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Rigid, Complete Annuloplasty Rings Increase Anterior Mitral Leaflet Strains in the Normal Beating Ovine Heart

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Abstract

Background—Annuloplasty ring or band implantation during surgical mitral valve repair perturbs mitral annular dimensions, dynamics and shape, which have been associated with changes in anterior mitral leaflet (AML) strain patterns and suboptimal long-term repair durability. We hypothesized that rigid rings with non-physiological 3-D shapes, but not saddle-shaped rigid rings or flexible bands, increase AML strains.

Methods and Results—Sheep had 23 radiopaque markers inserted: 7 along the anterior mitral annulus and 16 equally spaced on the AML. True-sized Edwards Cosgrove flexible, partial band (COS, n=12), rigid, complete St. Jude saddle-shaped annuloplasty ring (RSAR, n=12), Carpentier-Edwards Physio (PHYSIO, n=12), Edwards IMR ETlogix (ETL, n=11) and Edwards GeoForm (GEO, n=12) annuloplasty rings were implanted in a releasable fashion. Under acute open-chest conditions, four-dimensional marker coordinates were obtained using biplane videofluoroscopy along with hemodynamic parameters with the ring inserted and after release. Marker coordinates were triangulated and the largest maximum principal AML strains were determined during isovolumetric relaxation (IVR). No relevant changes in hemodynamics occurred. Compared to the respective Control state, strains increased significantly with RSAR, PHYSIO, ETL and GEO (0.14±0.05 *vs.* 0.16±0.05, p=0.024, 0.15±0.03 *vs.* 0.18±0.04, p=0.020, 0.11±0.05 *vs.* 0.14±0.05, p=0.042 and 0.13±0.05 *vs.* 0.16±0.05, p=0.009), but not with COS (0.15±0.05 vs. 0.15 ± 0.04 , p=0.973).

Conclusions—Regardless of 3-D shape, rigid, complete annuloplasty rings, but not a flexible, partial band, increased AML strains in the normal beating ovine heart. Clinical studies are needed

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to determine if annuloplasty rings affect AML strains in patients, and, if so, whether ring-induced perturbations in leaflet strain states are linked to repair failure.

Keywords

mitral valve; physiology; mitral regurgitation; surgery

INTRODUCTION

Surgical mitral valve repair most commonly includes the insertion of an annuloplasty band or ring. While bands are flexible devices that spare the anterior, fibrous portion of the mitral annulus, rings encircle the entire annulus and may be either flexible, semi-rigid or rigid. Rigid rings are available in various shapes. The most commonly used ring (Carpentier-Edwards Physio) is flat, semi-rigid and D-shaped. Recently, saddle shaped, rigid, complete annuloplasty rings have been introduced (e.g. Saint Jude Medical RSAR, Medtronic Profile 3-D or Carpentier-Edwards Physio II) in order to account for the physiological 3-D shape of the mitral annulus [1, 2]. Furthermore, rigid rings with non-physiological shapes and dimensions have been designed specifically for patients with functional/ischemic mitral regurgitation (e.g. Edwards GeoForm and IMR ETLogix). These rings aim to counteract the main determinants of functional/ischemic mitral regurgitation (i.e. mitral annular dilatation, left ventricular (LV) dilatation and papillary muscle displacement) on an annular level via their specific designs, all of which include disproportionate annular septal-lateral downsizing [3]. While some studies demonstrate that such rings may reduce mitral leaflet strains in the diseased heart [4], other studies suggest that, by perturbing the natural mitral annular saddle-shape, disease-specific or non-physiologically shaped rings may increase leaflet strains in the normal heart [5-7]. Due to these results from *in vitro* measurements the authors speculate that such perturbations in mitral leaflet strain patterns could be associated with impaired long-term results after mitral valve repair [5-7]. Our goal was, therefore, to assess the effects of one flexible partial band and four different, complete annuloplasty rings on anterior mitral leaflet strains in healthy, beating ovine hearts. We tested the hypothesis that rigid, complete rings with non-physiological 3-D shapes, but not saddle-shaped rigid rings or flexible partial bands, increase maximum principal strains across the anterior mitral leaflet.

