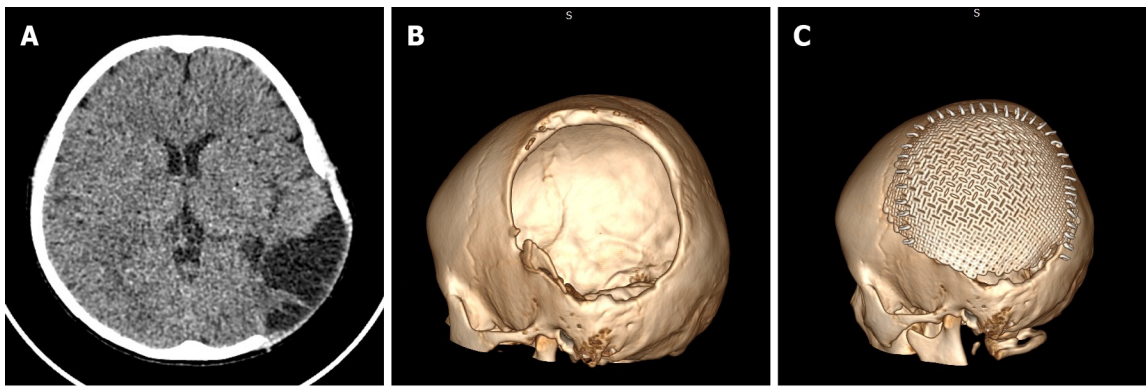
Physical examination disclosed a prominent 4 cm × 5 cm tender malformation of the temporo-parieto-occipital scalp.

Laboratory examinations

Results of routine blood and urine analyses were within normal limits.

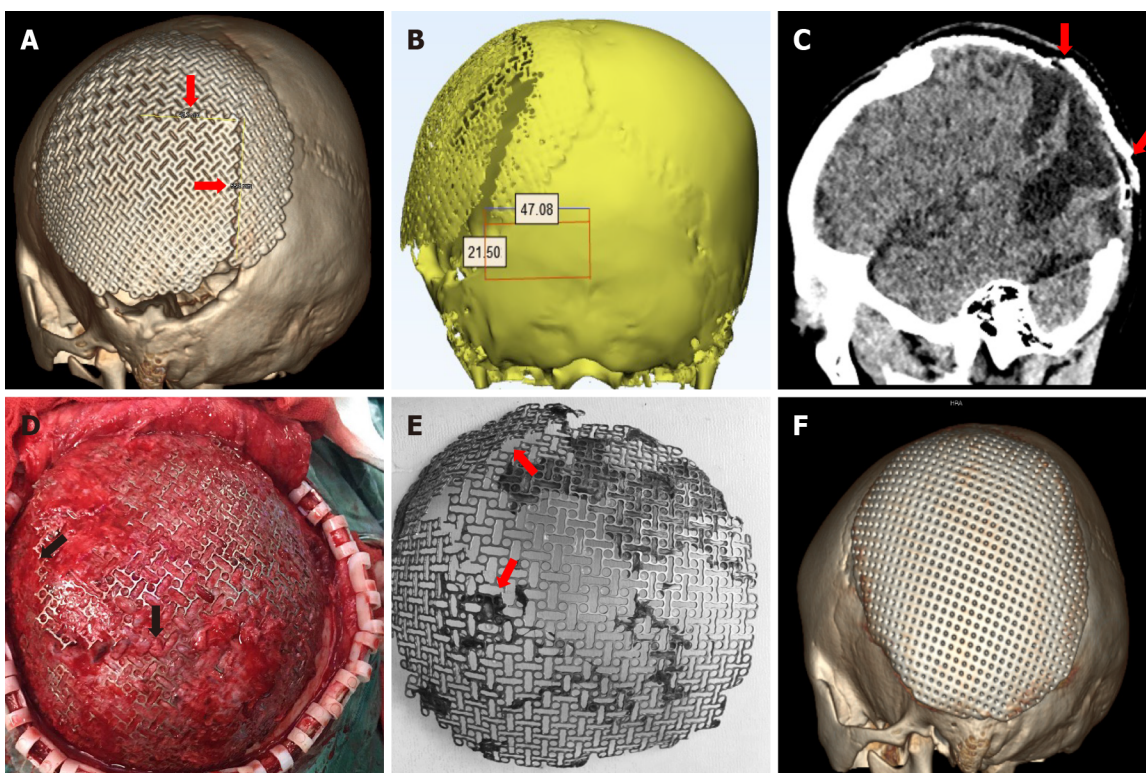
Imaging examinations

Three-dimensional (3-D) CT reconstruction displayed a clear edge of a titanium mesh fracture, which appeared as a reverse “L”-shaped fissure (Figure 2A-C) that originated from a point 2.21 cm superior to the external occipital protuberance and 4.51 cm left of the midline and extended 5.5 cm superiorly to the parietal bone and then turned anteriorly at a perpendicular angle (Figure 2A and B).



