

Optimization Control Method for Low-Voltage DC Microgrid with Low Carbon, Economy, and Reliability

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by the K-means clustering method to deal with the uncertainty of photovoltaic and load. Based on the time of use electricity price, the operating modes of the low-voltage DC microgrid system are divided to formulate relevant energy exchange strategies. The equivalent electricity weight method is used to evaluate the service

life of energy storage systems, and a multiobjective optimization control model of low-voltage DC microgrid for multiple scenarios is established with the objective functions of maximizing daily net income, minimizing equivalent charging and discharging capacity of energy storage systems, and minimizing carbon dioxide emissions. The NSAPOA is used to iteratively obtain the Pareto solution set, and the final optimal solution is determined by employing the multiattributive border approximation area comparison (MABAC) algorithm. Analysis results show that this can achieve economic and low-carbon optimization operation of the system throughout the whole life cycle of energy storage systems.

1. INTRODUCTION

Microgrids have garnered significant focus to enhance the efficiency of using renewable energy sources.^{[1](#page-13-0)} Primarily functioning as an alternating-current (AC) system, the microgrid system aids in the transfer of energy and the provision of power for AC loads. However, as the proportion of direction current (DC) load steadily rises and technology evolves, the development of DC power supply technology is steadily advancing toward full maturity.^{\angle} Currently, the bus voltage in DC microgrids predominantly operates at a low voltage state, and these low voltage microgrids are highly reliable in providing electricity to domestic consumers.^{[3](#page-13-0)} In DC microgrids, energy storage is crucial due to its benefits such as two-way output and adaptable configuration. The cost of investing in DC microgrid energy storage devices is relatively low at present due to their DC output character. As energy storage technology progresses and renewable energy becomes more prevalent, an increasing number of users are likely to switch to a low-voltage DC microgrid mode, incorporating energy storage devices for future power provision.⁴

Nonetheless, the operational optimization of each component in DC microgrids varies from that in AC microgrids. Within AC microgrids, busbars are capable of direct grid connection via switches, whereas in DC microgrids, the busbars' current output is DC, preventing a direct link to the AC grid. The transfer of

energy between the busbars and the AC grid must be facilitated by converters connected to the grid. Currently, the literature on optimizing low-voltage DC microgrids is quite limited. *AlDavood et al.*[5](#page-13-0) used a sturdy scheduling framework for isolated microgrids, taking into account the demand response. Utilizing sturdy optimization techniques, they simulated the unpredictability of generating renewable energy and its demand reaction, addressing the dual-layer optimization issue with a combined approach involving genetic algorithms and mixed integer programming; *LiuDan et al.*[6](#page-13-0) employed the multifaceted particle swarm optimization algorithm to address microgrid optimization issues, considering factors like power equilibrium and solar energy production, aiming to reduce daily operational expenses and enhance the rate of solar energy usage. *Hayashi R et al.*[7](#page-13-0) employed a mix of particle swarm optimization and quadratic programming techniques to perform numerical simulations aimed at reducing the combined initial and

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Figure 1. Structure of low-voltage DC microgrid system with photovoltaic and energy storage.

operational expenses of microgrids; *Liu Yong et al.*[8](#page-13-0) employed a refined particle swarm optimization technique to enhance the financial efficiency of microgrids. Altering the particle swarm algorithm's velocity and positional development using various normal random numbers, which confirmed the enhanced particle swarm's optimization capabilities and boosted the microgrid's economic productivity. *Rodriguez M et al.*[9](#page-13-0) used a refined system for managing islanded microgrids, utilizing fuzzy control to modify the parameters of fuzzy logic control via particle swarm optimization and a cuckoo search algorithm, aiming to lower the operational expenses of microgrids.

As microgrid power supply technology evolves and China actively pursues the "dual carbon goals″, [10](#page-13-0) microgrids operators must take into account not just economic effectiveness but also the environmental effects of carbon emissions and the longevity of different components in the system, like energy storage systems. *Fan Zixiao et al.*[11](#page-13-0) unveiled an enhanced thirdgeneration multiobjective genetic algorithm designed to address the economic challenges faced by microgrids, focusing on reducing operational expenses, energy storage and discharge capacities, and pollution. Factoring in limitations like the power equilibrium and each unit's output, they implemented quantum local search to address the issue, enhancing the overall search capability; *Wang Shizhen et al.*[12](#page-13-0) examined various operational tactics for microgrid clusters, focusing on reducing investment expenses and factoring in the lifespan of energy storage services. The particle swarm optimization algorithm was employed to enhance efficiency, reduce operational expenses, and prolong the lifetime of energy storage facilities; *Xiao Hao et al.*¹ suggested a two-tiered optimization approach for microgrids, taking into account operational expenses and the longevity of energy storage. This model employs a grid-adaptive direct search and particle swarm optimization algorithm to enhance performance, decreasing the depth of charging and discharging for energy storage batteries in order to extend their longevity, and boost the system's overall efficiency.

The existing research results indicate that both economic benefits and low-carbon factors are crucial in optimizing the operation of low-voltage DC microgrids, and an effective optimization method can significantly improve the operational

efficiency and reliability of microgrids. In response to the above issues, a diverse approach for optimizing control in low-voltage DC microgrids, utilizing the Nondominated Sorting Arctic Puffin Optimization Algorithm (NSAPOA) under given photovoltaic and energy storage capacities is proposed in this paper. In order to eliminate the uncertainty of output, Wasserstein Generative Adversarial Network with Gradient Penalty (WGAN-GP) and K-means clustering method are used to generate typical output scenarios of photovoltaic and loads. By analyzing the correlation relationship between various system operation modes and electricity prices, relevant energy exchange strategies are formulated. With the objectives of minimizing daily operating costs, equivalent battery charging and discharging capacity, and reducing carbon dioxide emissions, an optimization operation model of the low-voltage DC microgrid that takes into account battery lifespan is established to improve the reliability of the microgrid is established. In the optimization process, the Non-Dominated Sorting Arctic Puffin Optimization Algorithm (NSAPOA) is used to obtain the Pareto optimal solution set, and the final optimal solution is derived using the Multi Attribute Boundary Approximate Area Comparison (MABAC) algorithm, which can further improve the operational efficiency of the microgrid system. Due to the consideration of DC loads connected to the grid and power limitations of converters, the technique suggested in this document significantly enhances the system's energy efficiency, reduces carbon dioxide emissions, and maintains the reliability of the power supply.

