

Article

# Oxygenated VOC Detection Using SnO<sub>2</sub> Nanoparticles with Uniformly Dispersed Bi<sub>2</sub>O<sub>3</sub>

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**Abstract:** Bi<sub>2</sub>O<sub>3</sub> particles are introduced as foreign additives onto SnO<sub>2</sub> nanoparticles (NPs) surfaces for the efficient detection of oxygenated volatile organic compounds (VOCs). Bi<sub>2</sub>O<sub>3</sub>-loaded SnO<sub>2</sub> materials are prepared via the impregnation method followed by calcination treatment. The abundant Bi<sub>2</sub>O<sub>3</sub>/SnO<sub>2</sub> interfaces are constructed by the uniform dispersion of Bi<sub>2</sub>O<sub>3</sub> particles on the SnO<sub>2</sub> surface. The results of oxygen temperature-programmed desorption suggest that Bi<sub>2</sub>O<sub>3</sub>-loaded SnO<sub>2</sub> samples display improved surface oxygen ions than neat-SnO<sub>2</sub> NPs. As a result, the gas sensor based on 1 mol% Bi<sub>2</sub>O<sub>3</sub>-loaded SnO<sub>2</sub> (1Bi-L-SnO<sub>2</sub>) composites shows significantly higher sensitivity and a faster response speed toward various oxygenated VOCs compared with SnO<sub>2</sub>, especially at 200 °C and 250 °C. The results of catalytic combustion and temperature-programmed reaction measurements reveal the dominant role of adsorption and partial oxidation during ethanol combustion on SnO<sub>2</sub> and 1Bi-L-SnO<sub>2</sub> surfaces. In this case, the improvement in the sensing performance of the 1Bi-L-SnO<sub>2</sub> sensor can be associated with the increase in surface oxygen ions at Bi<sub>2</sub>O<sub>3</sub>/SnO<sub>2</sub> interfaces. The results confirm the significant role of surface functionalization for sensing materials. The obtained outstanding sensing performance provides the potential application for the simultaneous detection of total oxygenated VOCs in practice.



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**Keywords:** SnO<sub>2</sub> nanoparticles; Bi<sub>2</sub>O<sub>3</sub>-loading; oxygenated VOC detection; interface; surface oxygen ions

## 1. Introduction

As an important group of volatile organic compounds (VOCs), oxygenated VOCs (including organic alcohols, aldehydes, and ketones, etc.) are widespread in the atmosphere derived from various human activities and biogenic emissions, such as the oxidation of hydrocarbons, emission of oxygenated fuels in industrial application, burning of biomass, etc. [1–3]. The various oxygenated VOCs lead to the formation of ozone and secondary organic aerosols, resulting in the threat to environmental pollution and human health [4,5]. In addition, many kinds of oxygenated VOCs are concomitant and interconvertible during the chemical reactions [6,7]. Hence, the importance and necessity of achieving simultaneous detection of total oxygenated VOCs in the atmosphere is noticeable. Chemiresistive-type gas sensors using semiconductor metal oxides (SMOs) like SnO<sub>2</sub>, ZnO, WO<sub>3</sub>, and In<sub>2</sub>O<sub>3</sub> have garnered many outstanding performances for various gas detection in various applications including air quality monitoring, industrial safety, and so on [8–12]. In particular, SnO<sub>2</sub> has been considered as one of the most sensitive materials by continuous research for decades [13–15]. At present, researchers have proposed various types of SnO<sub>2</sub>-based gas sensors for the efficient detection of specific oxygenated VOCs, such as ethanol, acetone, formaldehyde, and so on [16–18]. However, it is still insufficient for the detection of total oxygenated VOCs in the practical application. This highlights the importance of exploring sensing material to detect total oxygenated VOCs.

The basic understanding of the sensing mechanism is crucial for the research of gas sensors. It is normally recognized that the sensitivities of SnO<sub>2</sub>-based resistive-type gas sensors to fundamental gases such as CO and H<sub>2</sub> are evaluated by the change in electrical resistances arising from the combustion reaction between gas molecules and adsorbed oxygen ions to form CO<sub>2</sub> and H<sub>2</sub>O on the surface of materials. However, many studies indicate the complete combustion of oxygenated VOCs on the surfaces of metal oxides tends to occur under high operating temperatures (almost above 300 °C), and considerable intermediates will be produced during the combustion reaction [19–21]. Interestingly, the reported research has indicated the considerable sensitivity of SnO<sub>2</sub>-based gas sensors to ethanol at 250 °C [22]. In this case, the detection mechanism for oxygenated VOCs at temperatures below 300 °C may be different from high temperatures. Therefore, it is necessary to investigate the basic reaction process during oxygenated VOC combustion on SnO<sub>2</sub>-based gas sensors at various temperatures.

According to reported research, the sensing performance of SnO<sub>2</sub>-based gas sensors can be further improved after surface functionalization by introducing foreign additives, such as metal oxides and noble metals [9,23–26]. Generally, the functionalized surface properties of SnO<sub>2</sub> by foreign additives mainly include the modulation of active oxygen ions, acidic sites, etc. The former parameter is directly responsible for the activity of the oxidation reaction of target gas molecules. The surface acid–base property concerns the specific adsorption and selective conversion of target gas molecules on the material surface [27–29]. Thus, the sensing properties of SnO<sub>2</sub>-based gas sensors to oxygenated VOCs may be further improved by modulating the surface properties using foreign additives. α-Bi<sub>2</sub>O<sub>3</sub> particles have stood out for their high stability and environmental promise, conducting to the application as a photocatalyst, selective oxidation catalyst, sensing material, etc. [30–32]. In particular, the Bi atoms in Bi<sub>2</sub>O<sub>3</sub> contribute to the electrical conductivity due to the hybridization between the O 2p orbital and Bi 6s or 6p orbitals [33]. Several studies have confirmed the facilitation of the sensing performance of SMOs-based gas sensors by employing Bi<sub>2</sub>O<sub>3</sub> particles as foreign additives [34–36]. Moreover, it is possible that Bi<sub>2</sub>O<sub>3</sub> shows different acid–base properties with SnO<sub>2</sub> due to the different electronegativity of Bi<sup>3+</sup> (13.3) than Sn<sup>4+</sup> (16.2) [37]. Consequently, Bi<sub>2</sub>O<sub>3</sub> may be a promising candidate as a foreign additive to improve the sensing properties of SnO<sub>2</sub>-based gas sensors to oxygenated VOCs.

Herein, in order to improve the selectivity to typical oxygenated VOCs, we employed Bi<sub>2</sub>O<sub>3</sub> particles as foreign additives on a SnO<sub>2</sub>-based gas sensor. Bi<sub>2</sub>O<sub>3</sub>-loaded SnO<sub>2</sub> materials were synthesized, and Bi<sub>2</sub>O<sub>3</sub> was uniformly dispersed on the surface of SnO<sub>2</sub> nanoparticles (NPs). Bi<sub>2</sub>O<sub>3</sub>-loaded SnO<sub>2</sub> materials showed increased surface oxygen ions than SnO<sub>2</sub> NPs. As a result, the gas sensor based on 1 mol% Bi<sub>2</sub>O<sub>3</sub>-loaded SnO<sub>2</sub> nanoparticles showed excellent sensitivities toward various oxygenated VOCs, especially at 200 °C and 250 °C. Meanwhile, catalytic combustion and temperature-programmed reaction measurements revealed that the adsorption–desorption, dissociation, and partial oxidation of oxygenated VOCs were dominant at temperatures lower than 300 °C. In conclusion, the improvement in sensing properties of the SnO<sub>2</sub> sensor by Bi<sub>2</sub>O<sub>3</sub>-loading could be ascribed to the increased surface oxygen ions at the contact interfaces between Bi<sub>2</sub>O<sub>3</sub> and SnO<sub>2</sub> accelerated the adsorption and partial combustion of oxygenated VOCs. This research provided the basic insight into the reaction mechanism of oxygenated VOCs at low temperatures (below 300 °C). Meanwhile, the results indicated the uniform dispersion of foreign additives played an active role in the sensing properties of gas sensors.

