

Blast-induced phenotypic switching in cerebral vasospasm

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Vasospasm of the cerebrovasculature is a common manifestation of blast-induced traumatic brain injury (bTBI) reported among combat casualties in the conflicts in Afghanistan and Iraq. Cerebral vasospasm occurs more frequently, and with earlier onset, in bTBI patients than in patients with other TBI injury modes, such as blunt force trauma. Though vasospasm is usually associated with the presence of subarachnoid hemorrhage (SAH), SAH is not required for vasospasm in bTBI, which suggests that the unique mechanics of blast injury could potentiate vasospasm onset, accounting for the increased incidence. Here, using theoretical and in vitro models, we show that a single rapid mechanical insult can induce vascular hypercontractility and remodeling, indicative of vasospasm initiation. We employed high-velocity stretching of engineered arterial lamellae to simulate the mechanical forces of a blast pulse on the vasculature. An hour after a simulated blast, injured tissues displayed altered intracellular calcium dynamics leading to hypersensitivity to contractile stimulus with endothelin-1. One day after simulated blast, tissues exhibited blast force dependent prolonged hypercontraction and vascular smooth muscle phenotype switching, indicative of remodeling. These results suggest that an acute, blast-like injury is sufficient to induce a hypercontraction-induced genetic switch that potentiates vascular remodeling, and cerebral vasospasm, in bTBI patients.

neurotrauma | mechanotransduction | tissue engineering | vascular mechanics

Blast traumatic brain injury (bTBI) is the hallmark injury among military personnel wounded in Afghanistan and Iraq (1, 2). While the injuries most commonly associated with TBI are diffuse axonal injury and compromise of the blood-brain barrier, cerebral vasospasm is a potentially lethal dysfunction whose incidence is elevated in bTBI, as compared to other forms of TBI (3). Cerebral vasospasm, characterized by chronic vascular hypercontraction followed by cell proliferation (4), extracellular matrix remodeling (5, 6), and arterial occlusion, is commonly diagnosed 3–7 d posttrauma (6), but its onset is often accelerated in bTBI patients (3). Traditionally cerebral vasospasm is attributed to subarachnoid hemorrhage (SAH), however, clinical reviews suggest that SAH is sufficient, but not necessary to potentiate cerebral vasospasm following bTBI (7). During blast injury, the cerebral vasculature likely bears significant acute pressure loads (8, 9). The role of chronically elevated luminal pressures in potentiating arterial thickening and stiffening to reequilibrate wall stress is well established (10); however, the vascular response to rapid acute pressure increases is unknown. The unique mechanics of blast pulse induced injury may contribute to the increased incidence of vasospasm in bTBI patients.

In vitro studies of vascular smooth muscle have revealed that direct stimulation of integrins induces enhanced calcium activity (11, 12) and myosin light chain phosphorylation (13). Cyclic mechanical stimulation within physiological ranges induces populations of vascular smooth muscle cells (VSMCs) to shift toward a contractile phenotype (14), while mechanical stresses of a higher magnitude, mimicking chronic hypertension, induce smooth muscle proliferation and extracellular matrix (ECM) remodeling

(15). Following the acute mechanical injury impulse associated with an explosion, the cerebrovasculature may be exposed to a range of stimuli, including SAH (7), increased endothelial endothelin production (16), delayed systemic hypotension (17), and inflammatory responses (18). We hypothesized that, even in the absence of these stimuli, a single, low-magnitude mechanical impulse of sufficient energy, such as a blast wave, could initiate progression of cerebral vasospasm.

Here, we present evidence for mechanotransduced vasospasms in bTBI. We present a unique in vitro experimental approach that combines uniaxial high-speed stretching of micropatterned vascular tissue mimics, and muscular thin films (19, 20) to measure mechanically induced vascular hypercontractility. We find that simulated blast injury induces short-term endothelin-1 hypersensitivity followed by prolonged hypercontractility and phenotypic switching, indicative of remodeling. This data suggests that initiation of cerebral vasospasm can be mechanotransduced by blast wave associated pressure pulses, accounting for the increased incidence in bTBI patients.

