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## A quantitative framework for the design of acellular hemoglobins as blood substitutes: implications of dynamic flow conditions

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### Abstract

The delivery of oxygen to tissue by cell-free carriers eliminates intraluminal barriers associated with red blood cells. This is important in arterioles, since arteriolar tone controls capillary perfusion. We describe a mathematical model for O<sub>2</sub> transport by hemoglobin solutions and red blood cells flowing through arteriolar-sized tubes to optimize values of  $p50$ , Hill number, hemoglobin molecular diffusivity and concentration. Oxygen release is evaluated by including an extra-luminal resistance term to reflect tissue oxygen consumption. For low consumption (i.e., high resistance to O<sub>2</sub> release) a hemoglobin solution with  $p50=15$  mmHg, Hill  $n=1$ ,  $D_{HBO_2}=3\times 10^{-7}$  cm<sup>2</sup>/s delivers O<sub>2</sub> at a rate similar to that of red blood cells. For high consumption, the  $p50$  must be decreased to 5 mmHg. The model predicts that regardless of size, hemoglobin solutions with higher  $p50$  will present excess O<sub>2</sub> to arteriolar walls. Oversupply of O<sub>2</sub> to arteriolar walls may cause constriction and paradoxically reduced capillary perfusion.

### Keywords

Facilitated diffusion; O<sub>2</sub> affinity; Transport simulation; Vasoconstriction; Blood Substitutes

## 1. Introduction

The purpose of this paper is to provide a quantitative framework for the design of acellular hemoglobins (Hb) to function as hemoglobin-based oxygen carriers (HBOCs), particularly O<sub>2</sub> equilibrium binding properties and modified Hb molecular size. Numerical simulations of O<sub>2</sub> transport from acellular Hb and RBCs in arteriolar-sized domains are calculated. The effects of variations of individual parameters on a generic Hb solution are considered. A range of extra-luminal transport resistances are used to understand the importance of intra-luminal O<sub>2</sub> transport processes versus consumption rates for prospective HBOCs. In the context of this study, we use the terms O<sub>2</sub> transport or O<sub>2</sub> delivery to refer to the total amount of O<sub>2</sub> transferred from a Hb solution flowing through a simplified, arteriolar-sized domain to the surrounding environment.

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Scientists have been searching for a viable oxygen carrying resuscitation fluid to serve as a temporary surrogate to blood for the better part of the past century [1]. Hemoglobin is the obvious choice as the functional compound in such a fluid because of its high O<sub>2</sub>-carrying capacity [1]. HBOCs are composed of acellular Hbs chemically modified to decrease renal toxicity due to Hb dimerization and to provide O<sub>2</sub> to hypoxic tissue. Modifications include cross-linking between Hb subunits, formation of Hb polymers, and surface conjugation of Hb molecules to poly(ethylene) glycol. Sites of modification are used to affect the O<sub>2</sub>-binding affinity of the HBOC. The resulting HBOCs display a wide variation in molecular size and O<sub>2</sub> equilibrium binding characteristics [2].

The O<sub>2</sub> affinities of HBOCs that have been developed and implemented in clinical trials may vary by as much as an order of magnitude. The *p*50s of a PEG-conjugated Hb product (MP4), 5 mmHg, and a polymerized bovine Hb product (PolyBvHb), 54 mmHg, represent this range. An extensive series of in vivo experiments with HBOCs of varied *p*50s have shown increased efficacy for HBOCs with high O<sub>2</sub> affinities [3–5]; this data has led to the theory of autoregulatory vasoconstriction by arteriolar over supply of O<sub>2</sub>, which we discuss elsewhere [6,7]. More recently, there has been a general agreement that increasing the molecular size of Hb is advantageous; the estimated molecular weights of both MP4 (~95 kDa) [8] and PolyBvHb (~200 kDa) [9] are larger than unmodified or intramolecularly cross-linked Hbs (64 kDa) [10]. The increased molecular size limits the diffusion of acellular Hb within the lumen and potentially decreases extravasation of Hb into the vessel wall.

As a consequence of the particulate nature of blood, the O<sub>2</sub> transport resistances associated with RBC suspensions are greater than those of acellular Hbs. The amount of O<sub>2</sub> delivered from whole blood is limited by the diffusion kinetics of dissolved O<sub>2</sub> ( $D_{O_2} \sim 2 \times 10^{-5} \text{ cm}^2/\text{s}$  [11]) and the relatively low solubility of O<sub>2</sub> in plasma ( $\sim 1.3 \mu\text{M mmHg}^{-1}$  [12]). The presence of acellular Hbs is often linked to increased O<sub>2</sub> fluxes as compared to RBCs for two main reasons: 1) The acellular location Hb within the cell-depleted layer near the vessel wall decreases the potential O<sub>2</sub> diffusion distance and elevates the local O<sub>2</sub> concentrations; 2) acellular HbO<sub>2</sub> freely diffuses throughout the plasma space, providing an additional pathway for lateral O<sub>2</sub> transport. An amended form of Fick's law can be written as (1), with contributions to the total radial transport of O<sub>2</sub> coming from the diffusion of dissolved O<sub>2</sub> ( $J_{O_2}$ ) and the "facilitated" diffusion of HbO<sub>2</sub> ( $J_{HbO_2}$ ).

$$J_{O_2, \text{tot}} = J_{O_2} + J_{HbO_2} = -D_{O_2} \frac{\partial [O_2]}{\partial r} - D_{HbO_2} \frac{\partial [HbO_2]}{\partial r} \quad (1)$$

The diffusivity of HbO<sub>2</sub> ( $D_{HbO_2}$ ) is in general 1–2 orders of magnitude smaller than the diffusivity of dissolved O<sub>2</sub> ( $D_{O_2}$ ), yet the concentration O<sub>2</sub> bound to Hb ( $[HbO_2]$ ) is typically 1–2 orders magnitude larger than dissolved O<sub>2</sub>, ( $[O_2]$ ). For combinations of  $D_{HbO_2}$  and  $[HbO_2]$  on the high end of these ranges, the effect of  $J_{HbO_2}$  is significant. This phenomenon has been thoroughly described in the literature [11]. Because of the difference in O<sub>2</sub> transport kinetics between HBOCs and RBCs, the effects of HBOCs parameters must be considered under dynamic, flowing conditions.

Several mathematical models have been developed to describe the O<sub>2</sub> transport from acellular Hb [13], RBCs [14], and RBC/acellular Hb mixtures [15] flowing through arteriolar-sized gas-permeable tubes. These models are well accepted, and have been extensively validated by gas-exchange experiments in arteriolar-sized conduits [14,16,17]. Such models provide O<sub>2</sub> transport behavior to be quantified under dynamic flowing conditions in the absence of biological flow regulation, and these previous O<sub>2</sub> transport experiments [7,14,16,17] and simulations [13–15] considered only small values of extra-luminal resistance. To increase the relevance of this type of mathematical modeling, we have applied additional extra-luminal

boundary conditions to *in vitro* studies. We use the mass transfer Biot number ( $Bi$ ) as a parameter to provide an estimate of the ratio of intra-luminal to extra-luminal  $O_2$  transport resistances. Although this parameter is a basic engineering construct that cannot describe the complexities of physiological  $O_2$  diffusion and consumption in tissue, the intention is to gain an understanding of the relative importance of HBOC design parameters when extra-luminal  $O_2$  processes are “fast”, i.e., low resistance, versus “slow”, i.e., high resistance. Increases in tissue  $O_2$  consumption rates correlate with decreased values of extra-luminal resistance [6]. For example, such differences could occur in tissues like brain compared to resting skeletal muscle, where  $O_2$  consumption is much larger ( $3.5 \times 10^{-2} \text{ ml } O_2 \text{ min}^{-1} \text{ g}^{-1}$  [18] vs.  $4.4 \times 10^{-3} \text{ ml } O_2 \text{ min}^{-1} \text{ g}^{-1}$  [19]), or skeletal muscle when it is contracting [20].

*In vivo*, processes that occur in the extra-luminal region are complex and somewhat controversial. For example, studies have indicated a large amount of  $O_2$  consumption within the microvascular wall, surrounded by a region of lower  $O_2$  consumption [21,22]. These findings are contrasted by a study that reveals the calculated vascular wall  $O_2$  consumption to be much larger than what has been observed in similar tissues [23]. There is no comprehensive model that describes the transport processes in this region. Thus, we have used diffusion-type boundary conditions with a variety of extra-luminal resistances. This works particularly well to reflect the increased *in vivo*  $O_2$  transport that was observed for higher  $O_2$  affinity Hbs [5, 24], and provides an effect that cannot be captured using a constant  $O_2$  flux.

In this report, numerical simulations of  $O_2$  delivery are presented in 25- $\mu\text{m}$  diameter domains for both pure acellular Hb and RBCs. Hb simulations are shown with variations of a single parameter ( $p50$ ,  $n$ ,  $[Hb]$ ,  $D_{HbO_2}$ ), with other parameters held constant. RBC suspensions are simulated for comparison purposes. All simulations were performed for at least two values of extra-luminal resistance ( $Bi$ ), intended to reflect the scope of potential  $O_2$  transport behavior for acellular Hb.

## 2. Methods

### Hb Equilibrium Binding

Hemoglobin is a tetrameric protein composed of four subunits, each of which contains an iron-containing heme group capable of reversibly binding  $O_2$ , represented by the generic reaction (2).



