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Development of a multi-parametric model predictive control algorithm for insulin delivery in type 1 diabetes mellitus using clinical parameters

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Abstract

A multi-parametric model predictive control (mpMPC) algorithm for subcutaneous insulin delivery for individuals with type 1 diabetes mellitus (T1DM) that is computationally efficient, robust to variations in insulin sensitivity, and involves minimal burden for the user is proposed. System identification was achieved through impulse response tests feasible for ambulatory conditions on the UVa/Padova simulator adult subjects with T1DM. An alternative means of system identification using readily available clinical parameters was also investigated. A safety constraint was included explicitly in the algorithm formulation using clinical parameters typical of those available to an attending physician. Closed-loop simulations were carried out with daily consumption of 200 g carbohydrate. Controller robustness was assessed by subject/model mismatch scenarios addressing daily, simultaneous variation in insulin sensitivity and meal size with the addition of Gaussian white noise with a standard deviation of 10%. A second-order-plus-time-delay transfer function model fit the validation data with a mean (coefficient of variation) root-mean-square-error (RMSE) of 26 mg/dL (19%) for a 3 h prediction horizon. The resulting control law maintained a low risk Low Blood Glucose Index without any information about carbohydrate consumption for 90% of the subjects. Low-order linear models with clinically meaningful parameters thus provided sufficient information for a model predictive control algorithm to control glycemia. The use of clinical knowledge as a safety constraint can reduce hypoglycemic events, and this same knowledge can further improve glycemic control when used explicitly as the controller model. The resulting mpMPC algorithm was sufficiently compact to be implemented on a simple electronic device.

Keywords

Biomedical control; Insulin delivery; Multi-parametric model predictive control; Type 1 diabetes mellitus

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1. Introduction

People with type 1 diabetes mellitus (T1DM) may have a life expectancy ten years less than their normal glucose tolerant counterparts due to complications resulting from chronic hyperglycemia, such as cardiovascular disease and strokes [1]. Hyperglycemia is an elevated blood glucose (BG) concentration, with a threshold defined as BG greater than 180 mg/dL [2]. Aggressive treatment with intensive insulin therapy (IIT), involving up to a total of 12 manual capillary glucose measurements and insulin injections per day, reduces hyperglycemia and can lead to a reduction in the prevalence of these complications [2]. IIT also increases the risk of hypoglycemic events and increases the burden on the caregiver and/or patient administering the therapy [3]. Hypoglycemia is any lower than normal BG; symptoms of hypoglycemia, such as tachycardia and nausea, occur at around 50–70 mg/dL [4,5].

The attraction of an efficient closed-loop device is thus threefold: increased life expectancy, decreased hypoglycemia, and reduction in the burden of administering effective therapy. Innovations in real-time continuous glucose monitoring (CGM) sensors and continuous subcutaneous insulin infusion (CSII) pumps mean that the components necessary for a closed-loop device suitable for use in ambulatory conditions are maturing [6], leaving the control algorithm as the limiting factor in development.

CGM sensors and CSII pumps use the subcutaneous (SC) route for glucose measurement and insulin delivery, respectively. Other routes, such as intravenous and intraperitoneal [7,8], offer reductions in lag time [9], but are associated with an increase in the risk of infection at the site of insertion [10,7]. The lag time associated with SC insulin infusion is an obstacle for a control algorithm: absorption of glucose into the blood from carbohydrate (CHO) raises BG faster than simultaneously injected SC insulin can lower it. Insulin delivery rates may also be limited by the physical limitations of the CSII pump and safety constraints driven by clinical parameters [11]. A controller framework known to be suitable for systems with large lag times and constraints is model predictive control (MPC); this control algorithm has been proposed as a candidate controller architecture for insulin delivery [12–14] and has been implemented in manual closed-loop trials overnight [15]. Central to each of these MPC implementations has been a dynamic model of the effects of subcutaneous insulin on glycemia.

The metabolic processes underlying insulin action involve complex interactions of hormones [16], which lead to significant variation in insulin sensitivity [17–20]. Insulin absorption variability is less than insulin action variability [21], but can be affected by biofilms and inflammation. Gut glucose absorption is highly dependent upon the composition of a meal [22]. Tracer studies involving radioactive isotopes have been reported in order to characterize subcutaneous insulin and gut glucose absorption [22–24]; such models may be representative of the variation inherent in a population, but are not practical for use in an MPC algorithm because adapting these models to an individual subject would require the repetition of an expensive experiment. The use of data driven, empirical models based only on data collected from ambulatory subjects is a more practical method for development of a personalized model; auto-regressive exogenous input models have been presented in literature [25,26]. The main caveat of developing models from data obtained from ambulatory subjects is that typically both model inputs—SC insulin and oral CHO—occur simultaneously, which gives an identifiability problem; the “best” empirical models can therefore have physically counterintuitive characteristics, such as an incorrect sign for a process gain [27]. Classic process control techniques, such as impulse response tests, have been executed in clinical trials in which insulin boluses and meals were separated by 3 h,

and support the notion that a simple model—with a gain, a time constant, and a time delay—can capture the critical bandwidth behavior of glucose–insulin interactions [28].

Physicians are calculating “gains” through interactions with their patients with T1DM, and these clinical parameters are the standard of care in endocrinology practices. The “correction factor” (CF) is the lowering effect of BG from administering one unit of rapid-acting insulin; the “insulin-to-carbohydrate ratio” (ICR) is the amount of carbohydrate offset by one unit of rapid-acting insulin. These parameters are used to guide insulin dosing decisions and are often refined throughout the life of the person with T1DM [29]. Due to this refinement process, the parameters obtained are considered reliable and should be included as a safety constraint in a closed-loop control algorithm [11].

Constrained MPC can necessitate the on-line solution of a quadratic program. This on-line optimization can be replaced with a single set of *a priori* optimizations via multi-parametric programming; the on-line problem is reduced to the evaluation of an affine function obtained from a lookup table [30]. This reformulation is valuable in any application where on-line computation should be minimized, due to low computational power, or in order to extend battery life by minimizing computation, or to minimize the foot-print on a chip. Multi-parametric MPC (mpMPC) has been evaluated in several biomedical applications [31], and has been investigated for use with intravenous insulin delivery in an intensive care unit *in silico* [32].

This study was designed to show the feasibility of using simple models, clinical parameters, and mpMPC for control of glycemia via the SC route. Elements of modeling *for* control were, for the first time, unified with clinical parameters derived by physicians. The resulting models and safety constraints were used to develop a novel mpMPC control algorithm for glucose control via subcutaneous insulin delivery. Closed-loop simulations were performed on two clinically verified virtual subject cohorts.

2. Methods

2.1. Virtual subject cohorts

Two clinically validated simulation models were used to represent a virtual subject with T1DM. Both models are semi-physiological, semi-empirical, and represent the effects of SC insulin and oral CHO on BG. The models are divided into three compartments as shown in Fig. 1: gut absorption of glucose from oral CHO, absorption of SC insulin into the plasma, and their effects via a glucose-insulin kinetic model on BG.

The first cohort of virtual subjects was based on the model of Hovorka et al. [23], with modifications to the insulin absorption model by Wilinska et al. [24]; four subjects were derived by using a multiplier κ_j on the plasma insulin concentration $I(t)$ in the insulin sensitivity state equations of the model [23]:

$$\dot{x}_{i,j} = -k_{ai}x_{i,j}(t) + k_{bi}\kappa_j I(t). \quad (1)$$

where subscripts i and j represent state i and subject j , respectively, x is the insulin sensitivity state, k_a and k_b are rate constants, and κ_j takes values of 0.5, 0.75, 0.25, and 1. This cohort will be referred to as the Hovorka cohort.

The second cohort of virtual subjects was based on the cumulative work of scholars at the Universities of Virginia and Padova [34–36], which has been accepted by the Food and Drug Administration (FDA) as a substitute for animal trials [33]. Ten virtual subjects

representative of the variation found in an adult population with T1DM were available. This cohort will be referred to as the UVa/Padova cohort.

2.2. Model development

Identification of parameters for first-order-plus-time-delay-with-integrator transfer function models for describing the effects of SC insulin and oral CHO on BG from impulse response tests has been proposed [28,37]. Impulse response data for 1, 2, 5, and 10 U insulin boluses and 25, 50, 75, and 100 g CHO meals were obtained from each virtual subject; the data used for parameter estimation spanned 6 h for the bolus insulin model and 3 h for the meal model. Six models were developed. The general form of models A–C was

$$Y(s) = \frac{K_B e^{-\theta_B s}}{s(\tau_B s + 1)} U(s) + \frac{K_M e^{-\theta_M s}}{s(\tau_M s + 1)} D(s), \quad (2)$$

where s is the Laplace variable, Y the deviation BG, U the deviation insulin input amount, D the CHO input amount, K , τ , and θ are the model gain, time constant, and time delay, respectively. Subscripts B and M represent the bolus insulin component of the model (bolus model) and meal CHO component of the model (meal model), respectively. The integrator element is included because over the timeframe of interest, the simulated subject has integrating characteristics; *in vivo*, integrator characteristics are more prominent in the impulse response [38]. Deviation variables are taken about nominal steady-state conditions corresponding to the lowest risk [39]; the nominal BG was 110 mg/dL, the nominal insulin delivery rate was that required to maintain the nominal BG, the nominal disturbance value was zero. For model A, the heuristics used to estimate each parameter were as follows:

1. K was the ratio of greatest deviation from nominal of Y to the input size U ;
2. θ was defined as $y(t = \theta) = 0.03Ku$, where u is the units of insulin input for the bolus insulin model, or the g CHO for the meal CHO model, and y is the glucose deviation from nominal in mg/dL. The threshold of 3% of final response for θ was chosen as it is just beyond the noise level in CGMs [40];
3. τ was defined as $y(t = \tau + \theta) = 0.632Ku$ [41].

