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Flexible method for generating needle-shaped beams and its application in optical coherence tomography

JINGJING ZHAO¹, YONATAN WINETRAUB^{1,2,3,4}, LIN DU⁵, AIDAN VAN VLECK¹, KENZO ICHIMURA^{6,7,8}, CHENG HUANG⁹, SUMAIRA Z. AASI¹⁰, KAVITA Y. SARIN¹⁰, ADAM DE LA ZERDA^{1,2,3,4,11,*}

¹Department of Structural Biology, Stanford University School of Medicine, Stanford, California 94305, USA

²Biophysics Program at Stanford, Stanford, California 94305, USA

³Molecular Imaging Program at Stanford, Stanford, California 94305, USA

⁴The Bio-X Program, Stanford, California 94305, USA

⁵Department of Electrical and Systems Engineering, University of Pennsylvania, Philadelphia, Pennsylvania 19104, USA

⁶Division of Pulmonary, Allergy and Critical Care, Stanford University School of Medicine, Stanford, California 94305, USA

⁷Vera Moulton Wall Center of Pulmonary Vascular Disease, Stanford University School of Medicine, Stanford, California 94304, USA

⁸Cardiovascular Institute, Stanford University School of Medicine, Stanford, California 94304, USA

⁹Department of Biology, Stanford University, Stanford, California 94305, USA

¹⁰Department of Dermatology, Stanford University School of Medicine, Stanford, California 94305, USA

¹¹The Chan Zuckerberg Biohub, San Francisco, California 94158, USA

Abstract

Needle-shaped beams (NBs) featuring a long depth-of-focus (DOF) can drastically improve the resolution of microscopy systems. However, thus far, the implementation of a specific NB has been onerous due to the lack of a common, flexible generation method. Here we develop a spatially multiplexed phase pattern that creates many axially closely spaced foci as a universal platform for customizing various NBs, allowing flexible manipulations of beam length and diameter, uniform axial intensity, and sub-diffraction-limit beams. NBs designed via this method successfully extended the DOF of our optical coherence tomography (OCT) system. It revealed clear individual epidermal cells of the entire human epidermis, fine structures of human dermal-

*Corresponding author: adlz@stanford.edu.

Supplemental document. See Supplement 1 for supporting content.

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epidermal junction in a large depth range, and a high-resolution dynamic heartbeat of alive *Drosophila* larvae.

1. INTRODUCTION

The needle-shaped beam (NB) [1, 2] capable of maintaining high transverse resolution over a large depth-of-focus (DOF) has significant applications for microscopy systems regarding particle manipulation [3,4], materials processing [5], deep optics [6], photolithography [7], and data storage [8], as well as bioimaging such as fluorescence microscopy [9,10], photoacoustic microscopy [11,12], and optical coherence tomography (OCT) [13,14]. Although NBS can be generated via annular phase masks [15] and Bessel beams [16], there is still no simple, universal method for free manipulation of the beam length, diameter, and axial intensity distribution. We proposed a flexible and accurate method for generating NBs using a quasi-random spatially multiplexed phase mask. It controls the beam length and flattens the axial intensity profile by creating numerous foci at specific axial positions. The beam diameter is controlled by delicate manipulation of the phase shifts between adjacent foci (Section 2 and Section 3.A). Various NBs were successfully created, including a super long DOF beam [length = 167 Rayleigh lengths (RLs), diameter = 1.6 times diffraction limit], a long DOF beam (75 RLs, one diffraction limit), and a super resolution beam (50 RLs, 0.75 times diffraction limit).

OCT is a noninvasive and versatile tool for rapid two/three-dimensional (2D/3D) imaging in clinical diagnoses and scientific research, including ophthalmology [17], cardiology [18], dentistry [19], angiography [20], oncology [21], dermatology [22], and neuroscience [23]. OCT's axial resolution depends on the coherence length of the light source and remains constant along depth. Contrastingly, its transverse resolution, controlled by the focused beam profile, consists of a small DOF—a mere fraction of the OCT's depth range, especially when using a high numerical aperture (NA) lens. To address this issue, dynamic focusing [24,25] can be applied to axially translate the focus through the region of interest. However, this is time inefficient and infeasible for dynamic imaging. Other approaches attempt to extend the DOF: digital focusing, annular phase filters, Bessel beams, multibeam optics, multimode lasers, and tailored chromatic dispersion, which are distinct methods of DOF extension with unique benefits and drawbacks. Digital focusing [26,27] utilizes a light source with high phase stability throughout the entire imaging process. However, its resolution enhancement in dense samples like human skin is limited due to the large disparity between the spherical wavefront used in the refocusing model and the practical wavefronts highly disturbed by the sample itself. Annular phase filters [28,29] are tailored to the incident beam and are mainly used in OCT endoscopes, whose DOF gain is usually no more than five. A similar method is annular apodization by obstructing the center of the beam [30]. Bessel beams [31,32] can magnify DOF 10 times, but they suffer from low efficiency (the central mainlobe contains about 5% of the energy in our simulation), sidelobe artifacts, and axial-intensity oscillations [33]. Furthermore, additional optical paths are required to install the Bessel beam generator into OCT and locate the beam within the desired depth range. The multibeam method [34,35] uses several (e.g., four) beams focused at different depths for parallel imaging, significantly complicating the optical and electronic configurations. Its DOF magnification

and system complexity are both proportional to the number of the beams. Multimode lasers, [36] generated by a multimode fiber, are used to extend the DOF in the OCT endoscope with a high efficiency, but this results in a very nonuniform beam profile. Tailored chromatic dispersion of a lens [14,37] allows for a DOF gain around three. A computational method like computed tomography (CT) is developed to enhance lateral resolution by extending the superior axial resolution to the lateral dimension [38]. Reference [39] proposes a metasurface-based bijective illumination and collection imaging tool for high-resolution OCT, but it scans the sample by moving the sample holder rather than directly scanning the laser due to the structural restriction, leading to a low scanning speed. In summary, OCT needs a solution providing a large DOF gain, a uniform beam profile, fewer sidelobe artifacts, and good system compatibility. The NBs created by our method satisfy these requirements, as proved in the following experiments.