The parameters commonly used to describe  $O_2$  and Hb concentrations are the partial pressure of  $O_2$  ( $p$ ) and Hb fractional saturation ( $Y$ ). We follow the common physiological convention by referring to  $O_2$  tension ( $p$ ) and  $O_2$  solubility ( $\alpha$ ) rather than  $[O_2]$ . The values for  $\alpha$  depend on hemoglobin concentration [25]; we use values interpolated between the properties of plasma and erythrocyte intra-cellular Hb [12,25]. The values of  $\alpha$  and other parameters used in the simulation are given in Table 1. The fraction of total Hb which has  $O_2$  bound is given by  $Y$  (3).

$$Y = \frac{[HbO_2]}{[Hb]_{tot}} \quad (3)$$

The most common model used to describe this behavior is the Hill equation (4) [26].

$$Y = \frac{(p/p50)^n}{1 + (p/p50)^n} \quad (4)$$

The  $p50$  is the  $p$  where  $Y = 0.5$  and is a measure of the Hb-O<sub>2</sub> binding affinity. The Hill number,  $n$ , is an empirical constant which gives Hb/O<sub>2</sub> binding cooperativity. The major shortcoming of the Hill equation is the reduced accuracy at regions where  $Y < 0.1$  and  $Y > 0.9$ . In the simulations we perform,  $Y$  values are always  $> 0.1$ , so this is not an issue.

The total O<sub>2</sub> content of an Hb solution is the sum of the dissolved O<sub>2</sub> and Hb-bound O<sub>2</sub> (5).

$$[O_2]_{tot} = \alpha p + [Hb]_{tot} Y \quad (5)$$

We use mixed-mean or bulk concentrations,  $c_b$ , (6) to describe the average value of  $p$  or  $Y$  at a given axial position [27], where  $u(r)$  is the flow profile,  $R$  is the tube radius,  $r$  is the radial position in the tube, and  $z$  is the axial position in the tube.

$$c_b(z) = \left( \int_0^R 2\pi r u(r) c(r,z) dr \right) / \left( \int_0^R 2\pi r u(r) dr \right) \quad (6)$$

Several idealized Hbs with regular variations in  $p50$ ,  $n$ , Hb diffusivity, and  $[Hb]$  are also simulated in this study to investigate effects of variations of individual parameters on O<sub>2</sub> transport. The base molecule on which these variations are imposed has the properties  $p50 = 15$  mmHg,  $n = 1$ ,  $D_{HbO_2} = 3 \times 10^{-7}$  cm<sup>2</sup>/s, and  $[Hb] = 10$  g/dl. The  $p50$  was chosen because it is close to that of unmodified Hb. The values for  $n$  and  $D_{HbO_2}$  are chosen because the most recently developed HBOCs have low cooperativity and increased molecular size (as compared to native Hb). The hemoglobin concentration is an intermediate value, although concentration effects are investigated.

### Hb Reaction Kinetics

The rate of O<sub>2</sub> liberation from Hb is related to HbO<sub>2</sub>, Hb, and O<sub>2</sub> concentrations, as well as the association and disassociation rate coefficients  $k'$  and  $k$ , respectively (7).

$$f = k[HbO_2] - k'[Hb][O_2] = k[Hb]_{tot} Y - \alpha k'[Hb]_{tot} p(1 - Y) \quad (7)$$

To reflect differences in  $k'$  and  $k$  due to equilibrium binding effects, Moll developed a technique that holds the association coefficient constant and varies the disassociation coefficient in the Hill equation as a function of saturation,  $Y$  (8) [28].

$$k = \alpha p50 k' \left( \frac{p}{p50} \right)^{1-n} \quad (8)$$

The value for  $k'$  is given by Gibson et al. as  $3.5 \times 10^6$  M<sup>-1</sup> s<sup>-1</sup> for Hb at 37°C [29]. The use of constant association and variable disassociation coefficients to define activity for different Hbs is consistent with kinetic measurements for native and chemically-modified Hb [30,31]. The underlying assumption for this method is that the offloading of O<sub>2</sub> from Hb is not a rate-limiting step and that intra-luminal O<sub>2</sub> transport rates are primarily dependent on the speeds of lateral diffusive processes.

### Acellular Hb Model

The coupled system of partial differential equations (PDEs) that describes transport of O<sub>2</sub> from acellular HbO<sub>2</sub> flowing through an arteriolar-sized, gas permeable tube is given in (9,10). The position variables  $r$  and  $z$  are given in the schematic in Fig. 1A.

$$u(r)\frac{\partial p}{\partial z}=D_{O_2}\left(\frac{1}{r}\frac{\partial}{\partial r}\left(r\frac{\partial p}{\partial r}\right)\right)+\left(\frac{1}{\alpha}\right)f(p,Y) \quad (9)$$

$$u(r)\frac{\partial Y}{\partial z}=D_{HbO_2}\left(\frac{1}{r}\frac{\partial}{\partial r}\left(r\frac{\partial Y}{\partial r}\right)\right)-\left(\frac{1}{[Hb]_{tot}}\right)f(p,Y) \quad (10)$$

The related linear problem (i.e. with no reaction term) is known as the Graetz problem and has an analytical solution for the cases of simple boundary and entry conditions. Because of the tubular, constrained geometry, fluid flow is assumed to be axisymmetric and fully developed. A homogeneous Hb solution is Newtonian and will have a parabolic velocity profile,  $u(r)$ . For high mass transfer Peclet numbers ( $Pe = U_{avg} R/D$ ,  $Pe_{O_2} \approx 10$ ,  $Pe_{HbO_2} \approx 10^2-10^3$ ,  $U_{avg}$  = average velocity), axial diffusion may be neglected [32]. As a consequence, only axial convection and radial diffusion need be considered. The system in (9,10) was first given by Lemon et al. [13] and validated by experiments in 25- $\mu$ m diameter artificial capillaries [16].

### RBC Suspension Model

For RBC suspensions flowing through narrow tubes, shear-induced particle migrations create a RBC depleted layer near the tube wall (Fig. 1A). For arteriolar-sized domains, it is suitable to treat a region containing RBCs as a non-diffusing pseudo-continuum with average Hb concentrations at a given radial position. The transport equations must account for the differences between the cell-rich core region of radius  $\lambda R$  and a concentric cell-depleted shell. The system of equations used to describe  $O_2$  transport within flowing RBC suspensions for the Hb-rich core region is given in (11,12).

$$u_c(r)\frac{\partial p}{\partial z}=D_{O_2}\left(\frac{1}{r}\frac{\partial}{\partial r}\left(r\frac{\partial p}{\partial r}\right)\right)+\left(\frac{h(r)[Hb]_{rbc}}{\alpha}\right)f(p,Y) \quad (11)$$

$$u_c(r)\frac{\partial Y}{\partial z}=-f(p,Y) \quad (12)$$

The local hematocrit,  $h(r)$ , is taken to be a constant value within the core region ( $0 \leq r \leq \lambda R$ ) and 0 in the shell ( $\lambda R \leq r \leq R$ ). The intracellular RBC Hb concentration,  $[Hb]_{rbc}$ , is taken to be 21.4 mM (heme concentration). The average Hb concentration in the core regions depends on the local hematocrit and the velocity profile, which is discussed below.

In the shell region, the absence of Hb leads to pure dissolved  $O_2$  diffusion (13).

$$u_o(r)\frac{\partial p}{\partial z}=D_{O_2}\left(\frac{1}{r}\frac{\partial}{\partial r}\left(r\frac{\partial p}{\partial r}\right)\right) \quad (13)$$

The velocity profile is blunted in the core region due to the presence of RBCs and is parabolic in the shell region. The profiles used in each region are (14) and (15).

$$u_c(r)=u_{max}\left(1-B\left(\frac{r}{R}\right)^2\right), \quad 0 \leq r \leq \lambda R \quad (14)$$

$$u_o(r)=u_{pl}\left(1-\left(\frac{r}{R}\right)^2\right), \quad \lambda R \leq r \leq R \quad (15)$$

The values for  $\lambda$  are taken from direct experimental measurements 25- $\mu$ m diameter tubes by Tateishi et al [33]. Because only values for 20%, 30%, and 40% hematocrits are available,

the values for 15% hematocrit and 45% hematocrit are extrapolated linearly. The  $\lambda$  values used for 5, 10, 15 g/dl Hb (i.e. 15%, 30%, 45% hematocrit) are 0.68, 0.74, and 0.90, respectively. Velocity magnitudes in each region may be found from the two-phase flow model of Sharan et al [34]. The values for  $u_{max}$ ,  $u_{pl}$ , and  $B$ , given in (16), (17) and (18) below, are functions of the core viscosity ( $\mu_c$ ), plasma viscosity ( $\mu_o$ ), average flow speed ( $u_{avg}$ ), and  $\lambda$ .

$$u_{max} = 2u_{avg} \left( 1 - \lambda^2 \left( 1 - \frac{\mu_o}{\mu_c} \right) \right) \left( \frac{\mu_o}{\mu_c} \lambda^4 + 1 - \lambda^4 \right)^{-1} \quad (16)$$

$$u_{pl} = 2u_{avg} \left( \frac{\mu_o}{\mu_c} \lambda^4 + 1 - \lambda^4 \right)^{-1} \quad (17)$$

$$B = \frac{\mu_o}{\mu_c} \left( 1 - \lambda^2 \left( 1 - \frac{\mu_o}{\mu_c} \right) \right)^{-1} \quad (18)$$

Core viscosity values of 1.5 cP, 2.5 cP, and 3 cP are used for hematocrits 15%, 30%, and 45%, based on the work of Pries et al. [35], and a plasma viscosity of 1 cP is assumed.