For model B, mean values were taken for τ and θ across all subjects in that particular cohort. Recognizing the units of K_B as mg/dL per U, K_M as mg/dL per g CHO, CF as mg/dL per U, and ICR as g CHO per U, the following relationships between clinical parameters and model gains were defined:

$$K_B = -CF \quad (3)$$

$$K_M = \frac{CF}{ICR}. \quad (4)$$

For model C, the gains were thus determined from the clinical parameters, CF and ICR, that are available with each virtual subject.

Due to the integrating element, models A–C have a pole at zero, yielding an unstable model. For stability, a set of second-order models that approximate the critical bandwidth behavior of models A–C were derived; the criteria for the second-order models were defined as

$$y(t=t^\dagger)=0.9Ku \quad (5)$$

$$y^\dagger(t=t^\dagger)=y_{\max}^\dagger, \quad (6)$$

where y^\dagger is the second-order model output, t^\dagger is the time at which the output of each of the first-order integrating models A–C would be equal to its proposed second-order partner (models D–F). The threshold of 90% of final output was chosen so that the bulk of the steady-state response was duplicated within the timescale of interest; other thresholds could be chosen but were not investigated in this proof-of-concept study. To meet the criteria defined in Eqs. (5) and (6), a nonlinear optimization was performed to obtain a transformed model gain and an additional time constant, denoted with subscript t in the following equations:

$$Y(s)=\frac{K_B e^{-\theta_B s}}{(\tau_{Bt} s+1)(\tau_B s+1)}U(s)+\frac{K_M e^{-\theta_M s}}{(\tau_{Mt} s+1)(\tau_M s+1)}D(s) \quad (7)$$

Models A–F are compared in Table 1.

The models were then discretized and converted into the state space:

$$x_{k+1}=Ax_k+Bu_{k-\theta_u}+B_d d_{k-\theta_d} \quad (8)$$

$$y_k=Cx_k, \quad (9)$$

where k is the sample index, calculated from $t = k\Delta t$ where Δt is the sampling period, and θ_u and θ_d correspond to θ_B and θ_M , respectively, after rounding to the nearest sample index. x is the state vector of dimension n -by-1, y the measurement scalar, u the manipulated variable, insulin, and d the disturbance variable, CHO.

2.3. Controller formulation

The optimization objective was to minimize tracking error Y over prediction horizon N_P , spanning 6 h and minimize control moves ΔU over control horizon N_M , spanning 30 min. The cost function for this purpose was

$$\min_{\Delta U} J=Y^T Q_y Y+\Delta U^T R \Delta U, \quad (10)$$

where ΔU is an N_M -by-1 vector of decision variables Δu_j , Y is a N_P -by-1 vector of predicted tracking error, and Q_y and R and matrices denoting penalties on tracking error and control moves, respectively. Assuming a set-point of 110 mg/dL, which corresponds to the nominal BG, the tracking error, Y , is given by

$$Y=T x_k+S_U U+S_D D+S_E e_k, \quad (11)$$

where matrices T , S_U , and S_D are calculated from matrices A , B , and B_d . S_E is a N_P -by-1 unit vector. U is of dimension N_P , and is the absolute value of the control variable in the future:

$$U_{k+i} = u_k + \sum_{j=0}^i \Delta u_j. \quad (12)$$

D is an (N_A+1) -by-1 vector of disturbances from the present up to N_A steps in the future, where N_A is the announcement horizon. Three disturbance modeling scenarios were considered.

1. Unannounced meal. No estimation of the meal size was made. The disturbance model was not used. This is pure feedback (FB) control.
2. Measured meal. The meal CHO content was measured at the time of ingestion. In this case, $N_A = 0$. This is feedback/feedforward (FF/FB) control.
3. Announced meal. The meal CHO content was measured 30 min before ingestion. In this case, $N_A = 6$ with a five minute sample time. This is also FB/FF control, with an augmentation of the FF component to look further into the future.

As can be seen from the definition of D , “measured” and “announced” meals are fundamentally the same, with “measured” meals being an “announced” meal with zero lead time.

The error model was an output additive disturbance, defined as

$$e_k = y_{m,k} - y_k, \quad (13)$$

where $y_{m,k}$ is the measurement at the current sample k , and y_k is the uncorrected, infinite step ahead model prediction.

Two constraint cases were considered.

1. Physical constraints only.
2. Physical constraints and insulin-on-board (IOB) safety constraints [11].

2.3.1. Physical constraints—Basic physical constraints were based determined from bounds on insulin delivery rates

$$-I_{D,basal} \leq U \leq I_{D,max} - I_{D,basal}, \quad (14)$$

where I_D is the absolute insulin delivery rate, subscript basal is the nominal value, and subscript max is the maximum insulin flow rate possible.

2.3.2. IOB constraints—Calculation of the IOB constraint [11] begins by considering the history of delivered insulin and calculating the remaining active insulin

$$IOB_k = \sum_{h=1}^{N_H} (u_{k-h} \cdot f_h), \quad (15)$$

where IOB_k is the active insulin at sample k , N_H is the oldest delivery of insulin considered, and vector f_h is the fraction of insulin remaining active after h samples [42]. The IOB rate constraint was calculated using an allowance for clinical parameters, less the active IOB, given by

$$U_{IOB,k} = \left(\frac{I_{CF,k} + I_{ICR,k} - IOB_k}{\Delta t} \right), \quad (16)$$

where $U_{IOB,k}$ is the maximum insulin delivery rate at sample k , $I_{CF,k}$ is the insulin allowed based on CF, and $I_{ICR,k}$ is the insulin allowed based on ICR. An allowance for insulin based on ICR was not given if the meal was unannounced.

Additionally, the nominal insulin infusion rate was always allowed:

$$U_{IOB,max,k} = \max(0, U_{IOB}). \quad (17)$$

The final IOB rate constraint was therefore

$$U \leq U_{IOB,max,k}. \quad (18)$$

2.4. Formulation of the multi-parametric program

The cost function in Eq. (10) can be reformulated by completing the square [30,43] into a more compact form suitable for solution as a multi-parametric program giving

$$\min_z J_{p_k}^* = \frac{1}{2} p_k^T H p_k \quad (19)$$

$$G z_k \leq W + S p_k \quad (20)$$

where the vector of optimization variables, z_k , is a function of the parameter vector, p_k , and the manipulated variable vector ΔU_k , defined as

$$z_k = \Delta U_k + H^{-1} F^T p_k \quad (21)$$

and S is obtained from

$$S = E + G H^{-1} F^T \quad (22)$$

The vector p_k is called the parameter vector because in the context of parametric programming, this is traditionally the name given to the set of variables (or parameters) over whose range optimal solutions are sought.

The multi-parametric programming problem as defined by Eqs. (19) and (20) was solved using the Multi-Parametric Toolbox [44] and YALMIP [45]. The parameter vector, p_k included the state vector, x_k , the last control move, u_k , the current error, e_k , the meal

measurement and announcement vector, d_k , and the IOB constraint, $u_{IOB,k}$. The maxima and minima of each component of interest in p_k were:

$$[-100 \ -100 \ -100 \ -100]^T \leq x_k \leq [1000 \ 20,000 \ 1000 \ 20,000]^T \quad (23)$$

$$-I_{d,basal} \leq u_k \leq 36 - I_{d,basal} \quad (24)$$

$$-2000 \leq e_k \leq 2000 \quad (25)$$

$$\mathbf{0}_{N_A+1 \times 1} \leq d_k \leq 100 \cdot \mathbf{1}_{N_A+1 \times 1} \quad (26)$$

$$0 \leq u_{IOB,k} \leq 36 - I_{d,basal} \quad (27)$$

The solution is the form of lookup table defined in the state space; the optimal control law was determined by searching the lookup table for the entry j satisfying the associated vector of inequalities

$$H_j p_k \leq K_j, \quad (28)$$

where H_j and K_j define the limits of the validity of optimality of entry j . The associated affine function is evaluated using

$$\Delta U = F_j p_k + G_j, \quad (29)$$

where F_j and G_j correspond to entry j in the lookup table for optimal control given parameter vector p_k .

3. Results and discussion

3.1. Model development

Comparison of each of the models A–F with the subject data was performed. For the Hovorka cohort, the critical bandwidth frequencies were captured in each of the personalized models, i.e., models A, B, D, and E. The calibration data from the Hovorka cohort and each model's response to a 1 U insulin bolus is shown in Fig. 2; models C and F, which have gains based upon clinical parameters, do not capture the asymptotic behavior as well as models A, B, D, and E. The model response to a meal is similar for all Hovorka subjects, as shown in Fig. 3.

