

# Phase and absorption retrieval using incoherent X-ray sources

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X-ray phase contrast imaging has overcome the limitations of X-ray absorption imaging in many fields. Particular effort has been directed towards developing phase retrieval methods: These reveal quantitative information about a sample, which is a requirement for performing X-ray phase tomography, allows material identification and better distinction between tissue types, etc. Phase retrieval seems impossible with conventional X-ray sources due to their low spatial coherence. In the only previous example where conventional sources have been used, collimators were employed to produce spatially coherent secondary sources. We present a truly incoherent phase retrieval method, which removes the spatial coherence constraints and employs a conventional source without aperturing, collimation, or filtering. This is possible because our technique, based on the pixel edge illumination principle, is neither interferometric nor crystal based. Beams created by an X-ray mask to image the sample are smeared due to the incoherence of the source, yet we show that their displacements can still be measured accurately, obtaining strong phase contrast. Quantitative information is extracted from only two images rather than a sequence as required by several coherent methods. Our technique makes quantitative phase imaging and phase tomography possible in applications where exposure time and radiation dose are critical. The technique employs masks which are currently commercially available with linear dimensions in the tens of centimeters thus allowing for a large field of view. The technique works at high photon energy and thus promises to deliver much safer quantitative phase imaging and phase tomography in the future.

X-ray imaging | differential phase contrast

Phase imaging is particularly well suited to many applications where relevant features are poorly revealed by absorption radiography. Images of improved clarity and contrast are produced by making use of additional information encoded in photons that are not absorbed by the sample. In mammography, for example, phase imaging not only leads to improved delineation (1, 2) but also allows higher energy X-rays to be used thus leading to dose reduction (3). Image contrast due to phase variations reduces more slowly than absorption contrast as photon energy increases thus suggesting that X-ray radiography could in the future be performed with a significantly reduced radiation dose. The method we present here results in both quantitative phase and absorption images from only two images using a totally incoherent source without collimation or filtering. This advance makes the method available to a much wider range of laboratories and opens the way to new applications; in particular, not having to collimate or filter the source results in the full emitted flux being available for imaging, which makes the method accessible to a broader range of applications, especially where radiation dose and acquisition time are critical.

Image contrast in absorption radiography is formed by the absorption of X-rays. Such images are interpreted assuming that X-rays propagate along a straight line through the sample, i.e., they are not refracted. In quantitative phase imaging we, however, seek to quantify the refraction of X-rays as well as their attenuation. A number of quantitative techniques have been demonstrated but have, hitherto, required X-ray fields with high

spatial and/or temporal coherence. Although some of these techniques have been demonstrated with an incoherent source, in each case, the spatial and/or temporal coherence of the resulting light field is increased by filtering or aperturing. One method, known as analyzer-based imaging (ABI) develops contrast using the rocking curve of an analyzer crystal (4). Algorithms have been developed to separate phase and absorption information using a variety of approximations (5–7). The technique requires a highly parallel beam with high temporal coherence thus restricting it to synchrotron light sources or monochromated laboratory sources (8, 9). Another method for performing quantitative X-ray phase contrast imaging (XPCI) is by using in-line holography (10) combined with phase extraction algorithms (11, 12). This technique requires a source of very high spatial coherence thus limiting it to synchrotron sources or microfocal laboratory sources. The final method is known as grating interferometry, which employs two (13, 14) or three gratings (15–17) to produce a periodic set of fringes through the phenomenon of Talbot self-imaging. The phase shift and attenuation due to an object is thus sensed according to the relative shift and attenuation of the fringes by phase stepping an analyzer grating. This method requires a source, albeit a secondary source, of high spatial coherence thus necessitating the use of a source grating when laboratory sources are employed to create an array of mutually incoherent but individually coherent sources.

The quantitative technique presented in this paper makes use of the coded aperture XPCI (CAXPCI) system (18, 19). The technique thus employs an unfiltered and unapertured laboratory X-ray source, consequently achieving short exposure times (20) and operating at high photon energies (21). The technique requires a single beam to be incident upon a pixel edge as shown in Fig. 1. Note that this may be an actual pixel edge or an opaque edge positioned in front of a pixel. If a single beam is used, the entire object must be scanned through the beam to build up an image. Alternatively, several beams can be combined in a periodic array to image an entire object simultaneously. The width of the apertures makes the system relatively insensitive to misalignment and also scalable to large fields of view. This, however, does not come at the expense of reduced sensitivity due to the pixel edge illumination contrast mechanism (18).

