# Inverse planning for four-dimensional (4D) volumetric modulated arc therapy<sup>a)</sup>

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**Purpose:** To develop a 4D volumetric modulated arc therapy (VMAT) inverse planning framework. **Methods:** 4D VMAT inverse planning aims to derive an aperture and weight modulated arc therapy treatment plan that optimizes the accumulated dose distribution from all gantry angles and breathing phases. Under an assumption that the gantry rotation and patient breathing are synchronized (i.e., there is a functional relationship between the phase of the patient breathing cycle and the beam angle), the authors compute the contribution from different respiration phases through the registration of the phased CT images. The accumulative dose distribution is optimized by iteratively adjusting the aperture shape and weight of each beam through the minimization of the planning objective function. For comparison, traditional 3D VMAT plans are also performed for the two cases and the performance of the proposed technique is demonstrated.

**Results:** A framework for 4D VMAT inverse planning has been proposed. With the consideration of the extra dimension of time in VMAT, a tighter target margin can be achieved with a full duty cycle, which is otherwise not achievable simultaneously by either 3D VMAT optimization or gated VMAT.

**Conclusions:** The 4D VMAT planning formulism proposed here provides useful insight on how the "time" dimension can be exploited in rotational arc therapy to maximally compensate for the intrafraction organ motion. © 2010 American Association of Physicists in Medicine. [DOI: 10.1118/1.3497271]

Key words: VMAT, inverse planning, intensity modulation, dose optimization, arc therapy

# I. INTRODUCTION

Volumetric modulated arc therapy (VMAT) is an advanced form of rotational arc radiation therapy,<sup>1-9</sup> which produces conformal dose distribution through the modulation of beam shape and weight while gantry rotates continuously. By spreading out the delivered dose angularly through a continuous arc delivery, VMAT has the potential to improve sparing of organs-at-risk (OARs) and reduce treatment time. Practically, a limiting factor that may hinder the maximal utilization of VMAT dose delivery scheme is the intrafractional organ motion when treating tumors in the thorax or upper abdomen. Several studies based on fluoroscopic and 4D imaging have revealed that the intrafraction motion can be as large as 0.5–5 cm for tumors in these regions.<sup>10,11</sup> The actual received dose distribution of the patient may well differ from the planned distribution if the intrafractional anatomy change is not taken into account properly.<sup>12</sup> Commonly, a large safety planning target volume (PTV) margin is used in VMAT to avoid possible target miss, which unavoidably irradiates a large amount of adjacent normal tissues with high doses and thus increases the toxicity. Respiratory gating is an option in fixed-gantry IMRT to reduce the PTV margin.<sup>10,13–15</sup> Gated VMAT is possible at the cost of increased duty cycle of dose delivery, but requires frequent stopping of the heavy LINAC gantry during dose delivery.

A 4D plan optimization strategy<sup>16–18</sup> presents a logical solution to account for the intrafractional organ motion. In essence, 4D VMAT is an extension of the 4D IMRT scheme, first proposed by Trofimov *et al.*,<sup>16</sup> to rotational arc therapy. In this delivery, the beam aperture and weight at each angle are determined by minimizing the difference between the prescribed dose and the accumulative dose from all phases and gantry angles. Coupled with the recent advances in real-time monitoring of tumor motion and MLC-based tracking, this delivery scheme may become a viable choice in future radiation therapy armamentarium. An important and necessary step toward the realization of 4D VMAT is the development of an effective treatment planning framework. In this



FIG. 1. A schematic view of 4D VMAT. The trajectory of the source and aperture center are represented by flat arc trajectory and wiggle arc trajectory dots, respectively. As the target oscillates in the SI direction, the aperture center follows. Target at 10% phase and 50% phase and the corresponding BEVs are plotted. The white lines are the central lines of the beams at different gantry angles.

work, we provide a feasibility study of such an inverse planning formalism and demonstrate the potential advantage of 4D VMAT.