The calibration data from UVa/Padova cohort and each model's response to a 1 U bolus is shown in Fig. 4; from an asymptotic perspective over the window of interest, models C and F do not capture the hypothesized gains. The data and model fits from a 25 g CHO meal for the UVa/Padova cohort are shown in Fig. 5. The lag time for each model is similar to the lag time of the data in all cases.

The model parameters identified for model 1 are summarized in Table 2 for the Hovorka cohort and Table 3 for the UVa/Padova cohort. Comparison of the bolus model gains, K_B across cohorts shows that the Hovorka cohort are much more sensitive to insulin than the UVa/Padova cohort. There is an order of magnitude difference in the CF of UVa/Padova adult subjects 3 and 4 indicating a wide range of insulin sensitivity in the cohort; this difference is maintained in the corresponding gain, K_B , of these subjects. The variation of τ and θ is significantly less than the variation of K , indicating that the gains, K , are the most important parameter in accounting for inter-subject variation.

A quantitative analysis of the model calibration is given in Figs. 6 and 7 using the FIT metric, defined as

$$FIT = 100 \left(1 - \frac{\sum_{i=1}^N |g_i - \hat{g}_i|}{\sum_{i=1}^N |g_i - \bar{g}|} \right), \quad (30)$$

where g is the measurement value, \hat{g} the uncorrected model estimate, and \bar{g} the mean measurement value. A score of 100 implies perfect fit, a score of zero implies predicting the mean measurement value would have equivalent performance. The models with gains based on clinical parameters perform poorly compared with models using gains obtained from impulse response tests.

The model gains and clinical parameters are compared in Fig. 8 for the UVa/Padova cohort. An increase in the size of the input excitation decreases the value of the model gain obtained, indicating nonlinearities. The trend is that the model gains have the strongest correlation with the clinical parameters when the input excitation is small. The implication is that the size of the impulse used in identification should be of a similar magnitude to those impulses, i.e., meals, expected in daily life. The clinical parameters assigned to an individual with T1DM are a reflection of this.

3.2. Controller performance

The control law was formulated using a prediction horizon of 6 h because this length of time was used to model insulin. The sample time was chosen as 5min, which is a common measurement frequency among CGM sensors in use. The control horizon was 30 min. Integrating states can be problematic for mpMPC, unless a larger search region is specified, which increases the size of the lookup table and thus may defeat the goal of minimizing the footprint on a chip. Thus, SOPTD models were preferable to FOPTDI models for control and the FOPTDI models were not used any further. This was reasonable from a modeling perspective because there was not significant loss of model performance when applying the empirical transformation. Additionally, the FOPTDI remain the best starting point because the parameters have clinical/physical meaning. Because the performances of models D and E were clinically similar, results from models D and F are shown in the following results. Extensive simulations showed that $Q_y/R = 0.1$ was a reasonable trade-off between robustness to uncertainty and avoiding a sluggish response. Closed-loop simulations were performed assuming a daily meal plan of 200 g CHO, divided into three meals of 50, 85, 65 g CHO ingested at 7 a.m., noon, and 7p.m.

Fig. 9 shows the closed-loop responses for the Hovorka cohort with a controller based on Model D. Performance characteristics associated with the three methods of controlling for disturbances are similar across all subjects. Unannounced meals of this size lead to

unacceptable low postprandial BG. The use of a disturbance model reduces the peak BG levels after CHO ingestion, while also generally increasing the BG minima. Meal announcement further reduces the peak BG levels, but at the cost of further decreasing the postprandial BG. The control algorithm delivers some insulin upon announcement of the meal. This delivery of insulin over several steps is a shift from the basal-bolus paradigm, and thus cannot be considered as a pre-meal bolus; indeed, the control algorithm makes no distinction between the two. The model and controller performance on the Hovorka subjects indicates that the system has only mild nonlinearities; as implemented, the variation in BG could be reduced with a modest reduction in daily CHO consumption, and the low postprandial BG could be avoided at the cost of higher peak BG by increasing the set-point. Indeed, dietary restriction and consistency are considered key to control of diabetes mellitus [46]. Meal announcement was not investigated any further due to decrease in BG minima associated with this controller performance and the practical implications of knowing meal CHO before meal time.

Fig. 10 shows the closed-loop responses for the UVa/Padova cohort with a controller based on Model D. Both unknown meals and measured meals were considered, along with the inclusion of the IOB constraint based on clinical parameters. The performance of an unconstrained controller with unknown meals is satisfactory for subjects 2, 7, and 9. Subjects 1, 3, and 10 require meal measurement to avoid hypoglycemia subjects 4, 5, and 8 require an IOB safety constraint to avoid hypoglycemia. The failure of the safety constraint for subject 6 indicates that the clinical parameters are not appropriately prescribed. This highlights the importance of hypoglycemia alarming and fault detection, which is in itself an active area of research for insulin delivery systems [47–49]. For subject 6, the associated clinical parameters were doubled to improve insulin dosing decisions in the following simulations. In this study, we have not investigated adaptive control; excellent strategies have been developed and could be applied to this control schema. For determining if a model is still valid, fault detection methods could be applied [50] to recommend obtaining a new model. Run-to-run methods [51] could be used to reset the nominal conditions used should insulin requirements change significantly. Iterative learning control [52] and run-to-run control [53] could also be used to determine a dynamic set-point, based on prior performance.

Fig. 11 shows the closed-loop responses for the UVa/Padova cohort with a controller based on Model F. Subjects 4 and 8 need the safety constraint to avoid hypoglycemia. For subjects 1, 3, 5, 7, 9, and 10, glycemic control is clinically identical with or without the safety constraint; the convergence of controller performance in this manner indicates that the model contains the same information used in the safety constraint in an optimal manner. The glucose trajectories for subject 6 show improved performance with modified clinical parameters; hypoglycemia is avoided with the IOB constraint. Although model D provided a better prediction of open-loop data than model F, the controller based upon model F performs better in a closed-loop scenario. This is because performance for open-loop prediction was measured in a least-squares sense, whereas performance for closed-loop control is measured in terms of safety. By considering the safety margins implicitly in the model, rather than explicitly in the constraint, improved performance without the IOB constraint occurs.

Fig. 12 shows the value of the upper limit on the rate constraint for the UVa/Padova cohort. The rate constraint increases with deviation from nominal and when meals are announced; the rate constraint also increases when insulin delivery is less than basal as active insulin decays. The insulin delivery rate from the controller without the IOB constraint frequently exceeds that of the controller with the IOB constraint.

The critical challenge for a control algorithm is robustness under uncertainty. Uncertainty in meal CHO content and subject insulin sensitivity were addressed. Each subject was simulated for 30 days; daily variation of insulin sensitivity was considered by parameter variation drawn from a normal distribution with standard deviation of 10%, and CHO content of each meal was assumed to vary following a normal distribution with standard deviation of 10%; these distributions were chosen to capture the expected variation in insulin sensitivity [54] and meal size estimates [55] observed in the literature. The low blood glucose index (LBGI) and high blood glucose index (HBGI) were calculated to summarize glycemic control for each day [39,56]. Calculation of LBGI and HBGI involves normalization of BG into risk space, to account for the asymmetry of the hazard associated with deviations from nominal. Threshold levels distinguishing low, medium, and high risk of hyperglycemic and hypoglycemic events have been associated with HBGI and LBGI, respectively; these thresholds relate to the risk of deleterious consequences associated with BG that is not at euglycemic levels.

A summary analysis of all BG data for the 30 days of simulations is shown in Fig. 13. In all instances, controller performance avoids a high risk of hypoglycemia; with the IOB constraint formulation, the risk of hypoglycemia was classified as “low” [39].

Due to the inevitable hyperglycemia that occurs postprandially with unrestricted CHO consumption, glycemic control was assessed by relaxing requirements on a 3 h postprandial period, which has precedent in the literature [57]. The LBGI and HBGI analysis was repeated for the closed-loop glucose trajectories, excluding the postprandial period, as shown in Fig. 14. There was a significant reduction in HBGI, with most data points falling below the “low” risk threshold, and those points above the “high” risk threshold were significantly reduced.

The threshold levels for interpreting LBGI and HBGI were developed before CGM sensors became available; the paucity of data available meant that a measurement showing hyperglycemia could reasonably be interpreted as a sustained hyperglycemic event. The glucose trajectories shown in Fig. 11 indicate that the hyperglycemia caused by daily CHO consumption of 200 g CHO is not sustained indefinitely; euglycemia is always restored overnight. Therefore, to interpret the HBGI results as meaning high risk may be overstating the problem.

3.3. Controller implementation

In order to retain the practical benefits of solving a multi-parametric program offline, the lookup table should be of a size that lends itself to portability on simple devices. Fig. 15 shows the size of the controllers for each subject that were implemented in the robustness simulations. All the controllers were of a reasonable size given modern portable computational devices. The size of the lookup table depends upon the complexity of the model, the cost function, and the constraint formulation. The increase in complexity from additional parameters in the program from measured meals leads to a modest increase in size; the increase in complexity due to the IOB constraint is more significant, but does not make the lookup table size a computational burden or memory issue.