2. TYPICAL SCENARIOS OF PHOTOVOLTAIC AND LOAD GENERATED BY WGAN-GP

2.1. The Structure of Low-Voltage DC Microgrid System with Photovoltaic and Energy Storage. The lowvoltage DC microgrid system consists of distributed photovoltaics, energy storage batteries, control systems, grid connected converters, and user loads. The aspect of power generation encompasses solar energy production, power grids, and energy storage devices; The central distribution system consists of a DC bus and a central control system, in which the DC bus is responsible for the flow of energy, and the control

system is responsible for collecting signals and executing control instructions; The user loads include smart meters, household loads, electric vehicle DC loads, etc.; Smart meters serve the purpose of collect, measure, and transmit energy information from user data, equipped with smart features like two-way multirate measurement and user management. The structure of low-voltage DC microgrid system with photovoltaic and energy storage is shown in [Figure](#page-1-0) 1.

In [Figure](#page-1-0) 1, energy storage and photovoltaic power generation systems coordinate with each other to achieve efficient energy utilization and stable system operation. When the photovoltaic power is greater than the load power, a portion of the photovoltaic power is converted into AC power by the inverter to supply power to the load, and the remaining inverter stores the electrical energy in the energy storage system; When the photovoltaic power cannot meet the load demand, the inverter will convert the stored energy in the energy storage system to supply the load, ensuring the continuity and stability of the entire system operation.

2.2. Typical Scenario Generation of Photovoltaic and Loads. Due to factors such as weather, photovoltaic and load output have strong uncertainty. To address the above issues, the Wasserstein Generative Adversarial Networks with Gradient Penalty (WGAN-GP 14 14 14) is used to generate typical output scenarios for photovoltaics and loads, and the K-means clustering method is applied to reduce the dimensionality of the generated scenarios. WGAN-GP enhances algorithmic efficiency by penalizing the gradient norm of the critic's inputs, rather than clipping weights. Compared to traditional WGAN, WGAN-GP demonstrates superior performance and facilitates a stable training process. Additionally, when using WGAN-GP, almost no hyperparameter adjustments are necessary.

[Figure](#page-2-0) 2 illustrates the core structure of WGAN-GP used for generating renewable energy and load scenarios. [Figure](#page-2-0) 2 primarily consists of a pair of deep neural network models, with generator *G* and discriminator *D*. Both *G* and *D* may include convolutional neural networks or fully connected neural networks. The generator *G*, through understanding the possible distribution of past renewable energy photovoltaic or load data, analyzes the noise signal *z*, adhering to the probability distribution *Pz*(*z*) (like Gaussian distributions), to derive the resultant data $f = G(z)$ in line with the probability distribution $P_G(z)$. *G*'s objective is to align the probability distribution $G(z)$ of the produced data with that of the historical data. The discriminator evaluates both the generator's generated data $G(z)$ and the historical data *r* which aligns with the probability distribution $P_{data}(r)$ and calculates the likelihood $D(G(z))$ of the produced data $G(z)$ mirroring the actual distribution $P_{data}(r)$. *D*'s aim is to ascertain as precisely as possible if the input data is historical or generated.

Once the training goals of *G* and *D* are established, constructing the loss functions L_G and L_D of G and D respectively, is essential for training purposes. In the case of *G*, a reduced *LG* indicates an increased likelihood of the produced data adhering to $P_{data}(r)$. In the case of *D*, a lesser L_D indicates *D*'s enhanced capability to differentiate among various data sources. L_G and L_D can be depicted in the following manner:

$$
L^{G} = -\mathbb{E}_{\mathbf{z} \sim p_{\mathbf{z}}(\mathbf{z})}[D(G(\mathbf{z}))]
$$
\n(1)

$$
L^{D} = -\mathbb{E}_{\mathbf{x} \sim p_{data}(\mathbf{x})}[D(\mathbf{x})] + \mathbb{E}_{\mathbf{z} \sim p_{z}(\mathbf{z})}[D(G(\mathbf{z}))]
$$

+ $\lambda \mathbb{E}_{\hat{\mathbf{x}} \sim p_{\hat{\mathbf{x}}}(\hat{\mathbf{x}})}[(\|\nabla_{\hat{\mathbf{x}}}D(\hat{\mathbf{x}})\|_{2} - 1)^{2}]$ (2)

where Original discriminator loss = $\mathbb{E}_{\mathbf{z} \sim p_{data}(\mathbf{z})}[D(\mathbf{x})] + \mathbb{E}_{\mathbf{z} \sim p_{z}(\mathbf{z})}[D(G(\mathbf{z}))],$ Gradient penalty = $\[\hat{\mathbf{x}}_{\mathcal{P}_{\hat{\mathbf{x}}}}(\hat{\mathbf{x}}) \left[\left(\left\| \nabla_{\hat{\mathbf{x}}} D(\hat{\mathbf{x}}) \right\|_{2} - 1 \right)^{2} \right]$ $\int_{\hat{\mathbf{x}}}(x)[(\|\nabla_{\hat{\mathbf{x}}}D(\hat{\mathbf{x}})\|_{2} - 1)^{2}]\hat{\mathbf{x}} = \xi \mathbf{x} + (1 - \xi)G(\mathbf{z}), \xi$ ∼ *U*[0,1],*λ* symbolizes the gradient penalty term's weight coefficient, while $\|\cdot\|_2$ signifies the *ι*₂-norm.