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Figure 1 Computerized tomography images before and after first cranioplasty. A: Axial computerized tomography (CT) image displayed the left temporo-parieto-occipital skull with local encephalocele; B: Three-dimensional (3-D) CT reconstruction revealing a 10 cm × 8 cm defect of the left temporo-parieto-occipital skull; C: 3-D CT reconstruction after first cranioplasty displaying an intact and ideally positioned prosthesis.



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Figure 2 Images before, during, and after second cranioplasty. A: Three-dimensional (3-D) computerized tomography (CT) reconstruction before the second cranioplasty displayed a reverse “L”-shaped fracture of the titanium mesh prosthesis; B and C: CT at the coronal and sagittal plane revealed the prosthetic fissure (red arrow); D: Intraoperative photograph showing the clear edge of the titanium mesh fracture; E: The fractured titanium mesh was removed during the second cranioplasty; F: 3-D CT reconstruction after the second cranioplasty disclosed an intact and ideally positioned implant.

FINAL DIAGNOSIS

The patient’s history, physical findings, laboratory examinations, and CT images were diagnostic of spontaneous fracture of the titanium mesh.

TREATMENT

A temporo-parieto-occipital cranioplasty was performed using a 0.8 mm titanium mesh. Temporal-occipital muscles were stripped from the dura, and the prosthesis was anchored to the base of the bony defect with titanium screws (Figure 2D and F). The temporal-occipital muscles were then fixed to the

prosthesis with nylon suture.

OUTCOME AND FOLLOW-UP

The patient was discharged in stable and asymptomatic condition on the 4th postoperative day.

DISCUSSION

Fractures of orthopedic titanium implants are not rare, especially among devices positioned in the spine and long bones, which are often subjected to weight loading[12-15]. Predisposing factors include: (1) Defective prosthetic material[16]; (2) Poor prosthetic design[17]; (3) Inadequate fixation[18]; (4) Deficient surgical technique[19]; (5) Skull growth; and (6) Biomechanical overload[11]. The titanium mesh used for our patient's first cranioplasty was patient-matched through computer-assisted design and manufacturing, and its quality was assured. Moreover, the patient did not suffer head trauma and the prosthesis was not subjected to weight loading. Therefore, the risks of defective material, poor design, and weight overloading were eliminated. Regarding fixation and surgical technique, the first titanium mesh was implanted by experienced neurosurgeons using a matched titanium screw fixator system. Thus, these two factors were also excluded, leaving the possibilities of pediatric growing fracture and biomechanical overload.

Growing skull fracture, a rare complication of pediatric head trauma, develops after linear fractures with underlying dural tears, and may cause brain herniation[20]. Our patient's dura was intact during the second reconstructive procedure. Hence, this possibility was also excluded. Therefore, the only remaining possibility was biomechanical overload. Jiang *et al*[11] reported a similar case in which head-pillow contact during sleep subjected the prosthesis to biomechanical overload. To explore whether head-pillow contact contributed to our patient's titanium mesh fracture, we performed a simple experiment using a skull model. We created a similar bony defect using a 3-D printed skull model and a plastic mesh to simulate the prosthesis (Figure 3). We fixed the plastic mesh to the model skull and rotated the model on a horizontal plate to simulate head rotation on a pillow (Figure 3A). Because the mesh was not anchored to the base of the bony defect, a remarkable stress line, originating from a point which was 2 cm superior to the protuberantia occipitalis externa and 4 cm left of the midline appeared as soon as the base of the mesh touched the plate (Figure 3B). The shearing force generated along the stress line may lead to fatigue, which could cause a linear fracture. However, this could not explain the reverse "L" rather than a linear configuration of our patient's fracture. We hypothesized that the stress line might change after dilaceration of a linear fracture. We incised the model mesh along the stress line and again rotated the model on a horizontal plate. This resulted in the emergence of a new perpendicular stress line on the mesh (Figure 3C). To further confirm our hypothesis, we invited Minggong Simulation Technology Co., Ltd to evaluate deformation and stress distributions using finite element analysis. We created a head-pillow contact scenario using a skull-implant assembly model and set the loading force at 50 N (gravitational force of the patient's head). As seen in Figure 4, finite element analysis showed a maximum stress of 42 MPa under a 50 N load on the head-pillow contact surface, which indicated that the skull-implant structure could bear the weight of the head under normal circumstances (Figure 4C). However, fatigue behavior analysis revealed that the titanium mesh might not tolerate cyclical loading (Figure 4D), implying that our patient's spontaneous titanium mesh fracture may have resulted from fatigue failure. Therefore, we selected a thickened titanium mesh and anchored it to the base of the bony defect during the second cranioplasty. Follow-up showed excellent results.