2. METHODS

A. Principle

The idea is to spatially multiplex a phase mask generating densely spaced foci along the axial direction, creating a NB. The phase profile of the objective fulfilling Abbe sine condition [40] is $P_{\text{Obj.}}(x, y, f) = 2\pi n \left[\sqrt{f^2 - (x^2 + y^2)} - f \right] / \lambda$ where (x, y) is the planar coordinate, λ is the free-space wavelength, f is the focal length in the medium, and n is the medium's diffractive index. The phase pattern

$$P_m(x, y, f_m, f) = [P_{\text{Obj.}}(x, y, f_m) - P_{\text{Obj.}}(x, y, f)], \quad (1)$$

placed at the back focal plane of the objective, can axially shift the focus from f to f_m (Supplement 1, Fig. S1. The $N \times N$ pixels of the phase mask are allocated equally into M groups. Each group is responsible for one shifted focus, formulated as $[P_m(x, y, f_m, f) - Pa_m] \times L_m(x, y)$ in Fig. 1 (a), where m is the focus index, Pa_m is a phase adjuster, $L_m(x, y)$ is a binary matrix whose value is either 1 or 0 to identify whether the pixel is allocated to the focus f_m , i.e., $L_m(x, y) = 1$ or not, i.e., $L_m(x, y) = 0$, and $\sum_{m=1}^M L_m(x, y)$ is $N \times N$ all-ones matrix. The final phase modulation for M foci respectively located at f_1, \dots, f_M is expressed in Eq. (2), with the schematic of Fig. 1 (b),

$$\begin{aligned} P(x, y, f, f_1, \dots, f_M, Pa_1, \dots, Pa_M) \\ = \sum_{m=1}^M \{ [P_{\text{Obj.}}(x, y, f_m) - P_{\text{Obj.}}(x, y, f)] - Pa_m \} \cdot L_m(x, y). \end{aligned} \quad (2)$$

An example of this allocation strategy is presented in Fig. 1 (c). Each contiguous 3×3 pixel set makes up one unit cell, which is randomly assigned to the nine foci. For example, the pixel labeled with f_1 means $L_1(x, y) = 1$ and $L_{m \neq 1}(x, y) = 0$. Since the unit cell area is tiny relative to the incident beam size, light distribution over one unit cell is even. Namely, the incident energy is naturally distributed uniformly over the foci. Another arrangement is that the positions of the pixels having a specific focus (e.g., f_1) in different unit cells are inconstant. It makes $L_m(x, y) = 1$ irregularly distributed over

the entire phase mask, having $FT[L_m(x, y)] = \delta(x, y)/M + BN(x, y) \approx \delta(x, y)/M$, where FT stands for Fourier transform, $\delta(x, y)$ is the unit impulse function, and $BN(x, y)$ is the random background noise with amplitudes far less than $1/M$ (Supplement 1, Fig. S2). Consequently, this quasi-random spatial multiplexing suppresses the higher-order diffraction (Supplement 1, Fig. S2), so there is no need for a pinhole spatial filter. In practice, the foci number can be huge (e.g., $M = 400$, with unit cell = 20×20 pixels). Supposing that the incident beam passing through the objective produces a focus $F(x, y, z, f)$, the phase mask $P(x, y, f, f_1, \dots, f_M, Pa_1, \dots, Pa_M)$ with the objective will lead to the output filled $O(x, y, z, f, f_1, \dots, f_M, Pa_1, \dots, Pa_M) = \sum_{m=1}^M \{ [F(x, y, z, f_m) \cdot \exp(-i \cdot Pa_m)] \otimes FT[L_m(x, y)] \}$. Given $FT[L_m(x, y)] \approx \delta(x, y)/M$, it has

$$\begin{aligned} O(x, y, z, f, f_1, \dots, f_M, Pa_1, \dots, Pa_M) \\ \approx \frac{1}{M} \cdot \sum_{m=1}^M [F(x, y, z, f_m) \cdot \exp(-i \cdot Pa_m)], \end{aligned} \quad (3)$$

indicating that M foci are produced at the expected axial locations of f_1, \dots, f_M to form a NB, Fig. 1 (d). Using an iterative algorithm (Supplement 1, Fig. S3), foci locations are optimized to flatten the axial intensity distribution. The basic idea of the algorithm is to adjust the spatial interval between every two adjacent foci according to their local intensity, linearly increasing the interval if the local intensity is larger than the average intensity of all the foci or decreasing it if lower. The initial positions of the foci are uniformly placed between f_1 and f_M with the constant interval of $(f_M - f_1)/(M - 1)$. With 12 loops of optimization iterations, the uniformity of the axial intensity is better than 95% in simulations.

B. Simulations

Two simulation methods were developed in this study. The first one, based on Eq. (3), provides an approximate model for rapid computation. The second is the Fourier transformation of Eq. (2), allowing accurate predictions of light distribution but requiring more computation time. According to our previous work [26], the focus function $F(x, y, z, f)$ in Eq. (3) is written as

$$\begin{aligned} F(x, y, z, f) = \frac{Ur}{W} \cdot \exp\left(-\frac{x^2 + y^2}{W^2}\right) \\ \cdot \exp\left[i\left(\frac{nkf}{2Rz}\rho^2 + kz - \arctan\frac{\Delta zf}{z_0 z}\right)\right. \\ \left.+ i\frac{nk}{2z}(x^2 + y^2) - i\frac{\pi}{2}\right], \end{aligned} \quad (4)$$

where U is the amplitude of the incident Gaussian beam, r is $1/e^2$ radius of the Gaussian beam, n is the refractive index of the surroundings (1.33 for water, 1 for air), $f = nf'$ is the objective focal length in the medium, f' is the equivalent focal length of the objective, λ is the light wavelength, $k = 2\pi/\lambda$ is the wavenumber, $\Delta z = z - f$, $W(\Delta z) = W_0 \left[(\Delta z/z_0)^2 + (z/f)^2 \right]^{0.5}$, $W_0 = \lambda f' / (\pi r)$, $z_0 = \pi n W_0^2 / \lambda$, and $R(\Delta z) = \Delta z \left[(z_0/\Delta z)^2 + (z/f)^2 \right]$. The analytic expression of Eq. (3) first optimized the axial