## 2. Materials and Methods

### 2.1. Materials Synthesis

**The synthesis of pure SnO<sub>2</sub> NPs.** SnO<sub>2</sub> NPs were synthesized via hydrothermal synthesis accompanied by calcination. Firstly, 1 M of SnCl<sub>4</sub>·5H<sub>2</sub>O (98.0%, special grade; FUJIFILM Wako Pure Chemical Corporation, Osaka, Japan) solution was dropwise added into 1 M of NH<sub>4</sub>HCO<sub>3</sub> (99.0%, special grade; FUJIFILM Wako Pure Chemical Corporation, Osaka, Japan) solution under stirring. Next, the obtained stannic acid gel was washed

to remove  $\text{Cl}^-$  and then mixed with deionized water. After adjusting the PH to 10.5 by tetramethylammonium hydroxide (15%, special grade, FUJIFILM Wako Pure Chemical Corporation, Osaka, Japan) solution, the mixture was heated in a 100 mL stainless steel reactor with Teflon inner cylinder at 200 °C for 10 h in an oven. Subsequently, the obtained transparent sol was dried at 120 °C and annealed at 600 °C for 3 h under  $\text{O}_2$  flow to prepare  $\text{SnO}_2$  NPs.

**The synthesis of  $\text{Bi}_2\text{O}_3$ -mixed  $\text{SnO}_2$  samples.** Firstly,  $\text{Bi}_2\text{O}_3$  particles were obtained by calcining the  $\text{Bi}(\text{NO}_3)_3 \cdot 5\text{H}_2\text{O}$  (99.5 %, special grade, KISHIDA Chemical Co. Ltd., Osaka, Japan) at 550 °C for 3 h under  $\text{O}_2$  flow. Next, 1.5 g  $\text{SnO}_2$  NPs and a stoichiometric amount of  $\text{Bi}_2\text{O}_3$  powders were mixed and ground manually for 15 min. Then the particles were calcined at 530 °C for 3 h under  $\text{O}_2$  flow to obtain  $\text{Bi}_2\text{O}_3$ -mixed  $\text{SnO}_2$  materials, which were labeled as 1Bi-M- $\text{SnO}_2$  and 3Bi-M- $\text{SnO}_2$  according to the concentration of  $\text{Bi}_2\text{O}_3$  (the atomic ratio of Bi to Sn was 1/100 and 3/100, respectively).

**The synthesis of  $\text{Bi}_2\text{O}_3$ -loaded  $\text{SnO}_2$  samples.**  $\text{Bi}_2\text{O}_3$ -loaded  $\text{SnO}_2$  samples with various Bi contents were synthesized by a simple impregnation method. 1.5 g  $\text{SnO}_2$  NPs dissolved in 20 mL deionized water was impregnated on an aqueous solution of a stoichiometric amount of  $\text{Bi}(\text{NO}_3)_3 \cdot 5\text{H}_2\text{O}$  with stirring for 24 h at room temperature. The resulting precipitates were washed by centrifugation, dried at 100 °C, and calcined at 550 °C for 3 h under  $\text{O}_2$  flow. The obtained samples were referred to hereafter as 1Bi-L- $\text{SnO}_2$  and 3Bi-L- $\text{SnO}_2$  (the atomic ratio of Bi to Sn was 1/100 and 3/100, respectively).

## 2.2. Material Characterization

Wavelength-dispersive X-ray fluorescence spectroscopy (WDX, Supermini 200, Rigaku, Tokyo, Japan) was used to evaluate the content of Bi ions in  $\text{Bi}_2\text{O}_3$ -loaded  $\text{SnO}_2$  materials. The crystal structures of as-synthesized  $\text{SnO}_2$ ,  $\text{Bi}_2\text{O}_3$ -mixed  $\text{SnO}_2$ , and  $\text{Bi}_2\text{O}_3$ -loaded  $\text{SnO}_2$  samples were investigated by X-ray diffractometry (XRD; MiniFlex, Rigaku, Tokyo, Japan) with  $\text{CuK}\alpha$  radiation. The specific surface reaction and pore volume of materials were respectively evaluated by  $\text{N}_2$  adsorption/desorption analyzer (BELSORP-mini II, MicrotracBEL Corp., Osaka, Japan), and calculated by Brunauer–Emmett–Teller (BET) method and Barrett–Joyner–Halenda (BJH) method, respectively. The distribution of  $\text{Bi}_2\text{O}_3$  on the surface of  $\text{SnO}_2$  was investigated by scanning electron microscopy (SEM; JCM-7000, JEOL, Tokyo, Japan) equipped with an energy-dispersive X-ray spectroscopy (EDS) attachment.

Temperature-programmed desorption of oxygen and ammonia ( $\text{O}_2$ -TPD and  $\text{NH}_3$ -TPD) measurements were expected to estimate the adsorption–desorption of oxygen and  $\text{NH}_3$  on sample surfaces using a catalyst analyzer (BELCAT II, MicrotracBEL Corp., Osaka, Japan) equipped with a thermal conductivity (TCD) detector. The system is also linked with a quadrupole mass spectrometer (QMS, BELMASS II, MicrotracBEL Corp., Osaka, Japan) to analyze the desorbed products emitted from the material surface. The gas adsorption–desorption on the materials' surfaces was analyzed using temperature-programmed reaction (TPR) measurement. The TPR system consisted of a gas mixing system, a reaction chamber, and a gas detector with a quadrupole mass spectrometer (QMS; PrismaPlus QMG220, PFEIFFER, Hessen, Germany). The catalytic combustion measurement was employed to monitor the consumption of gas molecules and production of intermediates caused by gas combustion on material surfaces using a self-assembled system consisting of a gas mixing system, reaction chamber, and gas chromatography (GC-4000 Plus, GL Science Inc., Tokyo, Japan) equipped with a flame ionization detector and a methanizer (MT221), followed by the connection with series to 2 m of Porapak Q and Porapak N columns (GL Science Inc., Tokyo, Japan). The details of measuring processes were described in Supporting Information.

## 2.3. Sensor Fabrication and Measurement

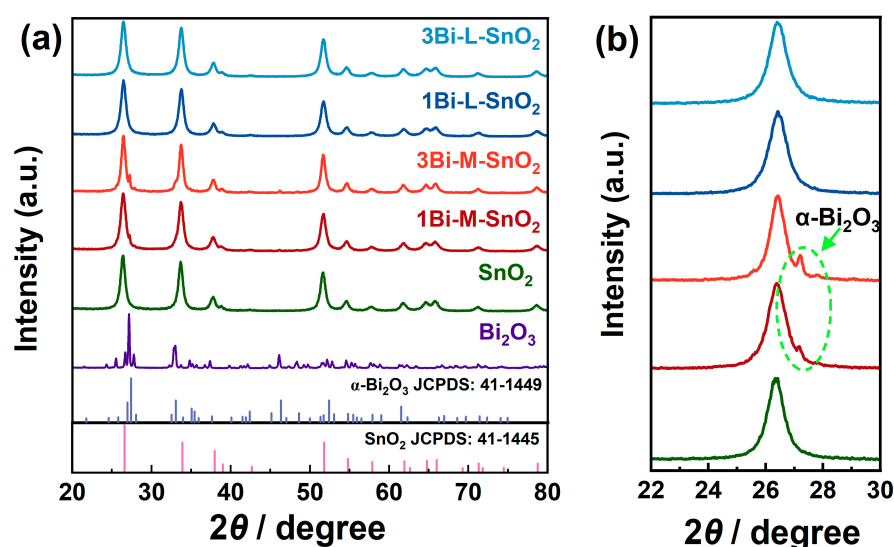
The gas sensors were fabricated by screen printing method. Firstly, Au electrodes were screen-printed on an alumina substrate ( $9 \times 13 \times 0.38 \text{ mm}^3$ ) followed by heat-treated at 850 °C for 3 h (line width: 180  $\mu\text{m}$ , distance between lines: 90  $\mu\text{m}$ , sensing area: 64  $\text{mm}^2$ ).

