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Micropore and nanopore fabrication in hollow antiresonant reflecting optical waveguides

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Abstract

We demonstrate the fabrication of micropore and nanopore features in hollow antiresonant reflecting optical waveguides to create an electrical and optical analysis platform that can size select and detect a single nanoparticle. Micropores (4 μ m diameter) are reactive-ion etched through the top SiO₂ and SiN layers of the waveguides, leaving a thin SiN membrane above the hollow core. Nanopores are formed in the SiN membranes using a focused ion-beam etch process that provides control over the pore size. Openings as small as 20 nm in diameter are created. Optical loss measurements indicate that micropores did not significantly alter the loss along the waveguide.

Subject terms

micropore; nanopore; antiresonant reflecting optical waveguide; microfluidic channels; focused ion beam; optical loss

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1 Introduction

This paper concentrates on the fabrication and integration of nanometer-sized openings (nanopores) in hollow antiresonant reflecting optical waveguide (ARROW)-based fluorescence platforms with solid-core waveguides and fluid reservoirs.^{1,2} These ARROWbased structures were previously demonstrated,^{3,4} but the inclusion of a nanopore into an ARROW represents a significant advancement in optofluidic integration targeted at single particle analysis. Biological and solid state nanopores have been fabricated using various techniques and successfully used to measure single particle signatures in electrical current blockade tests.⁵ For example, biological nanopores that spontaneously insert themselves in lipid membranes have been created using the α -hemolysin protein. Kasianowicz et al. showed that an electric field biased at 100 mV providing a continuous current of ~100 pA can drive single stranded RNA and DNA molecules through a 2.2-nm-diam α -hemolysin ion channel in a lipid membrane.⁶ Nanopores fabricated from solid state materials have been shown to be more mechanically and chemically stable and their sizes can be adjusted for specific applications. Heng et al. made solid state 1.2-nm-diam nanopores by sputtering a 30-nm-thick Si₃N₄ membrane using a high-energy focused electron beam, however, low etch rates limit the thickness of the membrane for this method.⁷ By applying an unfocused ion beam, Li et al.⁸ were able to reduce the diameter of a 100- to 150-nm nanopore sputtered in a Si_3N_4 membrane with a high-energy Ar⁺ beam to 5 nm. The membrane separated two compartments biased at 120 mV with a constant ionic current of 1.66 nA through the nanopore that they used to measure the diffusion of double-stranded DNA. Additionally, Storm et al.⁹ also used a high-energy electron beam to reduce the diameter of a 20-nm nanopore etched in a 10-nm-thick SiO₂ membrane to 2 nm. Allen et al. formed 50- to 200nm nanopores in SiN membranes by focused ion-beam drilling in combination with ionbeam-assisted thin film deposition.¹⁰ Siwy and Fulinski used electrochemical etching to create conical nanopores with diameters as small as 2 nm at the aperture of the cone tip in circular polyethylene terephthalate (PET) foils.¹¹ Particle detection and analysis in each of these cases was done electrically by measuring ionic current changes as a particle passed through the nanopore. The motivation for combining nanopores with ARROW platforms is the ability to correlate electrical current blockade and optical fluorescence signals providing sensitive nanoparticle detection.

Optical fluorescence is another primary method used to analyze small numbers of single particles.¹² Fluorescence is used to study molecular phenomena and interactions such as DNA structural rearrangements,^{13,14} ribosome kinetics,¹⁵ and protein conformational dynamics.^{16–18} Some examples of conventional fluorescence detection and analysis techniques include epifluorescence,¹² confocal microscopy,¹² evanescent field sensors,¹⁹ and fluorescence correlation spectroscopy.^{20,21} However, typical analysis schemes are based on bulky microscopy instruments, therefore, an integrated ARROW fluorescence platform that uses planar waveguides for analysis is an attractive approach to reduce cost, time, analyte volumes, and device size (~1 cm²). However, to use the ARROW to perform fluorescence analysis it is important that the fabrication techniques for the integration of the nanopore do not significantly alter the optical properties and structural integrity of the waveguide.