METHODS

All animals received humane care in compliance with the Principles of Laboratory Animal Care formulated by the National Society for Medical Research and the Guide for Care and Use of Laboratory Animals prepared by the National Academy of Sciences and published by the National Institutes of Health (DHEW [NIH] Publication 85 to 23, revised 1985). This study was approved by the Stanford Medical Center Laboratory Research Animal Review Committee and conducted according to Stanford University policy.

Surgical Preparation

Fifty nine adult, Dorsett-hybrid, male sheep (49±5kg) were premedicated with ketamine (25mg/kg intramuscularly), anesthetized with sodium thiopental (6.8mg/kg intravenously), intubated and mechanically ventilated with inhalational isoflurane (1.0-2.5%). A left thoracotomy was performed and the heart was suspended in a pericardial cradle. Thirteen miniature radiopaque tantalum markers were surgically implanted into the sub-epicardium to silhouette the LV chamber at the intersections of two longitudinal and three crosswise meridians as shown in Figure 1A. Using cardiopulmonary bypass and cardioplegic arrest a total of 33 radiopaque tantalum markers were sewn to the following sites (Figure 1B): 16

around the mitral annulus (17-32, Fig 2A, B), 16 equally spaced on the atrial aspect of the anterior mitral leaflet (AML, 1-16, Fig 2B) and 1 on the central edge of the middle scallop of the posterior mitral leaflet (PML, 33, Fig 2B). A single tantalum loop (0.6mm ID, 1.1mm OD, 3.2 mg) was used for each leaflet marker.

After marker placement, five different annuloplasty ring models, the Cosgrove-Edwards band (COS, Edwards Lifesciences, Irvine, CA, USA, n=12), St. Jude Medical rigid saddle ring (RSAR, St. Jude Medical Inc, St. Paul, MN, USA, n=12), Carpentier-Edwards Physio (PHYSIO, n=12), Edwards IMR ETlogix (ETL, n=11) and Edwards GeoForm (GEO, n=12, all three Edwards Lifesciences, Irvine, CA, USA) were implanted in a releasable fashion as described earlier [8]. In brief, the annuloplasty devices were prepared before the operation in the following manner: The middle parts of eight double-armed polyester braided sutures were stitched evenly spaced around the ring or band from the bottom to the top side using a "spring eye" needle. The resulting loops were "locked" with two polypropylene sutures. The polyester sutures were stitched equidistantly in a perpendicular direction from the ventricular to the atrial side through the mitral annulus. The annuloplasty devices were secured to the mitral annulus by tying these sutures. The "locking sutures" (polypropylene) and the drawstrings were exteriorized before closing the atrium. Ring and band sizes were determined by assessing the entire area of the anterior mitral leaflet using a sizer from Edwards Lifesciences. All annuloplasty devices were true-sized (as all animals had similarly sized leaflets, each received size 28 rings or bands). The left atrium (LA) was closed and the left circumflex artery (LCx) was encircled with a vessel loop for a parallel study [9]. Data from mitral annular and leaflet geometry using this dataset have been published earlier [8-11]. The animals were then transferred to the experimental catheterization laboratory for data acquisition under acute open-chest conditions.

Data Acquisition

Videofluoroscopic images (60 frames/sec) of all radiopaque markers were acquired using biplane videofluoroscopy (Philips Medical Systems, North America, Pleasanton, CA, USA). First, images were acquired under baseline conditions with the ring inserted (COS, RSAR, PHYSIO, ETL, GEO). Following the data acquisition under baseline conditions, 90sec of ischemia were induced, for a parallel study, by tightening the encircling LCx vessel loop with a tourniquet. Thereafter, the "locking sutures" were pulled out and the ring was lifted away from the mitral annulus towards the left atrial roof using the drawstrings. After hemodynamic values returned to baseline, a third data acquisition was performed and images were acquired under baseline conditions with the ring released (COS-CTRL, RSAR-CTRL, PHYSIO-CTRL, ETL-CTRL, GEO-CTRL). Marker coordinates from two consecutive sinus rhythm heart beats from each of the biplane views were then digitized and merged to yield the 3-D coordinates of each marker centroid in each frame using semiautomated image processing and digitization software [12]. Simultaneously, analog left ventricular pressures (LVP) as well as electrocardiogram (ECG) signals were recorded in real-time on the video images during data acquisition.

