

27 musculoskeletal system, including muscle atrophy and bone density reduction. Ground-based
28 microgravity simulations have provided insights, with vibrational bioreactors emerging as potential
29 mitigators of these negative effects. Despite the potential they have, the adaptation of vibrational
30 bioreactors for space remains unfulfilled, resulting in a significant gap in microgravity research.
31 This paper introduces the first automated low-intensity vibrational (LIV) bioreactor designed
32 specifically for the International Space Station (ISS) environment. Our research covers the
33 bioreactor's design and characterization, the selection of an optimal linear guide for consistent 1-
34 axis acceleration, a thorough analysis of its thermal and diffusion dynamics, and the pioneering
35 use of BioMed Clear resin for enhanced scaffold design. This advancement sets the stage for
36 more authentic space-based biological studies, vital for ensuring the safety of future space
37 explorations.

38

39 **Introduction**

40 The 21st century has witnessed notable advancements in the field of space exploration, as both
41 private and public sectors have made substantial efforts to expand the boundaries of human
42 presence beyond Earth¹⁻⁹. In order to ensure the continued viability of long-term spaceflight, it is
43 critical to address the physiological challenges that arise from microgravity as mission duration
44 and reach increase^{2,4,9,10}. Microgravity poses a unique challenge to astronaut health, particularly
45 affecting the musculoskeletal system. Muscle atrophy and bone density reduction are among the
46 most pressing health issues faced during extended missions, necessitating innovative solutions
47 to mitigate these effects¹⁰⁻¹⁹.

48

49 Ground-based studies have provided valuable insights into the challenges of microgravity.
50 Simulated microgravity experiments, particularly those employing low- and high-intensity
51 vibrational bioreactors, have shown promise in mitigating some of the adverse physiological
52 effects of simulated microgravity^{16,17,19-27}. In addition, pharmacological treatments for bone loss

53 resulting from exposure to microgravity are also being tackled and researched in both real and
54 simulated microgravity^{10,11,28}.

55

56 Nevertheless, the full mechanism and impact of microgravity on the human body, especially in
57 real space conditions, are still not entirely understood¹². Astronauts aboard the International
58 Space Station (ISS) undergo rigorous exercise regimens to combat the adverse effects of living
59 in space^{10–12,17–19,28}. While these exercises help, they don't completely negate the physiological
60 changes induced by microgravity^{12,19}.

61

62 These challenges highlight the crucial necessity of conducting direct cellular studies in a
63 microgravity setting and evaluating the possible advantages of interventions such as vibrational
64 bioreactors in the context of space exploration. While vibrational bioreactors have shown promise
65 on Earth^{14–17,21–26}, there is a conspicuous absence of such technology tailored for use in space¹⁹,
66 especially one that meets the stringent standards of the ISS.

67

68 Our research is motivated by the current limitations in understanding the effects of microgravity
69 at cellular level. The primary aim of our study is to design and characterize an automated low-
70 intensity vibrational (LIV) bioreactor for studying microgravity. This bioreactor is tailored to meet
71 the stringent requirements of the (ISS). Until now, there have been no vibrational bioreactors in
72 space. With the introduction of our LIV bioreactor, we aim to bridge this gap, enabling a direct
73 comparison between experiments conducted in space and those on Earth. This endeavor is
74 crucial for advancing our understanding and ensuring the safety and sustainability of future human
75 space exploration.

76

77 **Experimental Design**

78 The objective of our research was to engineer a low-intensity vibrational (LIV) bioreactor suitable
79 for microgravity conditions aboard the (ISS). Our design had to conform to the CubeLab Interface
80 Control Document (ICD)²⁹ standards, ensuring compatibility with the ISS's operational
81 environment. We utilized the CubeLab 9U module (**Supplementary Figure 2**), provided by Space
82 Tango³⁰, which offers a standardized platform for microgravity experiments^{2,31}, allowing for a
83 secure and controlled setting for our bioreactor.

84

85 In a precursor study within our laboratory, we developed a 3D bone analog scaffold utilizing gyroid
86 shapes to mimic the complex architecture of bone tissue³². For the current bioreactor design,
87 these scaffolds are integral to our assessment, serving as a platform to implement and evaluate
88 the bioreactor's capacity to support biological studies. The focus of our investigation is the
89 application of vibrational stimuli to bone cells, addressing the challenge of bone density
90 reduction—a significant concern for astronauts in microgravity conditions. This approach aims to
91 leverage the mechanical signals provided by our bioreactor to enhance bone cell function and
92 mitigate the effects of space-induced osteopenia.

93

94 For the delivery of precise vibrational stimuli, we selected the piezoelectric actuator (P-841.30,
95 Physik Instrumente (PI), Karlsruhe, Germany) and its closed-loop controller (E-610.S0, Physik
96 Instrumente (PI), Karlsruhe, Germany), chosen for their compliance with the CubeLab's size,
97 weight, and power constraints. These components were tasked with providing a consistent
98 vibration regime at 90Hz with a 0.7g peak-to-peak ($1g=9.81 \text{ m/s}^2$) acceleration, ensuring the
99 application of low-intensity vibrations to the cells.

100

101 Our methodology began with the selection of an appropriate linear guide to facilitate precise one-
102 axis acceleration. This selection process was informed by evaluating multiple linear guides
103 against our design criteria.

104 Next, we conducted thermal and vibrational analyses of the bioreactor's behavior using both
105 COMSOL simulations and empirical testing to ensure that the applied vibrations were within the
106 operational parameters and did not produce too much heat, compromising cell viability.
107 Additionally, we made sure that any resonant frequencies of the system are outside of its
108 operational range so that they do not interfere with the bioreactor's function.

109
110 To validate the bioreactor's compatibility with cellular studies, we performed XTT and Live/Dead
111 assays to confirm that the bioreactor design did not adversely affect cell viability. These assays
112 were critical in demonstrating the biocompatibility of our system.

113
114 Finally, we addressed the challenge of media exchange within the CubeWells. A diffusion study³³,
115 supported by COMSOL simulations and visual assessments using a real-time camera setup, was
116 conducted to ascertain the efficiency of media introduction and distribution within the wells,
117 ensuring that all cells received adequate nutrients without the risk of shear-stress-induced
118 damage.

119
120 **Methods and Data Collection**

121 In order to drive the our piezoelectric actuator's controller (E-610.S0) we needed to generate a
122 90Hz 0-10V signal from a Teensy microcontroller (PJRC, TEENSY41), which only provides a 0-
123 3.3V PWM output. A custom amplifier circuit was designed with a Sallen-Key³⁴ second-order
124 lowpass filter topology (**Supplementary Figure 1**). The filter was tuned to isolate a 90 Hz sine
125 wave from a modulated PWM signal, removing the extraneous frequencies. This process

126 produced a clean sine wave to drive the piezoelectric actuator, providing the precise vibrational
127 stimulus required for the biological experiments.

128

129 **Linear guide selection**

130 To select a linear guide capable of delivering precise one-axis acceleration, we conducted
131 performance evaluations on three different models. Using LabVIEW software, we measured the
132 acceleration profiles of each guide with a MEMSIC CXL04GP3 accelerometer (**Supplementary**
133 **Figure 3**). The guides were tested for their ability to sustain a 0.7g peak-to-peak acceleration at
134 a frequency of 90 Hz over a 20-minute duration. The objective was to identify a guide that would
135 restrict vibrations to the intended axis, ensuring accurate delivery of mechanical stimuli to the
136 samples. The tested guides (**Figure 1**) included: a custom-built roller-based guide (SS2EB,
137 Misumi, Schaumburg, IL), known for smooth motion; a low-maintenance plastic linear guide (N
138 Prism Preloaded, Igus Inc., Rumford, RI); and a Schneeberger roller-based linear guide (NKL 2-
139 95, Schneeberger Inc., Woburn, MA).

140

141 **Thermal Characterization**

142 The thermal performance of the LIV bioreactor was evaluated to determine its suitability for
143 sustaining biological experiments within the CubeLab module. The fully assembled bioreactor,
144 including the piezoelectric actuator, closed-loop controller, and the selected linear guide, was
145 installed inside the CubeLab. Thermocouples (Type K) were positioned: directly inside the
146 controller housing, above the actuator, adjacent to the biological sample area, and within the
147 external ambient environment of the CubeLab (**Figure 2**).

148

149 LabVIEW software with the NI 9211 DAQ card (National Instruments, Austin, TX, USA) was
150 utilized for both control of the vibrational input and data acquisition of the thermal output. The
151 system was tested with two different payload conditions, 400 grams and 1100 grams, to simulate

152 varying experimental loads. The operational test consisted of a 25-minute vibration cycle at 0.7g
153 peak-to-peak acceleration and a frequency of 90Hz.