Results

Simulated Blast in Engineered Arterial Lamellae. A pressure pulse in an artery would primarily manifest as acute circumferential stretching caused by luminal expansion. To mimic this deformation, we developed engineered arterial lamellae (Fig. 1*A*) composed of a highly aligned monolayer of VSMCs (Fig. 1*B*) on an elastic substrate, which were exposed to a simulated blast consisting of a single axial high-velocity stretch (Fig. 1*C*, [Movie S1](#)). Due to the viscoelasticity (21) and strain stiffening (22) of arterial tissues, as well as the incompressibility of the surrounding brain tissue and cerebrospinal fluid (23), we assumed that the blast would result in a rapid, but low-magnitude strain. We therefore applied simulated blast at 5% and 10% strain at a strain rate of 1,000% strain/s (Fig. 1*D*, [Movie S2](#)). Evidence of acute and chronic vasospasm were measured 1–24 h postblast. Simulated blast did not cause obvious trauma such as altered tissue architecture (Fig. 1*E*), cell density, induced membrane poration, or increased apoptosis (Fig. [S1](#))

Simulated Blast Induces Elevated Cytosolic Calcium Transients. Recently, a study of controlled cortical impact injury in the rat demonstrated a reduced lumen diameter in the pial arterioles 1 h after injury, coincident with a reduction in ipsilateral cerebral blood flow (24). Subsequently, an additional study suggested L-type Ca²⁺ blockade would restore cerebral vasoreactivity fol-

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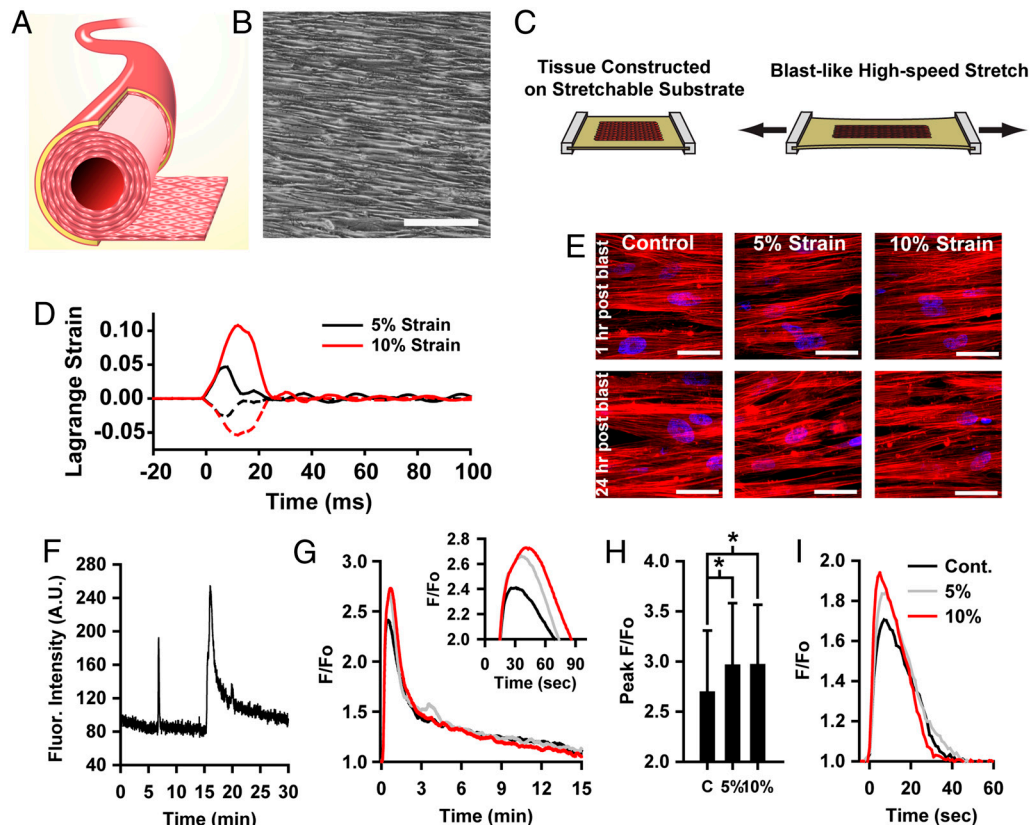