Next, the samples were mixed with  $\alpha$ -terpineol to form paste, and then screen-printed on the alumina substrate with Au electrodes. The resulting devices were calcined at 500 °C for 3 h in the air to remove the organic binder. The obtained gas sensors were placed in an electric furnace combined with a gas flow apparatus under the total flow rate of 100 cm<sup>3</sup>/min controlled by mass flow controllers. The operating temperatures of gas sensors were modulated at 200 °C, 250 °C, 300 °C, and 350 °C. Each sensor was connected in series to a standard resistor and applied a DC voltage of 4 V. An electrometer (2701; Keithley Instruments, Solon, OH, USA) was employed to measure the electrical resistances by evaluating the voltage across the standard resistor. The sensor response was evaluated by the change in electrical resistances in synthesis air and target gas atmospheres ( $S = R_a/R_g$ ). The response time was considered as the time required for the sensor to be 90% of maximum response change [38]. The target gases were diluted by N<sub>2</sub> with 21% O<sub>2</sub> to obtain the tested concentration (5 ppm) under a gas mixture system.

### 3. Results and Discussion

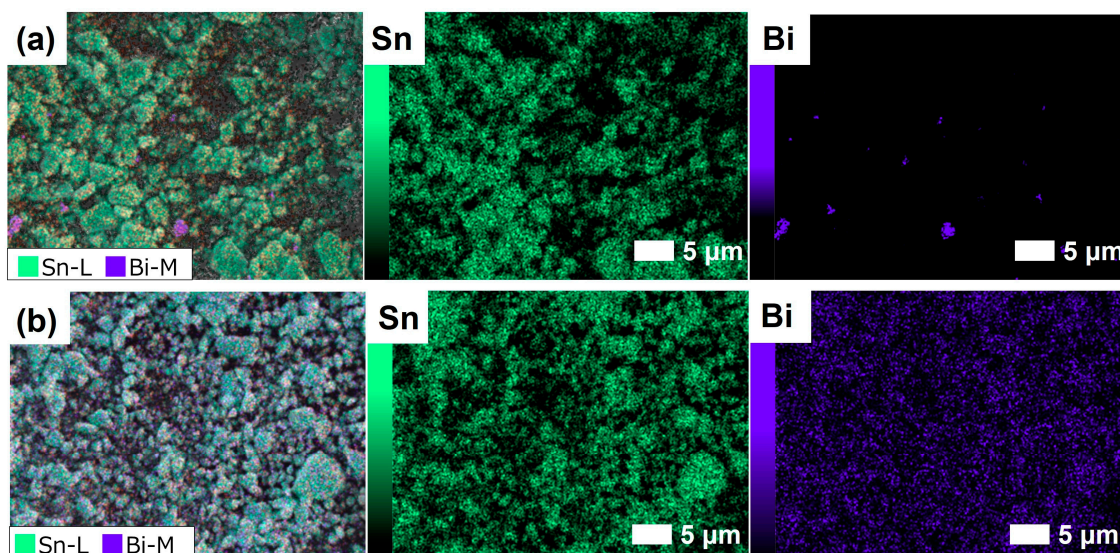
#### 3.1. Materials Characteristics

The actual concentration of Bi ions in Bi<sub>2</sub>O<sub>3</sub>-loaded SnO<sub>2</sub> materials was evaluated by WDX analysis using the calibration results of Bi<sub>2</sub>O<sub>3</sub>-mixed SnO<sub>2</sub> materials. The calculated amounts of Bi ions in 1Bi-L-SnO<sub>2</sub> and 3Bi-L-SnO<sub>2</sub> materials were 1.1 mol% and 2.8 mol%, respectively. The results indicated the comparable content of Bi ions in Bi<sub>2</sub>O<sub>3</sub>-loaded SnO<sub>2</sub> and Bi<sub>2</sub>O<sub>3</sub>-mixed SnO<sub>2</sub> materials. The XRD patterns of SnO<sub>2</sub>, Bi<sub>2</sub>O<sub>3</sub>-loaded SnO<sub>2</sub>, and Bi<sub>2</sub>O<sub>3</sub>-mixed SnO<sub>2</sub> materials (Figure 1) showed diffraction peaks matched well with tetragonal rutile structure SnO<sub>2</sub> with the space group of  $P4_2/mnm$  (JCPDS: 41-1445), indicating all as-synthesized materials had the same SnO<sub>2</sub> crystal phase. Meanwhile, the obtained Bi<sub>2</sub>O<sub>3</sub> particles were assigned to monoclinic  $\alpha$ -Bi<sub>2</sub>O<sub>3</sub> with the space group of  $P2_1/c$  (JCPDS: 41-1449). The diffraction peak appeared at about 27.15° of Bi<sub>2</sub>O<sub>3</sub>-mixed SnO<sub>2</sub> samples could be assigned to the (111) plane of  $\alpha$ -Bi<sub>2</sub>O<sub>3</sub>, proving that  $\alpha$ -Bi<sub>2</sub>O<sub>3</sub> particles were successfully complexed on the surface of SnO<sub>2</sub>. No diffraction peak of Bi<sub>2</sub>O<sub>3</sub> was observed on Bi<sub>2</sub>O<sub>3</sub>-loaded SnO<sub>2</sub> samples, which might be caused by the well-dispersion of Bi<sub>2</sub>O<sub>3</sub> particles. In addition, the average crystallite sizes of SnO<sub>2</sub> in as-prepared materials were calculated by the Scherrer formula, as shown in Table S1. The results indicated the nanostructure of obtained SnO<sub>2</sub> powders. There was no obvious change in crystallite size after Bi<sub>2</sub>O<sub>3</sub>-mixing and Bi<sub>2</sub>O<sub>3</sub>-loading on SnO<sub>2</sub> NPs.



**Figure 1.** (a) XRD patterns of SnO<sub>2</sub>, 1Bi-M-SnO<sub>2</sub>, 3Bi-M-SnO<sub>2</sub>, 1Bi-L-SnO<sub>2</sub>, 3Bi-L-SnO<sub>2</sub>; (b) the corresponding magnified region at 22–30°.

To investigate the distribution of  $\text{Bi}_2\text{O}_3$  on the  $\text{SnO}_2$  surface, we detected the SEM-EDS elemental mapping images of Sn and Bi in  $\text{Bi}_2\text{O}_3$ -mixed and  $\text{Bi}_2\text{O}_3$ -loaded  $\text{SnO}_2$  materials, as shown in Figures 2 and S2. For  $\text{Bi}_2\text{O}_3$ -mixed  $\text{SnO}_2$  materials (Figures 2a and S2a), Sn was observed almost across the whole imaged area, while Bi was exhibited only in localized regions. Meanwhile, there was little overlapping area between Bi and Sn, proving the separate distribution of  $\text{Bi}_2\text{O}_3$  and  $\text{SnO}_2$  particles with little contact interfaces in  $\text{Bi}_2\text{O}_3$ -mixed  $\text{SnO}_2$  materials. In contrast, Figures 2b and S2b revealed the uniform distribution of Sn and Bi elements in  $\text{Bi}_2\text{O}_3$ -loaded  $\text{SnO}_2$  materials, indicating  $\text{Bi}_2\text{O}_3$  particles were homogeneously dispersed on the surface of  $\text{SnO}_2$  NPs. As a result, abundant contact interfaces at  $\text{Bi}_2\text{O}_3/\text{SnO}_2$  were constructed in  $\text{Bi}_2\text{O}_3$ -loaded  $\text{SnO}_2$  materials, while major  $\text{Bi}_2\text{O}_3$  particles were agglomerated and physically mixed with  $\text{SnO}_2$  NPs in  $\text{Bi}_2\text{O}_3$ -mixed  $\text{SnO}_2$  materials. The specific surface area and average pore volume of  $\text{Bi}_2\text{O}_3$ -mixed  $\text{SnO}_2$  materials were comparable to those of  $\text{Bi}_2\text{O}_3$ -loaded  $\text{SnO}_2$  and slightly larger than that of neat- $\text{SnO}_2$  (Table S1). The indistinctive impact on the surface area and porosity of  $\text{SnO}_2$  NPs after introducing  $\text{Bi}_2\text{O}_3$  particles might be associated with the low concentration of  $\text{Bi}_2\text{O}_3$  particles, and the observed slight increase in neat- $\text{SnO}_2$  might be ascribed to the difference during the sample preparation process.