154

155 Thermal characterization was conducted under two distinct CubeLab configurations: an 'Open'
156 setup with the top cover removed and a 'Closed' setup where the module was entirely sealed.
157 These tests were performed without the integration of active cooling systems to assess the
158 bioreactor's inherent thermal management capabilities under operational conditions. Data
159 collected during these tests were analyzed to understand the thermal dynamics of the system,
160 with particular attention to the temperature stability and heat dissipation efficiency in both 'Open'
161 and 'Closed' states.

162

163 **Vibration Characterization**

164 The vibrational characteristics of our bioreactor were analyzed through both simulation and
165 experimental testing. In the simulation phase, COMSOL was used to study the system's
166 dynamics. A detailed CAD model of the bioreactor, which included the metal base, actuator, linear
167 guide, and payload holder, was integrated into the simulation environment. We follows a simple,
168 conservative approach in our analysis by assuming that , the material for the piezoelectric actuator
169 was the same as its housing - standard stainless steel. This assumption allowed us to focus on
170 the primary vibration modes crucial for the bioreactor's functionality in microgravity, without the
171 complexities of modeling the piezoelectric properties. This setup, which mirrored real-world
172 constraints and was executed with a standard mesh configuration, provided a robust and efficient
173 method to assess the vibrational dynamics of the bioreactor.

174

175 Concurrently, experimental tests were conducted to validate the simulation results and further
176 understand the bioreactor's vibrational behavior. The system was subjected to vibrations at a
177 targeted 0.4g peak-to-peak acceleration across a frequency range of 50 Hz to 500 Hz, with finer

178 increments around the critical 90 Hz range. Subsequent tests aimed for a 0.7g peak-to-peak
179 vibration; however, due to the actuator's stroke constraints, only at frequencies from 80 Hz to 150
180 Hz.

181

182 **Scaffold Viability**

183 Cell viability on SLA-printed scaffolds made from BioMed Clear resin was assessed using XTT
184 assays for quantitative analysis and Live/Dead imaging for qualitative evaluation. The resin was
185 selected for its precision in creating complex structures. Scaffolds were integrated with a hydrogel
186 to improve the biomimetic quality for cell culture studies.

187

188 Cell Culture and Seeding:

189 Murine mesenchymal stem cells (MSCs) were employed for this study. These cells were
190 encapsulated within a hydrogel^{35(p3)} composed of Thiolated Hyaluronic Acid (HA) (Advanced
191 Biomatrix, #GS22F), functionalized with specific amino sequences: PQ (GGGPQ↓IWGQGK
192 concentrated at 44.973 mgs/mL) and RGD (GRGDS concentrated at 73.7mgs/mL) with a volume
193 ratio of 4 HA:1 RGD: 1PQ. The encapsulated cells were then seeded into gyroid-shaped scaffolds,
194 designed to mimic the bone marrow microenvironment. These scaffolds were fabricated using the
195 BioMed Clear resin from Formlabs and were SLA printed using a Form 2 printer.

196

197 Osteogenic Media Preparation:

198 The osteogenic media used for cell culture was prepared using α -MEM, supplemented with 10%
199 FBS, 100 U/mL penicillin, 100 μ g/mL streptomycin, Vitamin C at 50ug/ml, and beta-
200 glycerophosphate ranging from 10mM-20mM.

201

202 Vibration Regime:

203 Post-seeding, the scaffolds were transferred to a 96-well plate containing the osteogenic media.
204 The entire setup was then placed in an incubator. A distinct vibration regime was implemented,
205 wherein the samples were subjected to a consistent vibration of 0.7g peak-to-peak at 90 Hz for
206 20 minutes. This vibration was administered twice daily, with a 2-hour interval between each
207 session.

208

209 XTT Assay:

210 On the first and fourth day, an XTT assay was performed to assess cell viability. The assay utilized
211 two primary reagents: an electron mediator solution and the XTT developer reagent (Cayman
212 Chemical, #10010200). Following the manufacturer's protocol, the samples were incubated for
213 approximately 2 hours at 37°C. The absorbance of the assay wells was then measured using a
214 microtiter plate reader, capturing values between 400-500 nm wavelengths.

215

216 Live/Dead Imaging:

217 On the fifth day, live/dead imaging was conducted. The cells were stained using Calcein AM
218 (green) to identify live cells, Propidium Iodide (red) to mark dead cells, and Hoechst 33342 (blue)
219 for nuclear staining according to the manufacturer's specifications (EMD Millipore #CBA415). The
220 stained samples were then visualized under a fluorescence microscope. While no quantitative
221 data was extracted from these images, they provided a visual representation of the ratio between
222 live and dead cells, offering insights into cell health and viability.

223

224 Controls and Replicates:

225 The study employed both vibrated and non-vibrated samples as experimental and control groups
226 (+LIV/-LIV), respectively. Each week's samples (n=4/week for 2 weeks) were biological replicas,
227 with fresh samples prepared for the subsequent week following the identical protocol as the initial
228 week.

229

230 **Diffusion dynamics within the CubeWells**

231 To ensure consistent cell culture conditions within the custom-designed CubeWells by Space
232 Tango, a diffusion study was conducted. Initial tests verified the CubeWells' structural integrity
233 through a visual leak assessment. The primary objectives of the diffusion study³³ were to evaluate
234 the efficiency of a miniaturized pump in introducing new media into the CubeWell and to confirm
235 uniform media distribution across the well. This was achieved through both COMSOL simulations
236 and real-time camera observations.

237

238 COMSOL Simulation:

239 To predict the diffusion dynamics within the custom-designed CubeWell system, a multiphysics
240 simulation was conducted using COMSOL. The study combined two primary modules: Laminar
241 Flow and Transport of Diluted Species. The Laminar Flow module was employed to simulate the
242 fluid flow into the CubeWell, while the Transport of Diluted Species module was used to visualize
243 the influx of new media, set at a concentration of 1 mol/m³. The simulation was constrained by
244 defining the inlet at the top and outlet at the bottom of the CubeWell (**Figure 5b**), along with the
245 boundary walls, ensuring a realistic representation of the media exchange process.

246

247 Experimental Setup:

248 For the in-vitro experiment, the CubeWells were pre-filled with 8 mL of water. Within this
249 environment, SLA-printed scaffolds made from BioMed Clear resin were introduced. These
250 scaffolds, measuring 5x5x5mm, were encapsulated in hydrogels (**Figure 4b**), mimicking the
251 cellular constructs intended for subsequent cell culture experiments.

252

253 Media Exchange and Observation:

254 To simulate the introduction of fresh media, a mixture of water and Royal Blue Icing color dye
255 (Wilton, #17111150) was prepared. This simulated medium was then pumped into the CubeWell
256 at a consistent rate of 1 mL/min. The entire process of media exchange, including the diffusion of
257 the dye and fluid movement within the CubeWells, was captured using a high-speed camera
258 (Photron FASTCAM MINI UX50) set at 1000 frames per second (fps). This recording spanned a
259 duration of 5 minutes, providing a detailed visual account of the diffusion dynamics.

260

261 Data Analysis:

262 Post-recording, the captured footage was analyzed to quantify diffusion within the CubeWell
263 system. Five distinct locations within the CubeWell were selected for this analysis. At these points,
264 the intensity values of the dye were measured over time, offering a quantitative perspective on
265 the diffusion rates and patterns.

266

267 **Results**

268

269 Linear guide selection

270 The vibration experiment results (**Figure 1**) confirmed the Schneeberger NKL 2-95 linear guide's
271 superior performance, with a 95.47% and 52.60% more consistent y-axis acceleration than the N
272 preloaded prism carriage and the custom-built laboratory guide, respectively. The Schneeberger
273 guide maintained a stable acceleration profile with lower mean values (X: 0.031g, Y: 0.704g, Z:
274 0.018g) and standard deviations (X: $\pm 0.000g$, Y: $\pm 0.005g$, Z: $\pm 0.006g$), indicating its precise
275 control over vibrational input. In comparison, the N preloaded prism carriage showed higher
276 variability, particularly in the x-axis ($0.473g \pm 0.024$) and z-axis ($0.133g \pm 0.008$), while the
277 laboratory guide using Misumi roller guides presented intermediate stability (X: $0.089g \pm 0.007$, Y:
278 $0.684g \pm 0.011$, Z: $0.071g \pm 0.000$). All guides met the experimental requirement of 0.7g peak-to-
279 peak acceleration in the y-axis, demonstrating their adequacy for the intended vibrational studies.

280

281 Thermal profile in the CubeLab environment

282 Thermal profile (**Figure 2**) of each component measured in the CubeLab maintained a steady
283 temperature in different conditions (Open and Closed), with variations within $\pm 0.80^{\circ}\text{C}$ over the 25-
284 minute LIV period. In the 'Open' CubeLab configuration, where the top cover was removed, the
285 temperature readings indicated a gradual increase over time in the controller and the ambient air
286 temperature 1 and 2 in the CubeLab. Although the ambient air temperature increased, the
287 temperatures for ambient 1 ($23\pm 0.72^{\circ}\text{C}$) and ambient 2 ($24\pm 0.60^{\circ}\text{C}$) still stabilized below the
288 critical threshold for cell viability. In the 'Closed' configuration, temperatures were consistently
289 higher, yet they remained within acceptable limits, suggesting that passive heat dissipation
290 mechanisms were sufficient to maintain a safe operational environment for the duration of the
291 experiments.