positions of the foci f_1, \dots, f_M , then scanned PA within the range of $[0, 2\pi]$ for the phase adjusters Pa_1, \dots, Pa_M ($Pa_m = PA \cdot m$ in this work), thereby quantifying the beam characteristics under different PA values, and selecting appropriate PA for a design. The phase adjusters shape the beam profile via modulating the optical interference among the foci, as illustrated by the simulations in Supplement 1, Figs. S4 and S5. With incident beam $G(x, y, r) = U \cdot \exp[-(x^2 + y^2)/r^2]$, the beam profile $O(x, y, z)$ described by the Fourier transform of Eq. (2) is given as Eq. (5). Centered on the above simulation models, the design flow chart is developed in Supplement 1, Fig. S6,

$$O(x, y, z) = \frac{\exp(inkz)}{i\lambda z/n} \exp\left[i\frac{nk}{2z}(x^2 + y^2)\right] FT\left\{G(x, y, r) \cdot \exp\left[-iP(x, y) + i\frac{nk}{2}(x^2 + y^2)\left(\frac{1}{z} - \frac{1}{f}\right)\right]\right\}. \quad (5)$$

C. Fabrication

The phase mask was created on a diffractive optical element (DOE) that was fabricated on a fused silica wafer via four rounds of lithography. The relationship between the phase modulation $P(x, y)$ and the height $H(x, y)$ of the DOE element is $P(x, y) = 2\pi(n_{\text{DOE}} - 1) \cdot H(x, y)/\lambda$, where n_{DOE} is the refractive index of the DOE material and λ is the wavelength. For fused silica, $n_{\text{DOE}} = 1.452$ at the wavelength of 910 nm, and the incremental thickness is 126 nm (equals $\pi/8$ in phase) for the 16 height levels. One DOE has 1024×1024 $10 \mu\text{m}$ pixels. The detailed fabrication procedure is shown in Supplement 1, Fig. S7. Figure 1(d) is the full view of DOE (VHX-6000, Keyence), and Fig. 1(e) is the scanning electron micrograph (Sigma FESEM, Zeiss) revealing the surface reliefs.

3. RESULTS

A. Beam Profiles

Our method's strength is the accurate and flexible modulation of the beam profiles. Beam length is determined by $(f_M - f_1)$, and we used $f_1 = f$ for all the NBs fabricated in this work. The average interval of the foci is maintained between $0.5 RL$ and RL for spatial continuity. RL stands for RL, which is $(\lambda/n)f^2/(\pi r^2)$ for an incident Gaussian beam with the radius r . The beam diameter is primarily regulated by the phase adjusters Pa_1, \dots, Pa_M . Here, we chose $Pa_m = PA \cdot m$ where m is the focus index $\in \{1, 2, \dots, M\}$ and PA is a coefficient $\in [0, 2\pi]$. Empirically, $0 < PA < 0.5\pi$ is the common range for NBs.

The beam profiles were measured using the setup shown in Supplement 1, Fig. S8(a) and S8(b). A $20\times$ water immersion objective coupled with different DOEs was used to focus a 910 nm Gaussian beam (4.6 mm diameter at $1/e^2$, $RL = 6 \mu\text{m}$). Referring to Supplement 1, Fig. S8(c), the cross section through the middle of the NBs and focused Gaussian beam were taken out to calculate the efficiency and sidelobe ratio. The efficiency is the ratio of the energy enclosed within the NB's central mainlobe to the energy of the Gaussian spot (focused by the same objective used for the NB). The sidelobe ratio of NB is the peak intensity ratio between the first sidelobe and the central mainlobe. The NBs in Figs.

2(a)–2(g) are 300 μm long, containing 81 foci, with various diameters due to different values of PA . The full width at half-maximum diameters of the two NBs in Fig. 2(a) are 3 μm ($PA = 0.040\pi$) and 1.2 μm ($PA = 0.222\pi$), respectively. Correspondingly, the Gaussian beam focal size is 1.6 μm , and the diameter increases to 21 μm at $z = 150 \mu\text{m}$. Notably, 300 $\mu\text{m} \times 1.2 \mu\text{m}$ (length \times diameter) NB features not only a DOF as long as 50-fold RLs but also a diameter smaller than the diffraction limit. Generally, this kind of long DOF super-resolution beam requires radially or azimuthally polarized lights [15,41,42], but here it was using the laser directly from a single-mode fiber without polarization control. The two NBs only present sidelobes around the middle of the beam. Their real profiles are congruent with the theoretical simulations (Supplement 1, Fig. S9), including the expected diameters in Fig. 2(b) and axial intensities in Fig. 2(c). The axial intensity fluctuation of 300 $\mu\text{m} \times 3 \mu\text{m}$ NB is less than 10%. There is a peak at the left end of 300 $\mu\text{m} \times 1.2 \mu\text{m}$ NB because fabrication errors allocate extra energy to the objective's native focus (coincides with the NB left end) and the induced intensity increase is comparable to the weak intensity of 300 $\mu\text{m} \times 1.2 \mu\text{m}$ NB (the same phenomena occur with the other narrow NBs listed in Supplement 1, Figs. S10 and S11). Seven 300 μm NBS with the diameters of 1.2 μm , 1.5 μm , 2 μm , 3 μm , 4 μm , 5 μm , and 6.5 μm were achieved (Supplement 1, Fig. S10), proving that the diameter is precisely regulated by PA in Fig. 2(d). As illustrated in 2(d)–2(g), increasing PA has several effects on beam characteristics: the beam diameter decreases, intensity and efficiency first increase then decrease, and sidelobe ratio will first increase then show some pseudo-periodic fluctuations. When $PA = 0.028\pi$, the maximum sidelobe ratio is no more than 10%, and the efficiency is between 9% and 22%. When $PA = 0.040\pi$, the sidelobe ratio fluctuates between 15% and 20%, with an efficiency below 5%. Energy efficiency is also inversely affected by beam length BL . Figure 2(h) shows one example, where PA is set at zero and the efficiency approximates $[0.145(BL - 2RL)/RL + 1]^{-1}$.