Fig. 1. In vitro model for bTBI in the vasculature. (A) Experimental model represents a single arterial lamella, isolated from surrounding tissue. (B) Phase contrast image of engineered lamella composed of micropatterned VSMCs. (Scale bar, 100 μm). (C) Lamellar tissue is engineered on an elastic membrane, which is acutely stretched to mimic a blast pulse. (D) Lagrange strain during 5% and 10% simulated blast. Solid lines: axial strain. Dashed lines: transverse strain. (E) Simulated blast does not result in acute or delayed structural reorganization. Red: actin, Blue: nuclei. (F) Example single-cell cytosolic Ca^{2+} trace showing two transients, pre-ET-1 spontaneous transient and prolonged ET-1 induced transient. (G) Mean ET-1 induced temporal transients for blasted tissues. Black: control, Gray: 5% strain, Red: 10% strain. Inset: transient peaks (H) Single-cell ET-1 induced transient peak values. Mean \pm standard deviation. (I) Mean pre-ET-1 spontaneous transients.

lowing lateral fluid percussion injury in rats (25). We asked if in our experimental model of blast-induced vascular injury, disrupted Ca^{2+} dynamics may play a role in initiating changes in vascular tone by contributing to the hypercontractility characteristic of acute vasospasm (26). We measured the temporal changes in cytosolic Ca^{2+} levels, or transients, in the engineered tissues 1 h after simulated blast (Fig. 1F, Movie S3). Endothelial injury following TBI can affect endothelin-1 (ET-1) production (16), and elevated cerebral spinal fluid levels of ET-1 have been implicated in cerebral vasospasm (27, 28), so we measured ET-1 induced calcium transients as well as spontaneous transients. Tissues exposed to simulated blast had transients with higher and more prolonged peaks following ET-1 stimulation than did control tissues (Fig. 1G and H). This trend was also apparent for spontaneous transients (Fig. 1I). This elevated response suggests that blast mechanics predispose VSMCs to hypercontraction through increased Ca^{2+} uptake and may act synergistically with elevated ET-1 levels to accelerate vasospasm.

Simulated Blast Induces Dysfunctional Contractile Dynamics. To characterize the functional effect of simulated blast, we measured contractile stress generation using a vascular muscular thin film (vMTF) assay (19, 20). The vMTFs are biohybrid constructs composed of a layer of polydimethylsiloxane (PDMS) and a layer of micropatterned VSMCs. When the muscle contracts, it bends the passive PDMS film whose curvature can be measured and used to calculate the tissue stress (Fig. 2B). The vMTFs were released from the stretchable substrate (Fig. 2A) and the temporal change in curvature (Fig. 2C, Movie S4) and tissue stress (Fig. 2D) were

measured during stimulation with ET-1 and rho kinase (ROCK) inhibitor HA-1077, allowing characterization of the basal tone and contractility of the tissue (Fig. S2).

An hour after simulated blast, tissues exhibited nearly twofold increases in ET-1 induced contraction (Fig. 2E), consistent with the observed elevated Ca^{2+} , but no change in basal contractile tone (Fig. 2F). To test whether stress during the blast is responsible for this hypercontraction, we inhibited ROCK prior to simulated blast, to relieve cytoskeletal contractile tension during the blast. This stress relief during the blast mitigated the ET-1 hypersensitivity (Fig. 2G) with no change in basal tone (Fig. 2H), suggesting that cytoskeletal mechanical tension during blast contributes to postblast hypercontractility.

Because vasospasm is a chronic dysfunction, we also tested tissue function 24 h after simulated blast. At this later time point, mildly and severely injured tissues showed markedly different contractile dynamics (Fig. 2I and J). Tissues strained 5% remained hypersensitive to ET-1 stimulation (Fig. 2I) and also developed elevated basal contractile tone (Fig. 2J), indicative of a chronic hypercontraction. However, the tissues strained 10% showed decreased ET-1 induced contraction (Fig. 2I) and no significant change in basal tone (Fig. 2J) compared to control.