Hemodynamic Parameters and Cardiac Cycle Timing

For each beat, the end-diastolic videofluoroscopic frame was defined as the frame that coincided with the peak of the R-wave on the ECG. In order to calculate leaflet strains, a reference configuration during diastole and a deformed configuration during peak systole were determined for each beat $(t_0$ and t_n , respectively, Figure 2). When defining these configurations the goal was to quantify strains with the mitral valve closed in both configurations and maximize the LVP difference between the two time points. To identify the reference configuration, the distance between AML central edge (#4, Figure 1B) and PML edge marker (#33, Figure 1B) was plotted throughout the cardiac cycle for each

animal. For each heartbeat the time point of leaflet opening was defined as the time point immediately before the AML and PML started to separate (Figure 2), thereby defining the reference state for beat 1 (t₀₁, Figure 2) and beat 2 (t₀₂, Figure 2). To identify the deformed configuration, LVP curves were plotted throughout the cardiac cycle. The time point of maximum LVP for each heartbeat was defined as the deformed state $(t_{n1}$ and t_{n2} , respectively, Figure 2). The embedded period between these two states closely reflects the period of isovolumetric relaxation (IVR, Figure 2). Maximum systolic dP/dt (dP/dt_{max}) was calculated for each beat for each animal. LV volumes (LVV) were calculated from space-

filling tetrahedral fit between all LV markers at each beat at end-diastole (LVEDV), t_{n1} , t_{n2} , t_{01} and t_{02} (See Ref [13] for details). Changes in LVP and LVV (Δ_{LVP} and Δ_{LVV} , respectively) from t₀₁ to t_{n1} and from t₀₂ to t_{n2} were calculated as $LVPt_{n1} - LVPt_{01}$, $LVPt_{n2}$ – LVPt₀₂, and LVVt_{n1} – LVVt₀₁, LVVt_{n2} – LVVt₀₂, respectively.

Mitral Annular Dimensions

At t_{n1} , t_{n2} , t_{01} and t_{02} distances between markers #20 and #28 and those between #32 and #24 (Figure 1B) were calculated to determine septal-lateral (S-L) and commissurecommissure (C-C) annular dimensions, respectively. Changes in mitral annular S-L and C-C dimensions (Δ _{S-L} and Δ _{C-C}, respectively) from t₀₁ to t_{n1} and from t₀₂ to t_{n2} were calculated as $t_{n1} - t_{01}$ and $t_{n2} - t_{02}$.

Global Maximum Principal (global εmax), Radial (global εrad) and Circumferential (global εcir) Strains

In order to determine the largest (global) maximum principal, radial and circumferential strains across the entire leaflet, the 16 AML mitral leaflet markers (#1-#16, Figure 1B) and the seven mitral annular markers (#17-#23, Figure 1B) were triangulated and 30 triangular membrane elements were generated. For each triangle, the co- and contravariant base vectors at time points t_{01} , t_{n1} , t_{02} , and t_{n2} , were calculated to determine the corresponding metric tensors and the resulting Euler-Almansi strain tensors for beats 1 and 2. The direction defined by the belly markers #9 and 11# (Figure 1B) in the deformed configuration, i.e., at times t_{n1} and t_{n2} for beat 1 and beat 2, respectively, was interpreted as the circumferential direction. The radial direction was defined orthogonal to the circumferential axis, passing through belly marker #10 (see Fig 1B). The largest projections of the Euler-Almansi strain tensor onto the circumferential and radial directions were defined as global maximum circumferential strain (global ε_{cir}) and global maximum radial strain (global ε_{rad}), respectively. These values were determined for two beats in each animal, and each state (with and without annuloplasty device implanted). The animal global maximum principal strain (global ε_{max}) was calculated as the two-beat average for each animal and each state by solving the eigenvalue problem for the Euler-Almansi strain tensor.