292

293 Vibration Characterization

294 Experimental characterization of the bioreactor's vibrational dynamics, supplemented by
295 COMSOL simulations, confirmed operational stability across the frequency spectrum of interest.
296 The simulations indicated no resonant frequencies within the operational range, with the first
297 mode of vibration occurring at 929 Hz (**Figure 3**), presenting minimal the risk of resonance
298 interference. Empirical tests validated the simulation, demonstrating effective vibrational isolation
299 at operational frequencies, with X/Y and Z/Y acceleration ratios remaining below 0.13 at lower
300 frequencies. As frequency increased, a corresponding rise in these ratios was observed,
301 suggesting higher transference of vibration to non-targeted axes. **Tables 1** and **2** encapsulates
302 these findings, showing the bioreactor's performance at various frequencies and accelerations,
303 with a clear delineation between low and high-frequency behavior.

304

305 Scaffold viability

306 The XTT assay results indicated no significant difference in metabolic activity between the
307 vibrated (+LIV) ($p=0.9973$) and non-vibrated (-LIV) ($p>0.9999$) samples from day 1 (D1) to day 4
308 (D4). Also, from D1 to D4, the metabolic activity of cells on the new scaffold material slightly
309 increased in both vibrated (D1 mean: 1.4584 to D4 mean: 1.5453) and non-vibrated (D1 mean:
310 1.4584 to D4 mean: 1.4986) conditions. This showed that the BioMed Clear resin used in the
311 scaffolds was biocompatible.

312

313 For a more direct observation of cell viability, Live/Dead imaging was employed. The imaging
314 results, presented in **Figure 4c-f** and (**Supplementary Figure 4**), visually demonstrate the
315 proportion of live (green) to dead (red) cells, providing a qualitative assessment of cell health. The
316 pictures show that there are mostly living cells in both +LIV and -LIV conditions. There does not
317 seem to be an increase in cell death after LIV was added or when the new material for the scaffold
318 was added. The comparative analysis of the live/dead ratio further supports the conclusion that
319 the new scaffold material, in conjunction with the LIV bioreactor, maintains a conducive
320 environment for cell growth and viability.

321

322 Diffusion Study

323 The diffusion characteristics within the CubeWells were initially modeled using COMSOL
324 simulations to establish an efficient media exchange protocol. According to the simulations
325 illustrated in **Figure 5b-c**, we observed that by employing a pumping rate of 1mL/min,
326 approximately 80% of the volume of CubeWell would be occupied by fresh media during a span
327 of 3 minutes. This rate of media replacement would result in total replacement of the media by
328 the 5-minute mark. These findings informed the operational parameters for the media pump in
329 subsequent in-vitro validation experiments.

330 In practice, the diffusion regime for the in-vitro experiment, visualized in **Figure 5a**, involved a 5-
331 minute media pumping phase at the same flow rate, followed by a 15-minute recirculation period.

332 The high-speed camera monitoring revealed a consistent media distribution pattern (**Figure 5d-**
333 **e**), with a notable 55-second delay in reaching the center, bottom-left, and bottom-right locations
334 compared to the simulation. Despite this delay, both the simulation and the experimental
335 observations confirmed that 100% media exchange was accomplished within the 5-minute
336 duration. The similarity between the predicted and actual diffusion patterns validates the
337 simulation's utility in setting practical experimental conditions and underscores the system's
338 capability to maintain cell viability by preventing prolonged exposure to stagnant media.

339

340 **Conclusions and Discussion**

341 This study presented a wide-ranging characterization of a LIV bioreactor designed for microgravity
342 conditions, such as those on the ISS. The research focused on validating the bioreactor's
343 mechanical and biological performance, ensuring its compatibility with the stringent requirements
344 of space missions.

345

346 The selection of the linear guide was critical for the bioreactor's performance. Our results indicated
347 that the Schneeberger NKL 2-95 linear guide provided consistent one-axis acceleration, crucial
348 for minimizing disturbances during vibration. Despite its larger size, it demonstrated superior
349 performance in maintaining the desired vibrational profile with minimal cross-axis acceleration, as
350 compared to the Igus N Prism guide and the Misumi linear guide. The Misumi linear guide,
351 previously used in the laboratory, served as an effective benchmark, confirming the reliability of
352 the Schneeberger guide under the test conditions.

353

354 Thermal characterization within the CubeLab environment demonstrated that the system could
355 sustain a stable temperature profile, with variations within $\pm 0.80^{\circ}\text{C}$ over a 25-minute operational
356 period. Notably, while the controller exhibited an increase in temperature, the duration of
357 operation and the volume of air within the CubeLab were such that the rise in the overall ambient

358 temperature did not create any problems in terms of either cell viability or piezoelectric controller's
359 operation range. The CubeLab's exterior design proved effective in dissipating heat from the
360 controller, thereby minimizing thermal transfer to the biological samples. This indicates that the
361 bioreactor's thermal management is adequate for the tested operational conditions without the
362 need for active cooling systems. Nonetheless, the design accommodates the integration of
363 minimal cooling solutions for experiments with cooler ambient requirements, ensuring adaptability
364 for a broad spectrum of research needs.

365

366 The vibrational characterization of the bioreactor was approached with a strategy that combined
367 predictive COMSOL simulations with empirical testing. The simulations provided theoretical
368 assurance that the bioreactor's design avoids resonant frequencies within the operational range,
369 with the first resonant mode predicted at 929 Hz. While empirical testing did not directly confirm
370 this resonant frequency, it did reveal an increase in the ratio of non-targeted to targeted axis
371 accelerations at higher frequencies. This trend suggests that the bioreactor's actual vibrational
372 isolation performance aligns with the simulation outcomes, especially since no resonance was
373 observed during the tested frequency range.

374

375 The increase in acceleration ratios at higher frequencies highlights the need for careful monitoring
376 of vibrational behavior as operational frequencies approach the upper limit. Still, the bioreactor
377 met the goals for vibration isolation, showing that it could keep accelerations under control on the
378 main axis and prevent transference to the non-vibrated axes. This finding is crucial for
379 microgravity research applications, where the fidelity of mechanical stimuli delivery to biological
380 samples is of utmost importance.

381 The simulation's finding that there is no resonance during routine operations, along with empirical
382 evidence of vibration isolation, points to the bioreactor as a promising tool for spaceflight
383 experiments. It is prepared to provide a stable environment for the study of microgravity's effects

384 on biological systems. Future design enhancements may focus on further reducing vibrational
385 transfers at higher frequencies, leveraging the insights gained from this study to refine the
386 bioreactor's performance.

387

388 The evaluation of the scaffold's biological performance within the LIV bioreactor demonstrated a
389 slight increase in metabolic activity by day four, with a marginally higher increase observed in the
390 vibrated (+LIV) samples. This increase, although subtle, hints at a potential positive interaction
391 between mechanical stimulation and cellular activity over time with the use of the new scaffold
392 material. The use of SLA-printed scaffolds across all samples ensures a consistent comparison
393 base, highlighting the specific effects of LIV on cell viability.

394

395 The BioMed Clear resin scaffolds, employed in both vibrated and non-vibrated conditions, have
396 shown promising compatibility for extended cell culture applications. This compatibility is crucial
397 for future microgravity studies, where material behavior under prolonged exposure to LIV can
398 significantly influence experimental outcomes. The data suggests that these scaffolds can support
399 cell growth and maintain viability, which is essential for the success of long-duration biological
400 experiments in space. Further research, with an extended timeline, will be instrumental in
401 understanding the full scope of LIV's effects on cellular systems in microgravity. The robustness
402 of the SLA-printed scaffolds for intricate designs also opens avenues for more complex tissue
403 engineering applications in space, where precise geometric control is crucial. The findings thus
404 far provide a solid foundation for the extended use of these materials and methods in microgravity
405 research.

406

407 Diffusion studies, supported by COMSOL simulations and in-vitro experiments, verified the
408 CubeWell system's media exchange efficiency. The congruence of simulation and experimental

409 outcomes validated the media pump's operational parameters, ensuring timely and uniform cell
410 nourishment without prolonged exposure.

411

412 In conclusion, the contributions of this research are versatile, addressing previous limitations in
413 space research and providing a comprehensive solution that enhances the scope of biological
414 experimentation in microgravity. The insights gained from this work are expected to have a
415 profound impact on the health and safety of astronauts by informing the design of future space
416 missions and the development of countermeasures against the adverse effects of living in space.

417

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421

422 ***Data Availability***

423 The datasets used and/or analyzed during the current study are available from the corresponding
424 author on reasonable request.