The transport model has two major modifications compared to a version of that presented and validated in RBC artificial capillary experiments by Nair et al. [14]. Because it has been shown that < 5% of the O<sub>2</sub> transport resistance is associated with diffusion in or near RBCs [14], we treat O<sub>2</sub> tension and O<sub>2</sub> solubility as constant inside and outside RBCs, rather than treating individual partitions of intra- and extra-cellular dissolved O<sub>2</sub>; this assumption has been validated elsewhere [36]. The thickness of the cell-depleted layer is taken directly from experimental observation instead of calculated from a set of algebraic equations which involve a number of hydrodynamic assumptions.

## Boundary Conditions

The solution of (9, 10) and (11, 12) requires six boundary conditions to be specified: one each in  $p$  and  $Y$  at the tube entry, inner radial boundary, and outer radial boundary. The entry conditions are set to  $p = 100$  mmHg (average  $p$  in the lungs) and  $Y$  of Hb is set to equilibrium with the  $p$  entry condition. The condition of axisymmetry requires that the radial partial derivatives of  $p$  and  $Y$  be set to zero at the centerline of the domain. The impermeability of the domain wall to the diffusion of Hb requires that the radial derivative of  $Y$  also be zero at  $r = R$ . The rate at which O<sub>2</sub> leaks from the intra- to the extra-luminal environment is dictated by a boundary condition of the form (19).

$$\left. \frac{\partial p}{\partial r} \right|_{r=R} = - \frac{Bi}{R} (p_w - p_\infty) \quad (19)$$

$Bi$  is the mass transfer Biot number, which is adjusted to control the rate at which O<sub>2</sub> is transported into the extra-luminal environment.  $Bi$  is used as a standardized method to quantify processes, such as O<sub>2</sub> diffusion and consumption, which occur outside of the lumen. Using this parameter, the rate at which O<sub>2</sub> leaves the lumen is compared to an estimate of the intra-luminal diffusion rate. The formula for  $Bi$  is  $(h_{Ext} \times L)/D_{O_2}$ , where  $h_{Ext}$  can be considered an extra-luminal mass transfer coefficient,  $L$  is a representative diffusion length, and  $D_{O_2}$  is the diffusivity of O<sub>2</sub> in solution. Thus,  $Bi$  provides an estimate of the ratios of intra-luminal to extra-luminal transport resistance ( $1/h_{Ext}$  to  $L/D_{O_2}$ ). A circuit diagram schematic of intra- and extra-luminal mass transfer resistances is shown in Fig. 1B. The intra-luminal transport resistances can be represented as the contributions due to O<sub>2</sub> diffusion ( $1/h_{O_2}$ ), facilitated HbO<sub>2</sub> diffusion ( $1/h_{Hb}$ ), and extra-luminal processes ( $1/h_{Ext}$ ). The value for  $h_{Ext}$  can

be thought of as a function of the Biot number and  $h_{O_2}$ , where  $h_{Ext} \sim Bi \times h_{O_2}$ . The  $Bi$  values primarily considered in this study are 1 and 10. All of the simulations performed assume  $p_{\infty} = 0$  mmHg.

### Relevant time scales

The PDE formulations contain axial variations in only the first, convective term. This term may be normalized by relevant velocity and length scales [37] to show that considering variations along the length of a tube is analogous to considering the amount of time a parcel of fluid has been within the domain. We relate axial changes as a function of residence time, defined as  $z/u_{avg}$ , where  $z$  is the axial position and  $u_{avg}$  is the average flow velocity. Examples of physiologically relevant residence times can be determined from *in vivo* data of the hamster arteriolar network (Table 2). The average flow velocities are less than the displayed centerline RBC velocities by a factor of  $\sim 0.6$ , according to the analysis in Sharan et al. [34]. The average residence time for blood in a particular arteriolar segment is therefore given as  $\Delta t = L/(0.6 \times v_{rbc})$ , with residence times in each arteriolar segment  $< 0.5$  seconds.

### Solution method

The system of coupled, nonlinear partial differential equations was solved with Comsol Multiphysics software (Comsol, Palo Alto, CA), a nonlinear, finite-element based solver that is commonly used for chemical/biological engineering applications. An automatic gridding function is used for the initial discretization of the domain, with subsequent grid resolutions applied manually in regions where high spatial resolution is necessary. This is particularly important near the radial boundary at the domain entry because of the occurrence of mass transfer boundary layer-type behavior. A typical grid using  $\sim 5000$  elements causes the convergence of a Galerkin error monitor. Solutions are exported to Matlab (Mathworks, Natick, MA) for post-processing.

## 3. Results

### Model validation

The model was validated by direct comparison of *in vitro* artificial capillary experiments performed in 27- $\mu$ m diameter silicone tubes Page et al. [17] and in 57- $\mu$ m diameter silicone tubes by McCarthy et al. [7]. The parameters used for the modeling are given in Table 3. Figure 2A shows the simulations replicating the Page deoxygenation experiments on RBCs, unmodified bovine Hb (BvHb), and polymerized bovine Hb (PolyBvHb). The simulation for each of these appears to be in good agreement with the experimental data. Figure 2B shows the data from the McCarthy experiments. The simulations for RBCs, PEG-conjugated Hb (PEGHb), and  $\alpha\alpha$ -cross-linked Hb ( $\alpha\alpha$ -Hb) are within reasonable agreement of the experimental data. A somewhat larger discrepancy between experiment and simulation is seen for unmodified, purified human Hb (HbA<sub>0</sub>), which may be due to dimer formation or other experimental problems that are not accounted for by this model.

### Extra-luminal Resistance Effects

Simulations were performed for a variety of  $Bi$  values, ranging from 0.1 to  $10^3$  on RBCs and generic acellular Hb. Increasing  $Bi > 100$  yields negligible increases in total  $O_2$  transport, thus the case of  $Bi = 100$  can be considered the maximum expected rate of  $O_2$  transport. This is comparable to the *in vitro* experiments of Page et al. [17] and McCarthy et al. [7]. The total  $O_2$  delivered versus apparent residence time is plotted in Fig. 3 for RBCs ( $p_{50} = 29$  mmHg,  $[Hb] = 15$  g/dl Hb). At 0.5 seconds,  $Bi = 1$  gives 40% of the  $O_2$  delivered at the maximum rate (i.e. for  $Bi = 100$ ), while  $Bi = 10$  gives 90% of this amount. The  $O_2$  delivery for  $Bi = 3$  is plotted to give an intermediate value between  $Bi = 1$  and  $Bi = 10$ , and to show that variations of  $O_2$

transport in this region are not linear with  $Bi$ . The  $O_2$  delivered for  $Bi < 0.1$  is small on the time scales we have considered and is not plotted.

### Effects of $O_2$ binding kinetics and cooperativity

Rates of  $O_2$  dissociation may, theoretically, become rate limiting in this system. We performed simulations on very small diameter tubes, where the speeds of lateral  $O_2$  transport may be comparable to the rates at which  $O_2$  disassociates from Hb. If the dissociation of  $O_2$  from Hb is limiting to the amount of  $O_2$  released into the surrounding environment, the reaction kinetics must be modeled more carefully than the generalized treatment in (7) and (8). We performed simulations with several dissociation rate constants ( $k$ ) to assess the magnitude at which the rate becomes limiting. Figure 4A shows the results of simulations carried out for  $Bi = 10$  with a HbOC similar to tetramer hemoglobin, ( $p50 = 15$  mmHg,  $n = 3$ ,  $D_{HbO_2} = 1 \times 10^{-6}$  cm<sup>2</sup>/s,  $[Hb] = 10$  g/dl). For clarity, we use the inverse of the expression in (8), so that a constant off-rate is applied and the on-rate is varied locally as a function of  $p$ ,  $p50$ , and  $n$ , although the expression (8) gives equivalent results. Increases in  $k$  lead to progressively larger amounts of  $O_2$  transport, until the  $O_2$  transport approached some maximum value. This begins to occur above  $k = 10$  s<sup>-1</sup>, where order of magnitude increases in  $k$  are required in order to raise the amount of  $O_2$  transport by similar, small amounts. The most common off rate used in Moll-type treatments (44 s<sup>-1</sup>) are in a range where  $O_2$  delivery is insensitive to small variations in  $k$ , and thus is adequate for the size scales we study. The off-rates reported in the literature are of a similar order [31]. However, significant limitations on  $O_2$  transport occur at either slower off-rates or smaller tube diameter than are considered here. For  $O_2$  dissociation kinetics to be a considerable limiting factor on the overall  $O_2$  transport behavior for our particular geometry,  $k$  must be reduced to on the order of  $\leq 1$  s<sup>-1</sup>.