Various NBS were generated by adjusting f_1, \dots, f_M and Pa_1, \dots, Pa_M (Supplement 1, Fig. S11). In Fig. 2(i), the 450 $\mu\text{m} \times 1.5 \mu\text{m}$ NB (100 foci, $PA = 0.190\pi$) extends the DOF to 75-fold RLs and has a diameter equal to the Gaussian focal spot size, 600 $\mu\text{m} \times 2 \mu\text{m}$ NB (144 foci, $PA = 0.104\pi$) and 1000 $\mu\text{m} \times 2.5 \mu\text{m}$ NB (196 foci, $PA = 0.129\pi$) own the DOFs up to 100-fold and 167-fold RLs. The 80 $\mu\text{m} \times 1.5 \mu\text{m}$ NB (16 foci, $PA = 0.210\pi$) is relatively short (13-fold RLs) but has a strong intensity equating to 12% of the Gaussian focal intensity and an axial intensity uniformity better than 90%. The dry lens was also able to cooperate with DOEs for NBs (Supplement 1, Fig. S12).

B. Needle-Shaped Beams in OCT

Our system (Supplement 1, Fig. S13) is a remodeled commercial OCT with a 910 ± 100 nm light source and a $20\times$ water immersion objective. Basically, the OCT signal intensity is proportional to the DOE efficiency (Supplement 1, Table S1). The focused Gaussian beam, 80 $\mu\text{m} \times 1.5 \mu\text{m}$ NB, and 300 $\mu\text{m} \times 3 \mu\text{m}$ NB developed in Fig. 2 were tested with 0.8 μm polystyrene (PS) beads embedded in degassed ultrasound gel. In the B-scan image generated by the Gaussian beam, Fig. 3(a), although the individual beads within the depth range marked by the red double-arrow line are recognizable, only the beads close to the focal plane are profiled without resolution loss due to the short 12 μm DOF (two RLs). 80 $\mu\text{m} \times 1.5 \mu\text{m}$ NB and 300 $\mu\text{m} \times 3 \mu\text{m}$ NB have DOFs of 80 μm and 300 μm , respectively. Figure 3(b)

shows XY planes at five depths (successive XY images with 20 μm depth interval are in Supplement 1, Fig. S14). At $z = 0$, all three beams can distinguish single beads clearly. At $z = 40 \mu\text{m}$, bead profiles captured by the Gaussian beam enlarge significantly, while 80 μm and 300 μm NBs maintain their resolutions. At $z = -40 \mu\text{m}$, Gaussian beam bead profiles deform significantly, but 80 μm and 300 μm NBs retain clarity. At $z = \pm 150 \mu\text{m}$, only the 300 μm NB provides high-quality images. Bead diameters were measured in Fig. 3(c) to evaluate resolutions. The Gaussian beam maintains its lateral resolution at 1.6 μm from $z = -5 \mu\text{m}$ to $z = 6 \mu\text{m}$. Contrastingly, the 80 μm NB maintains resolution around 1.6 μm from $z = -42 \mu\text{m}$ to $z = 46 \mu\text{m}$, a DOF 8 times that of the Gaussian beam. Additionally, the 300 μm NB has a resolution of 2.3–2.7 μm from $z = -160 \mu\text{m}$ to $z = 160 \mu\text{m}$. Since the Gaussian beam outperforms 300 μm NB from $z = -12 \mu\text{m}$ to $z = 19 \mu\text{m}$, the 300 μm NB's DOF magnification is 10. The peak-to-background ratios (PBRs) along depth and the signal-to-noise ratios (SNRs) in the 3D beam images are shown in Figs. 3(d) and 3(e). Here, $\text{PBR} = (\text{peak intensity} - \text{average background intensity}) \div \text{average background intensity}$, and $\text{SNR} = (\text{peak intensity} - \text{average background intensity}) \div \text{standard deviation of background intensity}$. It shows that the contrast and sensitivity keep basically constant within the entire DOF of every NB. And in some depths, the NBs outperform the focused Gaussian beam in terms of contrast and sensitivity.

Since the NB energy is axially distributed rather than focused at one point, NB maximum contrast is lower. For example, at $z = 0$ in Fig. 3(b), with the same input power, the contrast ratio between the Gaussian beam, 80 μm NB, and 300 μm NB is 9:1:0.5 (close to the efficiency ratio = 8.3:1:0.33). The direct method to enhance contrast is to increase the input power. Another concern of NBs is sidelobes. In Fig. 3(b), the sidelobe ratio of the 80 μm NB is 19% at $z = 0$; the ratio of 300 μm NB is 5% at $z = -40 \mu\text{m}$, 12% at $z = 0$, and 9% at $z = 40 \mu\text{m}$. Despite sidelobe effects, the boundary between two closely adjacent beads (red arrow) is dark and clear, indicating that the sidelobe is more sensitive to un-uniform structures than the central lobe. Similar results are observed in Supplement 1, Fig. S14. The adverse effect of sidelobes can be limited in the dense bio-samples, just as proved in the following experiments.

C. Skin Imaging

OCT is a promising tool for noninvasive visual biopsy in dermatology [43,44]. The first sample was taken from a man (62 years old, left jawline, healthy) and imaged by Gaussian beam (20 \times lens) and 300 $\mu\text{m} \times 3 \mu\text{m}$ NB. Although the sample has an uneven surface, all features on the exterior are contained within the 300 μm NB DOF and appear clearly in Fig. 4(a). Supplement 1, Fig. S15 contrasts the surface projections of the Gaussian beam and the 300 μm NB, showing the NB's clarity over the entire field-of-view (FOV) compared to the Gaussian beam's blurry and dark regions. Gaussian beam B-scans of the dermal-epidermal junction in Fig. 4(b) show loss of resolution in deeper regions (blue arrows), compared to the 300 μm NB's images. It is medically meaningful to precisely determine the dermal-epidermal junction, which is a location approximating that of malignant skin tumor formation [45]. In XY images at 250 μm depth, Fig. 4(c), sample boundaries as well as the interface between dermis and epidermis are clear with 300 μm NB. Contrastingly, in Gaussian beam imaging, the same features are barely recognizable and sometimes invisible

(red arrows). Both resolution and contrast are superior with the NB; in Fig. 4(c), the maximum contrast of 300 μm NB is 14, it is only 4 for Gaussian beam, and the gap widths are 35 μm and 10 μm in the regions indicated with dashed red lines, respectively.