2 Micropore/Nanopore Integrated Analysis Platform

The ARROW analysis platform is made up of alternating dielectric layers that act as Fabry-Pérot reflectors in the direction transverse to the propagation of light. When operating at antiresonance, the layers have a high reflectivity that enables light to be guided in the core of the hollow ARROW waveguide.²² The condition for antiresonance is satisfied by growing the dielectric layers to specific thicknesses given by

(1)

$$t_j = \frac{\lambda}{4n_j} (2N+1) \left(1 - \frac{n_c^2}{n_j^2} + \frac{\lambda^2}{4n_j^2 d_c^2} \right)^{-1/2},$$

where t_j is the thickness of the j'th layer; n_j and n_c are the indices of refraction of the j'th layer and the core, respectively; d_c is the thickness of the core; λ is the wavelength; and N is an integer representing the antiresonance order. An example of a side view of an ARROW waveguide is shown in Fig. 1. We use plasma-enhanced chemical vapor deposition (PECVD) SiN and SiO₂ as our dielectric layers at thicknesses of $t_{\text{oxide}}=270$ nm and $t_{\text{nitride}}=93$ nm when $n_{\text{nitride}}=2.05$, $n_{\text{oxide}}=1.47$, $n_c=1.33$, $d_c=5 \,\mu\text{m}$, N=0, and $\lambda=633$ nm, though this structure exhibits low propagation loss over a broad wavelength range from 500 to 700 nm. In addition, we deposited a SiO₂ layer that is 4 μ m thick over our top ARROW layers that we used to etch solid core waveguides in and provide structural support.

Figure 2 illustrates the functionality of a micropore and nanopore integrated with a hollow ARROW analysis platform. The integration with nanopores poses a unique challenge in integrated optics because ARROWs are constructed of dielectric layers that are a total of several micrometers thick and have a nonflat geometry. This makes it difficult to controllably mill nanopores with diameters of 25 to 100 nm through a complete dielectric stack. To provide a thinner starting layer, a micrometer-sized pore (micropore) was first etched into the ARROW. The micropore exposed a thin SiN layer directly above the hollow core of the ARROW that a nanopore was milled into. A zoomed in view of the micropore, nanopore, and the thin SiN layer are shown in Fig. 2(a). The hollow-core ARROW, the intersecting solid-core waveguides at the ends and middle of the hollow-core ARROW, and the location of the micropore and nanopore are shown in Fig. 2(b). The geometry of the hollow-core and solid-core waveguides was used in earlier experiments.³ Fluorescence detection takes place when fluorophores are excited by the solid-core waveguides intersecting the hollow-core waveguide. Placing a micropore/nanopore feature directly above the hollow-core ARROW will allow for control of particles entering the detection region.

3 Micropore and ARROW Fabrication

Figure 3 shows how fabrication of the micropore fits within our established ARROW fabrication process.^{3,23} Figure 3(a) shows the deposition of a 2- μ m layer of thermal oxide that provides isolation from the silicon wafer. Alternating layers of SiO₂ and SiN that form the bottom part of the hollow waveguide were deposited using PECVD at thicknesses dictated by the ARROW guiding condition,^{3,24} are also shown in Fig. 3(a). The PECVD SiN was grown with a mixture of 5% silane in helium (SiH₄/He) and ammonia (NH₃), at 250 °C, 70 W of rf power, and 1 Torr. The PECVD SiO₂ was grown with a mixture of 5% silane in helium (SiH₄/He) and form. A patterned and reflowed rectangular SU8-3005 (Ref. 3) photoresist core is shown in Fig. 3(b). The SU8 photoresist core was used as a sacrificial material that was removed in later processing steps that formed the hollow part of the waveguide. Figure 3(c) shows the first SiN ARROW layer that was deposited over the SU8-3005 core. Nanopore features were milled into this SiN layer in later processing steps.

The deposition and patterning of a chrome square etch stop feature is shown in Fig. 3(d). The etch stop feature is an $8 \times 8 - \mu m^2$, 200-nm-thick chrome square that was fabricated using a liftoff technique. The chrome etch stop feature keeps the SiN layer below it intact during a subsequent reactive-ion etching (RIE) that forms the micropore.

Figure 3(e) shows the remaining ARROW SiO₂ and SiN layers that were deposited to form the top and sides of the hollow waveguide. The introduction of the chrome etch stop feature does not change the process requirements for the remaining ARROW layers. The total thickness of these layers is 5 μ m. The micropore etch mask that was patterned and aligned directly over the chrome etch stop feature is shown in Fig. 3(f). This was accomplished by patterning a 4×4- μ m² SU8-3005 square directly on top of the hollow waveguide. A 200-nm layer of chrome was deposited over the SU8-3005 squares and then the wafer was placed in acid that lifted off the chrome over the SU8-3005 squares. Figure 3(g) shows the ARROW hollow waveguides after the micropore etch was completed and the micropore etch mask was removed. The chrome etch stop feature at the bottom of the micropore was removed using a wet chrome etchant, leaving the underlying SiN membrane exposed.