To facilitate concurrent game training for *G* and *D*, we merge eqs 1 and 2 to develop a minimum-maximization game model focusing on the value function *V*(*D*, *G*):

$$
\begin{aligned}\n\min_{G} \max_{D} V(D, G) &= \mathbb{E}_{\mathbf{x} \sim p_{data}(\mathbf{x})} [D(\mathbf{x})] - \mathbb{E}_{\mathbf{z} \sim p_{\mathbf{z}}(\mathbf{z})} [D(G(\mathbf{z}))] \\
&\quad - \lambda \mathbb{E}_{\hat{\mathbf{x}} \sim p_{\hat{\mathbf{x}}}(\hat{\mathbf{x}})} [(\|\nabla_{\hat{\mathbf{x}}} D(\hat{\mathbf{x}})\|_{2} - 1)^{2}] \tag{3}\n\end{aligned}
$$

As iterations advance, *G* modifies the generator network's weight to increasingly resemble the actual sample, while the discriminator network enhances its discriminant capacity via

learning. The process involves continuous cycles until the discriminator network fails to precisely identify the origin of the input data sample, after which the generator undergoes training to create photovoltaic and load situations. The load and PV data used for WGAN-GP model training both come from North China. [Figure](#page-2-0) 3 (a) displays the outcomes of creating photovoltaic and load scenarios via WGAN-GP, while [Figure](#page-2-0) [3](#page-2-0) (b) illustrates the effects of scenario reduction using the kmeans clustering technique.

2.3. Operation Mode and Working Condition Division of the System. The electricity of low-voltage DC microgrids in multiple scenarios comes from photovoltaic power generation and electricity purchased from the large grid. The principle of energy exchange is to prioritize the consumption of photovoltaics, the energy storage system charges when the load is low, the energy storage system discharges when the load is high, and the purchase of electricity is reduced from the grid in the peak period. Figure 4 displays the spot electricity pricing graph for a specific day, with the data from the time-of-use electricity prices in northern China.

Figure 4. Curve of time-of-use electricity prices

It can be seen from Figure 4 during 1:00−7:00 and 22:00− 24:00, the time-of-use electricity price belongs to the valley period, with a minimum of 0.0674 USD in the whole day; during 8:00−11:00 and 16:00−18:00, the time-of-use electricity price belongs to the flatting period, with a tariff of 0.1095 USD; during 12:00−15:00 and 19:00−21:00, the time-of-use electricity price belongs to the peek period, with the highest tariffs of 0.1544 USD in the whole day.

Compared to traditional AC microgrids, the energy flow of DC microgrids is achieved with the grid through grid-connected converters. Therefore, the different operating modes of the system are determined by the different working states of grid-connected converters.^{[15](#page-13-0)} The working states of grid-connected converters mainly include stop working, unidirectional connection, and bidirectional connection. The corresponding operating modes of DC microgrids are off-grid, unidirectional connection, and bidirectional connection. The grid-connected operation mode is divided into operating conditions 1−5, and the off-grid operation mode is divided into operating conditions 6−7. The different operating modes and operating conditions of the system combined with the time of use electricity price are shown in [Figure](#page-4-0) 5.

Figure 5. Operation mode and working condition division of the system.

2.3.1. Bidirectional Grid Connection Mode. The system purchases and sells electricity from the grid through gridconnected converters to meet the load demand, achieving bidirectional energy flow with the grid and reducing load shortage caused by insufficient power generation.

Condition 1. In the valley period, when the output of photovoltaic power P_V is 0, the output of the DC microgrid is sufficient, that is, $P_{grid} > P_{load}$. If the SOC of the energy storage system is less than 20%, the energy storage system is charged by purchasing electricity from the grid; If the SOC of the energy storage system is between 20% and 90%, the energy storage system is in a charging state; If the SOC of the energy storage system is greater than 90%, the system will switch to a discharge state and supply power together with the DC microgrid to meet the load demand; When *Pgrid* < *Pload*, switch to Condition 5.

Condition 2. In the flat period, when $P_V > P_{load}$, if the SOC of the energy storage system is greater than 90%, the excess electricity is sold to the grid through grid-connected converter, and the grid-connected interface is in an inverter state; If the SOC of the energy storage system is less than 90%, the energy storage system is in a charging state. When $P_V < P_{load}$, switch to working Condition 5.

Condition 3. In the peak period, when $P_V > P_{load}$, except for supplying the load, all excess electrical energy is sold to the grid through grid-connected converters, and the grid-connected interface is in an inverter state; When $P_V < P_{load}$, switch to Condition 5.

2.3.2. Unidirectional Grid Connection Mode. The energy flow of grid-connected converters operates in a unidirectional manner, meaning that the system can only purchase electricity from the grid through grid-connected converters and cannot sell electricity, resulting in the abandoned photovoltaic.

Condition 4. When $P_V > P_{load}$ if the SOC of the energy storage system is greater than 90%, it is in a state of the abandoned photovoltaic; If the SOC of the energy storage system is between 20% and 90%, the energy storage system switches to the charging state; If the SOC of the energy storage system is less than 20%, the system is charged by purchasing electricity from the grid through grid-connected converters; When $P_V < P_{load}$, switch to **Condition 5.**

Condition 5. When $P_V < P_{load}$ or $P_{grid} < P_{load}$, if the SOC of the energy storage system is greater than 20%, the energy storage system discharges to meet the load demand; If the SOC of the energy storage system is less than 20%, the load demand can be met by purchasing electricity from the grid through gridconnected converters.

2.3.3. Off-Grid Mode. The grid-connected converter stops working and only relies on the output of photovoltaic and energy storage system for power supply. The DC microgrid operates as an independent system in off grid mode, achieving independent generation and distribution of electricity.

Condition 6. When $P_V > P_{load}$ if the SOC of the energy storage system is greater than 90%, it enters the abandoned photovoltaic state; If the SOC of the energy storage system is less than 90% and the energy storage system is charging, then the energy storage system will be charged by all excess energy.

Condition 7. When $P_V < P_{load}$, When the SOC of an energy storage system exceeds 20%, it remains in a state of discharge to satisfy the load requirements; conversely, if the SOC falls below 20%, the insufficient power will be recorded as load loss of power.

In summary, through the analysis of energy exchange strategies, in the bidirectional grid connected operation mode, due to the bidirectional energy flow between the low-voltage DC

Figure 6. Relationship between weight factor values and SOC.

microgrid and the power grid, the system has advantages such as good economy, high reliability, and low abandoned photovoltaic. Therefore, this paper mainly focuses on the research of optimization control methods for low-voltage DC microgrid systems in connected-grid operation mode.