The second sample (69-year-old woman, cheek, healthy) was used for observing epidermal cells. The 80 μm x 1.5 μm NB was selected since it would allow cellular resolution through the sample's ~ 80 μm epidermal layer [46]. The Gaussian beam was focused at $z = 90$ μm . Its 3D image of Fig. 5(a) shows a bright, narrow layer (red double-arrow line) caused by the short DOF. Cells outside this focus were blurry (red ellipse). 80 μm NB in Fig. 5(b) profiled cells clearly with uniform image quality through the epidermis. In XY images, Figs. 5(c) and 5(d), at $z = 90$ μm , the Gaussian beam and 80 μm NB generated comparable images with coincident cells (e.g., ones in red circles). For other depths, the cells in Gaussian beam imaging became hazier (e.g., yellow ellipses) and even disappeared entirely (e.g., blue ellipses) while the 80 μm NB reliably discerned cells. Supplement 1, Fig. S16 shows the 80 μm NB generated XY images are coincident with the all-in-focus images from $z = 20$ μm to $z = 100$ μm , whereas the reliable range of the Gaussian beam only spans from $z = 80$ μm to $z = 100$ μm . NB allows for cellular-level resolution through a deep DOF. The increased resolution of NB could be incredibly powerful for virtual skin cancer biopsies, particularly for melanoma detection.

D. Dynamic Imaging of *Drosophila* Larva

Dynamic imaging of a heartbeat [47], digestive system [48], muscle motion [49], etc. in *Drosophila* larva, a common animal model, is necessary in biomedical research. A Gaussian beam focused by a 10 \times dry objective (LSM02-BB, Thorlabs) and a 700 μm NB were applied (Supplement 1, Fig. S17). In the first and second sections of Visualization 1, distinct profiles of a beating heart, digestive organs, and muscles in a *Drosophila* larva were simultaneously acquired with the 700 μm NB, with easily distinguishable walls and the lumen of the heart and the gut. Simultaneous imaging across such depth was impossible with the Gaussian beam. Similarly, in the third section of Visualization 1, the heartbeat and gut movement in a wriggling larva were observed clearly by 700 μm NB, while Gaussian beam images became blurred when they moved out of its narrower DOF. In this axial view, we saw movement of the heart valve within the heart tube that was invisible with a Gaussian beam.

4. DISCUSSION AND CONCLUSION

Our novel approach for the generation of NBS presents the following advantages. The first advantage is the high flexibility in manipulating the beam diameter and length. The quasi-random spatial multiplexing of the phase mask provides a straightforward platform for creating NBS, which determines the beam properties via placing axial foci and adjusting the phase shifts among the foci. Second, our approach offers uniform axial energy distribution. Traditionally, flattening the axial intensities of a beam with an extended DOF requires both the phase and amplitude modulation of the incident beam [50]. Our approach achieves this by optimizing the foci positions without amplitude modulation, resulting in 10–20% axial uniformity fluctuation in most cases. Finally, this method offers simple and straightforward system compatibility. Our phase mask can be directly placed just above the objective,

as shown in Supplement 1, Fig. S18 (other experiments utilized the configuration in Supplement 1, Fig. S13 to allow the addition and removal of DOEs frequently in order to compare the NB and Gaussian beam without changing the relative location between the objective and the sample). Contrastingly, optical systems must be specially modified for usage of a Bessel beam.

Our NB platform can be further improved in three aspects. First, complete utilization of the design freedom offered by the phase adjusters Pa_1, \dots, Pa_M . In this study, we set $Pa_m = PA \cdot m$ and only adjusted PA due to computational costs. Superior performance will be obtained by delicately selecting each phase adjuster for every single focus without the restriction of $Pa_m = P \cdot m$. Furthermore, currently, we first optimize the foci positions f_1, \dots, f_M and then determine the value of PA (Supplement 1, Fig. S6). If we can find a high-efficient algorithm to simultaneously optimize f_1, \dots, f_M and Pa_1, \dots, Pa_M , it should shape a NB more arbitrarily. Second, reducing pixel size to subwavelength levels decreases the differences between the real beam and the designed beam, increasing efficiency [51]. Furthermore, NB can be directly generated by a single metalens [52–54] whose phase is $P(x, y, f, f_1, \dots, f_M, Pa_1, \dots, Pa_M) = \sum_{m=1}^M \{ [P_{\text{Obj.}}(x, y, f_m) - Pa_m] \cdot L_m(x, y) \}$, referring to Eq. (1) and Eq. (2). Third, self-apodization methods [1] can be introduced to reduce sidelobes, and radially polarization [14] will contribute to the efficiency.

In summary, this work invented a common and flexible platform for the generation of NBs and had successfully applied it for OCT imaging, achieving cellular resolution of the entire human epidermis layer, fine structures of the human dermal-epidermal junction in a large depth range, and high-resolution dynamic imaging of alive *Drosophila* larvae. Our NBS will also be able to improve the resolution of other microscopy systems regarding particle manipulation, materials processing, confocal microscopy [55], photolithography, photoacoustic tomography, etc.

Supplementary Material

Refer to Web version on PubMed Central for supplementary material.

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Data availability.