Finally, Fig. 3(h) shows the ARROW after the rectangular SU8-3005 photoresist core was removed in a piranha solution $[(1:1) (H_2O_2:H_2SO_4)]$ at 130 °C, forming the waveguide's hollow core, which can be subsequently filled with liquids and test particles.

4 Micropore Etching Process

Etching a micropore into the top layers of an ARROW allowed us access to the SiN layer over the core where a nanopore could be milled. The most important consideration during the micropore etch was keeping the relatively thin SiN layer intact. We determined that depositing an etch stop layer over the SiN layer was a more reliable and higher yield approach to cover and protect the SiN layer than using a timed RIE etch process.

While the fabrication of this etch stop feature was straightforward, we had to select a material that was not sputtered away during the micropore RIE etch process. The micropore RIE etch process was performed using an Anelva RIE DEM-451, 13.56-MHz system employing tetrafluoromethane CF_4 . The CF_4 gas was chosen primarily for its high selectivity etching of SiO₂ and SiN films.

Six different materials were investigated as possible etch stop candidates: chrome, titanium, aluminum, nickel, positive photoresist AZ3330, and negative photoresist SU8-3005. Our selection criteria were based on the materials RIE etch rate selectivity. Table 1 shows that titanium and chrome both have very low etch rates under the conditions used for etching through SiO_2 and SiN layers. While specific etch rates will vary for different RIE machines and etch conditions, we expected the general trends to hold for fluorine-based etches. Chrome was chosen for the production of micropores because it had a highest RIE etch selectivity and it was straightforward to pattern and remove in a commercially available wet etchant.

Figure 4 shows two scanning electron microscope (SEM) images of micropores etched into ARROWs. A zoomed out view that also shows the intersection of a solid-core waveguide with a hollow-core waveguide is shown in Fig. 4(a). The smooth [5-nm root mean square (rms) measured by a Vecco Dimension 3100 atomic force microscope with a $1-\times 1-\mu m$ scanning region] flat SiN membrane surface at the bottom of the micropore is shown in Fig. 4(b).

5 Nanopore Formation

To demonstrate the ability to combine the micropore fabrication process with the addition of nanopores, we milled a nanopore in the thin SiN membrane at the bottom of the etched micropore using a focused-ion-beam (FIB) etching process.^{25,26} We used a dual-beam FEI Strata DB 235 FIB that had a 30-kV accelerating voltage for liquid Ga⁺ ions and current apertures ranging from 1 pA to 20 nA. The formation of nanopores that had diameters

between 20 and 100 nm is shown in Fig. 5. Initially, the diameter of the nanopore was 100 nm. While this size was generally adequate for the detection of particles that had the dimensions of large viruses (100 to 150 nm), subsequently shrinking the nanopore to smaller sizes (20 to 40 nm) would enable us to sense and size select smaller biomolecules. The shrinking process of the nanopore is based on the irradiation of the SiN layer area (about 1 μ m²) around the nanopore with Ga⁺ ions in the FIB scanning mode.^{25,26} Two main theoretical models are believed to be responsible for the shrinking of the nanopore. The first is the viscous flow model where an impinging Ga⁺ ion breaks the bonds in the SiN layer and allows for the flow of material. With the SiN layer in this fluidized state, the nanopore will deform to find a configuration with a lower surface free energy. If the diameter of the initial nanopore is less than the thickness of the SiN layer, then the nanopore can lower its surface free energy by shrinking its diameter.⁹ The second theory that explains the shrinking of the nanopore is the surface adatom diffusion model. This model is based on the theory that impinging Ga⁺ ions generate surface adatoms, which move about the surface of the SiN layer by diffusion. The shrinking of the nanopore happens when the adatoms diffuse into the nanopore and bind on its edge.²⁷ The initial size of our FIB milled nanopore was 100 nm. After a series of FIB scans, the diameter of the nanopore was controllably decreased to 20 nm.