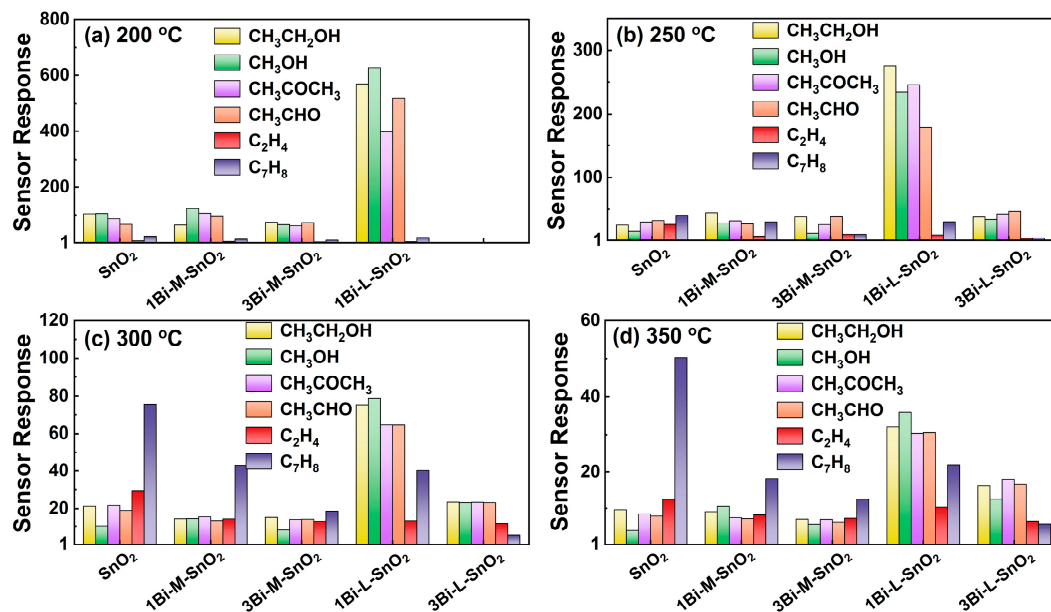


**Figure 2.** SEM-EDS elemental mapping images of Sn and Bi for (a) 1Bi-M- $\text{SnO}_2$  and (b) 1Bi-L- $\text{SnO}_2$  samples.

### 3.2. Gas Sensing Properties

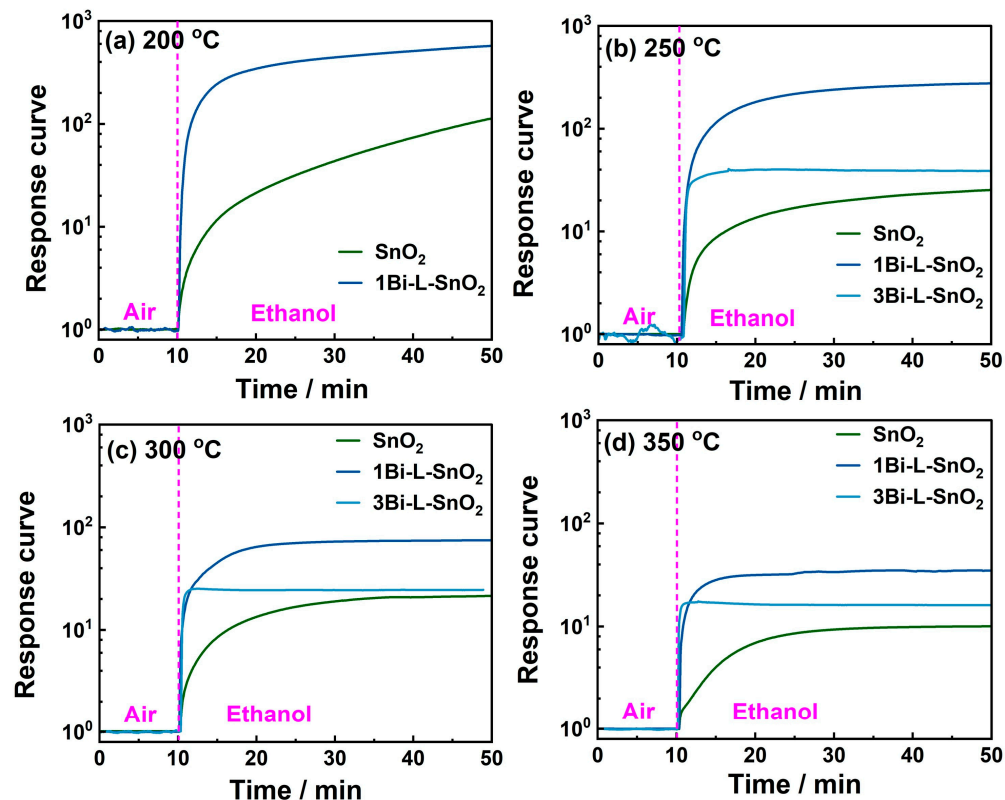
Figure S3 showed the electrical resistance in synthetic air ( $R_a$ ) of neat- $\text{SnO}_2$ ,  $\text{Bi}_2\text{O}_3$ -mixed  $\text{SnO}_2$ , and  $\text{Bi}_2\text{O}_3$ -loaded  $\text{SnO}_2$  gas sensors at 200 °C, 250 °C, 300 °C, and 350 °C. It was difficult to detect the sensing performance of the 3Bi-L- $\text{SnO}_2$  sensor at 200 °C due to the excessively high electrical resistance exceeding system limits. The  $R_a$  of  $\text{Bi}_2\text{O}_3$ -loaded  $\text{SnO}_2$  sensors were larger than that of neat- $\text{SnO}_2$  and  $\text{Bi}_2\text{O}_3$ -mixed  $\text{SnO}_2$  sensors at all detected temperatures, confirming the effect of uniform dispersion of  $\text{Bi}_2\text{O}_3$  particles on the conductivity of  $\text{SnO}_2$ -based sensor. We investigated the sensitivities of gas sensors to 5 ppm of various VOCs ( $\text{CH}_3\text{CH}_2\text{OH}$ ,  $\text{CH}_3\text{OH}$ ,  $\text{CH}_3\text{COCH}_3$ ,  $\text{CH}_3\text{CHO}$ ,  $\text{C}_2\text{H}_4$ , and  $\text{C}_7\text{H}_8$ ) at 200–350 °C. As displayed in Figure 3, the gas sensors based on  $\text{Bi}_2\text{O}_3$ -mixed  $\text{SnO}_2$  samples showed similar responses to tested oxygenated VOCs ( $\text{CH}_3\text{CH}_2\text{OH}$ ,  $\text{CH}_3\text{OH}$ ,  $\text{CH}_3\text{COCH}_3$ ,  $\text{CH}_3\text{CHO}$ ) with neat- $\text{SnO}_2$  sensor, indicating the agglomerated  $\text{Bi}_2\text{O}_3$  particles exhibited little effect on the reactivity of  $\text{SnO}_2$  for oxygenated VOCs detection. Meanwhile, the 1Bi-L- $\text{SnO}_2$  sensor showed dramatically improved sensitivities to tested oxygenated VOCs at all detected operating temperatures (especially at 200 °C and 250 °C). The phenomenon confirmed the uniform dispersion of  $\text{Bi}_2\text{O}_3$  particles on the  $\text{SnO}_2$  surface during the  $\text{Bi}_2\text{O}_3$ -

loading process played a vital role in the adsorption and combustion of oxygenated VOCs. However, the responses of the 3Bi-L-SnO<sub>2</sub> sensor to oxygenated VOCs were lower than that of the 1Bi-L-SnO<sub>2</sub> sensor, which might be attributed to the excessive dispersion of Bi<sub>2</sub>O<sub>3</sub> particles prevented the diffusion of gas molecules into the sensing layer of SnO<sub>2</sub> [39]. Besides, the neat-SnO<sub>2</sub> sensor showed clearly higher responses to C<sub>2</sub>H<sub>4</sub> and C<sub>7</sub>H<sub>8</sub> than Bi<sub>2</sub>O<sub>3</sub>-loaded SnO<sub>2</sub> and Bi<sub>2</sub>O<sub>3</sub>-mixed SnO<sub>2</sub> sensors. In conclusion, the 1Bi-L-SnO<sub>2</sub> sensor showed excellent sensitivity and selectivity to oxygenated VOCs, especially at 200 °C and 250 °C. Additionally, the responses toward oxygenated VOCs were decreased with the increase in temperature.