Rho/ROCK signaling plays an important role in vasomotor tone. Inhibition of ROCK has been shown to relieve SAH induced vasospasm in vivo (29, 30). To test how ROCK signaling mediates the observed contractile behaviors in injured tissue, we inhibited ROCK immediately following simulated blast. We found that blasted tissues maintained ET-1 hypersensitivity, though at a decreased level, 1 h after blast (Fig. S3), but that

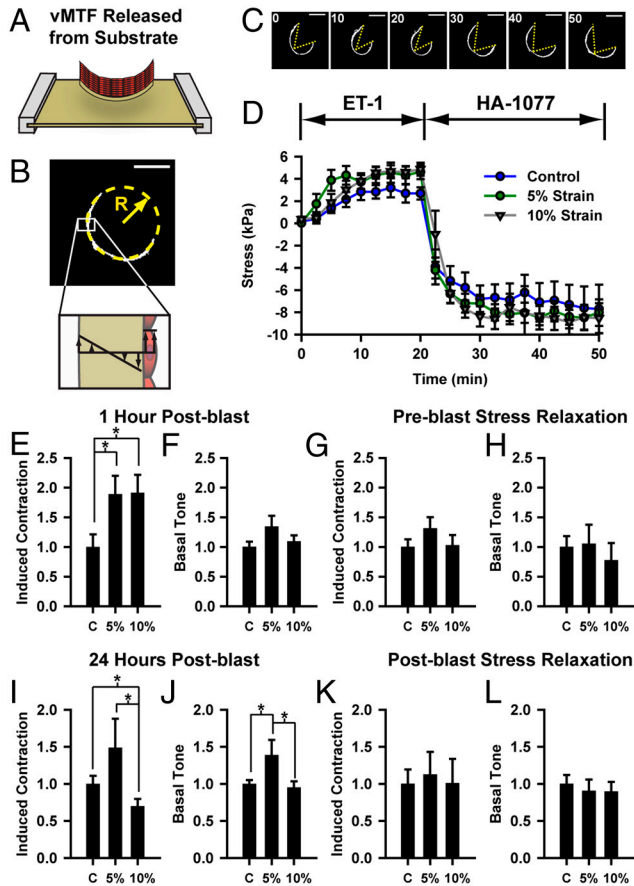


Fig. 2. Simulated blast induces dysfunctional contractility, as measured with vMTFs. (A) Immediately prior to contraction experiment, vMTF is released from the membrane. (B) Stress is calculated from the radius of curvature (Scale bar, 1 mm). (C–D) vMTFs were serially stimulated with ET-1 and HA-1077. (C) Single vMTF during experimental protocol. (Scale bar, 1 mm). (D) Temporal change in vMTF stress due to serial stimulation, 1 h after simulated blast. (E–F) Normalized ET-1 induced contraction and basal tone 1 h after simulated blast. (G–H) Normalized induced contraction and basal tone 1 h after simulated blast for tissues pretreated with ROCK inhibitor. (I–J) Normalized induced contraction and basal tone 24 h after simulated blast. (K–L) Normalized induced contraction and basal tone 24 h after simulated blast for tissues treated ROCK inhibitor immediately following the blast. All graphs: mean + / – SEM.

24 h postblast ROCK-inhibited tissues exhibited no differences in contractility between the blast exposed tissues and control (Fig. 2*K* and *L*). This result suggests that Rho-mediated postblast hypercontraction potentiates chronic contractile variation between mildly and severely injured tissues.

Dynamic Phenotype Switching Predicts Long-Term Contractility and Stress Remodeling. Given the reduction in contractile stress at 24 h in the severely injured tissues with respect to both control and mildly injured tissues, we reasoned that severely injured tissues were remodeling their stress state by changing the phenotype of a subpopulation of the VSMCs in the blast-induced hypercontractile tissues. We developed an elasticity-based computational model, based on previous models of stress-induced growth and remodeling (31, 32), to better understand how blast-induced hypercontraction potentiates the contractility observed 24 h postblast. The primary assumption of the model is that the tissue has an optimal stress state and actively remodels to return to this target value (33). Unlike previous models, we included a dynamic temporal interaction between tissue tension and VSMC phenotype (34), where for small perturbations in tissue tension, contractile adaptation dominates, while larger perturbations shift

VSMCs toward a synthetic phenotype, facilitating large-scale remodeling (see *Methods* for details). This assumption is consistent with previous experimental reports that physiological levels of stress induce VSMCs to become more contractile (14), while pathological stresses lead to vessel thickening and ECM remodeling (15), indicative of synthetic VSMCs. We further assume that contractile cells generate contractile stress when stimulated, but do not contribute to tissue remodeling, while synthetic cells generate no contractile stress but more rapidly remodel the tissue.