4. Conclusions

Low order transfer function models can have physically meaningful parameters and the necessary degrees of freedom to characterize the principle characteristics of clinically validated models of SC insulin effects on BG. The identification procedure for parameters for such models used only ambulatory data and would be relatively inexpensive to implement. Clinical parameters served a similar function in characterizing the most

important information and could be used as the basis of models useful for control derived from a minimum amount of data.

MPC provided an intuitive framework for a complex optimization problem, whereby tuning handles do not become too complicated for a non-specialist to understand. The robustness of the proposed control algorithm was demonstrated through physiologically significant changes in insulin sensitivity and mismatches between subject estimated and ingested CHO. The safety constraints implemented improved performance by reducing the occurrence of hypoglycemia. Using simple models and only the most important constraints led to a sufficiently compactly posed multi-parametric programming problem that was suitable for implementation on a simple computational device—"MPC-on-a-chip".

Abbreviations

BG	blood glucose
CGM	continuous glucose monitoring
CF	correction factor
CHO	carbohydrate
CSII	continuous subcutaneous insulin infusion
FDA	Food and Drug Administration
ICR	insulin-to-carbohydrate ratio
IIT	intensive insulin therapy
IV	intravenous
SC	subcutaneous
T1DM	type 1 diabetes mellitus

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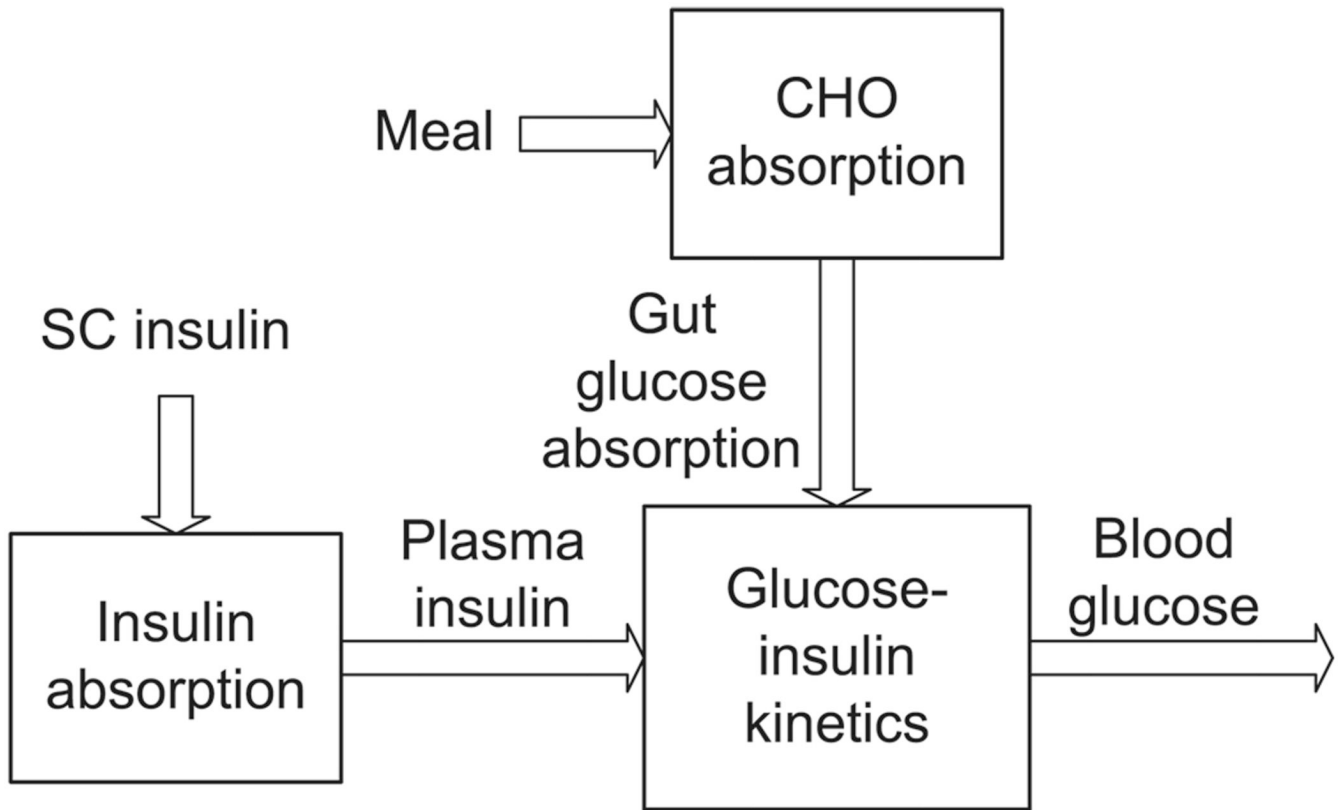


Fig. 1. General compartmental division of virtual subject models used by Hovorka and coworkers [23] and the UVA/Padova simulator [33].

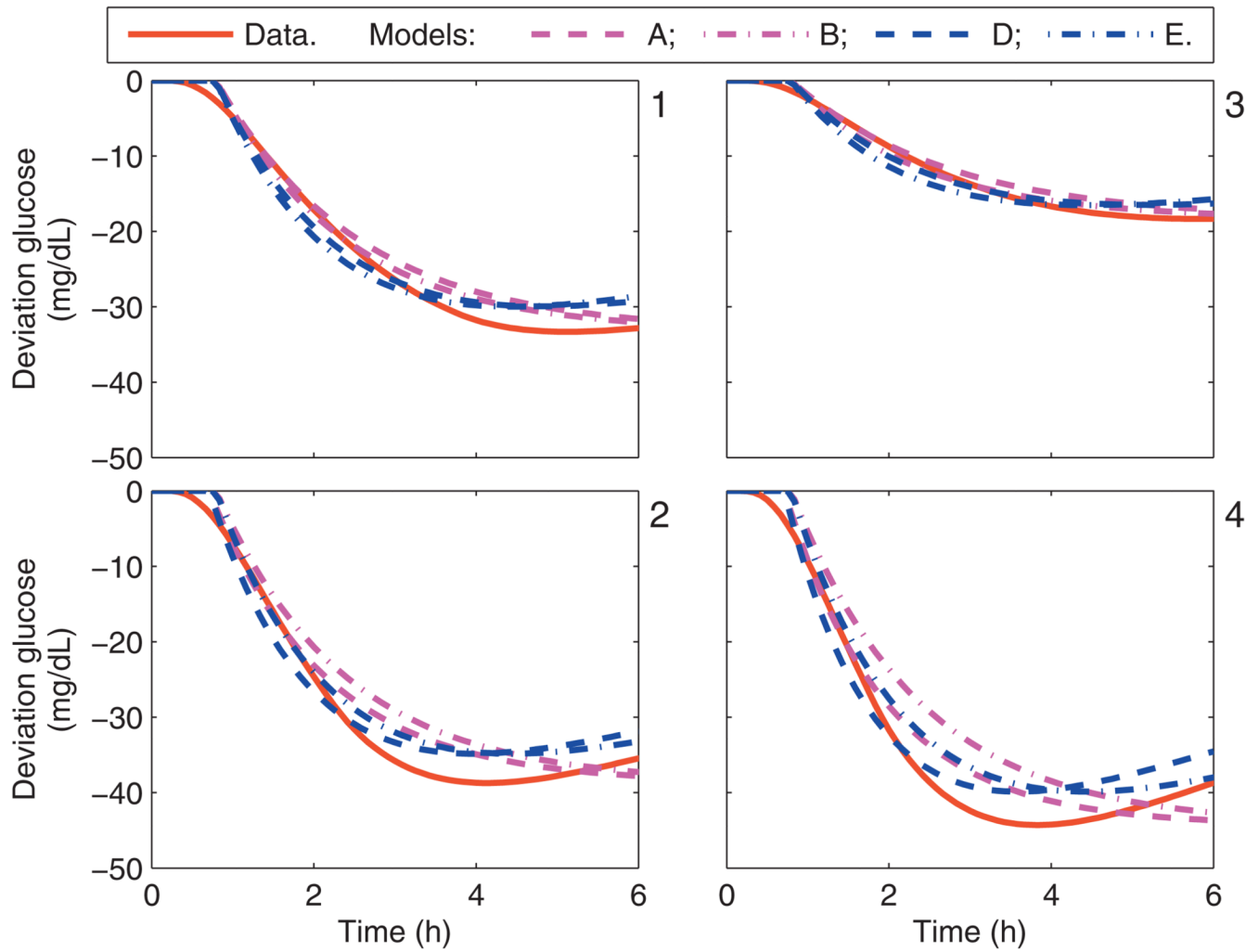


Fig. 2. Calibration data and the uncorrected model response from models A, B, D, and E, due to a 1 U bolus. Panels 1–4 correspond to the Hovorka subjects 1–4.