**Figure 3.** The responses of as-fabricated gas sensors to 5 ppm various VOCs at (a) 200 °C, (b) 250 °C, (c) 300 °C, and (d) 350 °C.

The response curve is a crucial parameter to estimate the sensing performance of gas sensors. The dynamic time-dependence response curves of obtained gas sensors based on SnO<sub>2</sub> and Bi<sub>2</sub>O<sub>3</sub>-loaded SnO<sub>2</sub> materials toward ethanol as the representative of tested oxygenated VOCs at 200–350 °C are shown in Figure 4. The corresponding response time required for the sensors to 90% of response changes are calculated in Table S2. Figures S4–S7 exhibited the dynamic response curves of all the obtained gas sensors toward tested oxygenated VOCs at 200–350 °C. Clearly, the responses of all sensors were rapidly increased during the initial period under the target gases' atmosphere. Generally, the initial rapid increase in response could be associated with the consumption of adsorbed oxygen ions on the surface of sensing materials. Bi<sub>2</sub>O<sub>3</sub>-loaded SnO<sub>2</sub> sensors showed an obviously improved increasing tendency at the initial period compared to neat-SnO<sub>2</sub> sensors. Moreover, the response time of SnO<sub>2</sub> to ethanol was decreased with the rising Bi<sub>2</sub>O<sub>3</sub>-loading content. In this case, the improved response speed of Bi<sub>2</sub>O<sub>3</sub>-loaded SnO<sub>2</sub> sensors to ethanol might be assigned to the improved amount of surface oxygen ions of Bi<sub>2</sub>O<sub>3</sub>-loaded SnO<sub>2</sub> surfaces. The response speeds of all sensors were increased with the rising temperature, corresponding to the enhanced reactivity of surface oxygen ions of sensing materials. Consequently, the rapid response and outstanding sensitivity to oxygenated VOCs combined with weak responses to C<sub>2</sub>H<sub>4</sub> and C<sub>7</sub>H<sub>8</sub> of the 1Bi-L-SnO<sub>2</sub> sensor proved the potential for sensitive and selective oxygenated VOCs detection. Additionally, the results indicated the different distribution of Bi<sub>2</sub>O<sub>3</sub> particles on the SnO<sub>2</sub> surface caused by Bi<sub>2</sub>O<sub>3</sub>-mixing and Bi<sub>2</sub>O<sub>3</sub>-loading processes showed various sensing performances, the abundant Bi<sub>2</sub>O<sub>3</sub>/SnO<sub>2</sub> interfaces formed by the uniform dispersion of Bi<sub>2</sub>O<sub>3</sub> particles might be the crucial parameter improving the sensing properties.

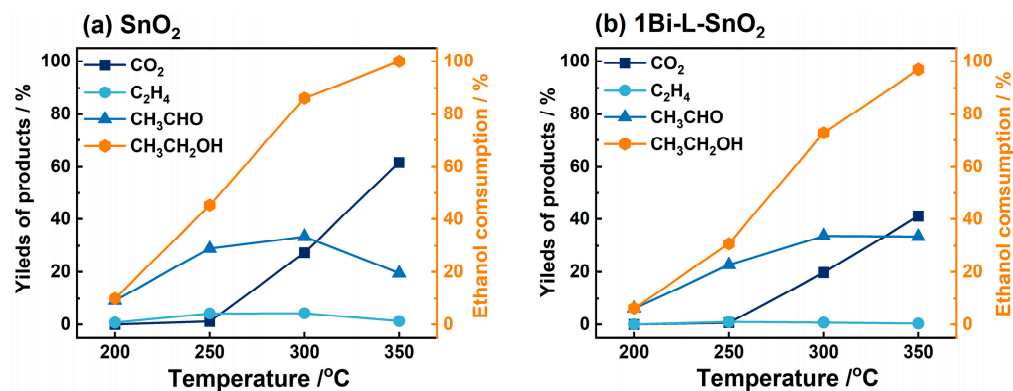


**Figure 4.** Dynamic time-dependence response curves of SnO<sub>2</sub> and Bi<sub>2</sub>O<sub>3</sub>-loaded SnO<sub>2</sub> sensors to 5 ppm of ethanol at (a) 200 °C, (b) 250 °C, (c) 300 °C, and (d) 350 °C.

### 3.3. Catalytic Combustion Measurement

Generally, the combustion of gas molecules on material surfaces plays a vital role in the sensing performance of gas sensors. As one of the typical oxygenated VOCs, the combustion of ethanol on neat-SnO<sub>2</sub> and 1Bi-L-SnO<sub>2</sub> surfaces under 200–350 °C was investigated, as shown in Figure 5. It was observed that the consumption of ethanol gradually increased from 200 °C and approximately reached 100% at 350 °C. Simultaneously, a number of CH<sub>3</sub>CHO and a little of C<sub>2</sub>H<sub>4</sub> were produced during 200–350 °C, which were caused by the dehydrogenation and dehydration of ethanol, respectively. Noteworthy, no CO<sub>2</sub> was detected at 200 °C and 250 °C, indicating the absence of complete combustion of ethanol. Hence, ethanol molecules were initially adsorbed on material surfaces and then converted to CH<sub>3</sub>CHO combined with a little C<sub>2</sub>H<sub>4</sub>. Subsequently, CH<sub>3</sub>CHO molecules were oxidized to intermediates (CH<sub>3</sub>COOH, CO, etc.) [40,41]. With the further increase in temperature, CO<sub>2</sub> was gradually produced by the complete combustion of ethanol. Meanwhile, the production of CO<sub>2</sub> was about 27% and 61% at 300 °C and 350 °C, revealing the presence of both partial and complete combustion of ethanol on the SnO<sub>2</sub> surface. Besides, the productions of CO<sub>2</sub> and C<sub>2</sub>H<sub>4</sub> on 1Bi-L-SnO<sub>2</sub> were smaller than those on the SnO<sub>2</sub> surface, as demonstrated in Figure S8. As reported previously, ethanol molecules could be converted to CH<sub>3</sub>CHO and C<sub>2</sub>H<sub>4</sub> on basic and acid material surfaces, respectively [19]. Hence, the almost disappeared yield of C<sub>2</sub>H<sub>4</sub> on the 1Bi-L-SnO<sub>2</sub> surface might be ascribed to the reduced surface acidity. Furthermore, the decreased CO<sub>2</sub> production corresponded to the declined complete combustion of ethanol. Consequently, the complete combustion of ethanol to CO<sub>2</sub> on the SnO<sub>2</sub> surface was weakened after Bi<sub>2</sub>O<sub>3</sub>-loading, and CH<sub>3</sub>CHO became the main intermediate combined with the reduced production of C<sub>2</sub>H<sub>4</sub>. As a result, partial combustion was dominant during the combustion of ethanol and CH<sub>3</sub>CHO on the surface of 1Bi-L-SnO<sub>2</sub> material below 300 °C. In addition, the combustion of acetone on SnO<sub>2</sub> and 1Bi-L-SnO<sub>2</sub> surfaces was investigated in Figure S9. It was obvious that no acetone consumption and CO<sub>2</sub> yields were detected at 200 °C and 250 °C, suggesting little

combustion of acetone occurred on material surfaces. As the temperature increased to 300 °C and 350 °C, part of the acetone was combusted to CO<sub>2</sub>, a little CH<sub>3</sub>CHO, and other intermediates. Similarly, neat-SnO<sub>2</sub> showed a higher amount of acetone consumption and CO<sub>2</sub> production than 1Bi-L-SnO<sub>2</sub>, indicating the improvement in partial combustion of acetone after Bi<sub>2</sub>O<sub>3</sub>-loading. As a result, the combustion of acetone on the 1Bi-L-SnO<sub>2</sub> surface exhibited a similar phenomenon to that of ethanol, which was mainly in accordance with partial combustion.