The effect of cooperative binding is dependent on both the  $p50$  of the Hb solution and the extra-luminal resistance (the Biot number). Cooperative Hbs bind a greater fraction of  $O_2$  at  $p$  values near the  $p50$  than non-cooperative Hb. For this reason, the amount of  $O_2$  available to be released tends to be greater for low  $n$  Hb, as long as  $p > p50$ . In cases where  $p50$ s are high, non-cooperative Hb is less saturated than cooperative Hb in the lungs. If the total  $O_2$  content is sufficiently reduced due to this, decreases in  $n$  may serve to reduce the amount of  $O_2$  released, although it also reduces the potential for  $O_2$  transport further downstream. An example of this behavior is given in Fig. 4B, which shows the  $O_2$  released from  $p50 = 5$  mmHg and  $p50 = 35$  mmHg Hb, each with  $n = 1$  and  $n = 3$  ( $D_{HbO_2} = 3 \times 10^{-7}$  cm<sup>2</sup>/s,  $[Hb] = 10$  g/dl,  $Bi = 10$ ). For  $p50 = 5$  mmHg, increasing  $n$  from 1 to 3 decreases  $O_2$  transport by about 20%. Hb with  $n = 1$  has only 4% less initial Hb saturation than Hb with  $n = 3$ , so the behavior is dominated by the differences in the available  $O_2$  when  $p > p50$ . For Hb with  $p50 = 35$  mmHg, the Hb saturation at initial conditions is 22% less for  $n = 1$  than  $n = 3$ . This leads to about a 40% increase in  $O_2$  transport for  $n = 3$  Hb as compared to  $n = 1$  Hb. At a  $p50 \sim 15$  mmHg, the two trends exhibited roughly cancel each other out and there is no appreciable cooperativity effect. We will show later that for  $Bi = 10$ , Hbs with  $p50 \leq 15$  mmHg are of primary interest, and in such cases, increased cooperativity would decrease  $O_2$  transport. When the Biot number is decreased to 1, Hbs with  $p50$ s less than 35 mmHg show decreased  $O_2$  transport with increased  $n$ .

### Facilitated Diffusion

The effect of modifying  $D_{HbO_2}$  is only significant for lower values of extra-luminal resistance, such as when  $Bi = 10$  (Fig 5). The additional  $O_2$  transport due to this effect is  $\sim 30\%$  for simulations ( $D_{HbO_2} = 1 \times 10^{-6}$  cm<sup>2</sup>/s versus  $D_{HbO_2} = 1 \times 10^{-8}$  cm<sup>2</sup>/s). The effect of decreasing  $D_{HbO_2}$  past  $1 \times 10^{-7}$  cm<sup>2</sup>/s is small. These facilitated-diffusion effects are not significant for  $Bi = 1$ , partly because of the decreased importance of intra-luminal diffusive processes when extra-luminal resistance is high, and partly due to the high degree of saturation of Hb. The values of  $D_{HbO_2}$  we simulated are  $\{10, 3, 1, 0.1\} \times 10^{-7}$  cm<sup>2</sup>/s. Assuming Hb as a spherical



molecule in the Stokes-Einstein equation (20),  $D_{\text{HbO}_2}$  values  $\{10, 3, 1\} \times 10^{-7} \text{ cm}^2/\text{s}$  correspond to molecular radii of  $\{2.3, 6.8, 23\} \text{ nm}$ .

$$D_{\text{Hb}} = \frac{kT}{6\pi\mu r_A} \quad (k=1.38 \times 10^{-23} \text{ m}^2\text{kg s}^{-2}\text{K}^{-1}, T=310\text{K}, \mu=1 \text{ cP}) \quad (20)$$

### Oxygen Affinity

Simulations were performed on a variety of idealized acellular Hbs with varying  $p50$  (base molecule:  $n = 1$ ,  $D_{\text{HbO}_2} = 3 \times 10^{-7} \text{ cm}^2/\text{s}$ ,  $[\text{Hb}] = 10 \text{ g/dl}$ ) and are summarized in Fig. 6A and Fig. 6B. Regardless of the applied extra-luminal resistance,  $p50$  has a significant effect on the amount of  $\text{O}_2$  transport. At the residence times that we study (0.5 seconds),  $\sim 1/10$  of the total  $\text{O}_2$  content is delivered to the surrounding environment for  $Bi = 1$  and  $\sim 1/3$  of the total  $\text{O}_2$  content for  $Bi = 10$ . At either  $Bi$  number evaluated, increasing the  $p50$  above 25 mmHg has a very small effect on the total  $\text{O}_2$  released. The largest variation in behavior is seen between  $p50 = 5$  and  $p50 = 15 \text{ mmHg}$ . For  $Bi = 1$ , RBC the total  $\text{O}_2$  transport is slightly less than Hb with  $p50 = 15 \text{ mmHg}$  and  $n = 1$ , despite the much lower  $\text{O}_2$  affinity of RBCs ( $p50 = 29 \text{ mmHg}$ ). For  $Bi = 10$ , RBCs deliver similar amounts of  $\text{O}_2$  as Hb with  $p50 = 5 \text{ mmHg}$ . In this case, an increase in  $p50$  from 5 to 25 mmHg has the potential to increase  $\text{O}_2$  transport by  $\sim 1/3$  as compared to RBCs.

### Hb Concentration

The effect of Hb concentration is given in Fig. 7A and Fig. 7B. For  $Bi = 1$ , the  $\text{O}_2$  transported by Hb with  $p50 = 15 \text{ mmHg}$ ,  $n = 1$ , and  $D_{\text{HbO}_2} = 3 \times 10^{-7} \text{ cm}^2/\text{s}$  matches reasonably well with RBCs at 5, 10, and 15 g/dl (Fig. 7A). Tripling  $[\text{Hb}]$  from 5 g/dl to 15 g/dl increases the amount of  $\text{O}_2$  delivered by less than 50%. For  $Bi = 10$ ,  $\text{O}_2$  transport from  $p50 = 15 \text{ mmHg}$  is larger at every  $[\text{Hb}]$  matched with that for RBCs (Fig. 7B). The increases in total  $\text{O}_2$  transport by tripling  $[\text{Hb}]$  is about 80% for Hb and 60% for RBCs.

### Optimal Hb Properties to mimic RBCs on a heme-per-heme basis

The properties of an acellular Hb that match the  $\text{O}_2$  transport from RBCs at the same Hb concentration are a function of the applied boundary conditions, especially the Biot number. We have already shown that Hb with  $p50 = 15 \text{ mmHg}$  and  $n = 1$  is a good match for RBCs when  $Bi = 1$ , or Hb with  $p50 = 5 \text{ mmHg}$  and  $n = 1$  is a good match with  $Bi = 10$  (Fig. 6A and Fig. 6B). Figure 8 shows the  $\text{O}_2$  transport from three acellular Hbs with significant binding cooperativity ( $n = 2.5$ ) that supply comparable amounts of  $\text{O}_2$  to 10 g/dl RBCs. The results for RBCs should not be confused with the results in Fig. 3, which are for RBCs at 15 g/dl. Assuming  $n = 2.5$  and  $D_{\text{HbO}_2} = 3 \times 10^{-7} \text{ cm}^2/\text{s}$ , the  $p50$ s that match  $Bi = 1, 3,$  and  $10$  are 20, 15, and 9 mmHg, respectively. For each of these cases, an increase in  $D_{\text{HbO}_2}$  would necessitate a decrease in the  $p50$  to provide the same amount of  $\text{O}_2$ .

### Lateral Oxygen Gradients

Thus far, we have reported simulated results for macroscopic transport of  $\text{O}_2$  from flowing Hb solutions into the surrounding environment, i.e., radial transport. Figure 9 shows the lateral intra-luminal  $\text{O}_2$  gradients for two of the Hb/RBC pairs plotted in Fig. 8, which give comparable  $\text{O}_2$  transport. These gradients are defined as the difference between  $p$  at the centerline and  $p$  at the radial lumen boundary. For each  $Bi$  number used in the simulations, the gradient for RBCs is larger than that for acellular Hb, an effect related to the reduction of intra-luminal  $\text{O}_2$  transport resistance for acellular Hb. For  $Bi = 1$ , the RBC lateral gradient is roughly twice as much as that for Hb; for  $Bi = 10$  it is roughly three times that of Hb. Decreasing extra-luminal resistance (increasing  $Bi$ ) increases the magnitude of lateral gradients.

## 4. Discussion

Hemoglobin-based oxygen carriers can offload O<sub>2</sub> more efficiently in arteriolar-sized vessels than red blood cells because they overcome transport barriers associated with low plasma O<sub>2</sub> solubility, increased distance for O<sub>2</sub> diffusion, and limited intracellular oxyHb diffusion (facilitated diffusion). Over supply of O<sub>2</sub> can lead to two potentially undesirable consequences: 1) the onset of autoregulatory vasoconstriction and consequent reduced tissue oxygenation; 2) a decrease in Hb-bound O<sub>2</sub> available for downstream O<sub>2</sub> delivery in capillary beds. Oxygen delivery in arteriolar-sized tubes can be controlled by O<sub>2</sub> equilibrium binding properties ( $p50$  and  $n$ ), diffusion kinetics ( $D_{\text{HbO}_2}$ ), and Hb concentration.

Animal studies have shown that isolated decreases in  $p50$  [24], increases in  $n$  [38], or increases in molecular size [39] all correlate with increased tissue perfusion. *In vivo* experiments have also shown that Hbs with a combination of high  $p50$  and small molecular size cause vasoconstriction and hypertension [3,4]. Hemoglobin molecules that are small (i.e. near the size of unmodified Hb) may diffuse fast enough to augment O<sub>2</sub> transport by carrying Hb-bound O<sub>2</sub> from the center of a vessel towards the wall. Decreases in O<sub>2</sub> affinity and increases in molecular size (i.e.  $D_{\text{Hb}}$  and consequently  $D_{\text{HbO}_2}$ ) have been observed to accelerate O<sub>2</sub> offloading for *in vitro* O<sub>2</sub> transport models [7,13,15–17]. This combination of *in vivo* and *in vitro* observations has contributed to the theory that an over supply of O<sub>2</sub> by acellular Hb in arterioles leads to autoregulatory vasoconstriction.