As indicated by our cytosolic calcium measurements, we assumed that more severe blast results in increased hypercontraction (Fig. 3*A*), and thus, increased tissue stress (Fig. 3*B*), necessitating an adaptive response to reequilibrate the stress. To compare with the contractility results, we determined the simulated basal tone and induced contraction. The model predicts that mild blast leads to increased hypercontractility (Fig. 3*C*) and basal tone (Fig. 3*D*). Following severe injury, hypercontraction leads to large increases in tissue tension (Fig. 3*B*), which results in greatly decreased induced contraction (Fig. 3*C*) and basal tone (Fig. 3*D*) mediated by a phenotype shift toward a synthetic, non-contractile population (Fig. 3*E*). With time, the tissue returns to

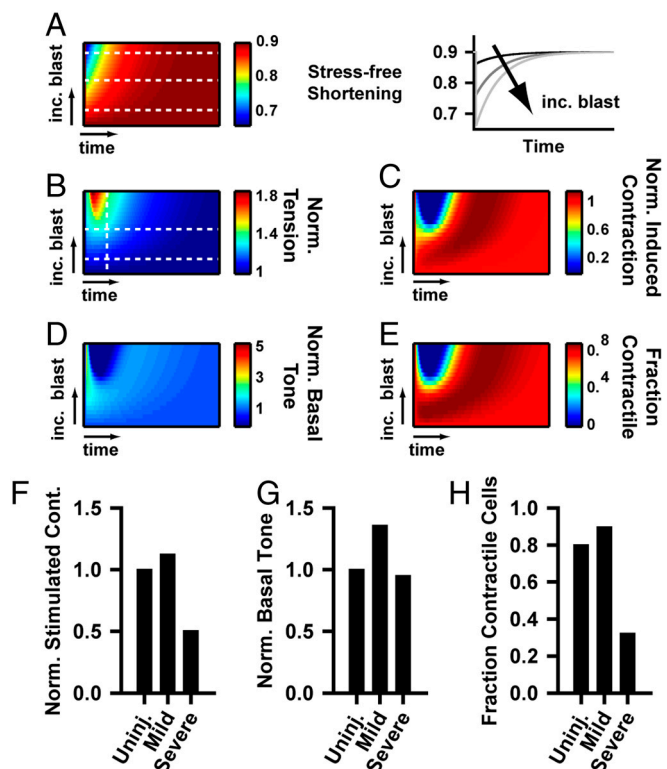


Fig. 3. Theoretical model for stress-induced remodeling and phenotype switching. (A) Blast injury induces increased hypercontractility, characterized by greater stress-free shortening (λ_s). (See *Methods* for details). Left box: contour plot of temporal evolution of contractile shortening. The y-axis represents tissues with increasing blast injury. The x-axis represents the time after the blast. Right box: Temporal plots of stress-free shortening for the tissues indicated by the white lines in the left box. (B–E) Contour plots of the temporal evolution of tissue tension, induced contraction, basal tone, and phenotype population for varying magnitudes of simulated blast. (B) Temporal stress evolution of remodeling tissue, (C) model predicted contractility, and (D) model predicted basal contractile tone for varying blast-induced hypercontraction. (E) Predicted temporal change in fraction of contractile cells for varying blast-induced hypercontraction and tissue remodeling. (F–H) Time point snapshots of (F) induced contraction, (G) basal tone, and (H) fraction contractile cells at an early time in vasospasm development, indicated by the vertical line in (B), for mild injury, indicated by the lower horizontal line in (B), or a more severe injury, indicated by the upper horizontal line in (B). These graphs correspond with the 24 h contractility experiments in Fig. 3*F* and *G*.

ET-1 treatment. Normalized temporal intensities of individual regions were registered by onset time to determine the mean curves in Fig. 1.

Tissue Stress Measurement. vMTF were constructed as previously published (19). The vMTF tissue stress was calculated as previously published (20). To inhibit ROCK during blast, tissues were treated with 100 μM HA-1077 for 30 min prior to simulated blast and immediately washed out following blast. To inhibit postblast ROCK activity, tissues were treated with 10 μM HA-1077 immediately following simulated blast. HA-1077 was washed out 30 min prior to vMTF experiments. Substrate and tissue thicknesses necessary for stress measurement were measured using stylus profilometry and confocal microscopy, respectively (Fig. S4).