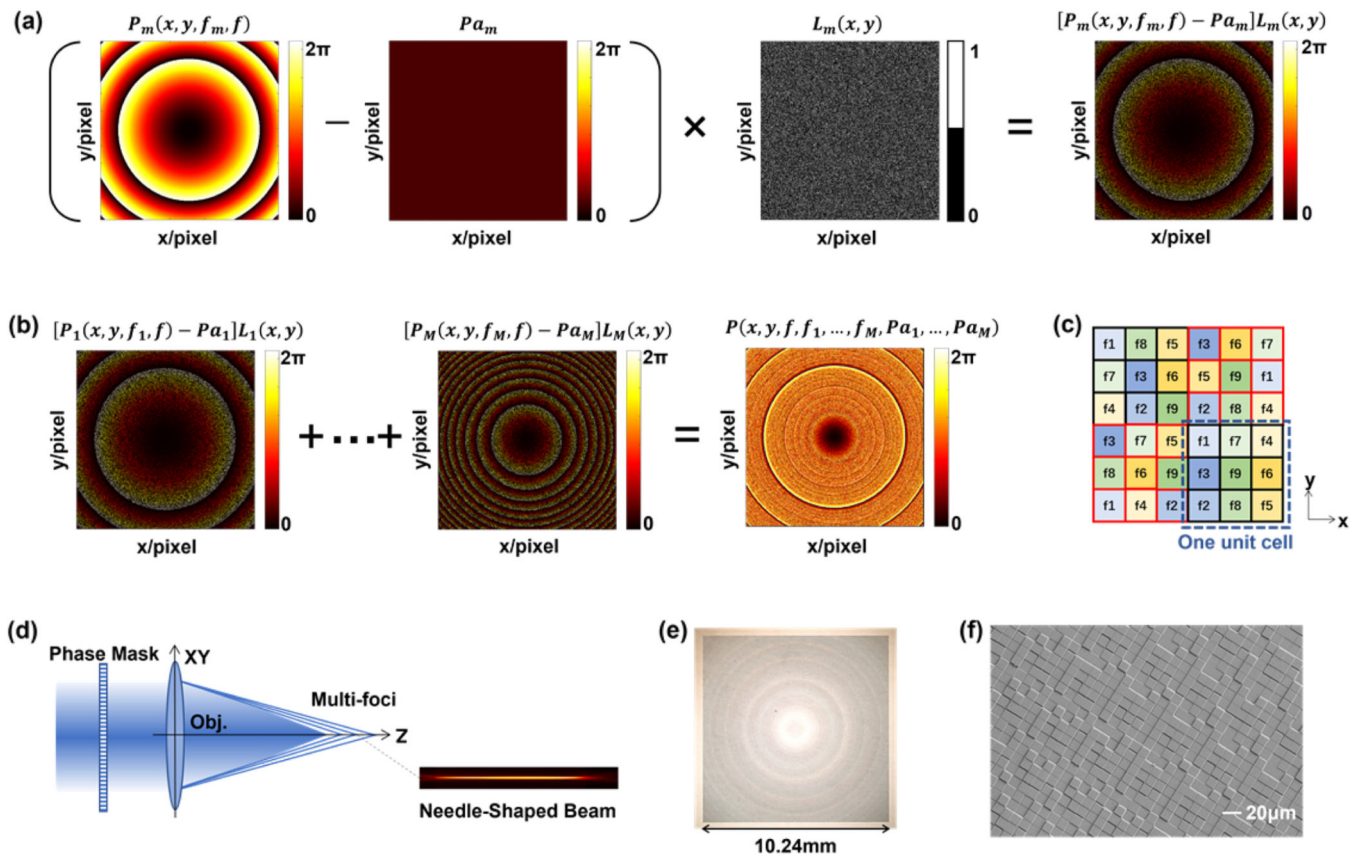
Data underlying the results presented in this paper are not publicly available at this time but may be obtained from the authors upon reasonable request.

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**Fig. 1.**

Principle. (a) Phase pattern P_m shifts the focus from f to f_m , P_{a_m} is a phase adjuster whose functionality is discussed in Section 2.B and Figs. 2(d)–2(g), binary pattern L_m selects the pixels for P_m , and the combination $(P_m - P_{a_m})L_m$ produces a focus at f_m . (b) The pixels are divided to M groups to convey the phase patterns $(P_1 - P_{a_1})L_1, \dots, (P_M - P_{a_M})L_M$; thus, the phase mask P has M foci positioned at f_1, \dots, f_M . (c) Simple example of nine foci to explain how to allocate the pixels to different foci. Unit cells comprise 3×3 pixel grids, with each of the nine pixels being randomly assigned one of the nine foci. (d) The spatial multiplexed phase mask with an objective creates densely spaced foci to form a needle-shaped beam. (e) Optical photograph of the phase mask (diffractive optical element) and (f) its scanning electron micrograph.