6 Optical Loss Measurement and Characterization

An important question was whether the micropore and nanopore features would lead to deterioration in the optical guiding properties if it was placed in the collection section of the ARROW hollow-core waveguide. Theoretically the size of the nanopore/micropore is small enough $(4 \times 4 \,\mu\text{m})$ that any additional optical losses it introduces in the modified layer structure of the ARROW will not have a significant effect on the total optical throughput. For example, even if the micropore/nanopore had introduced a high loss of 100 cm^{-1} , only 4% of the optical power would be lost because of the small dimensions of the micropore $(4 \times 4 \text{ } \mu\text{m})$ and nanopore (20 nm diameter) site. While low loss in the section of the ARROW with the micropore/nanopore site was confirmed with a commercial mode solver program (Photon Design), losses in realized devices can differ, for example, by design layer thickness deviations, transitions from multiple to single layers, and wall roughness. The optical loss was measured by observing optically induced motion of dielectric particles (1 μ m diameter, $n \sim 1.59$, Duke Scientific) in the hollow core waveguide.²⁸ The test configuration for the loss measurements is shown in Fig. 6(a). A particle in the reservoir entered the ARROW hollow-core waveguide where an Nd:YAG laser (power ≈ 12 mW) optically induced motion of the particle. The particle was optically pushed down the length of the waveguide and passed the micropore/nanopore site. The particle location was observed perpendicular to the chip plane through a microscope $[0.5 \text{ numerical aperture (NA)}, 50\times]$ and a tracking program was utilized for analysis. Figure 6(b) shows the experimentally observed trajectory (circles) of a particle in an ARROW that had a micropore/nanopore site, the calculated particle trajectory that did not have a micropore/nanopore site (solid line), and the calculated particle trajectory that had a micropore site with a loss of 100 cm^{-1} (dashed line). As we can see, the trajectory without a micropore site (solid line) is not measurably different, within experimental error, from the trajectory with a site of 100 cm^{-1} loss (dashed line). Additionally, the observed trajectory closely resembles the calculated trajectory without a nanopore site. Therefore, the results indicate the additional loss introduced by the micropore/nanopore is not significant.

7 Conclusion

Small, simple, cheap, and fast sensors to detect single nanoparticles are desirable. We demonstrated a fabrication technique that can be applied to these types of sensors by

combining synthetic nanopores and hollow ARROW waveguides. A hybrid micropore/ nanopore fabrication process was developed to define nanopores in ARROW waveguides that have walls that are several micrometers thick. A chrome etch stop feature keeps the thin SiN membrane, where the nanopore is drilled, intact during micropore etching. We demonstrated that nanopores of variable size down to 20 nm can be drilled in the SiN membrane using an FIB process. Optical measurements show that the addition of micropores and nanopores does not measurably alter the transmission of the ARROW waveguide. In the future, the integrated ARROW platform and nanopore can be used to combine and correlate electrical current blockade data and fluorescently detected signal with single nanoparticle resolution.

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Side view of an ARROW waveguide.



Fig. 2.

Cross section of a micropore/nanopore integrated with the ARROW hollow core waveguide lab-on-a-chip platform.



Fig. 3.

Fabrication flow diagram of the process of creating a micropore in a hollow ARROW waveguide.



Fig. 4.

(a) SEM of an intersection of a hollow and solid core waveguide and a micropore on the ARROW hollow waveguide and (b) SEM image of the top view close-up of micropore.



Fig. 5.

SEMs showing the size of the nanopore being reduced from 100 to 20 nm after a series of FIB scans. The smallest dimension is reported as a characteristic size of the nanopore.



Fig. 6.

(a) Setup used to perform the particle pushing experiment to measure optical loss and (b) axial particle position versus time for an experimentally observed particle trajectory (circles) in an ARROW with a micropore/nanopore site, the calculated trajectory in an ARROW without a micropore/nanopore site (solid line), and the calculated trajectory in an ARROW with a micropore/nanopore site loss of 100 cm^{-1} loss (dashed line).

Table 1

Average RIE etch rate (in nanometers per minute) for a set of possible etch stop materials.

Etch Rate (nm/min)	111	107	255	3.65	1.48	0.97	0.60
Average							

The recipe used is a CF4 etch gas at a flow rate of 25 standard cubic centimeters per minute (SCCM), rf power of 300 W, and a chamber pressure of 100 mTorr.