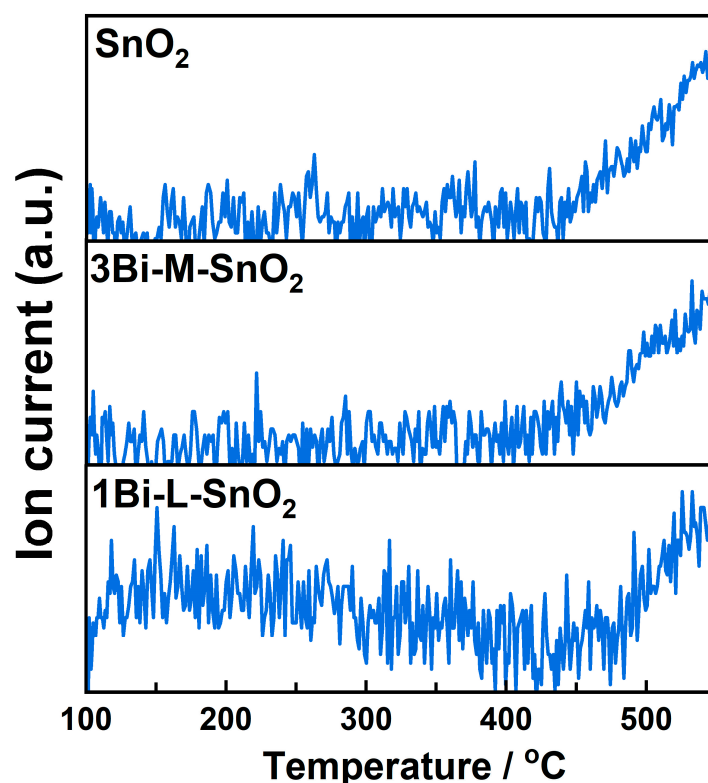


**Figure 5.** The temperature-dependence consumption of CH<sub>3</sub>CH<sub>2</sub>OH and the yields of products (CO<sub>2</sub>, CH<sub>3</sub>CHO, and C<sub>2</sub>H<sub>4</sub>) during ethanol combustion on the surfaces of (a) SnO<sub>2</sub> and (b) 1Bi-L-SnO<sub>2</sub> particles from 200 °C to 350 °C.

### 3.4. TPD and TPR Measurements

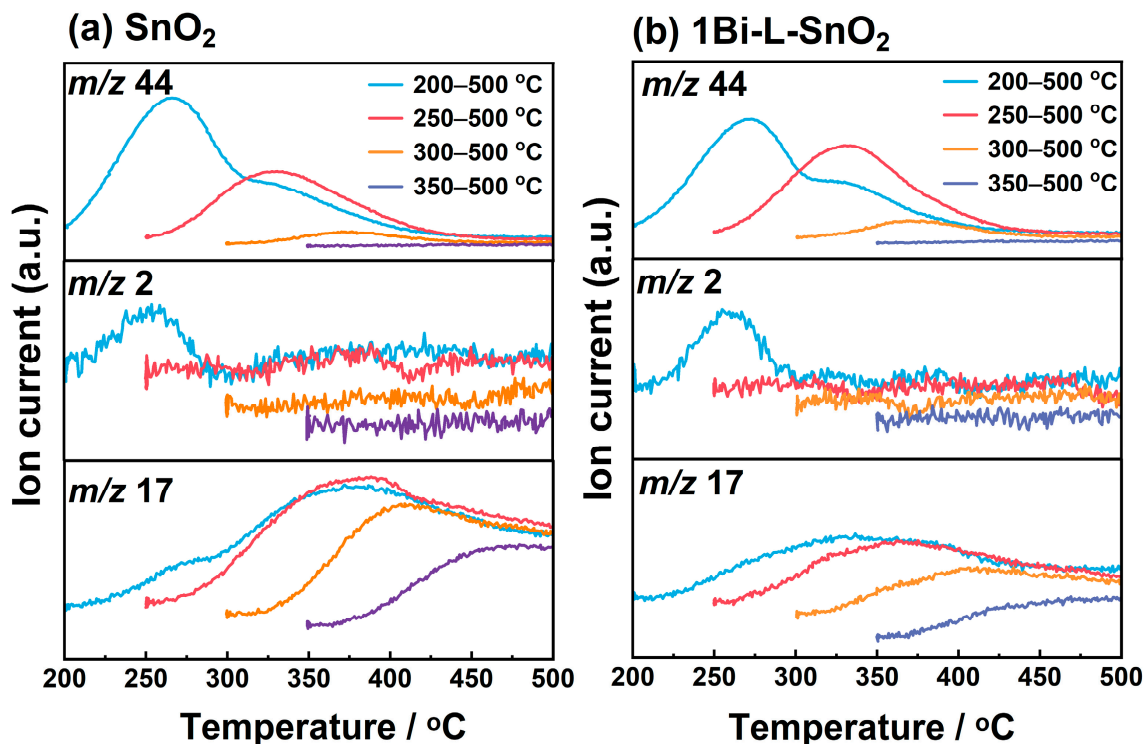
The desorption of oxygen on the surfaces of SnO<sub>2</sub>, 3Bi-M-SnO<sub>2</sub>, and 1Bi-L-SnO<sub>2</sub> materials was evaluated by O<sub>2</sub>-TPD combined with a mass spectrometer monitored at *m/z* 32, as depicted in Figure 6. Obviously, the desorption signal of SnO<sub>2</sub> gradually increased from approximately 450 °C, corresponding to the desorption of surface lattice oxygen (O<sup>2-</sup>) of SnO<sub>2</sub> [16,42]. 3Bi-M-SnO<sub>2</sub> sample showed a similar phenomenon with neat-SnO<sub>2</sub>, indicating the agglomerated Bi<sub>2</sub>O<sub>3</sub> showed little effect on the desorption of oxygen of SnO<sub>2</sub>. For 1Bi-L-SnO<sub>2</sub>, the temperature-dependent desorption signal could be roughly categorized as 100–400 °C and 400–550 °C. The former signal was assigned to the desorption of active oxygen ions (such as O<sub>2</sub><sup>-</sup>, O<sup>-</sup>, and O<sup>2-</sup>) [43,44]. The desorption at higher temperatures was caused by the desorption of O<sub>2</sub> arising from the surface lattice oxygen of SnO<sub>2</sub>. Consequently, the Bi<sub>2</sub>O<sub>3</sub>-loading onto the SnO<sub>2</sub> surface facilitated the desorption of surface oxygen ions during 100–400 °C, which might be attributed to the abundant Bi<sub>2</sub>O<sub>3</sub>/SnO<sub>2</sub> interfaces. Additionally, the effect of Bi<sub>2</sub>O<sub>3</sub> particles on the surface acidity of SnO<sub>2</sub> NPs was investigated by NH<sub>3</sub>-TPD measurements. As demonstrated in Figure S10, the desorption amount of NH<sub>3</sub> on the SnO<sub>2</sub> surface was decreased after Bi<sub>2</sub>O<sub>3</sub>-mixing and Bi<sub>2</sub>O<sub>3</sub>-loading processes, suggesting the exposure of acid sites on the surface of SnO<sub>2</sub> was declined by the introduction of Bi<sub>2</sub>O<sub>3</sub> particles. In this case, neat-SnO<sub>2</sub> showed the highest responses to C<sub>2</sub>H<sub>4</sub> and C<sub>7</sub>H<sub>8</sub> than other sensors, consistent with the amount of surface acidity. The result indicated that surface acidic sites might play a more vital role in the combustion of C<sub>2</sub>H<sub>4</sub> and C<sub>7</sub>H<sub>8</sub> than surface oxygen ions [45].





**Figure 6.** O<sub>2</sub>-TPD combined with mass spectrometer monitored at  $m/z$  32 of SnO<sub>2</sub>, 3Bi-M-SnO<sub>2</sub>, and 1Bi-L-SnO<sub>2</sub> materials.