Maximum Principal (εmax,), Radial (εrad) and Circumferential (εcir) Strains Across the Entire Anterior Mitral Leaflet

In order to provide a qualitative description of changes in strain patterns across the entire AML with and without annuloplasty device implanted, the two-beat averages of ε_{max} , ε_{rad} and ε_{cir} values of each triangular element were calculated for each animal in each state. These values were averaged for all animals (by extrapolating constant average element strains to the individual marker positions using super-convergent patch recovery to obtain smoothly varying strain profiles) and plotted onto color mapped schematics.

Statistical Analysis

Average values of all animals in the respective groups were reported as mean \pm 1 SD. All data reported for individual animals and all data used for quantitative statistical comparisons

are two beat averages. Data with and without annuloplasty ring (or band) were compared using 1-way repeated-measures analysis of variance with a Holm–Sidak post hoc test (Sigmaplot 11.0, Systat Software Inc). To look at strain differences between the ring groups, maximum principal (ε_{max}), radial (ε_{rad}) and circumferential (ε_{cir}) strains with rings (COS, RSAR, PHYSIO, ETL and GEO) were compared using 1-way analysis of variance. A *P* value of less than .05 was considered statistically significant.

RESULTS

Heart rate, LVEDV and dP/dtmax

Group mean heart rates, LVEDVs and dP/dt_{max} are shown in Table 1. No significant differences were found between ring and Control states in all five groups (except for Cosgrove, where dP/dt_{max} was slightly higher compared to Control).

LV Pressures and Volumes at Reference State (t0) and Deformed State (tn)

Table 2 shows LVPs and LVVs at t₀ and t_n as well as Δ_{LVP} and Δ_{LVP} and Δ_{LVP} are also graphically depicted in Figure 3 (top row). A significant increase in LVPs by approximately 80mmHg (note that changes in LVP and LVV (Δ_{LVP} and Δ_{LVV}) are described from t_0 to t_n , i.e. backward in time) occurred in both ring and Control states from t_0 to t_n , while no relevant LVV changes were observed.

Mitral Annular Dimensions at Reference State (t0) and Deformed State (tn)

Table 3 shows the mitral annular S-L and C-C dimensions at t_n and t_0 as well as Δ _{S-L} and $\Delta_{\text{C-C}}$. $\Delta_{\text{S-L}}$ and $\Delta_{\text{C-C}}$ are also graphically depicted in Figure 3 (middle row). Again, please note that Δ_{S-L} and Δ_{C-C} are described from t₀ to t_n, i.e. backward in time. Consequently, negative Δ_{S-L} and Δ_{C-C} represent an increase, whereas positive Δ_{S-L} and Δ_{C-C} represent a decrease in the respective dimension during the regular cardiac cycle. Relative to Control, implantation of either complete, rigid rings (RSAR, PHYSIO, ETL or GEO) or the flexible band (COS) resulted in significantly smaller mitral annular S-L and C-C dimensions. Decreases in S-L and C-C diameters from t_0 to t_n (negative Δ_{S-L} and Δ_{C-C} , Table 3) were observed for the Control cases (all groups). With the annuloplasty device implanted, the S-L dimension became slightly smaller from t₀ to t_n with COS (Δ _{S-L}: -0.9 ± 0.5 mm, Table 3 and Figure3, middle row) while no relevant decreases in S-L and C-C diameters from t_0 to t_n were found with RSAR, PHYSIO, ETL or GEO.

Global Maximum Principal (global εmax), Radial (global εrad) and Circumferential (global εcir) Strains

Table 4 shows global ε_{max} , ε_{rad} and ε_{cir} for all five groups with and without annuloplasty devices implanted. Global ε_{max} , ε_{rad} and ε_{cir} (average from all animals) are also graphically displayed in Figure 3 (bottom row). Compared to the respective Control state, strains increased significantly with RSAR, PHYSIO, ETL and GEO (0.14±0.05 *vs.* 0.16±0.05, p=0.024, 0.15±0.03 *vs.* 0.18±0.04, p=0.020, 0.11±0.05 *vs.* 0.14±0.05, p=0.042 and 0.13 \pm 0.05 *vs.* 0.16 \pm 0.05, p=0.009, respectively, all p<0.05), but not with COS (0.15 \pm 0.05 vs. 0.15±0.04, n.s., p=0.973). Global εrad increased significantly compared to the Control state only with RSAR, while greater global ε_{cir} values were found with RSAR, PHYSIO, ETL and GEO (however, insignificant for GEO, Table 4). No significant changes in global ε_{rad} or ε_{cir} were found with COS compared to the Control state. With no annuloplasty device implanted, global ε_{rad} was greater than global ε_{cir} in all five groups (COS-CTRL, RSAR-CTRL, PHYSIO-CTRL, ETL-CTRL, GEO-CTRL, Table 4 and Figure 3, bottom row). With annuloplasty device implanted, global ε_{rad} values were either greater than global ε_{cir} (COS, RSAR), smaller (PHYSIO) or similar (ETL, GEO, Table 4 and Figure 3, bottom row). No