3. ESTIMATION OF BATTERY LIFE USING THE EQUIVALENT ELECTRIC QUANTITY WEIGHTING METHOD

When lithium iron phosphate batteries participate in the optimization operation of low-voltage DC microgrids as energy storage links, their capacity progressively diminishes from the rated level, correlating with the rise in full charging and discharging cycles and alterations in discharge depth. The main methods for evaluating battery life include curve fitting method,¹⁶ rain flow counting method,^{[17](#page-13-0)} and equivalent power weight method.¹⁸ In contrast to the other two methods, the equivalent electricity weight method considers the equivalent discharge amount during battery charging and discharging cycles. In the optimized operation of low-voltage DC microgrids, batteries have different charging and discharging powers and depths at different times, and the equivalent electricity weight method can effectively evaluate the battery life and calculate the battery life loss based on the equivalent cumulative discharge amount. The calculation formula can be described as eq 4.

$$
L_{\text{loss}} = \frac{A_c}{A_{\text{total}}} \tag{4}
$$

where $A_{\rm total}$ represents a battery's total discharge capacity over its entire life cycle (kW·h), equivale to the product of the number of cycles of the battery and its rated capacity; A_c is the equivalent cumulative discharge of the battery during the period (kW·h).

The equivalent cumulative discharge of the battery can be yielded by eq 5.

$$
A_c = \lambda_{\rm soc} A_s \tag{5}
$$

where λ_{soc} is the weight factor; A_s is the actual discharge capacity $(kW·h)$.

The weight factor can be obtained by eq 6.

$$
\lambda_{\text{soc}} = \begin{cases}\n d_1, \ 0 < \text{SOC}(t) \le 0.5 \\
 d_2 \cdot \text{SOC}(t) + d_3, \ 0.5 < \text{SOC}(t) \le 1\n\end{cases} \tag{6}
$$

The relationship between weight factor values and SOC is shown in Figure 6^{19} 6^{19} 6^{19}

It can be seen from Figure 6 that when $0 < SOC(t) \le 0.5$, the weight factor is only related to d_1 , here $d_1 = 1.32$. When 0.5 < *SOC*(*t*) \leq 1, the weight factor is related to the values of *d*₂ and *d*₃, where here d_2 =-1.8, d_3 = 2.22. During operation, the life loss of the battery is accumulated to obtain the battery life at time *t*, as shown in eq 7.

$$
U_s = \frac{1}{\int_0^t \frac{\lambda_{\rm soc} A_s(t)}{A_{\rm total}} dt}
$$
\n(7)

4. OPTIMIZATION CONTROL MODEL FOR LOW-VOLTAGE DC MICROGRID BASED ON NSAPOA

The optimization control of low-voltage DC microgrid system aims at system economy, environmental protection, and safety, fully considering system balance and constraints such as energy storage charging and discharging power, to achieve economic and low-carbon operation of low-voltage DC microgrid system.

4.1. Objective Function. The objective function is to maximize daily net income, minimize equivalent total battery charge and discharge, and minimize $CO₂$ emissions. The overall objective function expression is described as eq 8.

$$
\begin{cases}\nf_1 = \max \sum_{t=1}^T (F(t) - C_{\text{con}}(t) - C_q(t)) \\
f_2 = \min \sum_{t=1}^T |P_{\text{Bd}}(t)| \cdot \Delta t \\
f_3 = \min \sum_{t=1}^N \left[\frac{(P_{\text{con}}(t)) + \sqrt{(P_{\text{con}}(t))^2}}{2} \Delta t \cdot e^{c\theta_2} \right]\n\end{cases} (8)
$$

4.1.1. Maximum Daily Net income. Assume that the purchase cost for photovoltaic panels and batteries based on a given capacity configuration is fixed. In actual operation, due to different daily loads, photovoltaic output and real-time electricity prices, the amount of electricity purchased and sold and the amount of abandoned solar energy each day are different. Therefore, the daily net income is mainly related to the income from selling electricity to the user load every day, as well as the cost of purchasing and selling electricity from the grid through grid-connected converters and the cost of abandoned solar energy. The objective function f_1 can be described as eq 9.

$$
f_1 = \max \sum_{t=1}^{T} (F(t) - C_{\text{con}}(t) - C_q(t))
$$
\n(9)

$$
F(t) = P_{\text{load}}(t) \cdot \Delta t \cdot R_{\text{price}}(t)
$$

$$
C_{\text{con}}(t) = \begin{cases} C_{\text{buy}}(t) \cdot P_{\text{con}}(t) \cdot \Delta t, P_{\text{con}}(t) \ge 0\\ C_{\text{sal}}(t) \cdot P_{\text{con}}(t) \cdot \Delta t, P_{\text{con}}(t) < 0 \end{cases}
$$

$$
C_q(t) = c \cdot P_q(t) \cdot \Delta t
$$
(10)

where $F(t)$ is the electricity sales revenue to the user load at time $t(USD)$; $C_{con}(t)$ is the cost of purchasing and selling electricity through the grid-connected converter at time $t(USD)$; $C_q(t)$ is the cost of abandoned photovoltaic at time t (USD); $P_{load}(t)$ is the user load at time t (kW); $R_{price}(t)$ is the real-time electricity price at time t (USD/kW·h); $\vec{P}_{con}(t)$ is the power of the gridconnected converter at time t (kW); When $P_{con}(t)$ >0, the system purchases electricity from the grid through a grid-connected converter, and sells electricity to the grid when $P_{con}(t)$ <0; $C_{\text{buv}}(t)$ and $C_{\text{scale}}(t)$ are the unit purchase price and unit sales price (USD/kW·h) at time *t*, respectively; $P_a(t)$ is the power of abandoned photovoltaic at time *t* (kW); *c* is the corresponding unit cost of abandoned photovoltaic (USD/kW·h).