The desorption signals on SnO<sub>2</sub> and 1Bi-L-SnO<sub>2</sub> surfaces after ethanol adsorption were investigated by ethanol-TPR measurements. Initially, ethanol molecules were respectively adsorbed on the materials at various temperatures (200 °C, 250 °C, 300 °C, and 350 °C) and then heated to 500 °C under Ar flow containing 21% of O<sub>2</sub>. The desorption signals at mass numbers 44 (the fragment of CH<sub>3</sub>CHO and CO<sub>2</sub>), 2 (H<sub>2</sub>), and 17 (H<sub>2</sub>O) were monitored during the heating period, as shown in Figure 7. Roughly, SnO<sub>2</sub> and 1Bi-L-SnO<sub>2</sub> materials showed similar TPR spectra. When ethanol was exposed at 200 °C,  $m/z$  44 and  $m/z$  2 exhibited distinct desorption peaks during 200–300 °C. According to the catalytic combustion result, no CO<sub>2</sub> was produced at 200 °C and 250 °C, indicating the peak at  $m/z$  44 was probably mainly caused by the desorption of CH<sub>3</sub>CHO. The peak at  $m/z$  2 was assigned to the production of H<sub>2</sub> arising from the deprotonation or dehydrogenation of ethanol. The phenomenon suggested that ethanol molecules could be dissociated to CH<sub>3</sub>CHO accompanied by the release of protons on SnO<sub>2</sub> and 1Bi-L-SnO<sub>2</sub> surfaces. When the materials adsorbed ethanol above 250 °C,  $m/z$  44 and  $m/z$  17 exhibited desorption peaks while no H<sub>2</sub> was produced during the heating process, indicating ethanol molecules were further oxidized. As a result, ethanol molecules on SnO<sub>2</sub> and 1Bi-L-SnO<sub>2</sub> surfaces were mainly followed by dissociation and partial oxidation at 200 °C and 250 °C. Besides, the desorption amount at  $m/z$  44 was drastically decreased when ethanol was exposed at 300 °C and 350 °C, illustrating ethanol molecules were easily oxidized and desorbed from the material surface at high temperatures.



**Figure 7.** TPR spectra of (a)  $\text{SnO}_2$  and (b)  $1\text{Bi-L-SnO}_2$  under  $\text{O}_2/\text{Ar}$  flow after exposing 100 ppm ethanol/ $\text{Ar}$  during heating period from 200 °C, 250 °C, 300 °C, 350 °C, to 500 °C at mass numbers 44, 2, and 17.

### 3.5. Sensing Mechanism

Based on the above discussions, we proposed the possible sensing mechanism of  $\text{SnO}_2$  and  $\text{Bi}_2\text{O}_3$ -loaded  $\text{SnO}_2$  gas sensors. Firstly, the reaction pathway of ethanol combustion on the  $\text{SnO}_2$  surface was investigated as the representative of oxygenated VOCs. For neat- $\text{SnO}_2$ , at 200 °C and 250 °C, ethanol molecules were initially adsorbed and then partially dissociated to ethoxides or  $\text{CH}_3\text{CHO}$  via deprotonation or dehydrogenation, respectively. Meanwhile, the dissociated protons could remain on the  $\text{SnO}_2$  surface by bonding with oxygen ions. Next, part of the ethoxides and  $\text{CH}_3\text{CHO}$  molecules were further oxidized to  $\text{CO}_2$  and intermediates ( $\text{CH}_3\text{COOH}$ ,  $\text{CO}$ , etc.) by combustion reaction as the increase in temperature (300 °C and 350 °C). On the other hand, a small amount of ethanol molecules was converted to  $\text{C}_2\text{H}_4$  and  $\text{H}_2\text{O}$  by dehydration at the acidic sites of  $\text{SnO}_2$ . In this case, the dissociation and partial oxidation of ethanol exhibited a significant effect on the sensitivities especially at 200 °C and 250 °C. According to the results of  $\text{O}_2$ -TPD measurements, the surface lattice oxygen of  $\text{SnO}_2$  tended to be active at higher temperatures. Hence, the surface oxygen ions were major active species for ethanol adsorption.

Figure 8 shows the reaction pathway of ethanol combustion on the  $1\text{Bi-L-SnO}_2$  surface.  $1\text{Bi-L-SnO}_2$  sensor showed a larger amount of surface oxygen ions, as demonstrated in  $\text{O}_2$ -TPD profiles. At 200 °C and 250 °C, the increased basic oxygen ions (mainly  $\text{O}^-$ ) could attract the adsorption of ethanol molecules by promoting the cleavage of acidic  $\alpha$ -H and O-H bonding. Subsequently, the ethoxides and  $\text{CH}_3\text{CHO}$  were partially oxidized with the increase in temperature, which was similar to neat- $\text{SnO}_2$ . Additionally, the catalytic combustion results indicated  $1\text{Bi-L-SnO}_2$  showed a declined production of  $\text{CO}_2$  than neat- $\text{SnO}_2$  material, revealing the improvement in surface oxygen ions improved the partial combustion of ethanol. In this context, the construction of  $\text{Bi}_2\text{O}_3/\text{SnO}_2$  interfaces mainly improved the initial adsorption, dissociation, and partial combustion of ethanol molecules. As a result, the  $1\text{Bi-L-SnO}_2$  sensor showed higher sensitivity and faster response speed to ethanol than neat- $\text{SnO}_2$ , particularly at 200 °C and 250 °C. Furthermore, oxygen vacancies would be exposed after consuming the surface oxygen ions, especially at high temperatures,

accelerating the adsorption of oxygen and gas molecules. In addition, catalytic combustion and TPR measurements confirmed the active combustion and desorption of ethanol on material surfaces at 300–350 °C, leading to a smaller change in the electrical resistance than at 200–250 °C. Hence, the SnO<sub>2</sub> and 1Bi-L-SnO<sub>2</sub> sensors showed fast response speeds but weak sensitivities to ethanol at high temperatures. Moreover, the production of C<sub>2</sub>H<sub>4</sub> almost disappeared due to the declined exposure of surface acidic sites by the Bi<sub>2</sub>O<sub>3</sub>-loading process. With the increasing concentration of Bi<sub>2</sub>O<sub>3</sub> (3Bi-L-SnO<sub>2</sub> sensor), the amount of surface oxygen ions was further increased, while the excessively dispersed Bi<sub>2</sub>O<sub>3</sub> particles on the SnO<sub>2</sub> surface disturbed the adsorption of gas molecules on SnO<sub>2</sub>, suppressing the further oxidation. Therefore, the 3Bi-L-SnO<sub>2</sub> sensor showed a higher response speed but lower sensitivity to oxygenated VOCs than the 1Bi-L-SnO<sub>2</sub> sensor.

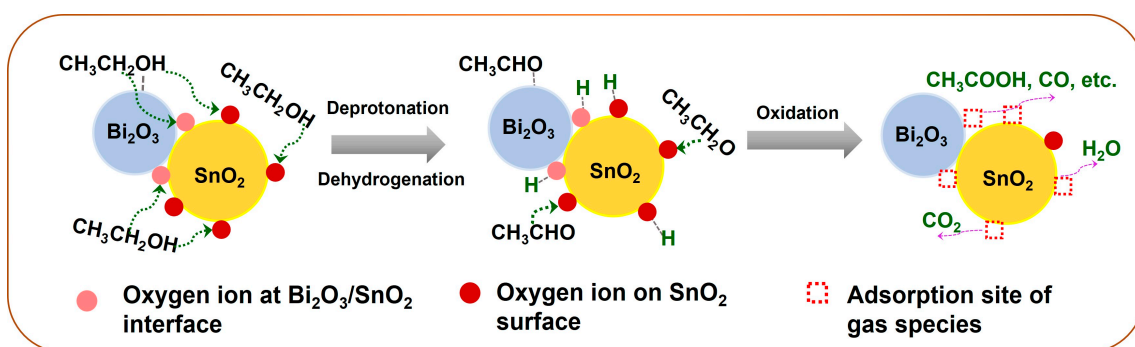


Figure 8. Schematic illustration of ethanol oxidation route on the 1Bi-L-SnO<sub>2</sub> material surface.