Each CAXPCI beam is shaped by aperture  $A_1$  in Fig. 1 and each corresponding pixel edge is formed by aperture  $A_2$ . Although not always the case, the widths of the apertures (i.e.,  $W$  and  $P$ ) often obey the relationship  $P = W(z_{so} + z_{od})/z_{so}$ . In this case we say that  $W(z_{so} + z_{od})/z_{so}$  is the projected width of  $A_1$ . When a wide field CAXPCI system is employed the projected pitch of the two periodic apertures must match. Positioning

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Eq. 2 has been omitted for brevity only because the system is not sensitive to phase gradients in this direction. The signal detected by the pixel is found by integrating  $|U_0|^2$  over the region of the pixel left exposed by the aperture. We can now relax the assumption of a point source by assuming the uncorrelated source focal spot to have a Gaussian distribution. When this is the case the detector signals  $I_L$  and  $I_R$  configurations may be found as (22)

$$I_L = \int_{-\infty}^{\infty} K(x, -P/2) |U_0(x)|^2 dx, \quad [3]$$

$$I_R = \int_{-\infty}^{\infty} K(x, P/2) |U_0(x)|^2 dx, \quad [4]$$

where  $K(x, \Delta P)$  is the effective pixel function developed in ref. (22) and defined as

$$K(x, \Delta P) = \frac{1}{2} \left[ \operatorname{erf} \left( \frac{1}{\sigma} \frac{z_{so}}{z_{od}} (x - \Delta P + P/2) \right) - \operatorname{erf} \left( \frac{1}{\sigma} \frac{z_{so}}{z_{od}} (x - \Delta P - P/2) \right) \right], \quad [5]$$

where  $\sigma = FWHM/2/\sqrt{\log 2}$  and  $FWHM$  is the full width at half maximum of the source focal spot and  $\operatorname{erf}$  is the standard error function  $\operatorname{erf}(z) = 2/\sqrt{\pi} \int_0^z \exp(-t^2) dt$ . Note that the spatial coherence of the source is embodied in  $K$  rather than in the expression of X-ray intensity. If a polychromatic source were employed, the quantities  $I_L$  and  $I_R$  would be found by integrating over each monochromatic component weighted by the source spectrum and detector response. In this case the measured values of  $\phi'$  and  $\mu$  refer to values averaged over the spectrum and are thus denoted by  $\bar{\phi}'$  and  $\bar{\mu}$ , respectively.

In order to extract  $\phi'$  and  $\mu$  from measurements of  $I_L$  and  $I_R$  we must simplify (Eqs. 3 and 4). We start by defining the function

$$h : [-W/2, W/2] \rightarrow \mathbb{R} \quad \xi \mapsto z_{od} \phi'(\xi) + M\xi, \quad [6]$$

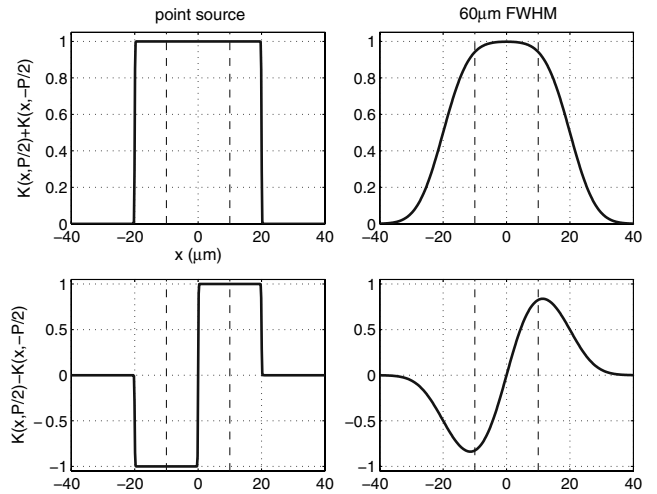
and substituting  $x = h(\xi)$  into (Eqs. 3 and 4), then after some manipulation we obtain expressions for  $I_L$  and  $I_R$  as