## **II. MATERIALS AND METHODS**

# II.A. Formulation of 4D VMAT inverse planning

The aim of 4D VMAT planning is to find a series of beam segments with optimal beam weight  $w_{\theta}$  and segment shape, defined by the coordinates of leaf ends  $\{x_{\theta,A}, x_{\theta,B}\}$  or each gantry angle  $\theta$ . A quadratic objective function is utilized to find the 4D VMAT solution<sup>19</sup>

$$S[D_{c}(n)] = \sum_{i=1}^{N_{\text{struct}}} \frac{1}{N_{i}} \left\{ \sigma_{i,1} \sum_{m=1}^{N_{i}} H[D_{i}^{\text{low}} - D_{c}(m)] + \sigma_{i,2} \sum_{m=1}^{N_{i}} H[D_{c}(m) - D_{i}^{\text{high}}] \right\} \times (D_{c}(n) - D_{i}^{p})^{2},$$
(1)

where  $D_i^p$  is the prescription dose for the *i*th structure, *n* is the voxel index,  $D_c(n)$  is the calculated dose distribution over voxel index,  $\sigma_{i,1}$  and  $\sigma_{i,2}$  are weighting factors for underdosing and overdosing of the structure *i*,  $N_i$  is the total number of voxels of the structure *i*, and H(x) is the Heaviside step function (it takes 1 for positive *x* and 0 otherwise). In this objective function, a penalty is applied to the voxels that receive doses higher than the upper-bound  $D_i^{high}$  or lower than the lower-bound  $D_i^{low}$ . For OARs, the lower-bound dose is set to zero and only overdosing of the structures is penalized.

In 4D VMAT treatment planning, the dose to a voxel is a superposition of the doses from all phases and segmented fields at different gantry angles. For a given phase, the dose distribution is computed by summing the contribution from each segment or gantry angle. When multiple phases are involved, a deformable registration model is used to track the movement of each voxel. The cumulative dose is expressed as

$$D_{c}(n) = \sum_{p} T_{p \to r} \sum_{\theta} w_{a_{\theta p}} K_{a_{\theta p}}(n), \qquad (2)$$

where  $K_a(n)$  is the dose at a voxel *n* from the segment depicted by  $a_{\theta p}$  with unit intensity and  $w_{a_{\theta p}}$  is the weight of aperture  $a_{\theta p}$ .  $T_{p \to r}$  is the matrix that links voxels of a voxel in a phase (p) to the reference phase (r) through the use of a deformable model, which transforms the dose contribution computed in the *p*th phase into the dose in the *r*th (reference) phase. In some special cases (e.g., when only the target moves back and forth in the system), however, the registration matrix takes a simple form and the 4D dose calculation is thus simplified.

For demonstration of principle, an assumption is made that the gantry rotation and patient breathing are synchronized, such that there is a functional relationship  $p = p(\theta)$ between the breathing phase p and the gantry angle  $\theta$ . For example, if the gantry rotates with constant rotational speed, the phase number depends on the gantry position in a deterministic manner, provided that the initial phase of the breathing motion is known. An example of 4D VMAT dose delivery scheme with constant gantry speed and sinusoidal breathing pattern is illustrated in Figs. 1 and 2, in which the trajectory of the source and aperture center are shown in flat arc trajectory and wiggle arc trajectory, respectively. The white (or the radial) lines are central lines of the beams at different gantry angles. As the target moves, the aperture center follows accordingly. For computational purposes, the arc in 4D VMAT planning is approximated by evenly spaced discrete source positions and the dose is a sum of contributions from all source position.



FIG. 2. Synchronization of gantry and organ motions. (a) The kinetic curves for gantry motion and patient breathing. (b) The patient CT images at 10% and 50% phases with apertures overlaid on them (upper panel) and the corresponding the schematic views (lower panel).