As the major intermediate during ethanol combustion, the oxidation of CH<sub>3</sub>CHO might show similar productions with that of ethanol combustion, such as CH<sub>3</sub>COOH and CO. In addition, the reaction pathway of methanol combustion frequently consisted with ethanol due to the same functional group. For example, CH<sub>3</sub>OH molecules can be dissociated to HCHO by dehydrogenation and further oxidized to HCOOH, CO, and CO<sub>2</sub>. For acetone combustion, we could not observe the main intermediates by catalytic combustion measurement except a little CH<sub>3</sub>CHO at 300 °C and 350 °C. However, the acidic  $\alpha$ -H bonding of acetone might be cleavage by the basic adsorption ions to form CH<sub>3</sub>COCH<sub>2</sub><sup>-</sup> and protons. Subsequently, CH<sub>3</sub>CHO and CH<sub>3</sub>COOH might be produced during acetone combustion like ethanol combustion [46,47]. In addition, the catalytic combustion results confirmed the combustion of acetone on the 1Bi-L-SnO<sub>2</sub> surface exhibited a similar phenomenon to that of ethanol, which was mainly in accordance with the adsorption–desorption and partial combustion. As a result, 1Bi-L-SnO<sub>2</sub> showed outstanding sensitivity and selectivity to oxygenated VOCs due to the improvement in surface oxygen ions.

#### 4. Conclusions

In this experiment, Bi<sub>2</sub>O<sub>3</sub>-mixed SnO<sub>2</sub> and Bi<sub>2</sub>O<sub>3</sub>-loaded SnO<sub>2</sub> materials were synthesized for fabricating efficient gas sensors toward multiple oxygenated VOCs. Bi<sub>2</sub>O<sub>3</sub> particles were uniformly dispersed on the SnO<sub>2</sub> surface for Bi<sub>2</sub>O<sub>3</sub>-loaded SnO<sub>2</sub> materials, leading to the construction of abundant Bi<sub>2</sub>O<sub>3</sub>/SnO<sub>2</sub> interfaces. While agglomerated Bi<sub>2</sub>O<sub>3</sub> particles were physically mixed with SnO<sub>2</sub> NPs in Bi<sub>2</sub>O<sub>3</sub>-mixed SnO<sub>2</sub> samples. O<sub>2</sub>-TPD spectra revealed the increased surface oxygen ions of Bi<sub>2</sub>O<sub>3</sub>-loaded SnO<sub>2</sub> materials than that of SnO<sub>2</sub> and Bi<sub>2</sub>O<sub>3</sub>-mixed SnO<sub>2</sub> materials. 1Bi-L-SnO<sub>2</sub> sensor showed improved sensitivity and selectivity to tested oxygenated VOCs, particularly at 200 °C and 250 °C. While the Bi<sub>2</sub>O<sub>3</sub>-mixed SnO<sub>2</sub> sensor exhibited similar sensing properties to the SnO<sub>2</sub> sensor. According to the results of catalytic combustion and TPR measurements, the detected sensitivities to ethanol of SnO<sub>2</sub> and 1Bi-L-SnO<sub>2</sub> sensors were primarily caused by the adsorption and partial oxidation of ethanol molecules. Meanwhile, the Bi<sub>2</sub>O<sub>3</sub>-loading process improved the partial combustion of ethanol on the SnO<sub>2</sub> surface. The phenomenon indicated the

effect of different distributions of  $\text{Bi}_2\text{O}_3$  on the sensing performance of  $\text{SnO}_2$ -based sensors. The abundant  $\text{Bi}_2\text{O}_3/\text{SnO}_2$  interfaces formed by the uniform dispersion of  $\text{Bi}_2\text{O}_3$  particles were responsible for the enhancement of surface oxygen ions and sensing properties. The research provided a promising application for achieving sensitive and selective gas sensors for total oxygenated VOC detection by modulating the surface properties of sensing materials using foreign additives.

**Supplementary Materials:** The following supporting information can be downloaded at: <https://www.mdpi.com/article/10.3390/nano14242032/s1>, Figure S1: Explanation of operating processes during (a)  $\text{O}_2$ -TPD-MS (b)  $\text{NH}_3$ -TPD-MS. Figure S2. SEM-EDS mapping images of Sn and Bi elements for (a) 3Bi-M- $\text{SnO}_2$  and (b) 3Bi-L- $\text{SnO}_2$  samples. Figure S3. The electrical resistances in synthetic air of as-fabricated gas sensors at 200 °C, 250 °C, 300 °C, and 350 °C. Figure S4: Dynamic time-dependence response curves of gas sensors to 5 ppm of (a)  $\text{CH}_3\text{CH}_2\text{OH}$ , (b)  $\text{CH}_3\text{CHO}$ , (c)  $\text{CH}_3\text{COCH}_3$ , (d)  $\text{CH}_3\text{OH}$  at 200 °C. Figure S5: Dynamic time-dependence response curves of gas sensors to 5 ppm of (a)  $\text{CH}_3\text{CH}_2\text{OH}$ , (b)  $\text{CH}_3\text{CHO}$ , (c)  $\text{CH}_3\text{COCH}_3$ , (d)  $\text{CH}_3\text{OH}$  at 250 °C. Figure S6: Dynamic time-dependence response curves of gas sensors to 5 ppm of (a)  $\text{CH}_3\text{CH}_2\text{OH}$ , (b)  $\text{CH}_3\text{CHO}$ , (c)  $\text{CH}_3\text{COCH}_3$ , (d)  $\text{CH}_3\text{OH}$  at 300 °C. Figure S7: Dynamic time-dependence response curves of gas sensors to 5 ppm of (a)  $\text{CH}_3\text{CH}_2\text{OH}$ , (b)  $\text{CH}_3\text{CHO}$ , (c)  $\text{CH}_3\text{COCH}_3$ , (d)  $\text{CH}_3\text{OH}$  at 350 °C. Figure S8. The temperature-dependence of (a)  $\text{CH}_3\text{CH}_2\text{OH}$  consumption, (b)  $\text{CO}_2$ , (c)  $\text{CH}_3\text{CHO}$ , and (d)  $\text{C}_2\text{H}_4$  yields during ethanol combustion on the surfaces of  $\text{SnO}_2$  and 1Bi-L- $\text{SnO}_2$  particles from 200 °C to 350 °C. Figure S9. The temperature-dependence of (a)  $\text{CH}_3\text{COCH}_3$  consumption, (b)  $\text{CO}_2$ , and (c)  $\text{CH}_3\text{CHO}$  yields during acetone combustion on the surfaces of  $\text{SnO}_2$  and 1Bi-L- $\text{SnO}_2$  particles from 200 °C to 350 °C. Figure S10. (a)  $\text{NH}_3$ -TPD profiles of as-prepared materials;  $\text{NH}_3$ -TPD combined with mass spectrometer spectra of (b)  $\text{SnO}_2$ , (c) 1Bi-M- $\text{SnO}_2$ , (d) 3Bi-M- $\text{SnO}_2$ , (e) 1Bi-L- $\text{SnO}_2$  and (f) 3Bi-L- $\text{SnO}_2$  materials. Table S1. Average crystallite size, BET, and BJH results of  $\text{SnO}_2$ , 1Bi-M- $\text{SnO}_2$ , 3Bi-M- $\text{SnO}_2$ , 1Bi-L- $\text{SnO}_2$ , 3Bi-L- $\text{SnO}_2$  materials. Table S2. Response time of  $\text{SnO}_2$  and  $\text{Bi}_2\text{O}_3$ -loaded sensors to 5 ppm of ethanol at 200–350 °C.

**Author Contributions:** Conceptualization: H.Y., K.S. (Koichi Suematsu), and K.S. (Kengo Shimano); Experimental: H.Y. and F.H.M.; Writing—original draft: H.Y.; Writing—review and editing: K.S. (Koichi Suematsu), K.W. and K.S. (Kengo Shimano); Funding acquisition: K.S. (Koichi Suematsu) and K.S. (Kengo Shimano). All authors have read and agreed to the published version of the manuscript.

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