425

426 ***Competing interests***

427 The author(s) declare no competing interests financial or otherwise.

428

429 ***Contributions***

430 Omor Khan: concept/design, data analysis/interpretation, manuscript writing

431 Will Gasperini: concept/design, data analysis/interpretation

432 Chess Necessary: concept/design

433 Zach Jacobs: concept/design

434 Sam Perry: concept/design

435 Paul Kuehl: concept/design
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445 final approval of manuscript
446 Gunes Uzer: concept/design, data analysis/interpretation, financial support, manuscript writing,
447 final approval of manuscript

448

449 **Figure 1: Comparison of peak-to-peak accelerations for three different linear guides under**
450 **90Hz, 0.7g peak-to-peak vibration.** The guides tested were an N-Prism linear guide, a
451 Schneeberger linear guide, and a Misumi linear guide. Box and violin plots represent the
452 distribution of peak-to-peak accelerations in the X, Y, and Z axes over a 20-minute test period.
453 The Schneeberger guide demonstrated the most consistent performance, with a peak-to-peak
454 acceleration of 0.7g in the Y-axis and minimal vibration translation to the X and Z axes.

455

456 **Figure 2: Differential Heating Effects on the Vibrational Bioreactor and Surrounding**
457 **Environment.** This figure illustrates the varying temperature profiles observed during a 25-minute
458 vibrational experiment conducted within a closed and open-lid system. Internal and external
459 thermocouples recorded the temperature of the vibrational controller (rising to 59°C) and the
460 ambient air within and outside the enclosure (increasing from 21°C to 25°C). The results confirm

461 that despite the significant heat generated by the vibrational actuator, the ambient conditions
462 remained within a safe range for cell viability.

463

464 **Figure 3: Vibrational analysis of the bioreactor using COMSOL Multiphysics. (a)** The
465 bioreactor assembly with components materials assigned. **(b)** The applied mesh ensuring
466 resolution for accurate mode shape determination. **(c)** Roller boundary conditions are applied to
467 simulate linear guide constraints **(d)** The first mode shape at 950.24 Hz, demonstrating primary
468 deformation.

469

470 **Figure 4: Analysis of Stem Cell Viability and Metabolic Activity in SLA-Printed Scaffolds.**

471 This figure presents the results of a 4-day experiment investigating the survival and metabolic
472 activity of stem cells grown in SLA-printed scaffolds (blue arrows). **(a)** Metabolic activity was
473 measured using an XTT assay at day 1 (mean = 1.4, SD = 0.23) and at day 4 (mean = 1.5, SD =
474 0.19), showing a slight increase over time despite high standard deviations due to a small sample
475 size (n = 4 per group). Analysis showed no significance between groups and days. Concurrently,
476 **(c-f)** Live/Dead staining and imaging highlighted a predominance of viable (green) cells over dead
477 ones, reinforcing the potential for successful cell growth within these scaffolds.

478

479 **Figure 5: Diffusion study of custom well plate for cell culture. (a)** For most efficient volume
480 change, a 5-minute pump followed by a 15 min. recirculation is implemented in the media change
481 regimen for the real experiment **(b)** COMSOL simulation depicting media concentration profile
482 and its **(c)** quantitative analysis. **(d)** Real experiment replicating the COMSOL simulation using
483 dye as new media for visualization and **(e)** intensity values of the real experiment showcasing the
484 concentration gradient within the 5 min. pump and 15 min. recirculation in highlighted region

485

486 **Supplementary Figure 1:** Custom circuit diagram (top) to generate sine wave signal from Teensy
487 4.0 microcontroller. PWM signal (square wave) coming from the microcontroller is filtered by the
488 demodulating circuit to get a sine wave output that will be used as an input signal for the LIV.

489

490 **Supplementary Figure 2:** CubeLab (top and bottom-left) facility that will house the vibrational
491 bioreactor and the biological samples. The PAUL (top and bottom-right) facility designed to house
492 and provide mechanical, electrical, and network interface from the outside.

493

494 **Supplementary Figure 3:** Experiment schematic of the LIV regimen from signal generation to
495 data acquisition and visualization in LabVIEW.

496

497 **Supplementary Figure 4:** Additional Live/Dead assay images across various scaffold locations
498 and samples, demonstrating a predominance of live cells over dead ones. These images further
499 validate the biocompatibility and cell-supportive nature of the scaffold materials used in the study.

500

501 **Supplementary Figure 5:** CubeWells within the CubeLab module, showcasing the custom-
502 designed well plates developed for holding hydrogel-encapsulated scaffolds. The design
503 incorporates a secure lid system to prevent sample spillage during spaceflight, with scaffolds
504 protected by a biocompatible PDMS layer, further sealed by a metal lid for added safety and
505 integrity during experiments in space.

506

507 **Table 1: Acceleration ratio in each non-targeted axes to the acceleration of target direction,**
508 **highlighting the relative distribution of vibrational energy across all axes.** The bioreactor
509 was subjected to vibration of 0.3g peak-to-peak across the entire 60 Hz to 500 Hz frequency
510 range.

Frequency (Hz)	X/Y	Z/Y
60	0.06	0.06
70	0.06	0.13
80	0.06	0.13
85	0.06	0.13
90	0.06	0.13
95	0.06	0.10
110	0.06	0.13
130	0.06	0.13
150	0.06	0.10
200	0.13	0.16
250	0.13	0.16
300	0.13	0.19
500	0.14	0.19

511

512 **Table 2: Acceleration ratio in each non-targeted axes to the acceleration of target direction,**
513 **highlighting the relative distribution of vibrational energy across all axes.** The bioreactor
514 was subjected to vibration of 0.7g peak-to-peak limited to frequencies between 80 Hz and 150 Hz
515 due to system constraints.

Frequency (Hz)	X/Y	Z/Y
80	0.06	0.09
85	0.06	0.09
90	0.06	0.09
95	0.055	0.09
110	0.07	0.09

130	0.09	0.09
150	0.06	0.10

516

517 **Abbreviations:** LIV means low intensity vibration, MSCs means Mesenchymal Stem Cells

518

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- 619

Development and characterization of a low intensity vibrational system for microgravity studies

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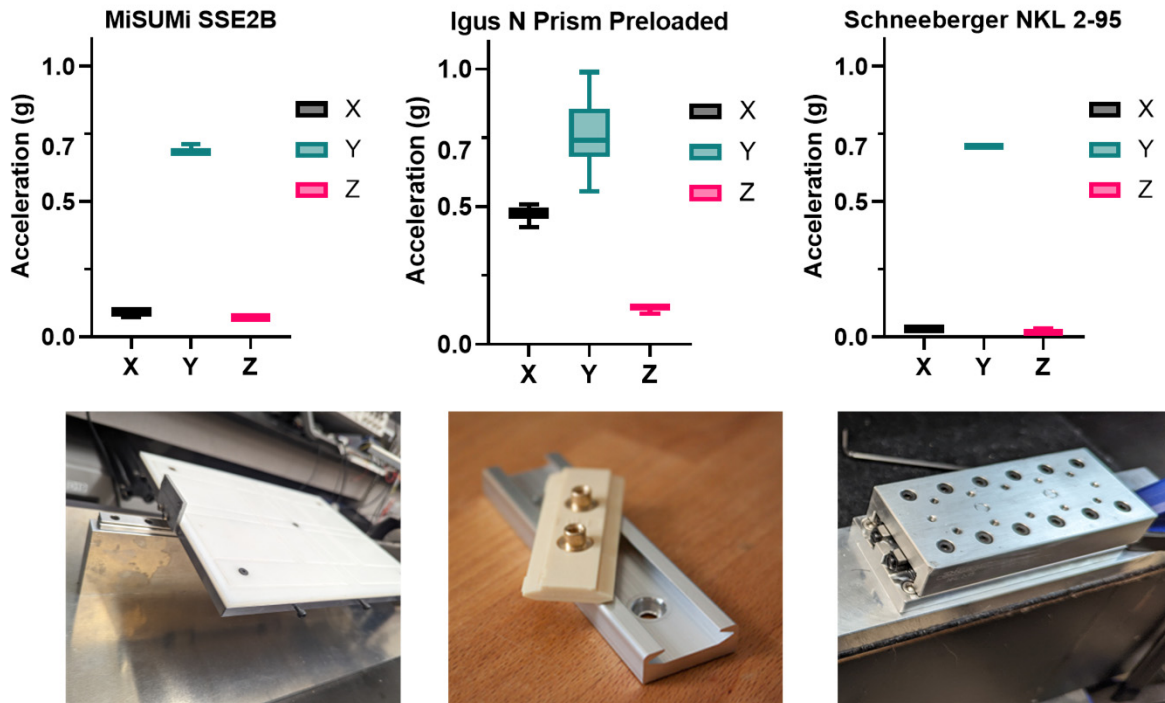


Figure 1: Comparison of peak-to-peak accelerations for three different linear guides under 90Hz, 0.7g peak-to-peak vibration. The guides tested were an N-Prism linear guide, a Schneeberger linear guide, and a Misumi linear guide. Box and violin plots represent the distribution of peak-to-peak accelerations in the X, Y, and Z axes over a 20-minute test period. The Schneeberger guide demonstrated the most consistent performance, with a peak-to-peak acceleration of 0.7g in the Y-axis and minimal vibration translation to the X and Z axes.