Here, we report mathematical modeling of O<sub>2</sub> transport from Hb solutions in arteriolar-sized domains to assess the efficacy of prospective HBOCs. There are differences between these simulations and relevant *in vivo* conditions to be considered: the simulated extra-luminal boundary conditions are simpler, the domain is long and non-branching, and the acellular Hb solutions are not mixed with RBCs. However, the model provides a useful tool in understanding the relative importance of  $p50$ ,  $n$ , [Hb], and  $D_{\text{HbO}_2}$  for acellular Hbs.

To reduce the number of variables for HBOC design, we limited direct comparisons of acellular Hb and RBCs to those at the same Hb concentration. It should be noted that humans can survive with significantly reduced hematocrits [40], and with the added efficiency of O<sub>2</sub> transport by acellular Hb solutions, it may not be necessary to create HBOCs that fully replace lost Hb content. The [Hb] for HBOCs that have been produced for clinical purposes vary from 4.2 g/dl to 13.1 g/dl, yet *in vivo* experiments have shown that low [Hb] HBOCs can provide adequate O<sub>2</sub> for respiration [5].

We first tested the assumption that O<sub>2</sub> dissociation kinetics do not limit overall O<sub>2</sub> transport processes. We find the off rates used for the model Hbs, which were taken from measured values in the literature [31], to be within a range of values that total O<sub>2</sub> transport is relatively insensitive.

Previous models of O<sub>2</sub> transport in arteriolar-sized domains by acellular Hbs [13,15] have not considered extra-luminal processes that set the O<sub>2</sub> gradient from intra- to extra-luminal space. At present there is no generally accepted model of arteriolar O<sub>2</sub> consumption, but to take these overall processes into consideration mathematically, we lumped all extra-luminal processes into one parameter, the Biot number ( $Bi$ ).  $Bi$  provides an inverse measure of extra-luminal resistance such that high resistance would reflect a relatively lower extra-luminal O<sub>2</sub> consumption rate and vice versa. There is a balance between the amount of O<sub>2</sub> available for transport, dictated by equilibrium binding effects ( $p50$  and  $n$ ) and the rate at which O<sub>2</sub> diffuses laterally. This balance is dependent on the value of the extra-luminal resistance. When desaturation processes are fast ( $Bi$  small), the magnitudes of  $D_{\text{O}_2}$  and  $D_{\text{HbO}_2}$  do more to limit the total amount of O<sub>2</sub> delivered than when desaturation processes are slower. Conversely, equilibrium binding effects are more important when the desaturation rates are slow. For 15

g/dl RBCs with  $Bi = 3$ , the average  $O_2$  flux at 0.5 seconds is  $4.4 \times 10^{-5} \text{ mlO}_2 \text{ cm}^{-2} \text{ s}^{-1}$  based on the results of the simulations shown in Fig. 3. The  $O_2$  flux,  $J_{avg}$ , is calculated as (21) where  $\Delta[O_2]_{total}$  is the change in total  $O_2$  content,  $R$  is the tube radius, and  $\Delta t$  is the elapsed residence time.

$$J_{avg} = \frac{R \Delta[O_2]_{tot}}{2 \Delta t} \quad (21)$$

Physiological measurements, such as those given in Table 2 use (21) to determine  $J_{avg}$  between two discrete points on a given arteriole. The value for  $J_{avg}$  is specific to the position on an arteriole and the time increment, thus it is an estimate. The measured  $O_2$  fluxes for arterioles were tabulated for a large number of *in vivo* studies by Vadapalli et. al. [23]. The average  $O_2$  fluxes from 7 vessels with diameters between  $19.5 \mu\text{m}$  to  $35 \mu\text{m}$  (compiled in [23], original data from [41–44]) is  $4.6 \times 10^{-5} \text{ mlO}_2 \text{ cm}^{-2} \text{ s}^{-1}$ . The  $Bi$  values we considered in this study (1 and 10) provide RBC fluxes which bracket this value, an attempt to describe a range of potential behavior.

Of the three design parameters we considered, the effect of  $D_{HbO_2}$  is the most straight-forward. Facilitated diffusion is only significant for larger Biot numbers when the overall  $O_2$  transport is relatively fast. This is partially due to the emphasis on intra-luminal processes when extra-luminal resistance is small. This phenomenon may also be partly understood from a circuit representation of mass transfer processes (Fig. 1B). The intra-luminal transport resistances can be represented as the contributions due to  $O_2$  diffusion ( $1/h_{O_2}$ ), facilitated  $HbO_2$  diffusion ( $1/h_{Hb}$ ), and extra-luminal processes ( $1/h_{Ext}$ ), where  $h$  is a generalized mass-transfer coefficient. The total resistance,  $\Omega$ , between the lumen and the far field may be written as (22).

$$\Omega = \frac{h_{O_2} + h_{Hb} + h_{Ext}}{(h_{O_2} + h_{Hb})h_{Ext}} \quad (22)$$

According to this, the value of  $h_{Hb}$  has the greatest proportionate effect on the value of  $\Omega$  when extra-luminal resistance is small (i.e.  $h_{Ext}$  is large). The high degree of Hb saturation for the high extra-luminal resistance cases considered here also limit the potential gradients in  $Y$ . Decreasing  $D_{HbO_2}$  by an order of magnitude from  $10^{-6} \text{ cm}^2/\text{s}$  to  $10^{-7} \text{ cm}^2/\text{s}$  suppresses most of the facilitated diffusion effect. If we consider a spherical molecule diffusing through water (according to the Stokes-Einstein equation), a molecular radius  $\sim 23 \text{ nm}$  (i.e.  $D_{HbO_2} = 10^{-7} \text{ cm}^2/\text{s}$ ) would define the minimal size to eliminate additional transport due to facilitated diffusion. Hb polymers have been tested above this size range [45], with the intention of decreasing interactions of Hb with the endothelium; such modifications would not have an appreciable effect in reducing facilitated diffusion.

It may not be feasible to create PEG–Hb molecules that are large enough to completely eliminate facilitated diffusion, because PEG–Hb molecular size is enlarged by increasing the number and/or the length of attached PEG chains, which causes an increase in colloid osmotic pressure (COP) through hydraulic interactions with PEG. Increasing the molecular weight of native Hb by  $\sim 30 \text{ kDa}$  due to PEGylation correlates to an increase in COP of  $34 \text{ mmHg}$  for  $4.2 \text{ g/dl}$  Hb solutions [46]. Such an increase in molecular weight leads to a 3-fold increase in molecular radius (to  $9.3 \text{ nm}$ ). The amount of PEG required to increase the molecular size to  $23 \text{ nm}$  (i.e. increasing  $D_{HbO_2}$  to  $10^{-7} \text{ cm}^2/\text{s}$ ) is likely to cause increases in COP  $> 100 \text{ mmHg}$ . For such cases, it appears that the best strategy would be to further decrease  $p50$ . This model allows a quantitative estimation at how large such a reduction should be.

The effects of  $O_2$  affinity and binding cooperativity are inter-related and each is a function of the applied extra-luminal resistance. Regardless of the extra-luminal resistance value, varying

the  $p50$  has the potential to have a large effect on the amount of  $O_2$  released by Hb. The range of  $p50$ s for which  $O_2$  offloading is the most sensitive in our model (5–15 mmHg) is much lower than the  $p50$  of RBCs (29 mmHg). In the context of this model, any increase in  $p50$  above 25 mmHg does not serve a purpose. The  $p50$  of an HBOC must be dropped by about 10 mmHg in order to see the same amount of  $O_2$  delivered relative to RBCs in the  $Bi = 10$  case compared to the  $Bi = 1$  case. The specific choices of  $p50$  are also subject to the value of  $n$ , which is itself subject to extra-luminal conditions, and the value of  $p50$ . For the faster desaturation rate we studied, with  $p50 > 15$  mmHg, increasing  $n$  increases  $O_2$  transport. For Hbs with high  $p50$  and low cooperativity, a significant fraction of Hb will not bind  $O_2$  in the lungs; this Hb will be non-functional in terms of supplying  $O_2$  and may potentially participate in oxidative processes [47]. In either case, this leads to a flawed design. For  $p50$ s below 15 mmHg, cooperative binding decreases the amount of  $O_2$  supplied. This allows for the use of slightly higher  $p50$  Hb to provide equivalent  $O_2$  transport as a lower cooperativity, lower  $p50$  Hbs.

A brief investigation shows that the intra-luminal lateral  $p$  gradients required to deliver a given amount of  $O_2$  are much greater for RBCs than for acellular Hb. This is a consequence of the transport resistance associated with the cell-depleted layer (for RBCs) and the reduction in transport resistance due to facilitated diffusion (for acellular Hb).

The cell-depleted layer acts as an insulator to the cell-rich core region of RBCs, thus requiring larger gradients to drive  $O_2$  diffusion through the cell-depleted layer, and causing the total  $O_2$  delivery to be less sensitive to conditions at the vessel wall. The lack of a cell-depleted layer allows acellular Hb to have a lower  $p50$ , although it is more subject to extra-luminal conditions. As a consequence of this increased sensitivity, acellular Hb cannot be formulated to deliver  $O_2$  like RBCs for all potential extra-luminal environments. RBCs deliver  $O_2$  most like an acellular Hb with a  $p50$  of 15 mmHg when  $Bi = 1$  or 5 mmHg when  $Bi = 10$ . Therefore, low  $p50$ , increased  $n$ , and decreased  $D_{HbO_2}$  are all strategies to artificially impose transport resistance onto acellular Hb and suppress  $O_2$  transport in the precapillary microcirculation.