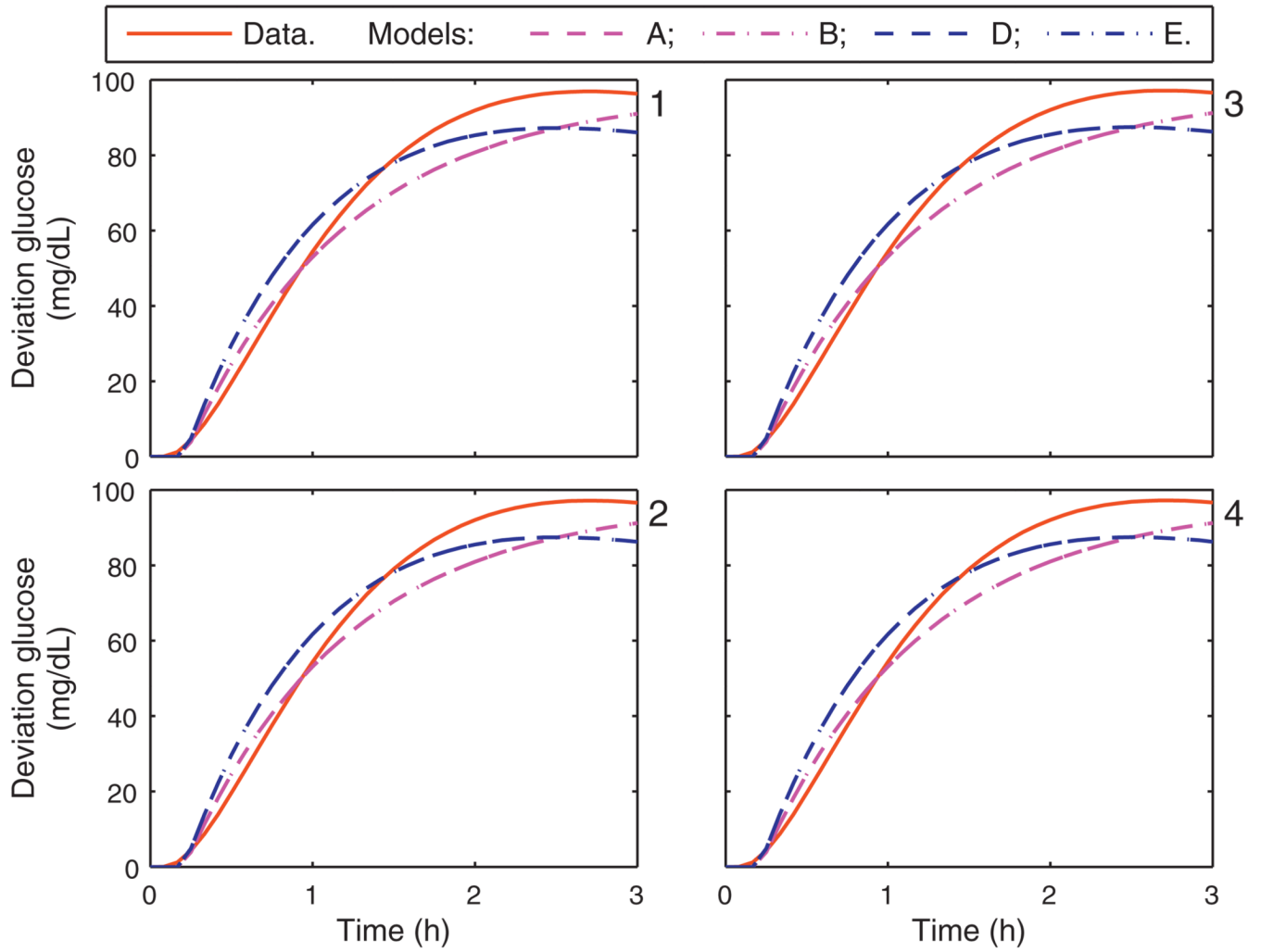


Fig. 3. Calibration data and the uncorrected model response from models A, B, D, and E, due to a 25 g CHO meal. Panels 1–4 correspond to the Hovorka subjects 1–4.

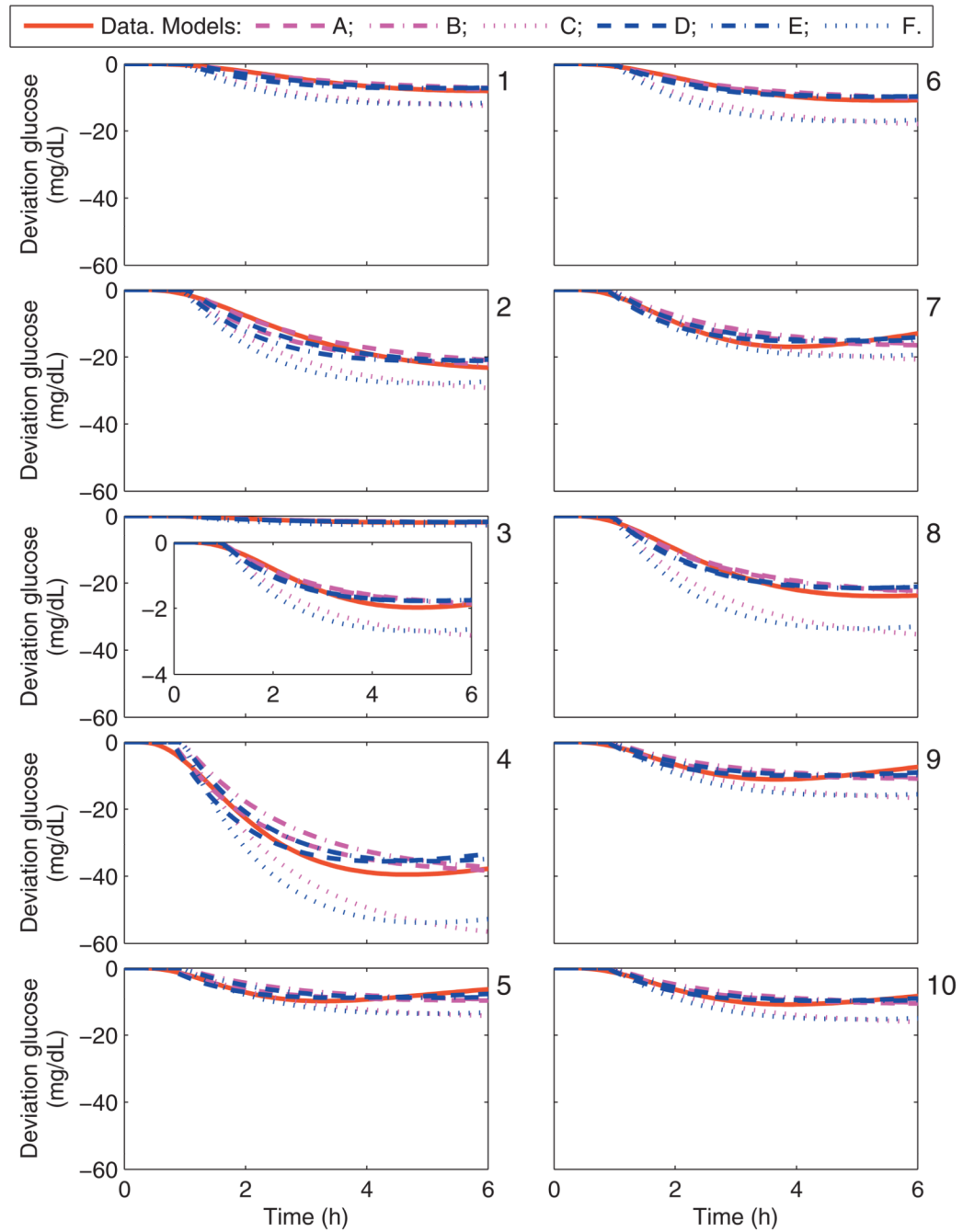


Fig. 4. Calibration data and the uncorrected model response from models A–F due to a 1 U bolus. Panels 1–10 correspond to the UVa/Padova adult subjects 1–10.

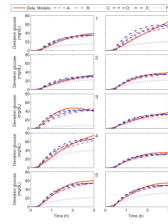


Fig. 5. Calibration data and the uncorrected model response from models A–F due to a 25 g CHO meal. Panels 1–10 correspond to the UVa/Padova adult subjects 1–10.