4.1.2. Minimum Equivalent Full Cycle Counts of the Battery. A battery's time of service can be accurately calculated using the equivalent electric quantity weighting method, and the total equivalent discharge amount is equivalent to the total discharge amount under the charging and discharging cycle of the battery at different discharge depths. During operation, it is also necessary to consider the battery's SOC to store excess electricity to absorb photovoltaic energy. Therefore, the objective function f_2 is to minimize the equivalent charge and discharge capacity of the battery, as shown in eq 11.

$$
f_2 = \min \sum_{t=1}^{T} |P_{\text{Bd}}(t)| \cdot \Delta t \tag{11}
$$

$$
P_{Bd}(t) = \begin{cases} \lambda_{\text{soc}} \cdot P_B(t), \, P_B(t) \ge 0 \\ P_B(t), \, P_B(t) < 0 \end{cases}
$$
\n
$$
\lambda_{\text{soc}} = \begin{cases} 1.32, 0 < SOC(t) \le 0.5 \\ -1.8 \cdot SOC(t) + 2.22, 0.5 < SOC(t) \le 1 \\ (12) \end{cases}
$$

where $P_{\text{Bd}}(t)$ represents the equivalent power of charging and discharging at time t (kW); $P_B(t)$ represents the battery's actual output/input power at time t (kW); $\lambda_{\rm soc}$ is the weight factor; $SOC(t)$ is the battery's state of charge at time t.

4.1.3. Minimum Carbon Emission. Based on the dual carbon target background, minimize emissions of $CO₂$ during operation and add the minimum emissions of $CO₂$ to the objective function. In the system operation model, there are no diesel generators, gas turbines, and other units. The load is met by photovoltaic, energy storage, and electricity purchase from the grid. Only when the electricity is purchased from the grid through grid-connected converters, carbon emissions can occur. Therefore, the minimum emissions of $CO₂$ is regarded as the objective function f_3 . It can be given in eq 13.

$$
f_3 = \min \sum_{t=1}^{N} \left[\frac{(P_{\text{con}}(t)) + \sqrt{(P_{\text{con}}(t))^2}}{2} \Delta t \cdot e^{\omega_2} \right]
$$
(13)

where e^{c_0} is the amount of carbon dioxide (kg/kW·h) that needs to be emitted from the power grid for every kW·h.

4.2. Constraints. *4.2.1. Power Balance Constraint.*

$$
P_{\text{load}}(t) = P_{\text{pv}}(t) + P_{\text{con}}(t) + P_{\text{B}}(t) \tag{14}
$$

where $P_{load}(t)$ is the load power of the user at time t (kW); $P_{pv}(t)$ is the photovoltaic power at time t (kW); $P_{con}(t)$ is the power of the grid connected converter at time t (kW); $P_B(t)$ is the energy storage charging and discharging power at time t (kW).

At every moment, the total load power should be equal to the total of the power from energy storage, (both charging and discharging) the power emitted from photovoltaic sources, and the energy exchanged from the grid via grid-linked converters.

4.2.2. Current Limitation Constraint. Ensuring that the current used for charging and discharging lithium iron phosphate batteries during use is not excessively high is crucial to avoid permanent harm and potential ignition of the battery. The current should not be greater than 0.3*I*_{in} when charging, and 0.5*I*_{in} when discharging.

$$
\begin{cases}\n-0.3I_{\text{in}} \le I_c \le 0 \\
0 \le I_d \le 0.5I_{\text{in}} \\
I_{\text{in}} = \frac{E_b}{(U_{EV} \cdot 1h)}\n\end{cases}
$$
\n(15)

where I_c is the charging current (A) ; I_d is the discharging current (A); U_{EV} is the discharging voltage (A); E_b is the rated capacity $(kW·h)$.

4.2.3. Power Limitation Constraint. The charging and discharging power ought to be less than the power rated for energy storage. When the power used for charging and discharging exceeds the rated limit, the battery's over elevated temperature can trigger explosions, compromising its safety and operational stability.

$$
-P_{\text{rate}} \le P_{\text{B}}(t) \le P_{\text{rate}} \tag{16}
$$

where P_{rate} represents the battery's rated power (kW). *4.2.4. SOC Constraint.*

$$
SOC_{\text{min}} \leq SOC(t) \leq SOC_{\text{max}} \tag{17}
$$

$$
SOC(t) = SOC(t - 1) - \begin{cases} \frac{P_B(t) \cdot \Delta t}{E_{rate} \eta_{dc}}, & P_B(t) > 0\\ \frac{P_B(t) \cdot \Delta t \cdot \eta_{ch}}{E_{rate}}, & P_B(t) < 0\\ \end{cases}
$$
(18)

where SOC*min* and SOC*max* are the upper and lower limits of the SOC of the battery, respectively; $η_{dc}$ refers to the energy conversion efficiency of the battery in discharging; $η_{ch}$ represents the energy conversion efficiency of the battery in charging.

Figure 7. Process of the NSAPOA

4.2.5. Grid-Connected Converter Constraints. The gridconnected converter adjusts its transmission power based on power instructions, and when it reaches its power limit, it operates at rated power.

$$
-P_{\text{rcon}} \le P_{\text{con}}(t) \le P_{\text{rcon}} \tag{19}
$$

where $P_{\text{con}}(t)$ is the power of the grid-connected converter at time t (kW); P_{rcon} is the rated power of the grid-connected converter (kW).

4.3. Model Solving. *Wang et al.*[20](#page-13-0) introduced the Arctic puffin optimization algorithm (APOA) in 2023, introduces an innovative meta heuristic algorithm centered on population dynamics, drawing inspiration from the collective dynamics and survival abilities of Arctic puffins in aerial and diving hunting. The APOA includes two stages: exploration and exploitation, corresponding to aerial flight and underwater foraging. In the APO algorithm, the behavioral conversion factor *B* demonstrates both adaptability and dynamic behavior, adeptly harmonizing the dynamic interplay of exploration and exploitation and play an important role in the algorithm's robustness. The algorithm employs Levy flight coefficients and synergy factor to boost convergence in its development stage, incorporating behavioral transition factors to maintain a balance between exploration and exploitation, thereby offering almost universally optimal answers to intricate optimization challenges.

Solving multiobjective optimization issues often involves addressing a range of contradictory goals, with some focusing on maximizing functions and others on minimizing functions.^{[21](#page-13-0)} For addressing the issue of multiobjective optimization, NSAPOA, a hybrid algorithm for nondominant sorting, has been created, utilizing the technology of nondominant sorting optimization. Figure 7 illustrates the methodology of the NSAPOA.