differences in ε_{max} (p=0.331, F=1.178), ε_{rad} (p=0.188, F=1.598) or ε_{cir} (p=0.160, F=1.716) with rings implanted were found between the groups (COS, RSAR, PHYSIO, ETL and GEO).

Maximum Principal (εmax), Radial (εrad) and Circumferential (εcir) Strains Across the Entire Anterior Mitral Leaflet

Figure 4 shows ε_{max} , ε_{rad} and ε_{cir} across the entire AML for both states, with and without annuloplasty device implanted in all five groups. Increases in ε_{max} can be appreciated with RSAR, PHYSIO, ETL and GEO compared to the respective Control state and predominantly occur in the belly and edge region of the anterior mitral leaflet. No major changes in strain patterns (ε_{max} , ε_{rad} or ε_{cir}) were observed with COS. ε_{max} values across the AML of the respective Control states were slightly different between groups with COS-CTRL, RSAR-CTRL and PHYSIO-CTRL being more strained than GEO-CTRL and ETL-CTRL.

DISCUSSION

The principle finding of this study was that, with no relevant changes in hemodynamics, implantation of rigid, complete annuloplasty rings (RSAR, PHYSIO, ETL and GEO), but not of the flexible partial band (COS), increased global maximum principal strains of the AML. These changes predominantly occurred in the region of the AML belly and edge.

Several studies have determined mitral leaflet strains and stretches using a variety of different techniques [4-7, 14-19]. *In vitro* studies have been employed to characterize dynamic stretches on the anterior and posterior leaflet of excised porcine mitral valves using a left heart simulator [6, 14-17]. *In vivo* studies, using sonomicrometer technology, quantified AML strains in the beating ovine heart [16] and lastly, finite element studies investigated strain patterns across the AML [4, 5, 18, 19].

Salgo et al. demonstrated in a numerical simulation that the native mitral annular shape is important to minimize stresses acting on the leaflet [5]. In a previous analysis from the same dataset we demonstrated that implantation of the Physio, IMR ETLogix and GeoForm, but not RSAR, perturbed the physiological saddle-shape of the mitral annulus [11]. The increased maximum principal leaflet strains observed with these three rings are therefore consistent with engineering intuition quantified through the results of Salgo et al.. However, to our surprise, the supposedly physiologically shaped RSAR also led to an increase in maximum principal leaflet strains. Assuming that the shape of this ring is physiological it could be speculated that the dynamic motion of the mitral annulus rather than its 3-D shape is of major importance to preserve AML strain distribution. This hypothesis, however, is contrary to previous studies that suggested changes in the physiological mitral annular 3-D saddle shape lead to increases in leaflet strains [6]. It may therefore also be speculated that the shape of the RSAR does not fully represent the natural 3-D annular shape and that, as discussed earlier [6], increased strains are also a result of a non-physiological annular shape.

The partial, flexible band (COS) has been found to preserve the mitral annular saddle shape [11] and allow minimal mitral annular S-L dynamics (Figure 3, middle row) during the observed time period (from t_0 to t_n). However, COS significantly reduced mitral annular dimensions compared to the Controlstate (Table 3 and Ref [11]). Since COS did not affect AML strains (Figure 3, bottom row) we speculate that preserving physiologic mitral annular dynamics and shape rather than absolute mitral annular dimensions are the key components to maintaining a physiological strain distribution across the AML.