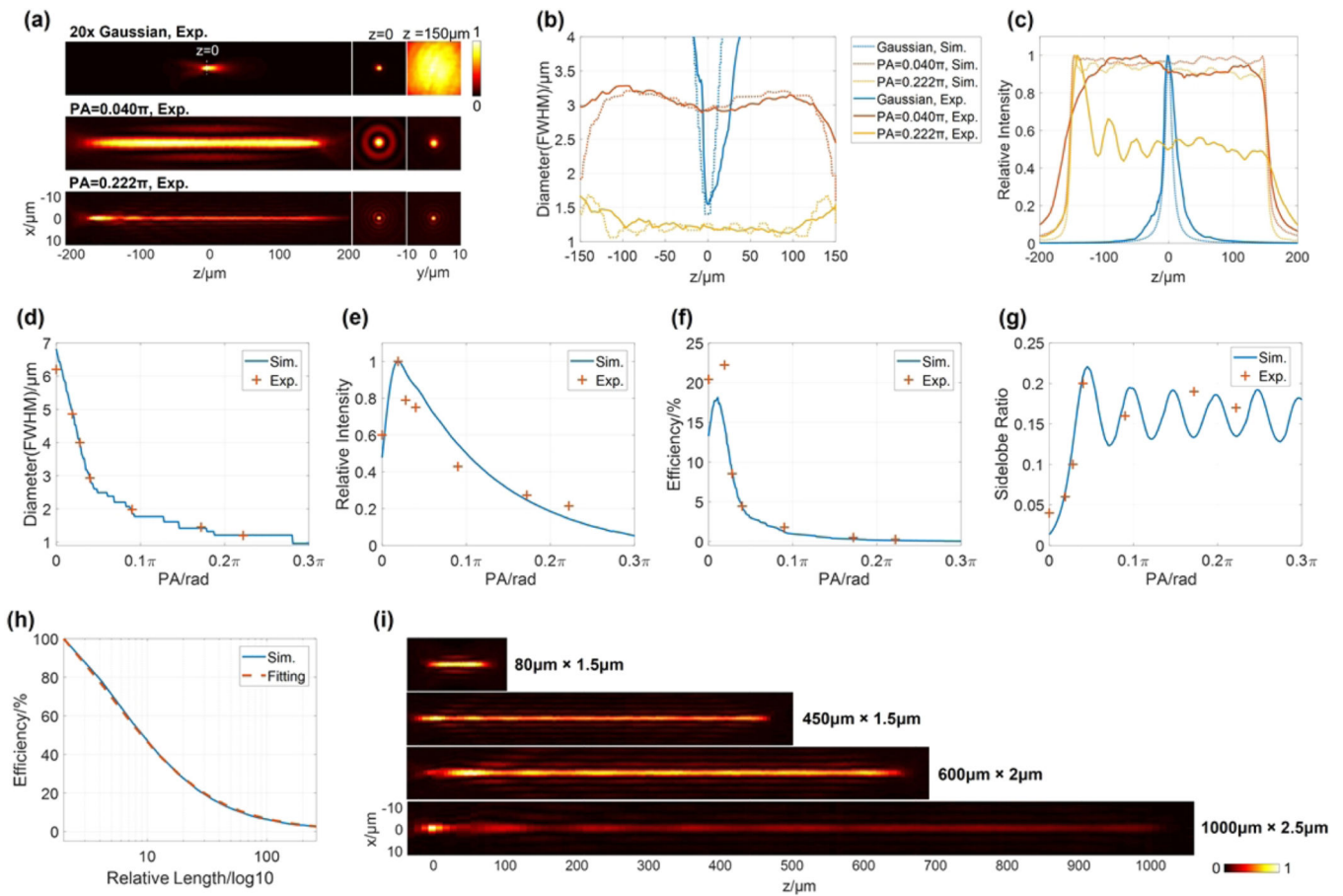


Fig. 2.

Beam profiles. (a) Profiles of the Gaussian beam (20 \times lens) and two 300 μm NBs with the phase adjusters of $Pa_m = 0.040\pi \cdot m$ and $0.222\pi \cdot m$. $Pa_m = PA \cdot m$ and the focus index $m \in \{1, 2, \dots, 81\}$. (b) Experimental and simulated diameter profiles of the three beams are congruent; (c) shows their axial intensity distributions. The effects of PA on seven 300 μm NBs' (d) beam diameter, (e) beam intensity, (f) beam efficiency, and (g) sidelobe ratio at the middle of a NB. (h) Simulation where $PA = 0$, proving beam efficiency is inversely proportional to the beam length (BL). Its fitting curve is $(0.145rL + 1)^{-1}$, and $rL = (BL - 2RL)/RL$ is the relative length. (i) Other NBs generated by the same 20 \times objective and incident Gaussian beam. NB, needle-shaped beam; Sim., simulated; Exp., experimental; RL, Raleigh length; FWHM, full width at half-maximum.

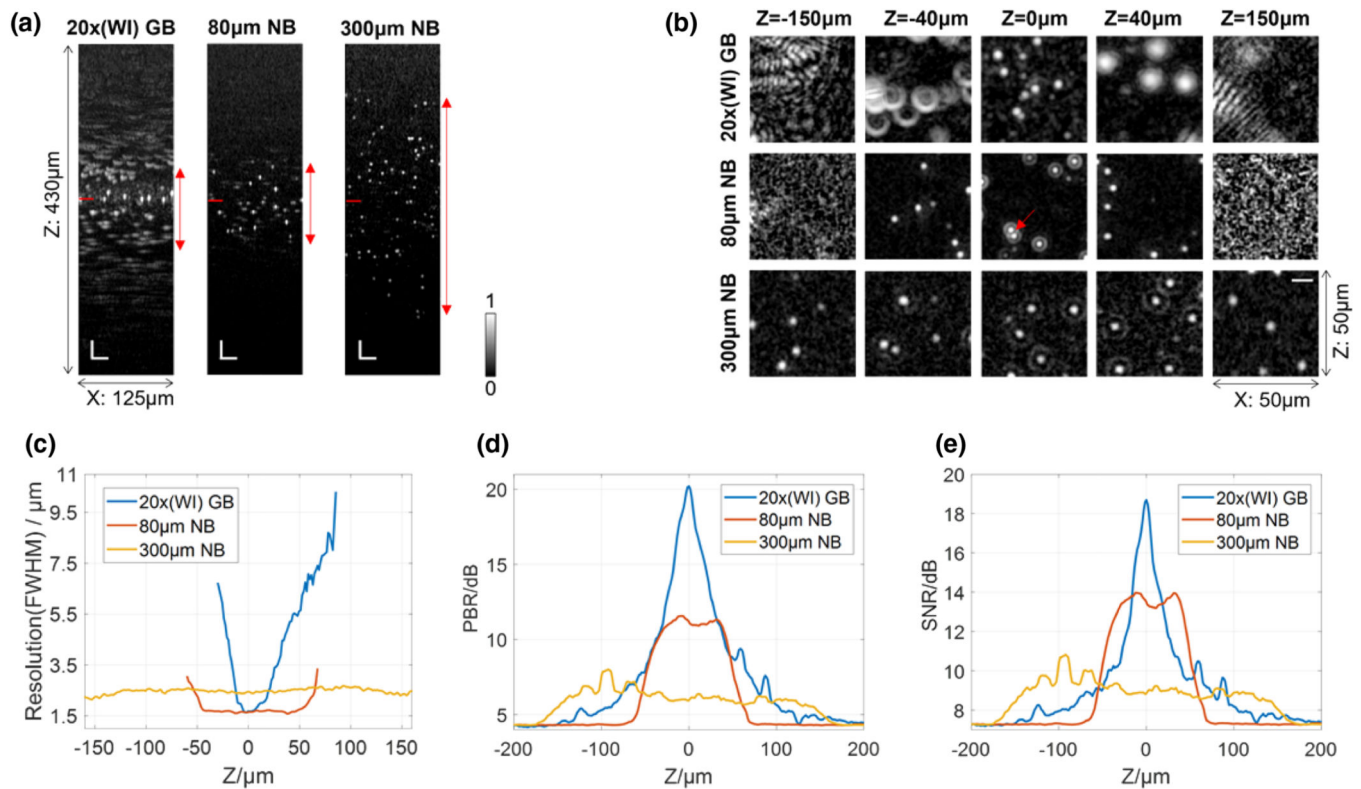


Fig. 3. OCT images of $0.8 \mu\text{m}$ microbeads. The focused Gaussian beam ($20\times$ objective), $80 \mu\text{m} \times 1.5 \mu\text{m}$ NB, and $300 \mu\text{m} \times 3 \mu\text{m}$ NB are compared. (a) B-scan images where position $z = 0$ is marked by short red lines. White scale bars at bottom left corners, $25 \mu\text{m}$. (b) XY planes at five depths. A red arrow identifies two closely adjacent beads, whose boundary is distinguishable even under the effect of the sidelobes. White scale bar in the last sub-image, $10 \mu\text{m}$. (c) Lateral resolutions measured from bead sizes. The Gaussian beam's plot begins at $-30 \mu\text{m}$ and ends at $85 \mu\text{m}$ —outside this range, beads are barely recognizable. (d) Peak-to-background ratios (PBRs) along depth and (e) the signal-to-noise ratios (SNRs) in the bead images. GB, Gaussian beam; NB, needle-shaped beam; WI, water immersion.