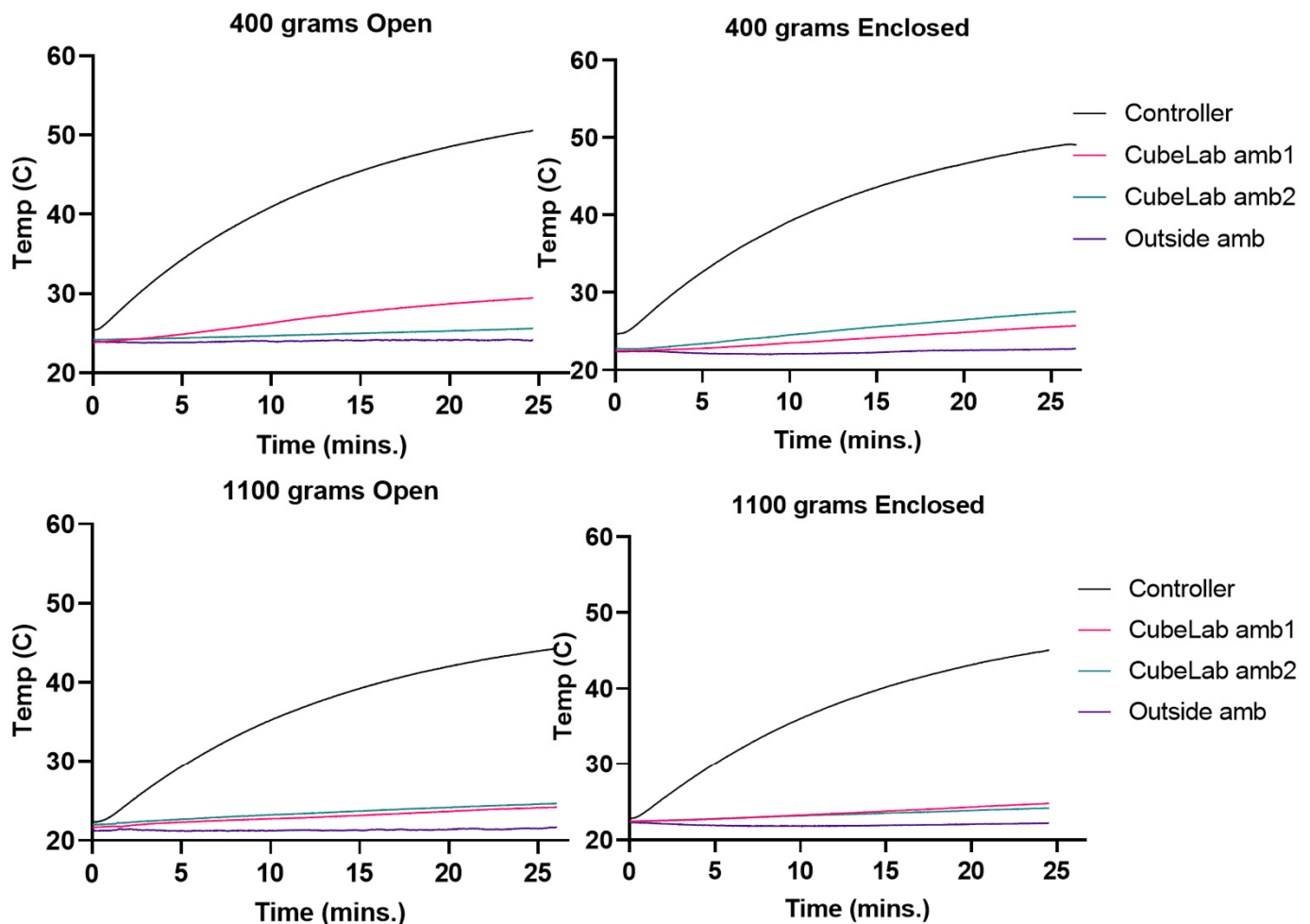
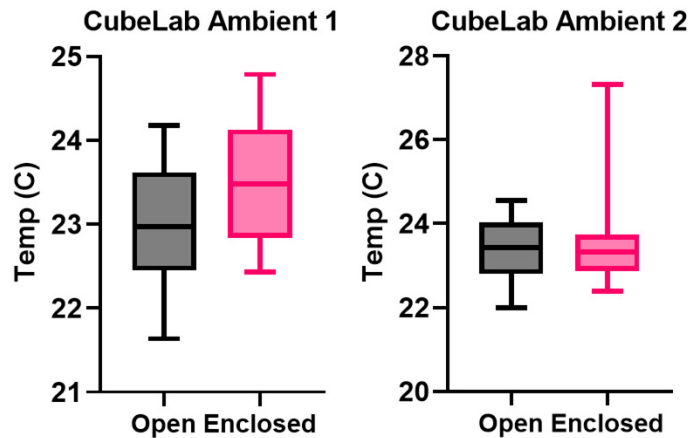
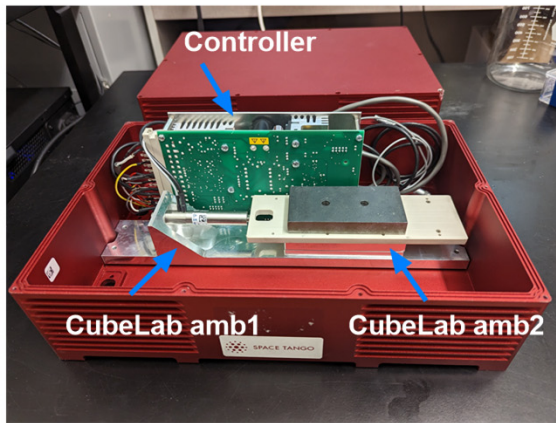


Figure 2: Differential Heating Effects on the Vibrational Bioreactor and Surrounding Environment. This figure illustrates the varying temperature profiles observed during a 25-minute vibrational experiment conducted within a closed and open-lid system. Internal and external thermocouples recorded the temperature of the vibrational controller (rising to 59°C) and the ambient air within and outside the enclosure (increasing from 21°C to 25°C). The results confirm that despite the significant heat generated by the vibrational actuator, the ambient conditions remained within a safe range for cell viability.