To our knowledge, Votta et al. were the only group that quantified the effects of annuloplasty rings (GeoForm and Physio) on mitral leaflet strains and stresses [4]. The group used a finite element model and demonstrated that the GeoForm, but not the Physio, reduced maximum principal mitral leaflet stresses during simulated functional mitral regurgitation [4]. In our study we found that all rigid rings (RSAR, PHYSIO, ETL and GEO) increased maximum principal AML strains, irrespective of their 3-D shape. However, unlike Votta et al., we used an *in vivo* model of the normal, beating heart. We therefore cannot comment on the potential effects of FMR/IMR rings in the diseased state and it is possible that these rings restore a physiological strain distribution in hearts with dilated LVs.

In our study we report the effect of different annuloplasty devices on radial and circumferential strains. While global ε_{rad} was only greater with RSAR, global ε_{cir} was greater with all rigid, complete rings (RSAR, PHYSIO, ETL and GEO, Table 4) compared to the Control state (however, insignificantly for GEO), suggesting that rigid, complete annuloplasty devices affect circumferential strains more than radial strains. The reason for the insignificant increase in global ε_{cir} observed with GEO could be a result of the larger commissure to commissure dimension of this ring compared to RSAR, PHYSIO or ETL [3], suggesting that the physiological circumferential AML strain distribution is sensitive to the amount of mitral annular C-C decrease.

Study Limitations

Several limitations should be addressed to allow a better interpretation of these data. First, the data were acquired from open-chest, anesthetized ovine hearts with normal preoperative anatomy. Considerable caution must therefore be exercised when extrapolating these findings to the human heart. This is especially true for the GeoForm and IMR ETLogix rings that have been designed for patients with IMR/FMR (with distorted annular, leaflet and ventricular geometry and function). As mentioned above, if these rings are implanted in the setting of FMR/IMR, it could well be that they reduce (or restore physiological) leaflet strains as demonstrated by Votta and colleagues in a computer simulation [4]. In future analyses we aim to use our experimental *in vivo* data to determine whether these two FMR/ IMR-specific rings (GEO and ETL) are more efficient than conventional rings in terms of reducing leaflet strains during acute myocardial ischemia. Second, AML strains were quantified for only the IVR phase of the cardiac cycle and it could be that the rings affect strain patterns differently in other phases of the cardiac cycle [20]. Third, although perturbed leaflet strains have been associated with impaired mitral valve repair durability [6, 7] currently no study exists that proves causation. Consequently, it remains to be determined whether perturbations in AML strains impair long-term function of the mitral valve after repair. Fourth, when radial and circumferential strains were plotted onto color mapped schematics (Figure 4), we did not only observe tensile, but also compressive strains in both Control states and with rings implanted (green and blue areas, Figure 4). Compressive strains do not occur, *e.g*., in purely computational models that use simplified AML shapes with the leaflet being entirely convex to the left ventricle [4] and, thus, may be a result of the complex AML shape [21] that was included in our analyses. The finding of compressive strains warrants further investigation; however, we focused on the tensile aspects of strain in this manuscript and did not perform detailed analyses of compressive strain patterns. Fifth, no statistically significant differences in strains were found between the different ring types. We therefore cannot draw any conclusions from these data whether one ring design is superior to another; however, this study was not adequately powered to demonstrate differences between the different ring types. Sixth, we only studied a partial, flexible band. Since no complete, flexible ring was examined in this experiment it is not possible to distinguish whether the observed lack of increase in AML strains with a partial band is due to its partial design, its flexibility, or due to a combination of the two. Lastly, strain patterns

Conclusions

In conclusion, regardless of their three-dimensional shape, rigid, complete annuloplasty rings (RSAR, PHYSIO, ETL, GEO), but not a partial flexible band (COS), increased maximum principal anterior mitral leaflet strains predominantly in the belly and edge regions in the normal beating ovine heart. Large, randomized, clinical trials are needed to answer the question whether the observed ring-induced alterations in mitral leaflet strain states exist in patients, and if so, whether they adversely affect long-term mitral valve repair durability.

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Fig 1.