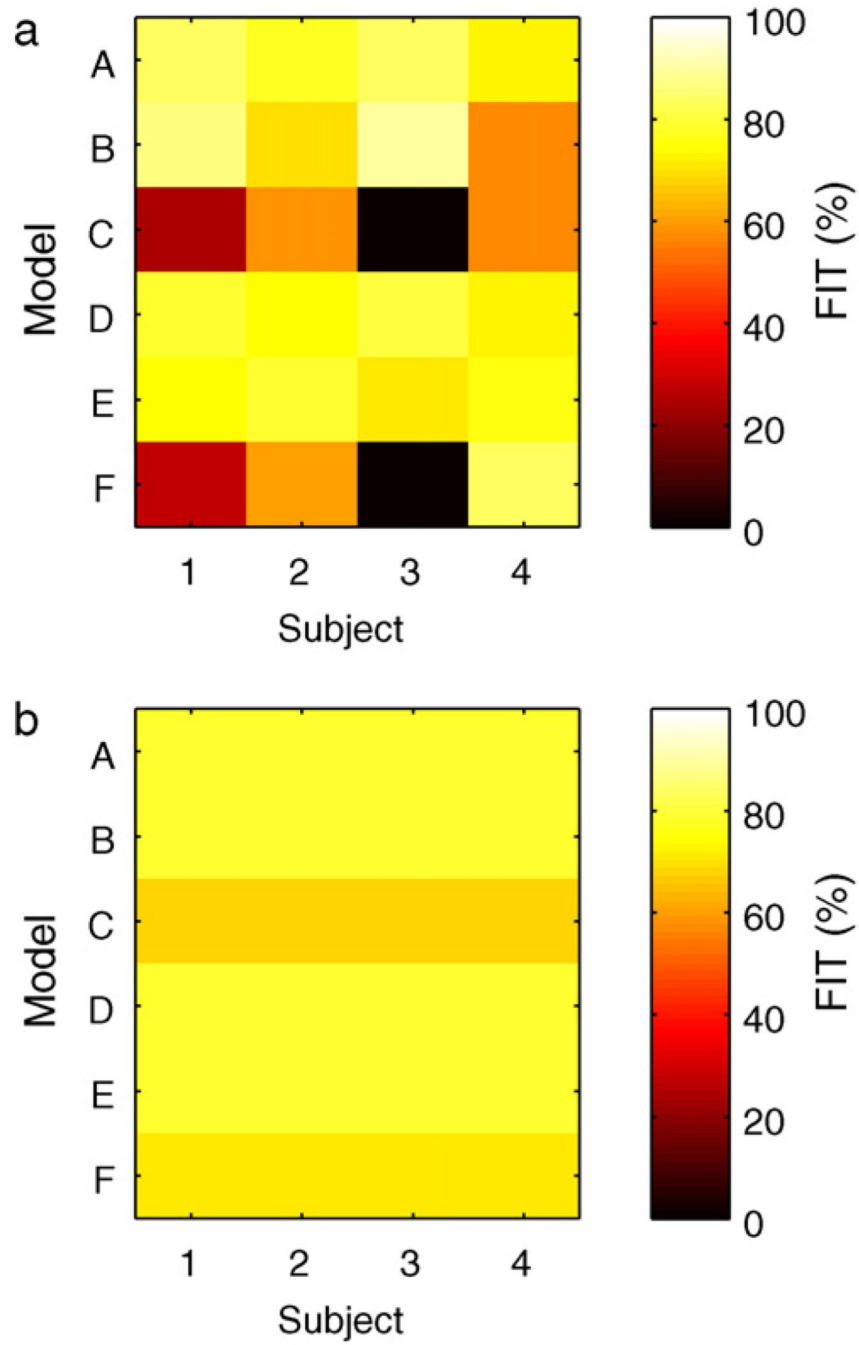


Fig. 6. The FIT metric for Hovorka subjects 1–4 for each model identified from the impulse response data. Left: bolus response. Right: meal response.

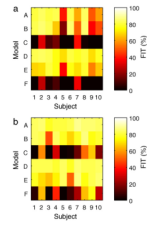


Fig. 7.
The FIT metric for UVa/Padova adult subjects 1–10 for each model identified from the impulse response data. Left: bolus response. Right: meal response.

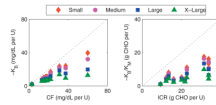


Fig. 8. Clinical parameters from UVa/Padova cohort compared with identified model gains. Series descriptors denote excitation size; small: 1 U, 25 g CHO; medium: 2 U, 50 g CHO; large: 5 U, 75 g CHO; x-large: 10 U, 100 g CHO. Left: correction factor. Right: insulin-to-carbohydrate ratio.

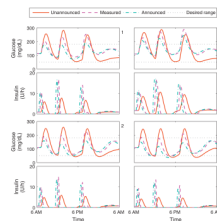


Fig. 9. Closed-loop results for the Hovorka cohort. Meal plan is 50, 85, and 65 g CHO at 7 a.m., noon, and 7 p.m. Control algorithms compared are the unannounced, measured, and announced meal scenarios, using model D. Panels 1–4 correspond to the Hovorka subjects 1–4.

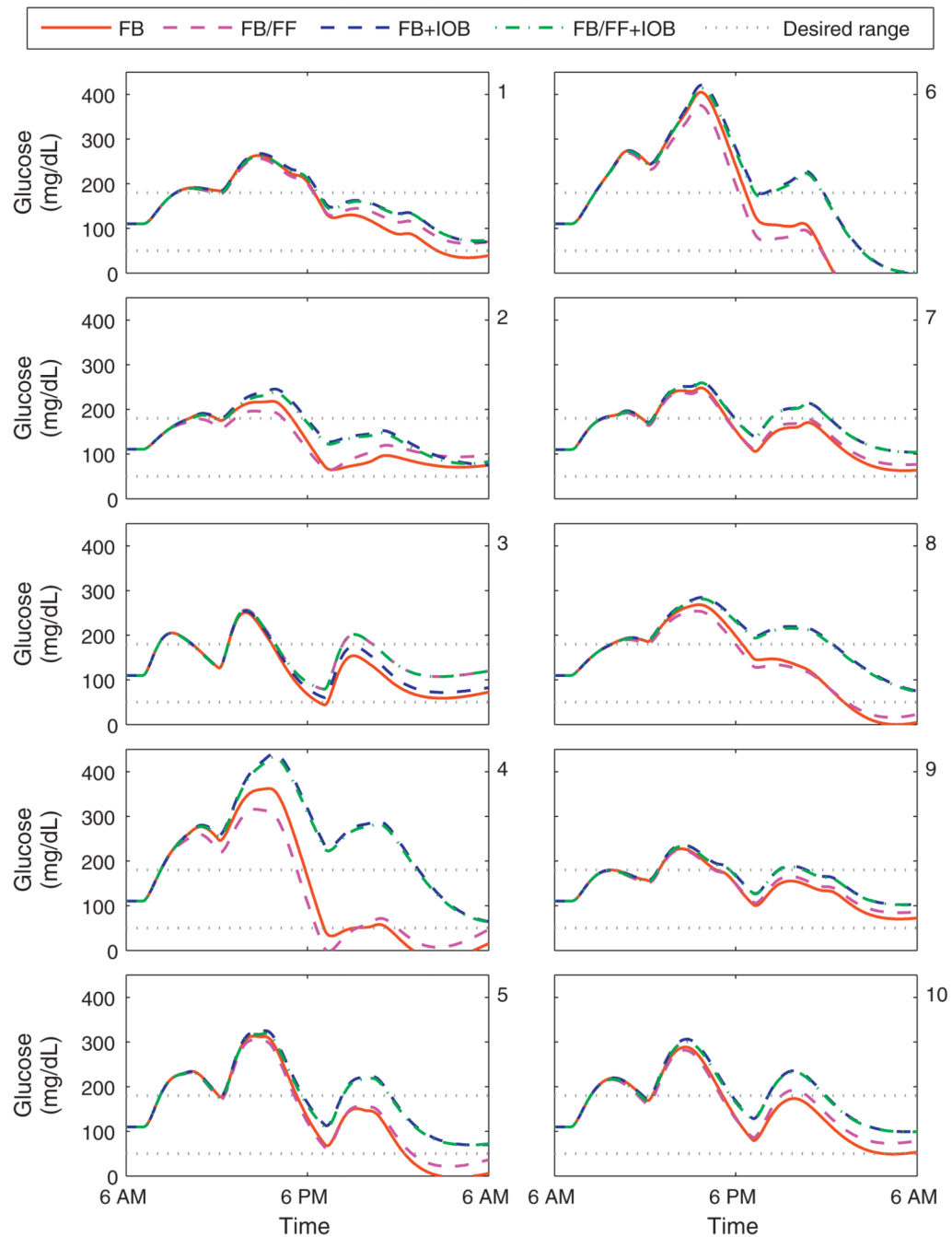


Fig. 10. Closed-loop results for the UVa/Padova cohort. Meal plan is 50, 85, and 65 g CHO at 7 a.m., noon, and 7 p.m. Control algorithms compared are the unannounced (FB) and measured (FB/FF) meal scenarios, with and without the IOB constraint, using model D. Panels 1–10 correspond to the UVa/Padova adult subjects 1–10.