The algorithm implementation process of the NSAPOA is as follows:

4.3.1. Step1: Set control parameters, initialize the number individuals in the Arctic puffin colony, the number of iterations, cooperative factor, factor reference value of behavior conversion and initializing positions of Arctic Puffins.

4.3.2. Step2: Evaluate each position of Arctic Puffins and finding the one with the best fitness in all of Arctic Puffins. Calculate the behavior conversion factor *B* of the one has best fitness.

$$
B = 2 * log(1/rand) * (1 - t/T)
$$
\n(20)

where *rand* represents a random figure within the range $(0,1)$, and *t* and *T* denote the present and maximum iteration numbers, in that order. During its initial phase, the Arctic Puffin tends to seek appropriate feeding waters, but in its advanced stages, it shifts its focus to scuba diving for sustenance.

4.3.3. Step3: Compare the size of the behavioral conversion factor *B* with its reference value *C* to deter mine the next behavior phase of the Arctic Puffin.

4.3.3.1. Exploration Phase.

1) Aerial Search Strategy

$$
\overrightarrow{Y_i^{t+1}} = \overrightarrow{X_i^t} + (\overrightarrow{X_i^t} - \overrightarrow{X_r^t})^* L(D)
$$

+ round(0.5*(0.05 + rand))^* α (21)

where *r* represents a random integer ranging from 1 to *N*

− 1, excluding *i*; *Xi t* → denotes the population's present *i*th potential solution; $X_r^t \rightarrow$ represents a randomly chosen candidate solution from the existing population, with $X_i^t \rightarrow$ $\neq X_r^t \rightarrow$; $L(D)$ represents a stochastic figure produced via Levy flight; *D* signifies the dimensionally; *α* ∼

Normal(0,1) symbolizes a stochastic shape conforming to a standard normal distribution sequence.

2) Swooping Predation Strategy

$$
\overline{Z_i^{t+1}} = \overline{Y_i^{t+1}} * S \tag{22}
$$

where $S = \tan ((\text{rand} - 0.5) * \pi)$ serves as a speed variable to modify the puffin's movement during a swoop.

$$
\overrightarrow{P_i^{t+1}} = \overrightarrow{Y_i^{t+1}} \cup \overrightarrow{Z_i^{t+1}}
$$
\n
$$
\overrightarrow{new} = sort(\overrightarrow{P_i^{t+1}})
$$
\n
$$
\overrightarrow{X_i^{t+1}} = new(1: N)
$$
\n(23)

where $X_i^{t+1} \rightarrow$ is the new population; $Y_i^{t+1} \rightarrow$, $Z_i^{t+1} \rightarrow$ indicate different positions in the current phase.

4.3.3.2. Exploitation Phase.

1) Gathering Foraging

$$
\overrightarrow{W_i^{t+1}} = \begin{cases} \overrightarrow{x_{r1}} + F^*L(D)^* (\overrightarrow{X_{r2}^t} - \overrightarrow{X_{r3}^t}) rand \ge 0.5\\ \overrightarrow{X_{r1}^t} + F^* (\overrightarrow{X_{r2}^t} - \overrightarrow{X_{r3}^t}) rand < 0.5\\ (24) \end{cases}
$$

where *F* symbolizes the collaborative element, modifying the predatory actions of Arctic puffins. Within this document, F is set to 0.5; Random integers *r*1, *r*2, *r*3 fall within the range of 1 to $N-1$, *i* not included, and $X_{r1}^t \rightarrow$, $X_{r2}^t \rightarrow X_{r3}^t \rightarrow$ represent randomly chosen potential solutions from the existing population, and $r1 \neq r2 \neq r3$, $X_{r2}^t \rightarrow \neq X_{r3}^t \rightarrow$.

2) Intensifying Search

$$
\overrightarrow{Y_i^{t+1}} = \overrightarrow{W_i^{t+1}} * (1 + f)
$$
\n
$$
f = 0.1 * (rand - 1) * \frac{(T - t)}{T}
$$
\n(25)

where *T* signifies the aggregate count of iterations, and *t* indicates the present iteration tally. *rand* is a stochastic figure, symbolizing variations derived from the original position.

3) Avoiding Predators

$$
\overrightarrow{Z_i^{t+1}} = \begin{cases}\n\overrightarrow{X_i^t} + F^*L(D)^* (\overrightarrow{X_{r1}^t} - \overrightarrow{X_{r2}^t}) rand \ge 0.5 \\
\overrightarrow{X_i^t} + \beta^* (\overrightarrow{X_{r1}^t} - \overrightarrow{X_{r2}^t}) rand < 0.5\n\end{cases}
$$
\n(26)

where *β* represents a random number distributed evenly from 0 to 1; *F* serves as an adaptive variable to modify the Arctic puffin's location in aquatic environments.

$$
\overrightarrow{P_i^{t+1}} = \overrightarrow{W_i^{t+1}} \cup \overrightarrow{Y_i^{t+1}} \cup \overrightarrow{Z_i^{t+1}}
$$
\n
$$
\overrightarrow{new} = sort(\overrightarrow{P_i^{t+1}})
$$
\n
$$
\overrightarrow{X_i^{t+1}} = new(1: N)
$$
\n(27)

where $X_i^{t+1} \rightarrow$ is the new population; $W_i^{t+1} \rightarrow$, $Y_i^{t+1} \rightarrow$, Z_i^{t+1} → indicate different positions in the current phase.

4.3.4.. Step4: Update the phase, stages and position of Arctic puffins, and redo fitness computations to derive the Pareto optimal set of solutions until the cycle count is attained, and terminate the output.

4.3.5.. Step5: The algorithm concludes once the quantity of public iterations is restricted. Otherwise, move on to 4.3.2.

4.3.6.. The MABAC method. While the NSAPOA is capable of deriving the Pareto optimal solution set for multiobjective programming, it lacks the capability to directly acquire the optimal solution. Utilizing the $MABAC^{22}$ $MABAC^{22}$ $MABAC^{22}$ technique is essential for achieving the best solution. MABAC, an impartial method for assigning weights, calculates the size of the weight by analyzing the relationship between target values or the extent of variation in these values during data processing. To determine the best solution, assess how closely each solution aligns with either the positive or negative ideal solution by analyzing both positive and negative ideal solutions of the issue.