## Conclusion

If the goal of HBOC design is to limit precapillary  $O_2$  transport, this study provides some general guidelines for desired properties. High  $O_2$  binding affinity and cooperativity are desired, as well as an increase in molecular size and decreased diffusivity compared to native Hb. The  $p50$  should be reduced to the  $p50$  of unmodified Hb (15 mmHg) or less, depending of extra-vascular  $O_2$  consumption rates. For some classes of chemically modified Hbs, there are practical limitations on the ranges of design parameters available.

As we have shown, the problem with the design of HBOCs is not the difficulty of creating a molecule capable of carrying  $O_2$  to tissues; it is that the HBOCs tend to do their job too well, delivering  $O_2$  with higher efficiency than RBCs. An HBOC designed to transport  $O_2$  like RBCs must take into account the large scale reduction in intra-luminal transport resistance innate to acellular Hb solutions and find additional methods to limit  $O_2$  in the arterioles. The theory that HBOCs should be designed to target  $O_2$  release in specific, downstream sections of the vasculature has come about only after a large body of a research had been performed on early-generation HBOC products. In the context of this study, we can see that HBOCs that have  $p50$ s similar or greater than that of RBCs, tend to unload  $O_2$  faster than RBC suspensions. High  $O_2$  affinity HBOCs with decreased  $D_{HbO_2}$  have shown increased efficacy as blood substitutes in animal models, as compared to the first-generation Hb products [3,5].

So far our studies have focused on the effects of HBOC design parameters on  $O_2$  delivery from solutions containing only RBCs or pure acellular Hb. Future studies will be aimed at more physiologically relevant conditions, such as Hb/RBC mixtures that would result from with the clinical use of HBOCs. An additional concern in the design of HBOCs is the uptake of nitric

oxide from vessel walls by acellular Hb, another phenomenon that has been related to the onset of vasoconstriction. This removal of NO is thought to be accelerated in the presence of HBOCs due to the decreased diffusion distance and the high diffusivity of acellular Hb. Coupled O<sub>2</sub> delivery and NO uptake simulations can be performed using a mathematical model with the same general form as the one presented here. Studies to investigate Hb-NO binding kinetics are planned for the future.

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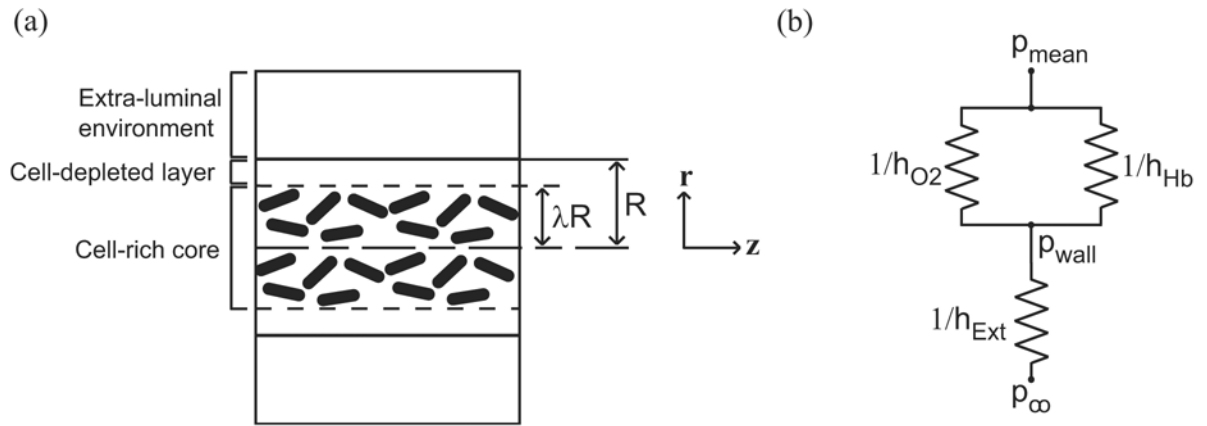
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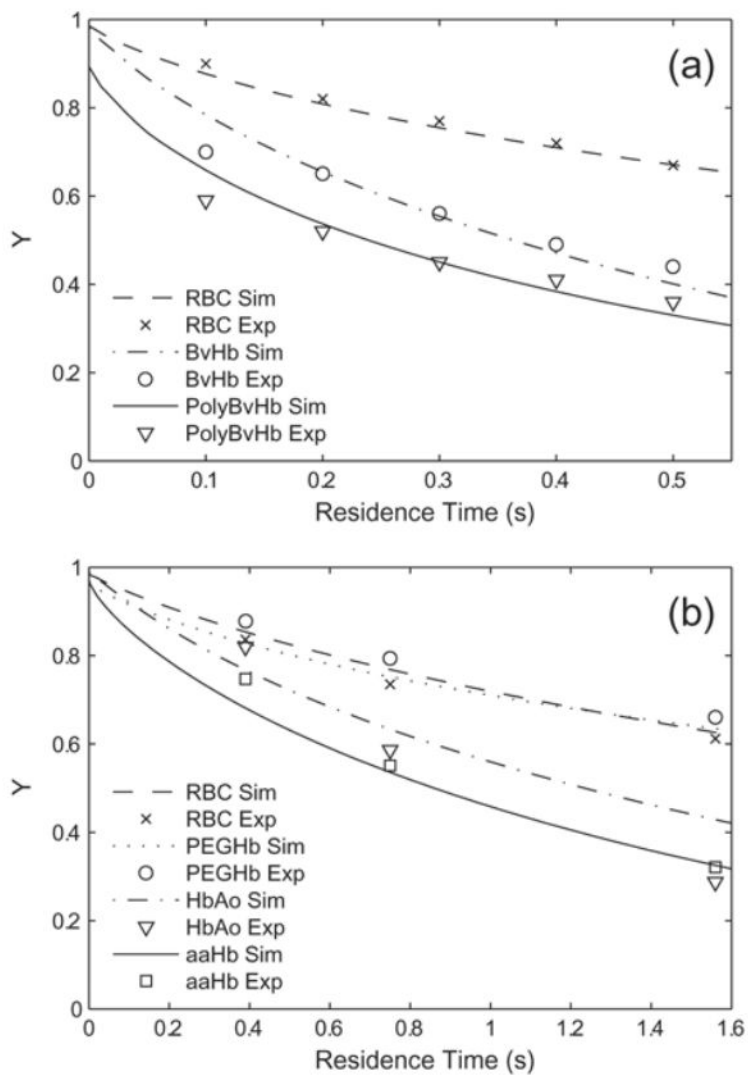
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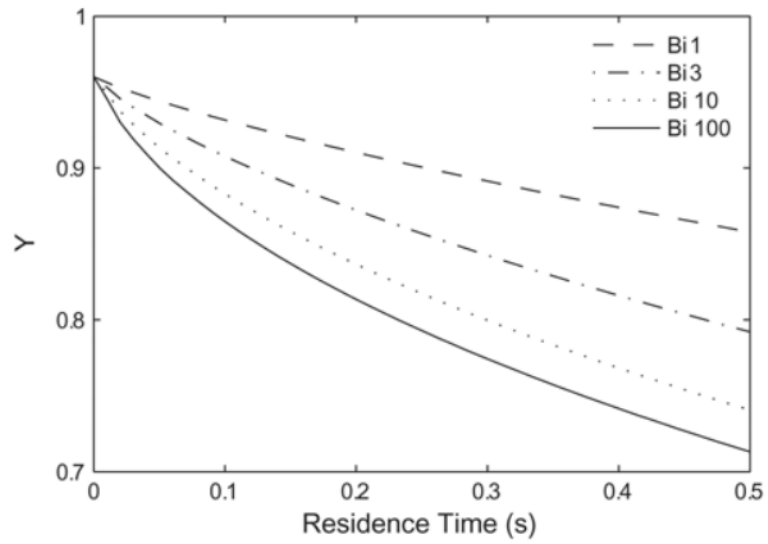
**Figure 1.**

(a) Schematic of tube geometry and thickness of cell-depleted layer when red blood cells are present. (b) Oxygen transport resistance schematic.  $1/h_{\text{O}_2}$  and  $1/h_{\text{Hb}}$  are the resistances associated with dissolved  $\text{O}_2$  and Hb.  $1/h_{\text{Ext}}$  is associated with the applied external resistance and is a function of the Biot number.