Theoretical Model. The model methods are presented briefly here, and in more extensive detail in *SI Text*, Figs. S5, S6, S7, and S8.

We employ finite elastic growth theory (46) adapted for pseudocontraction (47) to model the evolution of stress in the tissue. Within this framework, Cauchy stress (σ) is considered a function of elastic stretch ratio F_e such that

$$\sigma = F_e \cdot \frac{\partial W(F_e)}{F_e^T} - pI, \quad [1]$$

where W is the strain-energy density function, and p is a Lagrange multiplier. F_e is a component of the total deformation (F) which is also composed of the remodeling deformation ($F_g = \text{diag}(\lambda_g, 1, 1)$), and active deformation ($F_a = \text{diag}(\lambda_a, 1, 1)$), which represent the change in the zero-stress configuration due to remodeling and contraction, respectively. (e.g., λ_a is the stretch ratio representing the stress-free shortening that the tissue would undergo if it was unconstrained.) Total deformation is defined as

$$F = F_g \cdot F_a \cdot F_e. \quad [2]$$

The tissue is composed of a mixed population of contractile and synthetic cells and is treated as a constrained mixture (48) of both cell types. Total tissue tension and remodeling rate are dependent on the fraction of the population of each cell type, with synthetic cells being noncontractile ($\lambda_a = 1$), but remodeling more quickly. The total stress is given by

$$\sigma = \phi_c \sigma_c + \phi_s \sigma_s, \quad [3]$$

where ϕ_c and ϕ_s are the fraction of total cells expressing contractile or synthetic phenotypes, respectively and $\phi_c + \phi_s = 1$.

We assume that the tissue grows to reequilibrate both tissue stress and basal contraction (32). The relationship between the magnitude of

the perturbation from a homeostatic tissue-level target stress and the rate of remodeling $\dot{\lambda}_g$ is given by

$$\dot{\lambda}_g = \frac{\phi_s}{\tau_\sigma} (\sigma - \sigma_o) + \frac{\phi_s}{\tau_a} (\lambda_a - \lambda_{ao}), \quad [4]$$

where σ_o is the tissue's target stress and τ_σ and τ_a are time constants (32, 33, 49). We further assume that perturbation from the target stress results in a change in the phenotype population, with small perturbations inducing a more contractile population and large perturbations causing the population to become more synthetic. We characterize this phenotype switching by the rate of change of contractile population fraction ($\dot{\phi}_c$) given by

$$\dot{\phi}_c = -\frac{1}{\tau_{\phi\sigma}} \left(\frac{-1}{(\gamma\sigma_o)^2} |\sigma - \sigma_o|^2 + \frac{2}{\gamma\sigma_o} |\sigma - \sigma_o| \right) + \frac{1}{\tau_{\phi\phi}} (\phi_{co} - \phi_c), \quad [5]$$

where the first term represents the influence of stress perturbation on phenotype and the second is a corrective term that acts to bring the phenotype distribution back to equilibrium. γ is a constant, $\tau_{\phi\sigma}$ and $\tau_{\phi\phi}$ are time constants and ϕ_{co} is the homeostatic fraction of cells expression a contractile phenotype, here assumed to be 0.8.

Following the blast, we assume an acute hypercontraction followed by a temporal return to equilibrium, described by

$$\lambda_a = 0.9 - \alpha e^{-\beta t}, \quad [6]$$

where α is a constant that is dependent on the degree of hypercontraction, assumed to be proportional to the blast severity (Fig. 3A), β is a time constant and t is time after blast. In response to the perturbed contractile stress, the tissue temporally remodels and undergoes phenotype switching to reequilibrate the tissue tension.

To simulate the vMTF experiments, induced contraction and basal tone are calculated by setting $\lambda_a = 0.6$ (fully contracted) and $\lambda_a = 1$ (fully relaxed) respectively, and comparing the resulting stress to the unstimulated tissue.

Biochemistry. Western blotting and RT-PCR were performed using standard methods detailed in the online supplement.

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