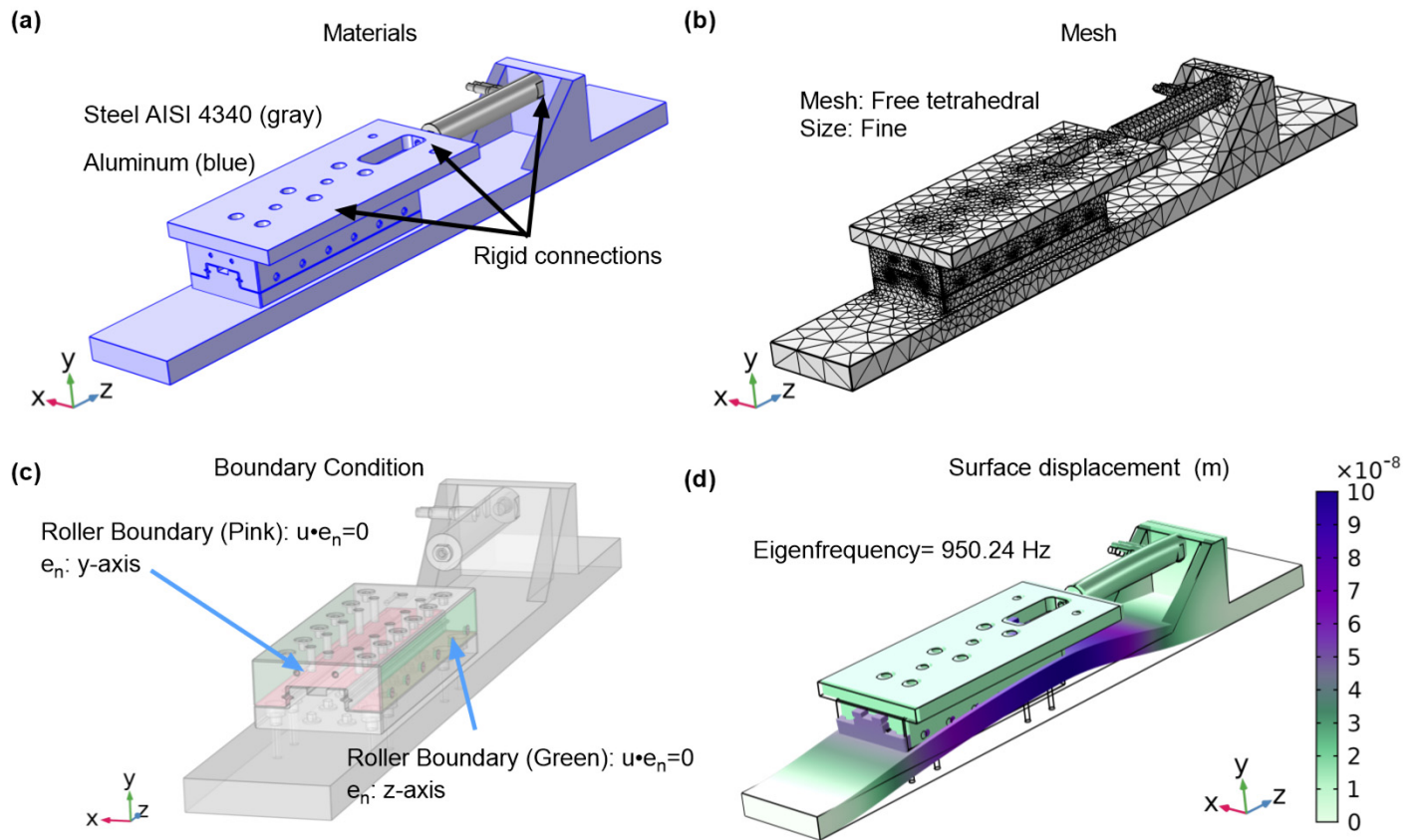


Figure 3: Vibrational analysis of the bioreactor using COMSOL Multiphysics. (a) The bioreactor assembly with components materials assigned. (b) The applied mesh ensuring resolution for accurate mode shape determination. (c) Roller boundary conditions are applied to simulate linear guide constraints (d) The first mode shape at 950.24 Hz, demonstrating primary deformation.

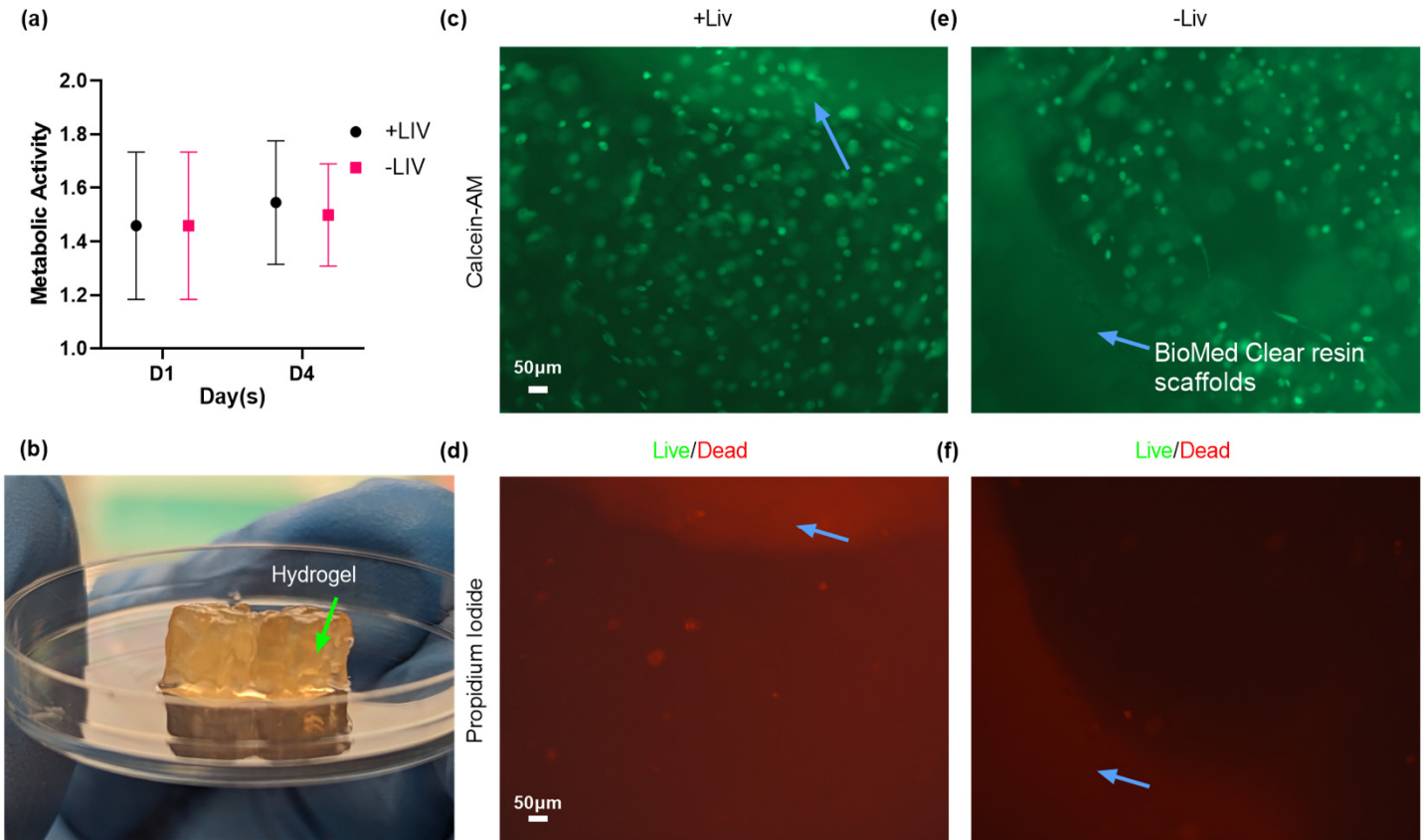


Figure 4: Analysis of Stem Cell Viability and Metabolic Activity in SLA-Printed Scaffolds. This figure presents the results of a 4-day experiment investigating the survival and metabolic activity of stem cells grown in SLA-printed scaffolds (blue arrows). **(a)** Metabolic activity was measured using an XTT assay at day 1 (mean = 1.4, SD = 0.23) and at day 4 (mean = 1.5, SD = 0.19), showing a slight increase over time despite high standard deviations due to a small sample size (n = 4 per group). Analysis showed no significance between groups and days. Concurrently, **(c-f)** Live/Dead staining and imaging highlighted a predominance of viable (green) cells over dead ones, reinforcing the potential for successful cell growth within these scaffolds.