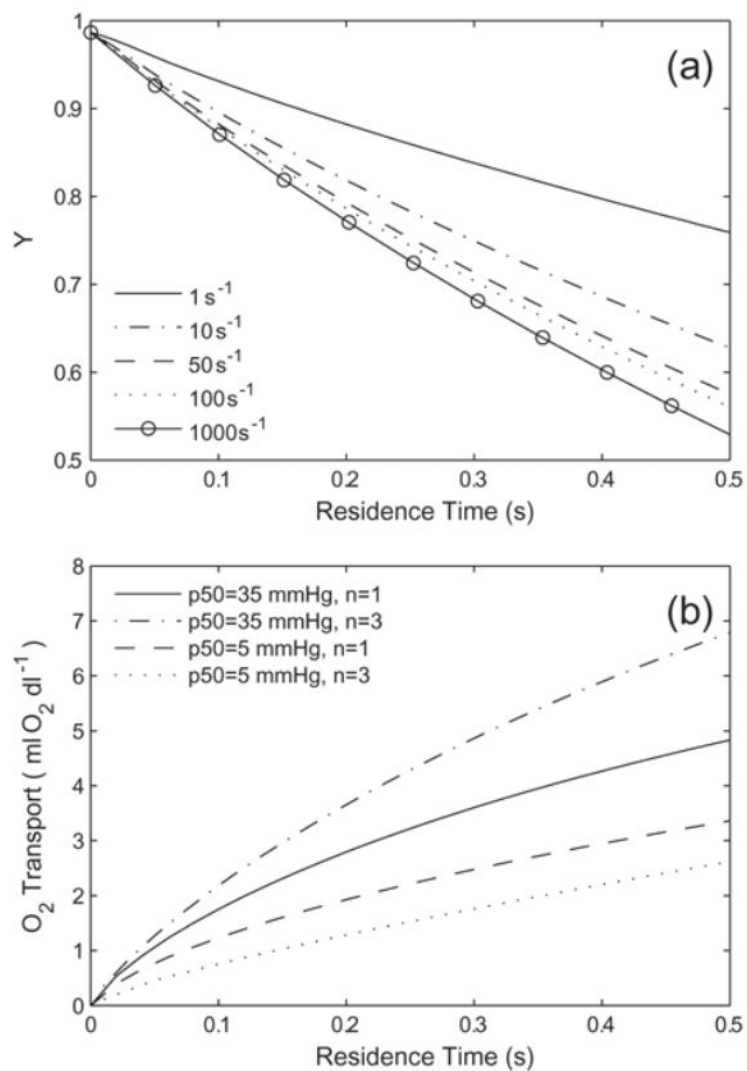




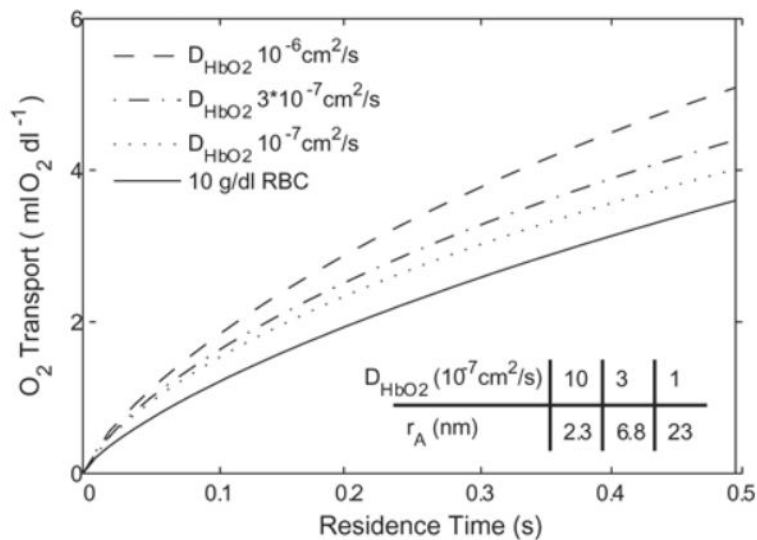
**Figure 2.** Results of simulations (Sim) compared to experiments (Exp) in (a) 27-µm diameter silicone tubes [Page, 1998a] and (b) 57-µm diameter silicone tubes [McCarthy, 2001]. Hb fractional saturation is plotted versus apparent residence time. The time scales are different because of the difference in tube diameters.



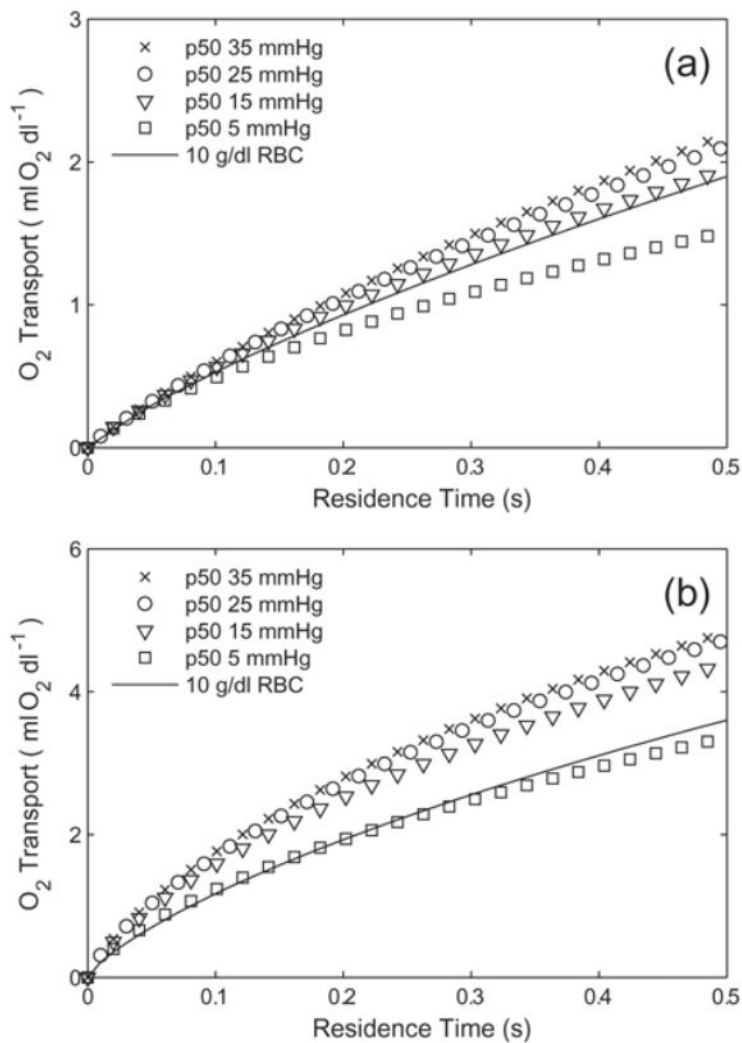
**Figure 3.** Effect of Biot number on the deoxygenation of a red blood cell suspension ( $[\text{Hb}] = 15 \text{ g/dl}$ ,  $p50 = 29 \text{ mmHg}$ ,  $n = 2.6$ ). Increasing the extra-luminal  $\text{O}_2$  transport resistance (decreasing  $Bi$ ) slows the rate of desaturation.



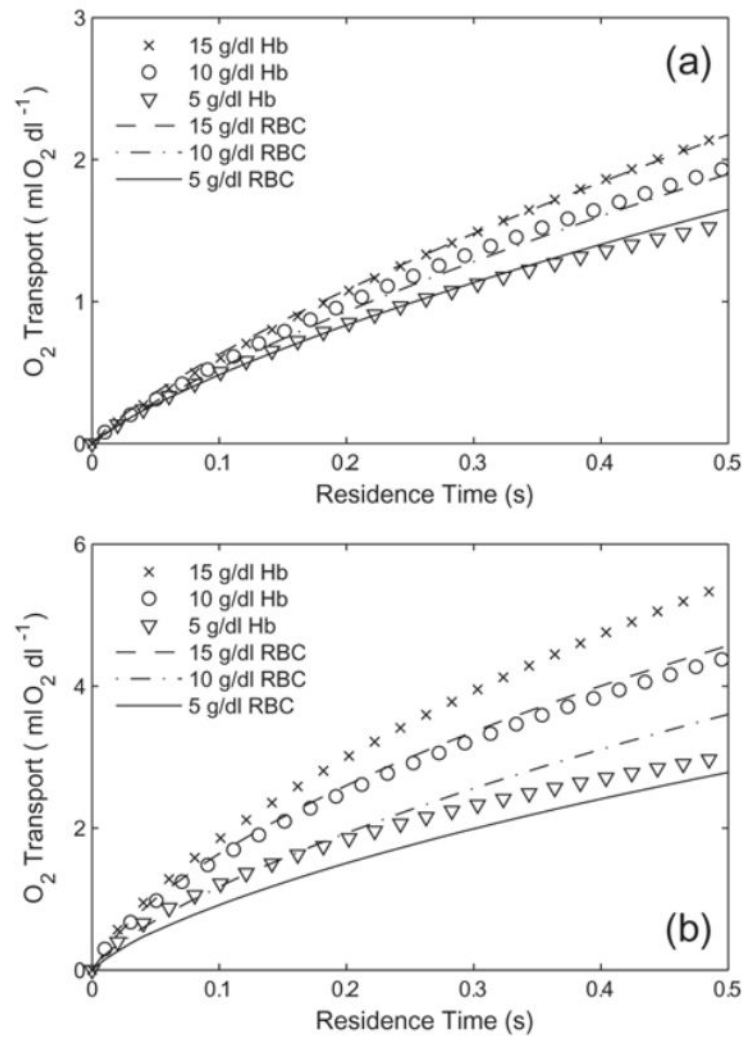
**Figure 4.** (a) Variations in Hb desaturation as a function of the off rate ( $k$ ,  $s^{-1}$ ) when  $Bi = 10$ . The Hb has the properties  $p_{50} = 15$  mmHg,  $n = 3$ ,  $D_{HbO_2} = 1 \times 10^{-6}$   $cm^2/s$ , and  $[Hb] = 10$  g/dl. (b) Effect of varied O<sub>2</sub> binding cooperativity on O<sub>2</sub> transport for generic Hb with  $p_{50} = 5$  mmHg and  $p_{50} = 35$  mmHg ( $D_{HbO_2} = 3 \times 10^{-7}$   $cm^2/s$ ,  $[Hb] = 10$  g/dl Hb) with  $Bi = 10$ . Cooperativity increases O<sub>2</sub> delivery for high  $p_{50}$  Hbs and decrease O<sub>2</sub> delivery for low  $p_{50}$  Hbs.