#### **II.B.** Optimization Algorithm

The objective function [Eq. (1)] was optimized by using simulated annealing (SA) technique.<sup>20</sup> The segment shapes were initialized to conform to the projection of the target in the beam's eye view (BEV) at the corresponding breathing phase and gantry angle. A positive weight value randomly selected was initially assigned to each segment. The shapes and weights of the segments were updated for each SA iteration, which is similar to the typical segment based optimization method.<sup>21</sup> For every variation in segment shape, the check whether the MLC constraint is violated or not is performed. The MLC constraint ensures that the leaf displacement in two source points does not exceed a maximum value determined by maximum MLC leaf travel speed  $v_l^{max}$  and gantry angular rotational speed  $\varpi_{gantry}$ 

$$d \le d_{\max} = \frac{v_l^{\max}}{\varpi_{\text{gantry}}} \Delta \theta, \tag{3}$$

where  $\Delta \theta$  is the angular separation between consecutive angles. For Varian Trilogy system, the values of  $v_l^{\text{max}}$  and

TABLE I. Summary of the lung IMRT plan statistics for the 4D and 3D planning. In this table,  $V_5$  are defined as percentage volume that receives 5 Gy or more dose. Conformity index is defined as the ratio of volume of reference isodose (95% isodose) and target volume.

Lung	4D VMAT	3D VMAT
GTV mean dose	58 Gy	58 Gy
GTV dose std	2.5 Gy	2.5 Gy
GTV D <sub>90</sub>	95.1%	95.0%
Esophagus V <sub>5</sub>	24%	40%
Heart V <sub>5</sub>	85%	95%
Conformity index	1.38	1.41

 $\varpi_{gantry}$  are 2 cm/s and 6 deg/s, respectively. If the MLC constraint test is satisfied, the change of objective function  $\Delta S$  was evaluated and the calculation continues; otherwise, a new trial was sampled. A trial was either accepted or rejected according to the conventional SA probability determined by the change of the objective function  $\Delta \varepsilon$  and system temperature T. The SA procedure is repeated until either the objective function stops decreasing or the maximum number of iterations is reached.

## II.C. Case study

Two digital phantom cases were used to demonstrate the performance of the proposed 4D VMAT planning scheme. For simplicity, a tumor motion pattern proposed by Lujan *et al.*<sup>22,23</sup> was used to model the tumor motion in the superior-inferior (SI) direction

$$z(t) = z_0 - b \cos^{2n}(\pi t / \tau - \phi),$$
(4)

where  $z_0$  is the organ position at end-expiration, *b* is the amplitude of motion,  $z_0-b$  is the organ position at end-inspiration,  $\tau$  is the period of breathing cycle,  $\phi$  is the start phase of the breathing cycle, and *n* is the parameter that describes the asymmetric feature of the model. Studies on the Lujan model observed that the intrafraction motion of liver is well correlated with the diaphragm motion.<sup>24</sup> In this work, we set  $\tau$ =4.0*s*, *n*=3, and *b*=3.0 *cm*. With the gantry rotational speed being 6 deg/s, the angular separation between consecutive control points is 2.4°. The 4D VMAT dose optimization was done using an in-house treatment planning system written with PYTHON programming language. The

TABLE II. Summary of the pancreas IMRT plan statistics for the 4D and 3D planning. In this table,  $V_{20}$  is defined as percentage volume that receives 20 Gy or more dose. Conformity index is defined as the ratio of volume of reference isodose (95% isodose) and target volume.

Pancreas	4D VMAT	3D VMAT
GTV mean dose	60 Gy	62 Gy
GTV dose std	2.9 Gy	2.9 Gy
GTV D <sub>90</sub>	98.0%	98.0%
Stomach V <sub>20</sub>	28%	31%
Duodenum V <sub>20</sub>	20%	41%
Conformity index	1.24	1.37



FIG. 3. Dose distribution for the lung case. 4D VMAT (left) versus 3D VMAT (right).

voxel-based Monte Carlo algorithm dose calculation engine<sup>25,26</sup> is used for the dose calculation. For evaluation purpose, the 3D VMAT inverse plans were also created for the two study cases. For these studies, a composite target volume (the union of target volumes of different phases) was used as the internal target volume (ITV).