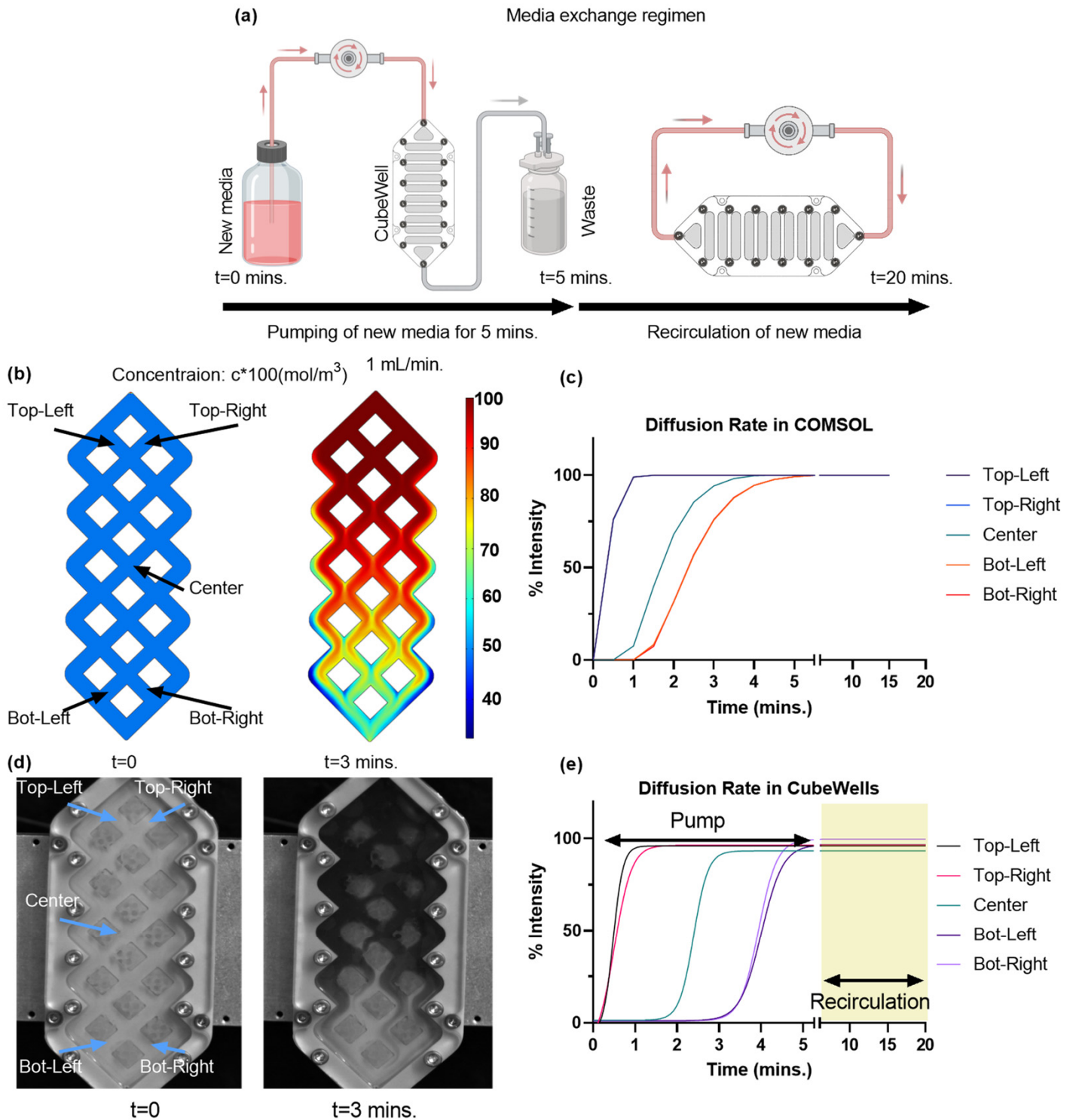


Figure 5: Diffusion study of custom well plate for cell culture. (a) For most efficient volume change, a 5-minute pump followed by a 15 min. recirculation is implemented in the media change regimen for the real experiment (b) COMSOL simulation depicting media concentration profile and its (c) quantitative analysis. (d) Real experiment replicating the COMSOL simulation using dye as new media for visualization and (e) intensity values of the real experiment showcasing the concentration gradient within the 5 min. pump and 15 min. recirculation in highlighted region

Supplementary Figures:

Development and characterization of a low intensity vibrational system for microgravity studies

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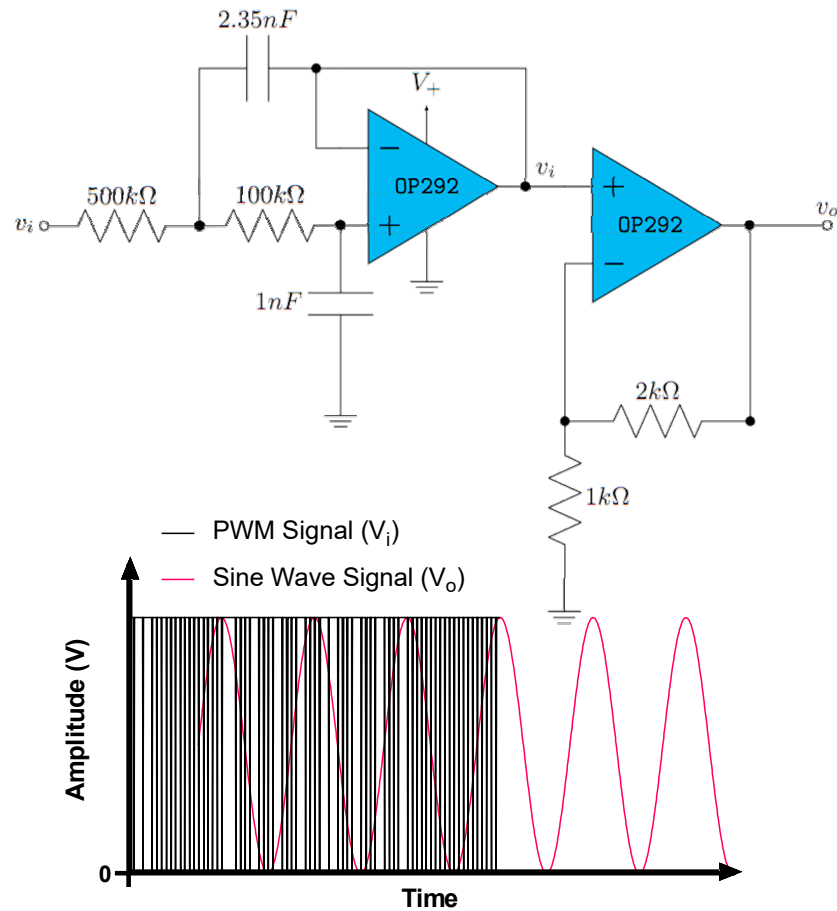
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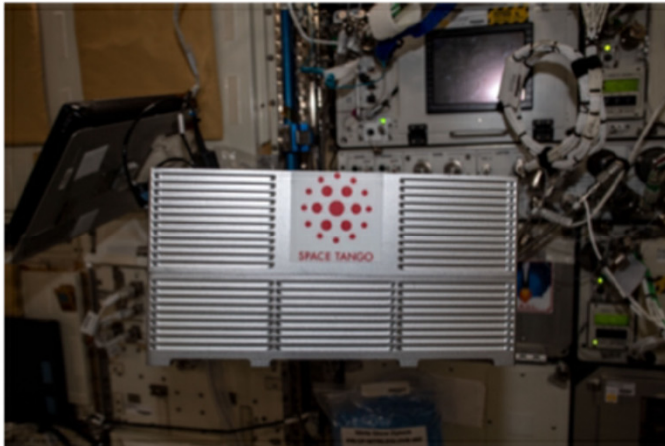
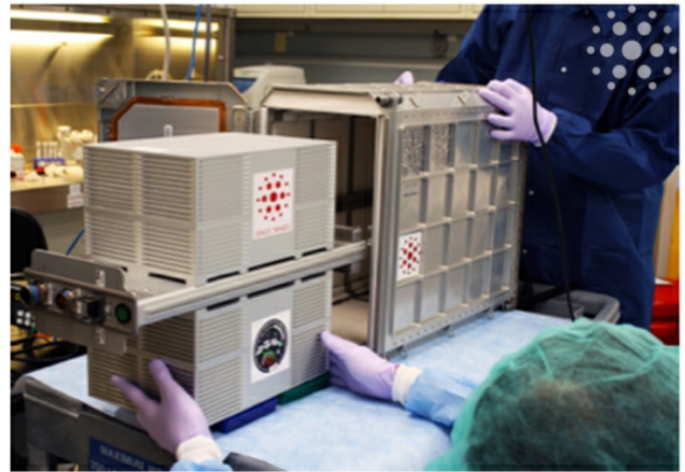
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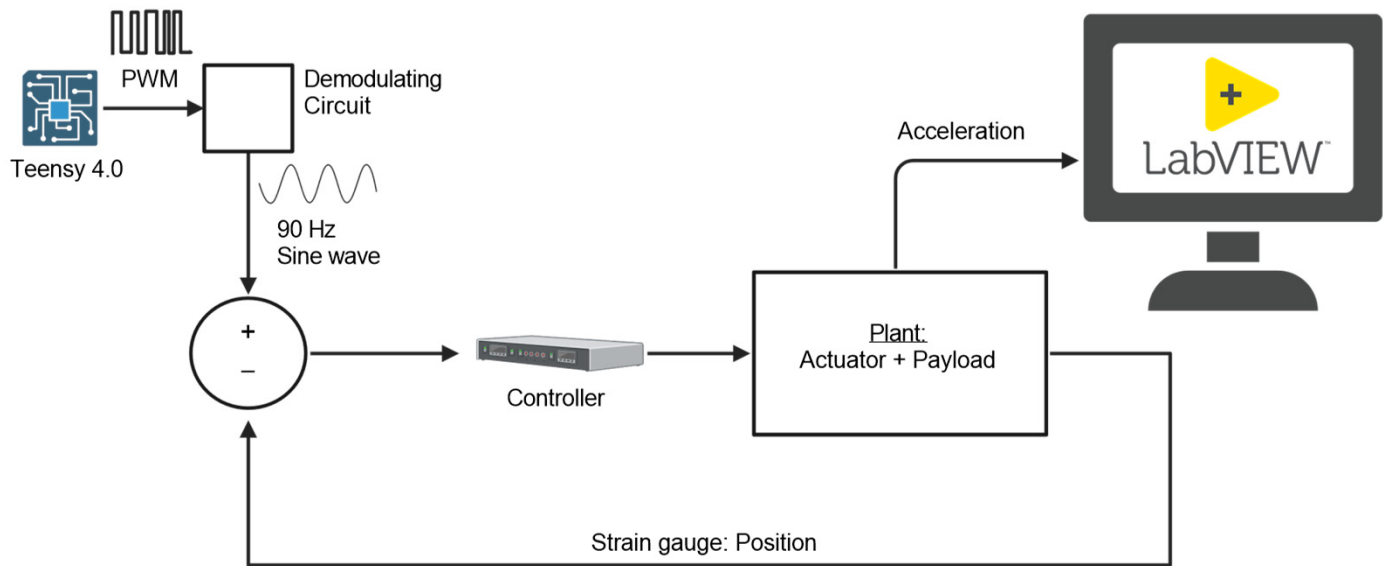
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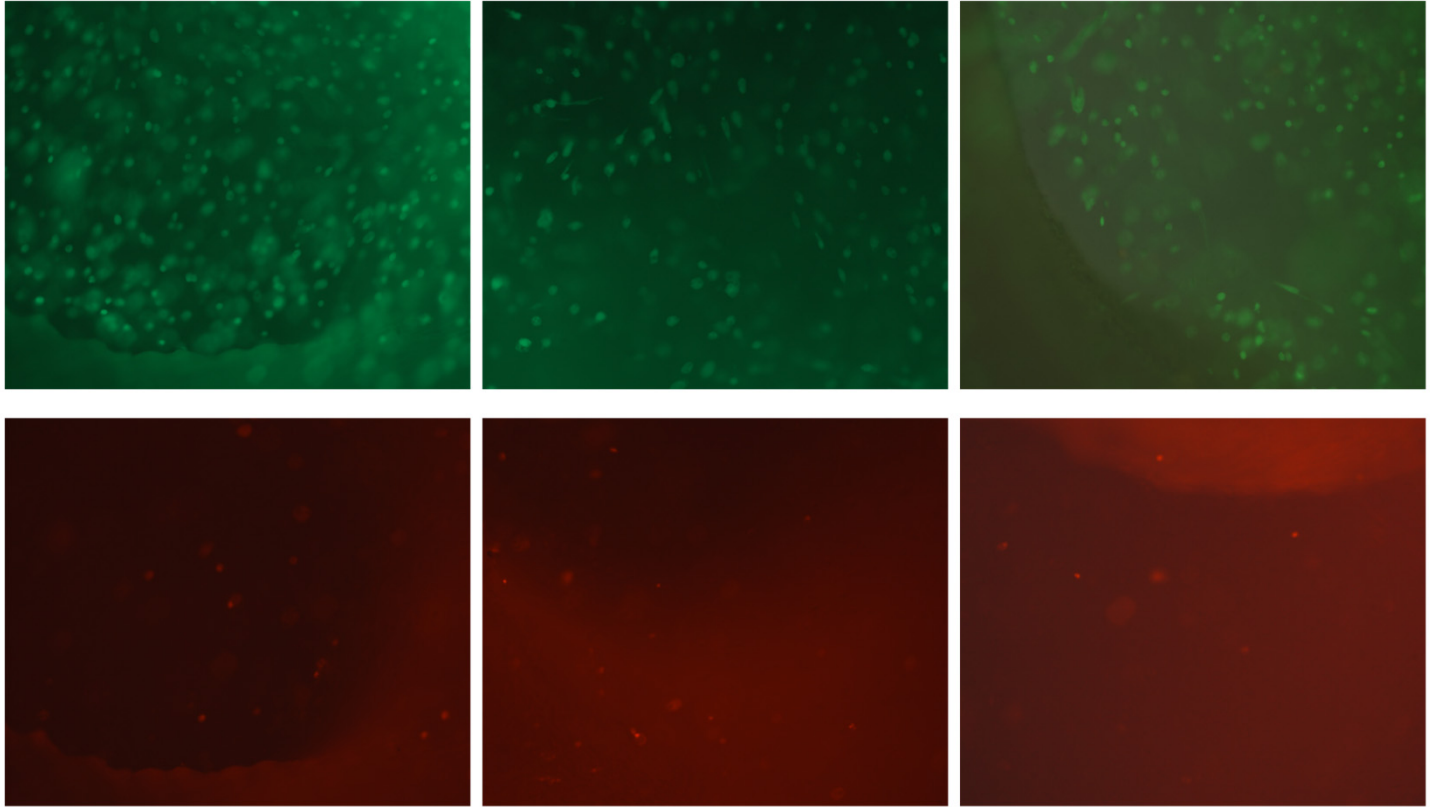
Supplementary Figure 1: Custom circuit diagram (top) to generate sine wave signal from Teensy 4.0 microcontroller. PWM signal (square wave) coming from the microcontroller is filtered by the demodulating circuit to get a sine wave output that will be used as an input signal for the LIV.