**Figure 5.** Effect of varied HbO<sub>2</sub> diffusivity on O<sub>2</sub> transport for generic Hb ( $p50 = 15 \text{ mmHg}$ ,  $n = 1$ ,  $[\text{Hb}] = 10 \text{ g/dl}$ ) with  $Bi = 10$ . These effects are not seen to be significant at  $Bi = 1$ . Table gives equivalent molecular radii for each  $D_{\text{HbO}_2}$  value, assuming a spherical Hb molecule diffusing through plasma.

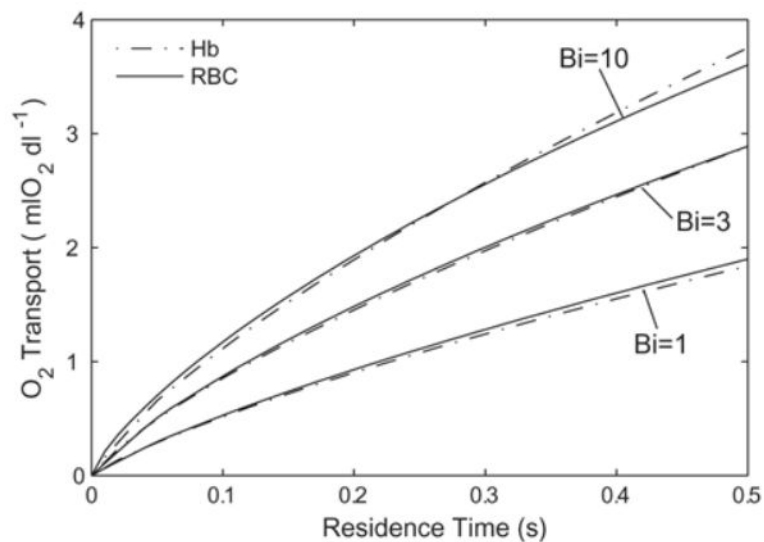


**Figure 6.** Oxygen transport by a generic Hb ( $n = 1$ ,  $D_{\text{HbO}_2} = 3 \times 10^{-7} \text{ cm}^2/\text{s}$ ,  $[\text{Hb}] = 10 \text{ g/dl Hb}$ ) with varied p50s for (a)  $Bi = 1$  and (b)  $Bi = 10$ . RBCs ( $p50 = 29 \text{ mmHg}$ ,  $n = 2.6$ ,  $[\text{Hb}] = 10 \text{ g/dl}$ ) are plotted for comparison.



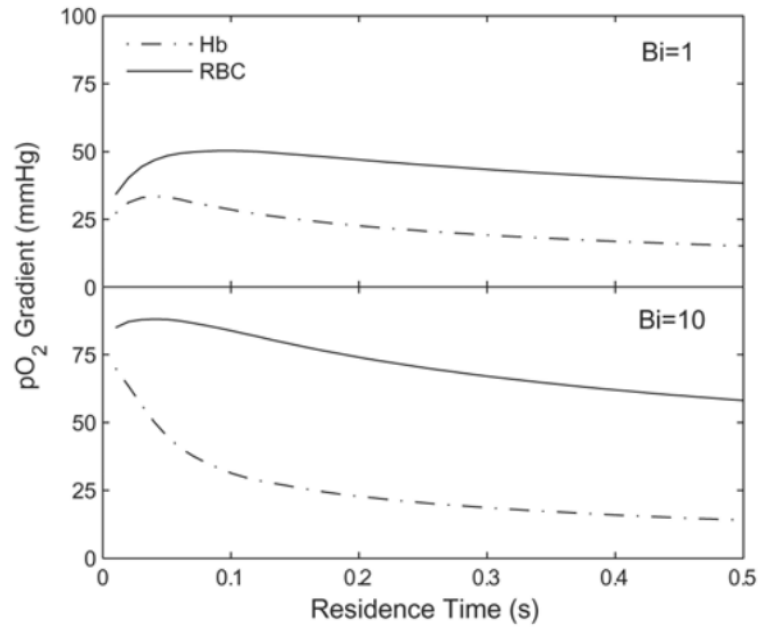
**Figure 7.**

Oxygen transport by a generic Hb solution ( $p50 = 15$  mmHg,  $n = 1$ ,  $D_{HbO_2} = 3 \times 10^{-7}$  cm<sup>2</sup>/s) with varied Hb concentration for (a)  $Bi = 1$  and (b)  $Bi = 10$ . RBCs ( $p50 = 29$  mmHg,  $[Hb] = 5$ – $15$  g/dl) are plotted for comparison.



**Figure 8.**

Oxygen transport from RBCs and from Hbs at various values of extra-luminal resistance that deliver similar amounts of  $O_2$ . The Biot numbers for each grouping, starting from the bottom are 1, 3, and 10. The RBCs and Hb both have a  $[Hb]$  of 10 g/dl. The Hb has  $n = 2.5$  and  $D_{HbO_2} = 3 \times 10^{-7} \text{ cm}^2/\text{s}$ . The  $p50$ s for  $Bi = 1, 3,$  and  $10$  are 20 mmHg, 15 mmHg, and 9 mmHg, respectively. Non-cooperative Hb choices can be seen in Fig. 6.



**Figure 9.** Lateral O<sub>2</sub> gradients for Hb solutions and RBC suspensions which give equivalent O<sub>2</sub> transport. The results are for the same simulations as shown in Fig. 8.



**Table 1**

Parameters used in the calculations

Symbol	Description	Value	Source
$r$	radial coordinate		independent parameter
$z$	axial coordinate		independent parameter
$R$	tube radius	12.5 $\mu\text{m}$	simulation parameter
$Bi$	mass transfer Biot number	1, 3, or 10	simulation parameter
$\alpha_{\text{pl}}$	$\text{O}_2$ solubility coefficient, in plasma	1.33 $\mu\text{M}/\text{mmHg}$	[12]
$\alpha_{\text{rbc}}$	$\text{O}_2$ solubility coefficient, inside RBC	1.47 $\mu\text{M}/\text{mmHg}$	[25]
$D_{\text{O}_2,\text{pl}}$	$\text{O}_2$ diffusivity in plasma	$2.75 \times 10^{-5} \text{ cm}^2/\text{s}$	[11]
$D_{\text{O}_2,\text{rbc}}$	$\text{O}_2$ diffusivity inside RBC	$1.48 \times 10^{-5} \text{ cm}^2/\text{s}$	[48]
$[\text{Hb}]_{\text{rbc}}$	heme concentration inside RBC	21.4 mM	[49]
$\alpha$	$\text{O}_2$ solubility coefficient	linearly interpolated between $\alpha_{\text{pl}}$ and $\alpha_{\text{rbc}}$ by $[\text{Hb}]$	
$D_{\text{O}_2}$	$\text{O}_2$ diffusivity	linearly interpolated between $D_{\text{O}_2,\text{pl}}$ and $D_{\text{O}_2,\text{rbc}}$ by $[\text{Hb}]$	
$D_{\text{HbO}_2}$	$\text{HbO}_2$ diffusivity	$\{1, 3, \text{ or } 10\} \times 10^{-7} \text{ cm}^2/\text{s}$	simulation parameter
$[\text{Hb}]_{\text{total}}$	total $[\text{Hb}]$ for RBC suspensions	5, 10, or 15 g/dl	simulation parameter
$\lambda$	normalized radius of RBC rich core	0.68, 0.74, or 0.90	[33]
$\mu_{\text{c}}$	core viscosity	1.5, 2.5, or 3 cP	[35]

**Table 2**

Description of Hamster retractor muscle arteriolar network. RBC velocities are taken at centerline. Data from [42].

order	d, $\mu\text{m}$	Y	P, mmHg	$v_{\text{RBC}}$ , mm/s	length, mm	$J_{\text{O}_2}$ , $\text{mlO}_2 \text{ cm}^{-2} \text{ s}^{-1}$	$\Delta t$ , sec
A1	55	0.67	39.7	15	3.67	$4.0 \times 10^{-5}$	0.41
A2	45	0.63	36.9	11	1.78	$4.2 \times 10^{-5}$	0.27
A3	34	0.61	35.8	5	0.48	$6.5 \times 10^{-5}$	0.16
A4	22	0.55	32.3	2.5	0.31	$4.8 \times 10^{-5}$	0.21

**Table 3**

Parameters used for validation simulations.

Hb type	[Hb], g/dl	p50, mmHg	n	$D_{HbO_2}$ , $cm^2/s$	Source
RBC	10.2	27	2.7	0	[15]
BvHb	10.2	25	2.7	$5.7 \times 10^{-7}$	[15]
Poly/BvHb	10.2	54	1.4	$2.7 \times 10^{-7}$	[15]
RBC	4.8	29	2.6	0	[7]
PEG-Hb	4.2	10	1.4	$0.8 \times 10^{-7}$	[7]
HbA <sub>0</sub>	4.8	15	3.0	$8.0 \times 10^{-7}$	[7]
aa-Hb	4.8	33	2.4	$8.0 \times 10^{-7}$	[7]