The specific procedure of the MABAC method is as follows:

- 1) Determine the decision matrix: The performance data of all optional solutions form a decision matrix, where each row represents a solution and each column represents a decision criterion.
- 2) Standardize the decision matrix: Standardize the decision matrix to ensure that the values of different criteria have the same weight.
- 3) Calculate relative importance: Determine the relative importance of each solution under different criteria by calculating the performance score of each solution under different criteria.
- 4) Calculate the fuzzy matrix: Calculate the fuzzy matrix of each solution to other solutions based on relative importance.
- 5) Calculate the fuzzy comprehensive score: Using the fuzzy matrix, calculate the fuzzy comprehensive score of each solution.
- 6) Sort and select: Sort all solutions according to the fuzzy comprehensive score, and select the solution with the highest fuzzy comprehensive score as the best solution.

5. RESULTS AND DISCUSSION

5.1. Data Sources. The bus voltage of a low-voltage DC microgrid project in a certain area is ± 375 V, the rated power of grid-connected converters is 200 kW, the rated power of photovoltaic power stations is P_{pv} = 488 kW, the rated power of the energy storage is $P_{\text{rate}} = 220.03$ kW, and the capacity of the energy storage is $E_b = 1265.77$ kW \cdot h. The operation process of the DC microgrid is optimized every 15 min, and the gridconnected converter adopts a bidirectional grid connected operation mode. The actual operation data including load, PV and electricity price are from North China. In order to compare the economic performance of low-voltage DC microgrid systems based on energy storage under different objectives, $MOPSO₁²³ NSGA-II₁²⁴ and NSAPOA were used for com MOPSO₁²³ NSGA-II₁²⁴ and NSAPOA were used for com MOPSO₁²³ NSGA-II₁²⁴ and NSAPOA were used for com$ parative analysis.

The parameter settings of three optimization algorithms are shown in [Table](#page-9-0) 1. The three objective functions are divided as follows:

*f*1: Maximize net income;

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f 2: Minimize carbon emissions;

f 3: Minimize equivalent charging and discharging capacity of the battery.

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Table 1. Parameter Settings for Different Algorithms

5.2. Comparison of Optimization Effect under Different Targets and Different Methods. *5.2.1. Comparison of Optimization Effects Considering Net Income Only.* For the optimization model established under a single objective function, PSO, GA and APOA are used to solve the model. The optimization results under a single objective are shown in Table 2. The charging and discharging curve of the energy storage system under a single objective obtained by PSO, GA and APOA is shown in Figure 8.

Table 2. Optimization Results of Different Optimization Algorithms under a Single Objective

f_1	net income/ USD	carbon emissions/kg	equivalent charging and discharging capacity/kW·h
PSO	1520.6	1197.59	2798.40
GA	2397.79	1304.72	3042.50
APOA	2425.52	1307.36	2957.57

It can be seen from Table 2 and Figure 8 that compared with the other two algorithms, the net profit of the DC microgrid system obtained by the APOA is the maximum of 2425.52 USD. However, due to only taking daily net income as the objective function without considering the impact of carbon emissions on the environment, the achievement of the "dual carbon" goal has been hindered. The carbon emission is the maximum of 1307.36 kg. And the equivalent charging and discharging capacity of the energy storage system is 2957.57 kW·h, which is relatively high and can lead to the aging of the energy storage battery.

5.2.2. Comparison of Optimization Effects Considering Net Revenue and Carbon Emissions. To diminish carbon emissions and showcase the benefits of renewable energy in lowering carbon in DC microgrid systems, carbon emissions are incorporated as the goal function, and a two-pronged optimization model is formulated, taking into account both the overall advantages and carbon emissions. Given that the two goal functions aim for the highest net gains and lowest carbon emissions, a negative indicator precedes the net gains in establishing the function, and a multiobjective algorithm resolves the minimum to fulfill both goals of maximizing net income and reducing carbon emissions.^{[25](#page-13-0)} The Pareto optimal sets obtained by MOPSO, NSGA-II and NSAPOA are shown respectively in [Figure](#page-10-0) 9.

It can be seen from [Figure](#page-10-0) 9 that the Pareto solution set obtained by the NSAPOA algorithm is optimal compared to the other two algorithms; When the net benefit is equal, the carbon emission obtained by the NSAPOA is the lowest; When carbon emissions are equal, the algorithm optimizes the net benefit to its highest level. The optimal solution is selected from the Pareto sets generated by three optimization algorithms using the MABAC method, with results of 0.097286 (MOPSO), 0.098037 (NSGA-II), and 0.10749 (NSAPOA), respectively.

The power output curves of the battery energy storage system and the optimization results obtained by the three optimization algorithms under the optimal solution are shown in [Figure](#page-10-0) 10 and [Table3,](#page-10-0) respectively.

It can be seen from [Table](#page-10-0) 3 and [Figure](#page-10-0) 10 that compared with the other two algorithms, the score obtained by the NSAPOA is the highest. The net income of the DC microgrid system is the maximum of 1357.64, 17.8% higher than the lowest. Carbon emissions is between the results of the other two algorithms in order to achieve a balance between the two goals, but only 1.1% more than the minimum. However, since the third objective is not considered, the equivalent charging and discharging capacity of the three algorithms are all relatively high.

5.2.3. Comparison of Optimization Effects Considering Net Profit, Carbon Emissions, and Service Life of the Battery. To prolong the battery's service lifespan, the corresponding charge and discharge potential of the energy storage battery are incorporated into the stated objective function, leading to the creation of a multiobjective function optimization system that

Figure 8. Charging and discharging curve of the energy storage system under a single objective obtained by three algorithms.

Figure 9. Pareto optimal solution set obtained through MOPSO, NSGA-II and NSAPOA.

Figure 10. Battery's output curves of different algorithm's optimal solution.

Table 3. Comparison Results of MOPSO, NSGA-II and NSAPOA Considering Two Goals

accounts for net profit, carbon emissions, and the battery's equivalent charge and discharge capacities. Figure 11 illustrates the range of Pareto solutions derived from MOPSO, NSGA-II and NSAPOA for three goals, where the NSAPOA's Pareto solution set distribution stands out as the most consistent and comprehensive, boasting robust overall search capabilities.