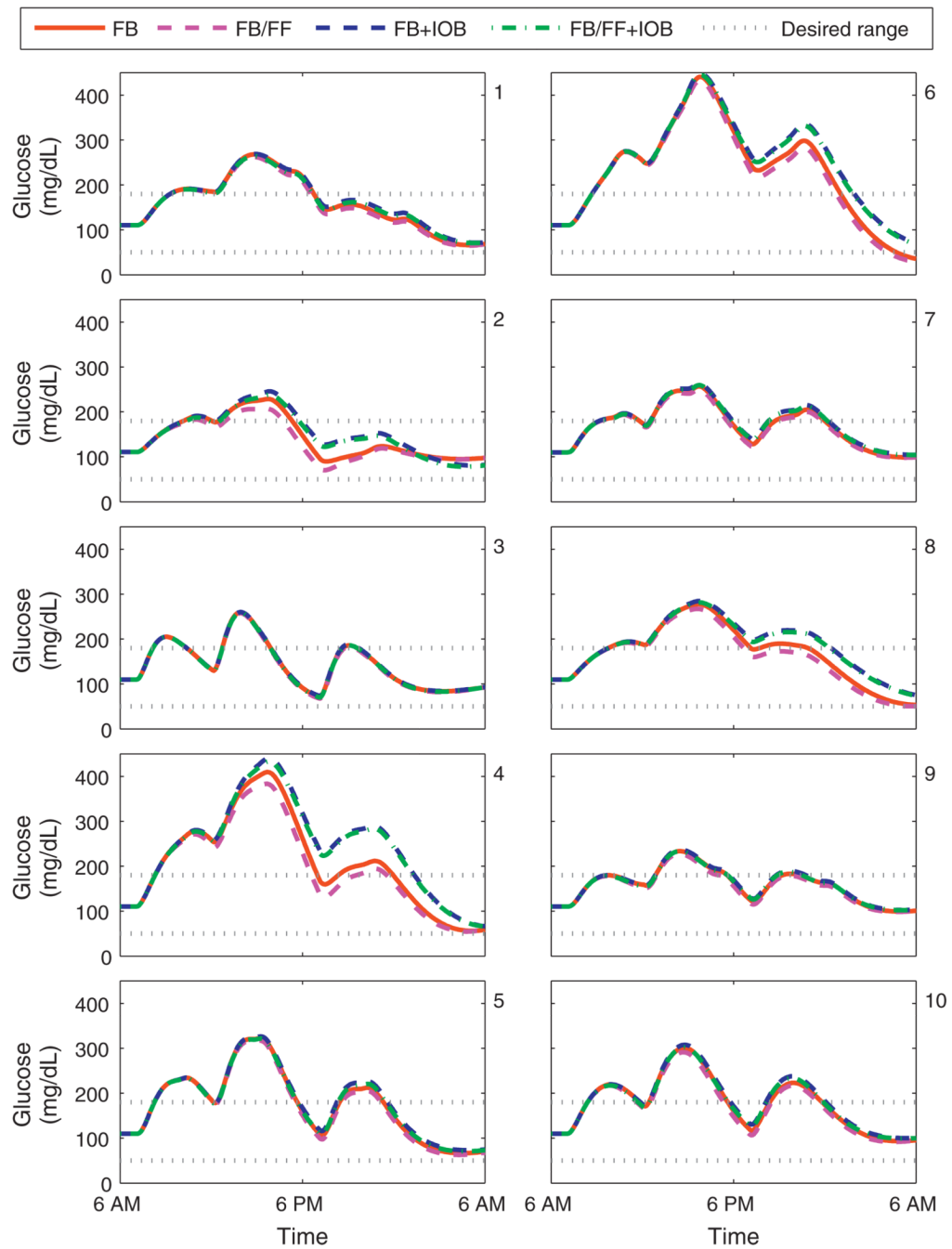


Fig. 11. Closed-loop results for the UVa/Padova cohort. Meal plan is 50, 85, and 65 g CHO at 7 a.m., noon, and 7 p.m. Control algorithms compared are the unannounced (FB) and measured (FB/FF) meal scenarios, with and without the IOB constraint, using model F. Panels 1–10 correspond to the UVa/Padova adult subjects 1–10.

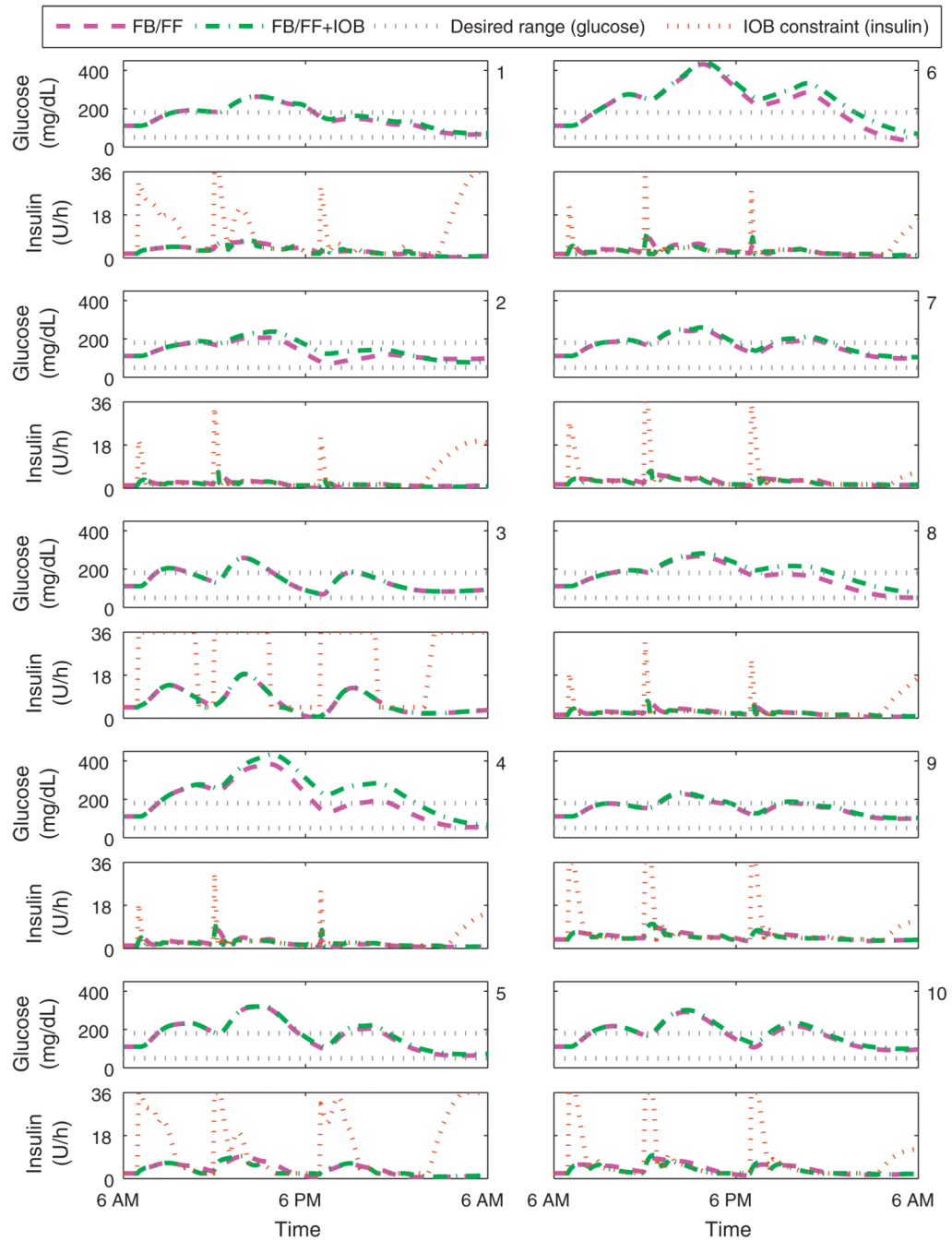


Fig. 12. Closed-loop results for the UVa/Padova cohort. Meal plan is 50, 85, and 65 g CHO at 7 a.m., noon, and 7 p.m. The control algorithms both consider measured meals (FB/FF), one has the IOB constraint, using model F. The IOB safety constraint for one controller is shown in the insulin delivery panels. Panels 1–10 correspond to the UVa/Padova adult subjects 1–10.