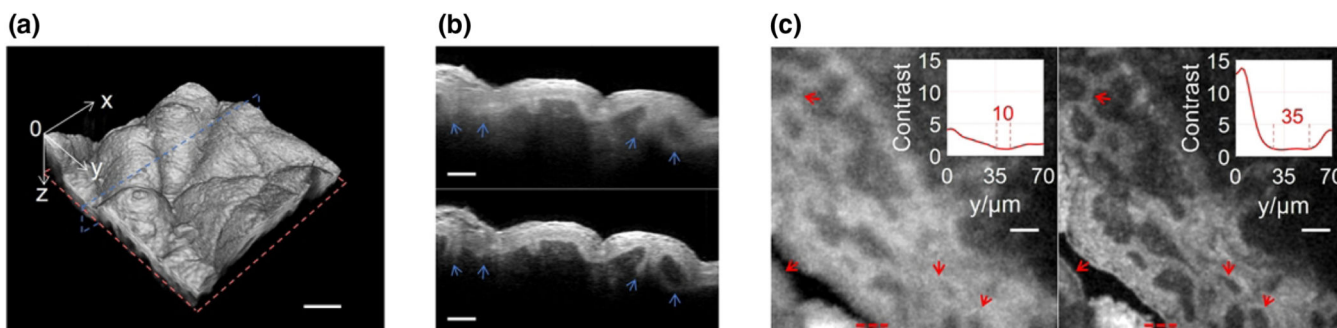


Fig. 4.

Human skin imaging. (a) 3D image captured by $300\ \mu\text{m} \times 3\ \mu\text{m}$ NB. Despite the wavy surface, all surface features are distinguishable due to the long DOF. Scale bar, $200\ \mu\text{m}$; $XY = 1\ \text{mm} \times 1\ \text{mm}$. (b) B-scans at $y = 360\ \mu\text{m}$, blue plane in (a). Indicated by blue arrows, the dermal-epidermal junction in deep regions are fuzzy in Gaussian imaging (upper) but clear in $300\ \mu\text{m}$ NB imaging (lower). Scale bar, $100\ \mu\text{m}$. (c) XY images at $z = 250\ \mu\text{m}$, red plane in (a). The left figure is taken by Gaussian beam, and the right is by $300\ \mu\text{m}$ NB. Some comparisons are marked by red arrows. Two insets describe the contrast profiles along the red dashed lines. The contrast is the ratio of the intensity along the red dashed lines to the average intensity of the air gap (background). Scale bar, $100\ \mu\text{m}$.

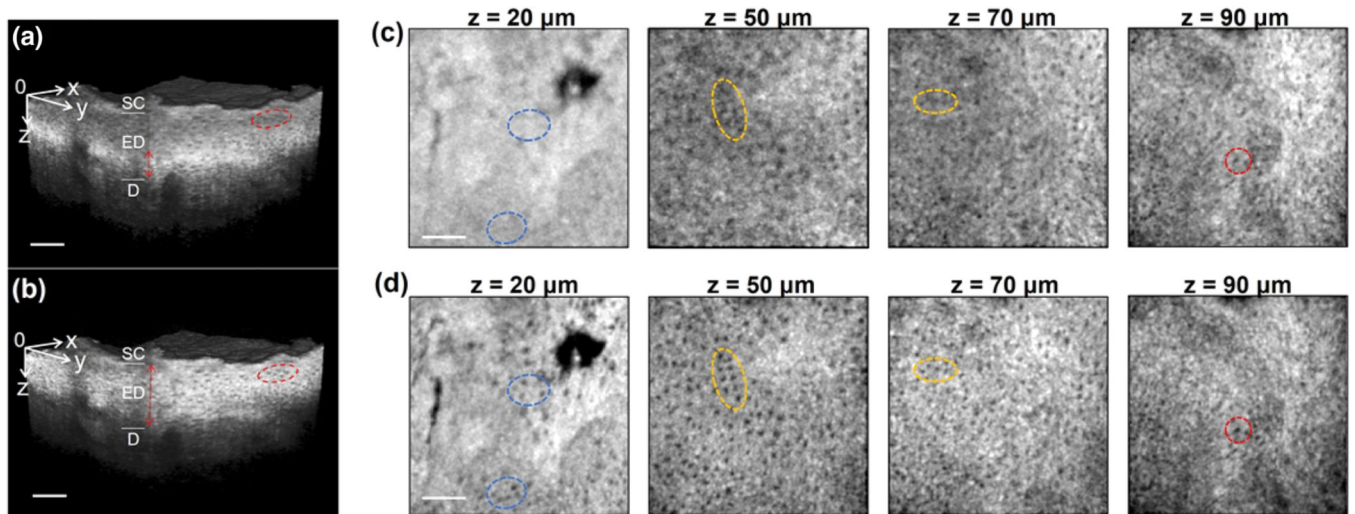


Fig. 5.

Human skin epidermis. Gaussian beam was focused at 90 μm depth. 80 μm \times 1.5 μm NB started at $z = 20$ μm and ended at $z = 100$ μm . (a) Volumetric data of Gaussian beam imaging. The bright and narrow layer marked by the red double-arrow line is within DOF. The cells in the red circle are fuzzy. (b) 3D data captured by 80 μm NB. (c), (d) XY images at five depths demonstrate the resolution disparity between Gaussian beam and 80 μm NB. Cells highlighted in red ellipses have good visibility with both beams while the cells in yellow ellipses are clear in 80 μm NB imaging but noisy in Gaussian beam imaging. Cells in blue ellipses are visible with 80 μm NB but completely disappear with Gaussian beam imaging. Scale bar, 100 μm ; XY = 0.5 mm \times 0.5 mm; SC, stratum corneum; ED, epidermis; D, dermis.