The optimal solution is selected from the Pareto sets generated by three optimization algorithms using the MABAC

a) MOPSO

b) NSGA-II

c) NSAPOA

Figure 11. Pareto solution sets obtained by different optimization algorithms under three objectives

method, with results of 0.1233(MOPSO), 0.14476(NSGA-II), and 0.17476(NSAPOA), respectively. The optimization results under three objective functions are shown in Table 4. The output curve of the energy storage system under three objective functions obtained by three multiobjective algorithms is shown in Figure 12.

Table 4. Comparison Results of MOPSO, NSGA-II and NSAPOA Considering Three Goals

It can be seen from Table 4 and Figure 12 that compare with the other two algorithms, the score obtained by the NSAPOA is the highest (0.17476). The net income of the DC microgrid system is the maximum of 1082.11, 59.1% higher than the lowest. However, due to the consideration of equivalent charging and discharging capacity, the net income needs to be compromised, which is lower than both in the single and dual goal cases. Carbon emissions is only 1.8% more than the minimum and is the lowest among the three cases. Equivalent charging and discharging capacity is slightly higher but is 7.7% lower than the maximum, also the lowest among the three cases. Considering three goals resulted in the most comprehensive solution, which improves the battery's operational lifespan and reduces environmental pollution with the reduction of carbon emissions.

The optimized operational curve for DC microgrid system obtained by the NSAPOA, taking into account three different optimization goals is shown in [Figure](#page-12-0) 13.

It can be seen from [Figure](#page-12-0) 13 that during 0:00−7:00, real-time electricity prices are the lowest, and the generation from the PV plant is close to zero. During this period, the load is primarily supplied by energy storage and electricity purchased from the grid via grid-connected converters. Due to the low demand, energy storage and the grid-connected converters alternate in supplying power, ensuring a stable energy provision. During 7:00−11:00, electricity prices are in the middle level, while the generation from the PV plant steadily increases to its maximum. When the generated energy exceeds the load demand, the

energy storage system begins charging to store excess energy. If capacity limitations restrict energy storage, surplus electricity is fed back into the grid via grid-connected converters, thus avoiding photovoltaic curtailment. During 11:00−17:00, electricity prices remained at a relatively high level, and the photovoltaic output continues to exceed the load demand. The energy storage system remains in charging mode until reaching full capacity, after which the surplus electricity is sold back to the grid through the grid-connected converters to generate profits. During 17:00−21:00, electricity prices reach the highest level, coinciding with a peak in energy demand. As the generation from the PV plant drops to zero, the energy storage system discharges a significant amount of previously stored energy, reducing the cost of electricity purchases during this peak pricing period. The combination of energy storage and grid-supplied electricity, delivered through grid-connected converters, meets the high electricity demand during this period. During 21:00− 24:00, electricity prices become low again, and demands began to decrease. The energy storage and grid-connected converters continue to supply power alternately to meet the demands.

5.3. Comparison of Optimization Effect under Different Scenarios. For the different typical scenarios in 2.2, the optimization model established in this paper is used for solution. The optimized operation results under different scenarios are shown in [Table](#page-12-0) 5, and the charging and discharging curves of energy storage batteries is shown in [Figure](#page-12-0) 14.

It can be seen from [Table](#page-12-0) 5, compared with the normal weather scenario, in severe weather, due to the significant reduction of photovoltaic output, the energy obtained by the energy storage battery from renewable energy sources is reduced, the load is primarily purchased from the grid via grid-connected converters, resulting in a reduction in the net income and carbon emissions to 757.36USD and 810.52 kg, which is 30.1% and 5.5% lower than that in normal weather. It can be seen from [Figure](#page-12-0) 14, the energy storage charging amount in the severe weather scenario from 4:00 to 12:00 is significantly lower than that in the normal weather scenario, resulting in insufficient power for discharge after the electricity price rises after 18:00, and thus leading to a decrease in revenue. Despite a reduction in net income, there's a notable decrease (19.1%) in the battery's equivalent charging and discharging capacity, enhancing its operational lifespan.

Figure 12. Output curves of energy storage batteries obtained by different algorithm.

Figure 13. Optimized operational curve for DC microgrid obtained by the NSAPOA considering three objectives.

Table 5. Comparison of the Optimal Solution Search Results of Different Weather Conditions

6. CONCLUSIONS

From the perspectives of economy, low-carbon, and safety in the operation of low-voltage DC microgrids, this paper proposes a multiscenario optimization control method of low-voltage DC microgrids based on the NSAPOA. The operation model of lowvoltage DC microgrids considering the service life of energy storage is established with the objective functions of maximizing net income, minimizing equivalent charging/discharging capacity of the energy storage system, and minimizing carbon emissions. The main conclusions are as follows:

1) By comparing and analyzing the energy exchange strategies and economy of time of use electricity prices and different operating modes of the system in multiple scenarios, the optimal economic efficiency of the lowvoltage DC microgrid system in bidirectional gridconnected operation mode is obtained;

- 2) The NSAPOA introduced in this study demonstrates robust search capabilities and effective optimization by evaluating various optimization algorithms across distinct objective functions, achieving the highest score obtained by the MABAC algorithm than those obtained by the MOPSO and NSGA-II;
- 3) Taking into full consideration the daily net income, service life and carbon dioxide emissions, compared with the operating results under only one goal, the equivalent charging and discharging capacity of the battery is reduced by 17.7%, improving the service life of energy storage systems. And the carbon dioxide emissions is reduced by 450.06 kg, which leads to the balance between cost-effective and carbon-efficient functioning of energy storage in the low-voltage DC microgrid system.

■ **ASSOCIATED CONTENT**

Data Availability Statement

The data underlying this study are not publicly available due to data owned by a third party. The data underlying this study were provided by Guoneng Qinghai Yellow River MaerDang

Figure 14. Output curves of energy storage batteries under different weather.

Hydropower Development Co., Ltd. under license/by permission. Data are available from the corresponding author upon reasonable request with the permission of Guoneng Qinghai Yellow River MaerDang Hydropower Development Co., Ltd.

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Notes

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