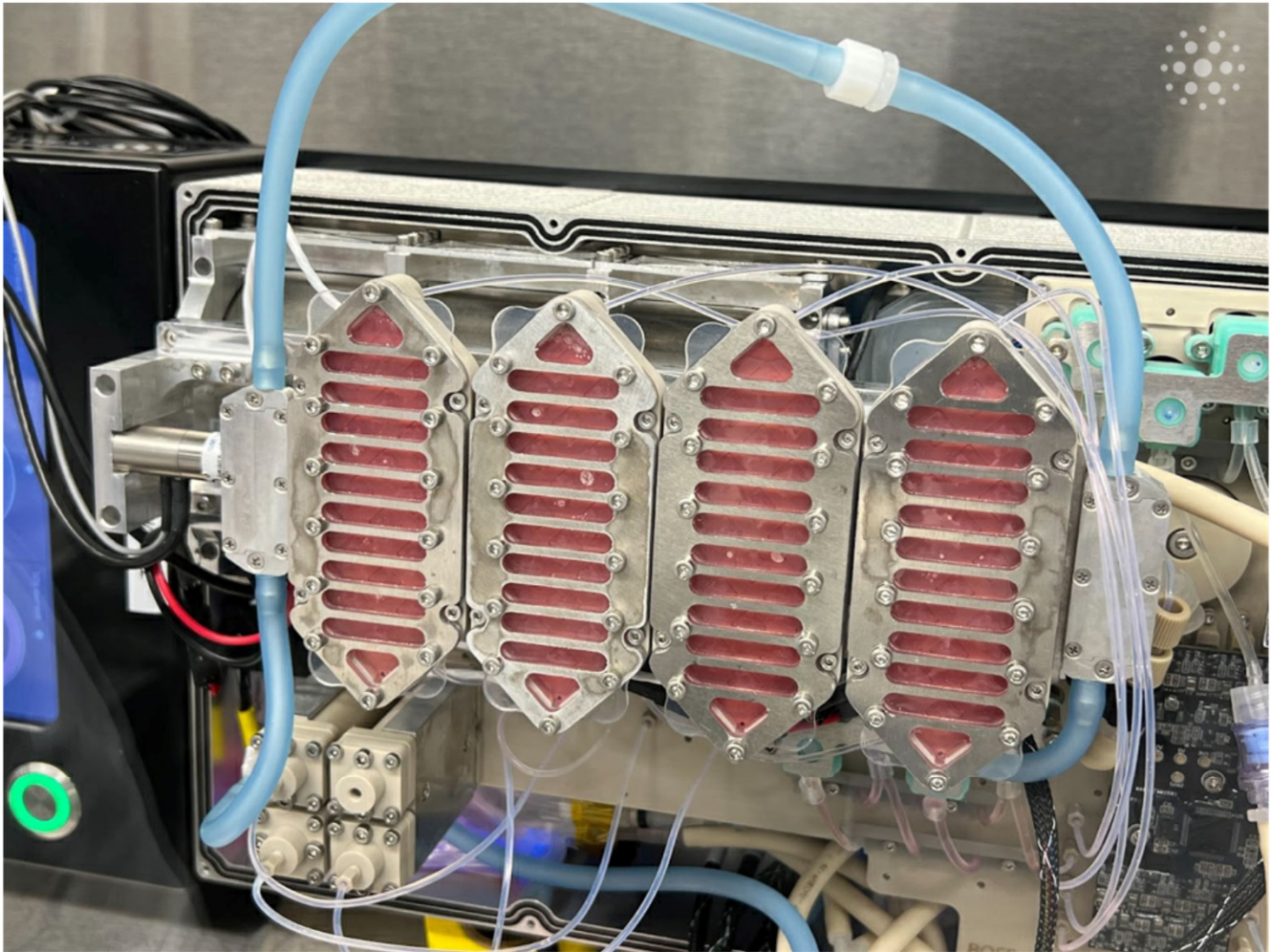
Supplementary Figure 2: CubeLab (top and bottom-left) facility that will house the vibrational bioreactor and the biological samples. The PAUL (top and bottom-right) facility designed to house and provide mechanical, electrical, and network interface from the outside



Supplementary Figure 3: Experiment schematic of the LIV regimen from signal generation to data acquisition and visualization in labVIEW



Supplementary Figure 4: Additional Live/Dead assay images across various scaffold locations and samples, demonstrating a predominance of live cells over dead ones. These images further validate the biocompatibility and cell-supportive nature of the scaffold materials used in the study.



Supplementary Figure 5: CubeWells within the CubeLab module, showcasing the custom-designed well plates developed for holding hydrogel-encapsulated scaffolds. The design incorporates a secure lid system to prevent sample spillage during spaceflight, with scaffolds protected by a biocompatible PDMS layer, further sealed by a metal lid for added safety and integrity during experiments in space.