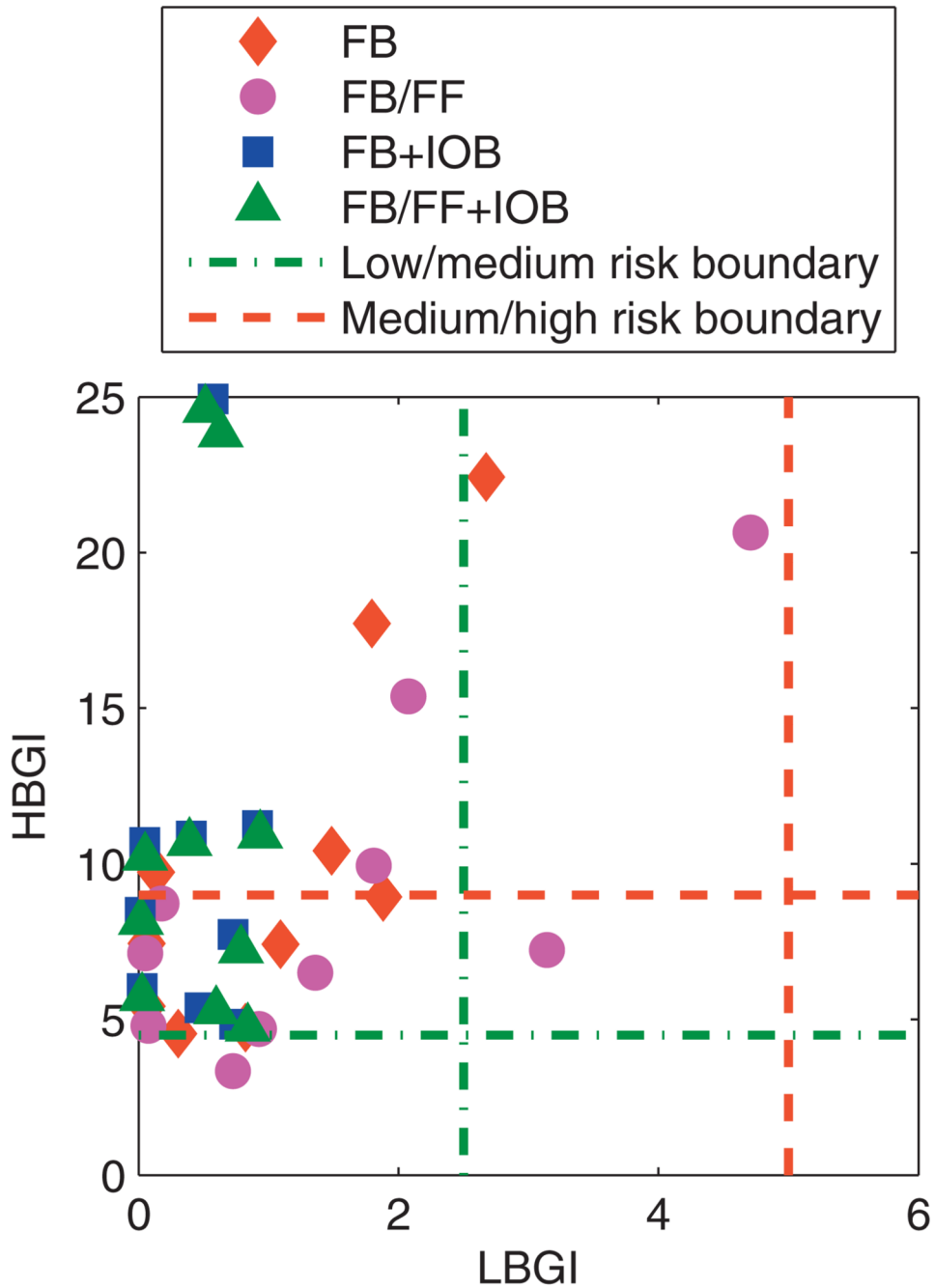


Fig. 13. Mean values of the daily LBGI and HBGI obtained over 30 days for the UVa/Padova cohort. Control algorithms compared are the unannounced (FB) and measured (FB/FF) meal scenarios, with and without the IOB constraint, using model F.

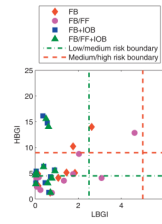


Fig. 14.

Mean values of the daily LBG and HBGI obtained over 30 days for the UVa/Padova cohort excluding the postprandial period. Control algorithms compared are the unannounced (FB) and measured (FB/FF) meal scenarios, with and without the IOB constraint, using model F.

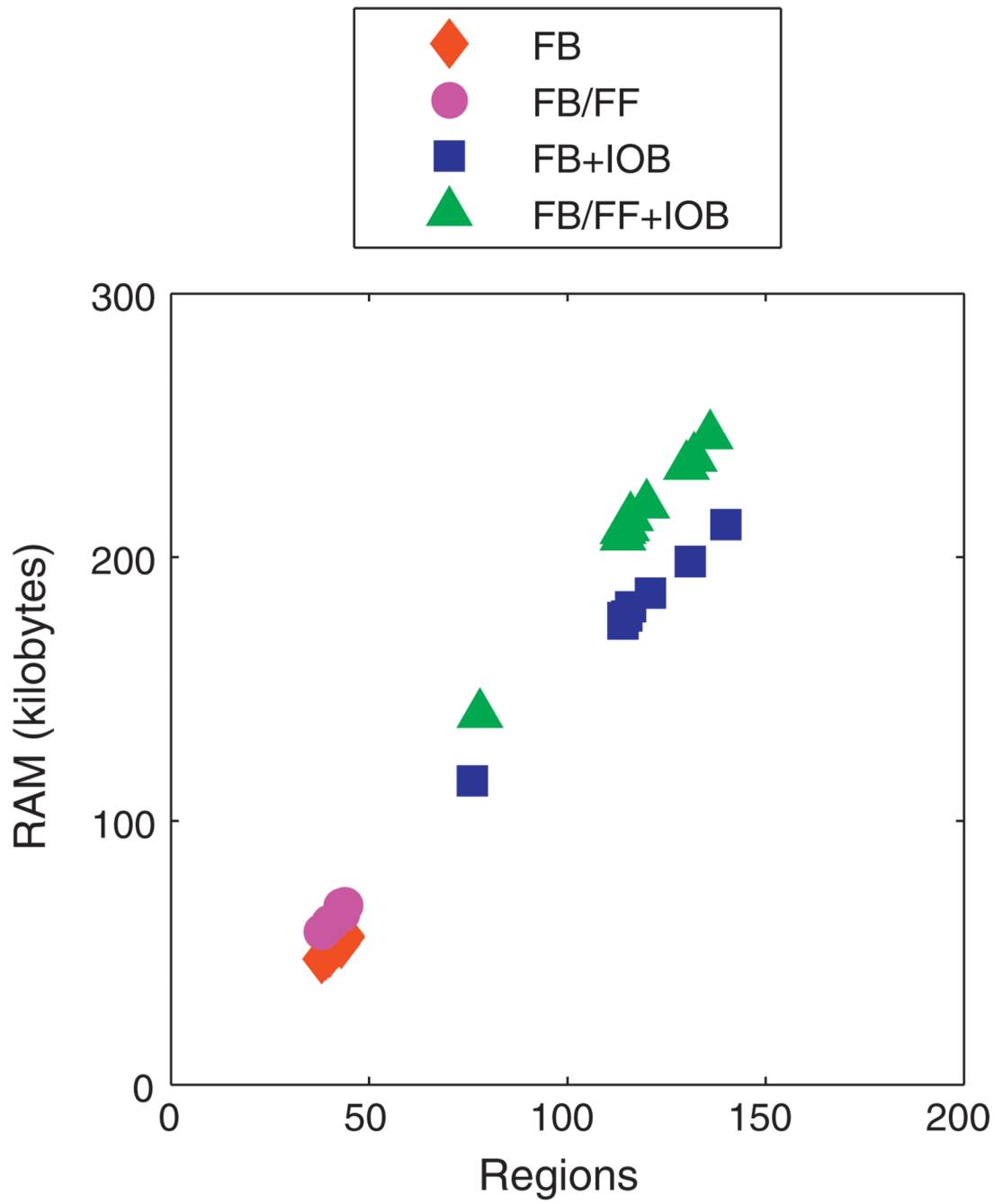


Fig. 15. Size of control law for UVa/Padova cohort based on model F for unannounced (FB) and measured (FB/FF) meals with and without the IOB constraint.

Table 1

A comparison of features of models A–F.

Model	Integrating	Second order
Personalized	A	D
Mean dynamics	B	E
Clinical parameters	C	F

Table 2
Parameters for models A and D identified from the Hovorka cohort using impulses of 1 U insulin and 25 g CHO.

Subject	Bolus model				Meal model						
	$-K_B$ (mg/dL/U)	τ_B (min)	θ_B (min)	$-K_{BI}$ (mg/dL)/(U/min)	τ_{BI} (min)	K_M (mg/dL)/g CHO	τ_M (min)	θ_M (min)	K_M (mg/dL)/g CHO/min	τ_M (min)	
1	33.3	105	40	31,400	766	3.88	60	10	2090	438	
2	38.7	85	35	29,600	620	3.89	60	10	2100	438	
3	18.4	115	40	19,000	839	3.89	60	10	2100	438	
4	44.3	75	35	29,900	547	3.89	60	10	2100	438	
Mean	33.7	95	37.5	27,500	693	3.88	60	10	2100	438	
S.D.	11.2	18.3	2.89	5740	133	0.00525	0	0	2.83	0	

Table 3
Parameters for models A, D, and F identified from the UVa/Padova cohort using impulses of 1 U insulin and 25 g CHO.

Subject	Bolus model					Meal model					Clinical parameters				
	$-K_B$ (mg/dL/U)	τ_B (min)	θ_B (min)	$-K_{BI}$ (mg/dL)/(U/min)	τ_{BI} (min)	K_M (mg/dL/g CHO)	τ_M (min)	θ_M (min)	K_{MI} (mg/dL/g CHO/min)	τ_{MI} (min)	CF (mg/dL/U)	ICR (g CHO/U)	$-K_B/K_M$ (g CHO/U)		
1	8.09	135	60	9820	984	1.57	70	25	986	510	13.2	20.1	5.17		
2	23.6	135	55	28,600	984	1.35	80	25	973	583	31	31.5	17.4		
3	1.98	110	50	1950	802	1.89	50	15	851	365	2.99	9.32	1.04		
4	39.5	90	40	32,000	656	2.96	90	15	2400	656	59.9	33.9	13.3		
5	9.86	75	35	66,600	547	2.4	65	20	1410	474	15.1	16	4.1		
6	10.9	120	50	11,800	875	2.65	95	25	2260	693	19	21.8	4.13		
7	17	85	45	13,000	620	1.54	55	25	763	401	22	22.8	11		
8	23.9	110	50	23,600	802	1.48	80	20	1060	583	37.4	33.9	16.2		
9	11.1	80	45	80,100	583	1.39	55	25	686	401	17.6	13.5	8.03		
10	10.9	85	45	83,200	620	2.19	65	20	1280	474	17	12.2	4.97		
Mean	15.7	103	47.5	14,400	747	1.94	70.5	21.5	1270	514	23.5	21.5	8.54		
S.D.	10.8	22.5	7.17	10,100	164	0.576	15.4	4.12	602	112	15.9	9.06	5.64		