A: Schematic illustrating ventricular and annular marker locations. Marker #20 represents the mitral annular saddle horn marker and markers #17 and #23 the anterior and posterior commissural markers, respectively. **B**: Schematic magnification of a top view of the mitral valve showing annular as well as leaflet markers. Sixteen markers were placed on the mitral annulus (#17-#32), 16 markers were placed on the anterior mitral leaflet (#1-#16) and one marker was placed on the free edge of the mid part of the posterior leaflet (#33). Inset shows the radial (rad) and circumferential (cir) directions used for strain definitions.

Fig 2.

Illustration of time point definitions. Time point t_n (strained state) was defined as maximum LV pressure for beat 1 (t_{n1}) and beat 2 (t_{n2}). Time point t_0 (reference state) was defined as last time frame before mitral leaflet separation (as represented by the rapid increase in plotted curve of distances (cm) between marker #33 and #4, see Fig 1) for beat 1 (t_{01}) and beat 2 (t_{02}) .

Fig 3.

Changes in LV pressure and volumes (ΔLVP and ΔLVV, respectively (top row), mitral annular dimensions (middle row) from reference state (t_0) to strained state (t_n) as well as global maximum principal (ε_{max}), radial (ε_{rad}) and circumferential (ε_{cir}) (bottom row). Note that changes from t_0 to t_n include a calculation from a time point later in the cardiac cycle (t₀) to an earlier time point of the cardiac cycle (t_n). COS=Edwards Cosgrove band, RSAR=St Jude Medical rigid saddle-shaped annuloplasty ring, ETL=Edwards IMR ETlogix, GEO=Edwards GeoForm. Values are mean±1SD.

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Fig 4.

Color-mapped schematics of maximum principal (ε_{max} , two top rows), radial (ε_{rad} , two middle rows₎ and circumferential (ε_{cir} , two bottom rows) strains across the entire anterior mitral leaflet for the Control state (CTRL) and with annuloplasty device implanted (RING). Markers #17 and #23 depict anterior and posterior commissures, respectively, marker #20 represents the mid-septal mitral annulus (saddle horn, see Figure 1). COS=Edwards Cosgrove band, RSAR=St Jude Medical rigid saddle-shaped annuloplasty ring, ETL=Edwards IMR ETlogix, GEO=Edwards GeoForm.

TABLE 1

Animal no Mean±1SD

 $Mean+ISD$

Heart rate (HR), LV end-diastolic volume (LVEDV) and dP/dt $_{\rm max}$ Heart rate (HR), LV end-diastolic volume (LVEDV) and $\text{dP/dt}_{\text{max}}$

Animal no

 $\begin{tabular}{c} \hline \textbf{1} & \textbf{1}$ $\frac{1}{4}$

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TABLE 2

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All values from individual animals are two beat averages, t_I=strained state (time point Ofference strain state (time point before mitral valve opening, see METHODS), COS=Edwards Cosgrove band, RSAR=St Jude Medical rigid All values from individual animals are two beat averages, _{In}=strainds are two basines are fund to and the point of the NGS-RAV (10=8. NETHODS), COS grove b annuloplasty ring, ETL= Edwards IMR ETlogix, GEO=Edwards GeoForm, SD=standard deviation

TABLE 3

Mitral annular septal-lateral (S-L) and commissure-commissure (C-C) dimensions at reference state (t0) and strained state (tn) Mitral annular septal-lateral (S-L) and commissure-commissure (C-C) dimensions at reference state (t0) and strained state (tn)

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rigid saddle-shaped All values from individual animals are in mm and two beat averages, t_h=strained state value of the point of maximum LVP), t0=reference strain state (time point before miral value opening, cosgrove band, RSAR=St Jude Medi annuloplasty ring, ETL= Edwards IMR ETlogix, GEO=Edwards GeoForm, SD=standard deviation annuloplasty ring, ETL= Edwards IMR ETlogix, GEO=Edwards GeoForm, SD=standard deviation

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TABLE 4

Global maximum principal (global $\varepsilon_{\rm max}$), radial (global $\varepsilon_{\rm rad}$) and circumferential (global $\varepsilon_{\rm cir}$) strains Global maximum principal (global εmax), radial (global εrad) and circumferential (global εcir) strains

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