CONCLUSION

We report a case of spontaneous fracture of a titanium mesh cranioplasty implant. The current case and literature review indicate that titanium mesh prosthetics should be well-anchored to the base of bony defects to prevent fatigue-induced fractures.

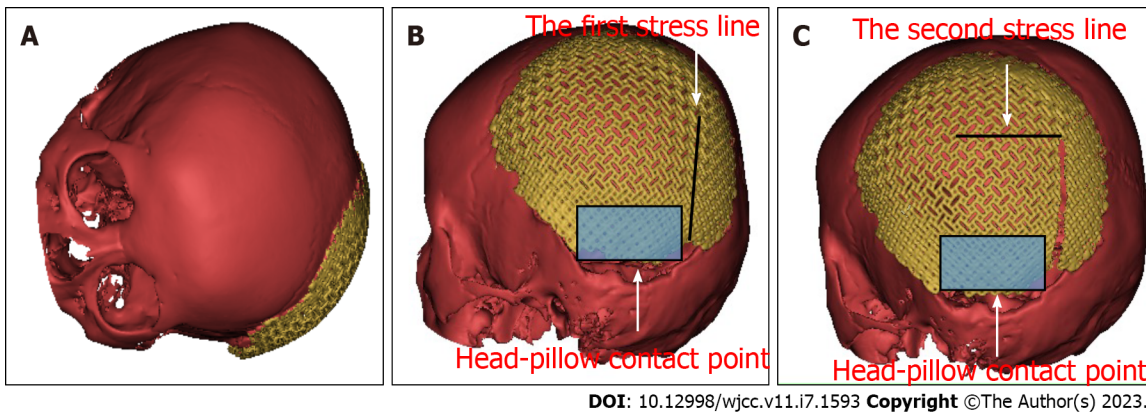


Figure 3 Three-dimensional model of skull-implant. A: Three-dimensional (3-D) printed skull model rotated on a horizontal plate simulated head rotation on a pillow; B and C: Force analysis model of head rotation on a pillow.

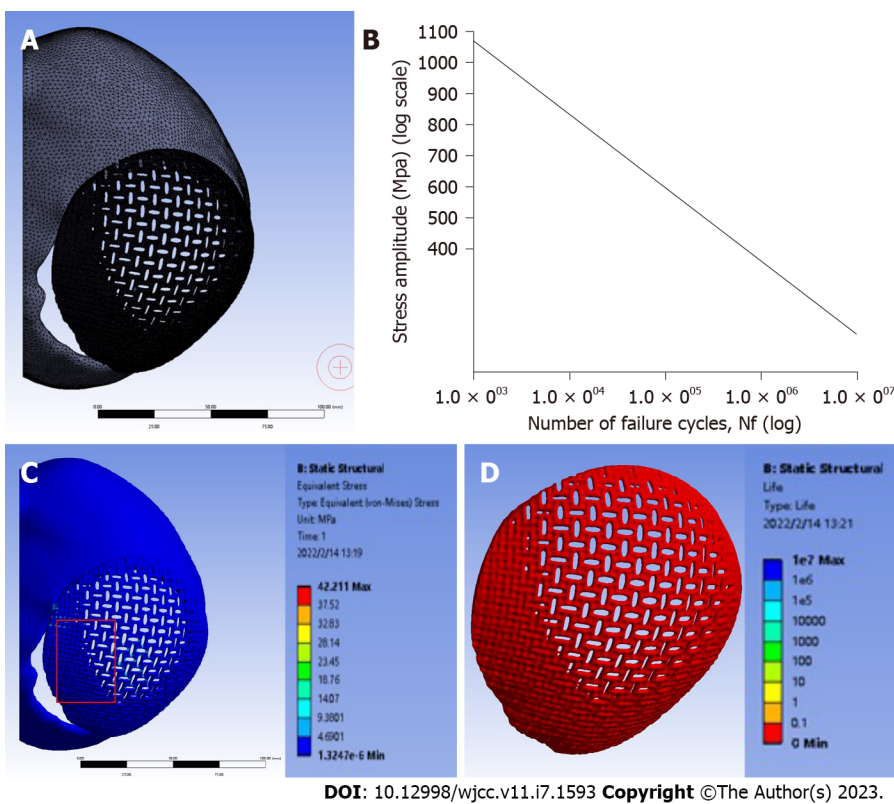


Figure 4 Finite element analysis model. A: Model of skull-implanted mesh; B: Stress life fatigue curve of the skull-implant model; C: Stress distribution analysis of the skull-implant model in contact with a pillow; D: Fatigue behavior analysis of the titanium mesh.

FOOTNOTES

Author contributions: He JP and Wang G contributed to the conception and design; Gao Z, Zhu YJ and Wang XF contributed to the acquisition of data; Zhang R drafted the article; All authors critically revised the article and reviewed submitted version of manuscript; He JP approved the final version of the manuscript on behalf of all authors.

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