# **III. RESULTS AND DISCUSSION**

The resultant dose distributions and the corresponding dose-volume histograms (DVHs) of the lung cancer case are presented in Figs. 3 and 4, respectively. In Fig. 3, the isodose lines (95%, 85%, 75%, 30%, and 10%) for the cumulative dose of the 4D VMAT plan is plotted on the left panel as compared to the 3D VMAT plan on the right panel. It is observed that in the case of 4D VMAT plan, the 95% isodose line conforms tightly around the PTV. This conformality re-



FIG. 4. DVHs for the lung case. The solid and dotted lines represent the results of 4D VMAT planning and 3D VMAT planning, respectively.

sults from the fact that the treatment beam is tracking the target's motion in the SI direction while the gantry is rotating around the patient. The dose is effectively delivered to the target while avoiding irradiation of the surrounding regions. In the case of 3D VMAT, the PTV is defined as the union of the target at all phases and thus is an elongated region in SI direction leading to isodose lines that are elongated. As a result, the OARs and other regions receive more dose than in the 4D VMAT plan. The DVHs in Fig. 4 show that although the PTV achieves similar coverage, the heart and esophagus receive a less dose by using the 4D VMAT. The percentage volumes of heart that receives 5 Gy or more  $(V_5)$  are 85% for 4D planning versus 95% for 3D planning. The V<sub>5</sub> values for esophagus are 24% for 4D planning versus 40% for 3D planning. The conformity index (CI) is 1.38 for 4D planning versus 1.41 for 3D planning (Table I). Figure 5 shows the resultant apertures for ten consecutive control points covering a full duty cycle for the 4D planning of the lung case. The first aperture represents the optimized segment shape at  $0^{\circ}$  of the gantry angle (i.e., 10% phase as shown in Fig. 5).

The resultant dose distributions and the corresponding DVHs of the pancreas cancer case are presented in Figs. 6 and 7, respectively. In Fig. 6, the isodose lines (95%, 90%, 80%, 50%, and 10%) for the accumulative dose of 4D VMAT plan is plotted on the left panel as compared to the 3D VMAT plan (right). It is observed that in the case of 4D VMAT planning the 95% isodose line conforms very well the ITV, because the treatment beam tracks the target motion while the gantry is rotating around the patient. The dose is effectively delivered to the target while avoiding the irradiating of the surrounding region. In 3D plan, the isodose lines are elongated and OARs and other regions receive more dose than that of 4D VMAT plan. The DVHs in Fig. 7 shows that although the PTV achieves similar coverage, the kidneys, liver, stomach, and duodenum receive much less dose by using the 4D VMAT. The percentage volumes of duodenum that receives 20 Gy or more  $(V_{20})$  are 20% for 4D planning



FIG. 5. Resultant apertures for ten consecutive control points for the lung case. The leaf index is indicated by the label. R19 indicates the 19th leaf on the right bank, for example.



FIG. 6. Dose distribution for the pancreas case. 4D and 3D VMAT plans are shown in the left and right panels, respectively. In these figures, isodose lines (95%, 90%, 80%, 50%, and 10%) are plotted.



FIG. 7. DVHs for the pancreas case. The solid and dotted lines represent the results of 4D VMAT planning and 3D VMAT planning, respectively.



FIG. 8. Resultant apertures for ten consecutive control points for the pancreas case. The leaf index is indicated by the label. R19 indicates the 19th leaf on the right bank, for example.

versus 41% for 3D planning. The  $V_{20}$  values for stomach are 28% for 4D planning versus 31% for 3D planning. The CI is 1.24 for 4D planning versus 1.37 for 3D planning (Table II). The resultant apertures for ten consecutive control points covering a full duty cycle is shown in Fig. 8 for the 4D planning of the pancreas case. The first aperture represents the optimized segment shape at 0° of gantry angle (i.e., 10% phase as shown in Fig. 8).

In this work, we have presented a feasibility study of 4D VMAT inverse planning and demonstrated the potential benefit of the modality. For simplicity, we have only studied the ideal situation where the breathing motion is regular. In practice, this sets the theoretical limit of the dosimetric gain against 3D VMAT. Real-time monitoring of tumor motion and effective feedback of the tumor motion information plays an important role in dealing with realistic clinical situation where breathing irregularities may occur. This and issues related to the practical delivery of 4D VMAT will be a logical subject of future studies.

## **IV. CONCLUSION**

An inverse planning framework for 4D VMAT has been proposed to provide tempospatially optimized arc therapy plans. A significant dosimetric benefit of the 4D VMAT has been observed as compared to its 3D counterpart. 4D VMAT has the potential of reducing treatment time and producing highly conformal dose distribution.

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