$$I_L = C \int_{-W/2}^{W/2} K(h(\xi), -P/2) \exp(-2k\mu(\xi)) d\xi, \quad [7]$$

$$I_R = C \int_{-W/2}^{W/2} K(h(\xi), P/2) \exp(-2k\mu(\xi)) d\xi, \quad [8]$$

where  $C$  is a constant. See the *SI Text* for a thorough derivation of Eqs. 7 and 8. This result is valid under either of two conditions. Either the signal arising from the interference of different terms in the summation of Eq. 2 can be neglected, or,  $g'(\xi, x) = 0$  has at most one solution for each  $x$ . The first condition holds when an incoherent source is used. The second condition holds also for the vast majority of resolvable samples encountered in practice given typical presample aperture sizes of between 15  $\mu\text{m}$  and 50  $\mu\text{m}$  although the apertures may be larger than this. We then form the sum and difference of  $I_L$  and  $I_R$  as

$$\begin{aligned} I_R + I_L &= C \int_{-W/2}^{W/2} [K(h(\xi), P/2) + K(h(\xi), -P/2)] \\ &\quad \times \exp(-2k\mu(\xi)) d\xi \\ I_R - I_L &= C \int_{-W/2}^{W/2} [K(h(\xi), P/2) - K(h(\xi), -P/2)] \\ &\quad \times \exp(-2k\mu(\xi)) d\xi. \end{aligned} \quad [9]$$



**Fig. 3.** Plots of the sum and difference of the  $K(x, \pm P/2)$  functions for a point source and a source with focal spot FWHM of 60  $\mu\text{m}$ . The broken lines indicate the position of the projected presample aperture.

Fig. 3 shows plots of the sum and difference of the  $K(x, \pm P/2)$  functions for a typical lab setup for both point sources and a source focal spot FWHM of 60  $\mu\text{m}$ . Values of  $z_{so} = 1.6$  m and  $z_{od} = 0.4$  m were used. By assuming that  $\phi'$  and  $\mu$  are approximately constant within the presample aperture we can write, to a good approximation:

$$I_R + I_L \approx CW \exp(-2k\mu), \quad [10]$$

where this result is exact in the case of a point source. In this case,  $I_R - I_L$  is easily evaluated as

$$I_R - I_L = 2C \frac{z_{od} \phi'}{M} \exp(-2k\mu). \quad [11]$$

In the case of an extended source, we expand  $\operatorname{erf}$  in a Taylor series about  $x = 0$  which allows us to obtain

$$I_R - I_L \approx 2CW \frac{z_{so} \phi'}{\sqrt{\pi} \sigma} \exp(-2k\mu), \quad [12]$$

which gives the following formulae for retrieving the differential phase (DP) image:

$$\bar{\phi}' = \begin{cases} \frac{\sigma \sqrt{\pi} I_R - I_L}{2z_{so} I_R + I_L} & \text{extended source} \\ \frac{P}{2z_{od}} \frac{I_R - I_L}{I_R + I_L} & \text{point source.} \end{cases} \quad [13]$$

where the overline has been included to emphasize the mean nature of the measured phase gradient when a polychromatic source is employed. It is interesting to note the similarity between Eq. 13 and those of Chapman et al. (4) who demonstrated phase and absorption retrieval using an analyzer crystal. We indeed took inspiration from this synchrotron method in developing our incoherent source method that is, nonetheless, based on a different sensing principle. One might note the possibility of an absorption gradient alone producing a potentially spurious phase gradient in Eq. 13. However, the subpixel images acquired by scanning the sample by a subpixel amount allow this phenomenon to be detected because each part of the sample is imaged by both the  $I_R$  and  $I_L$  configurations. Evaluation of Eq. 13 for  $I_R$  and  $I_L$  corresponding to the same part of the sample is compared to the standard evaluation thus revealing any potentially erroneous phase gradients. This phenomenon was not, however, detected in the presented results. One reason for this is that this effect is made practically negligible by the use of an extended source because it acts to average any absorption gradient as is shown

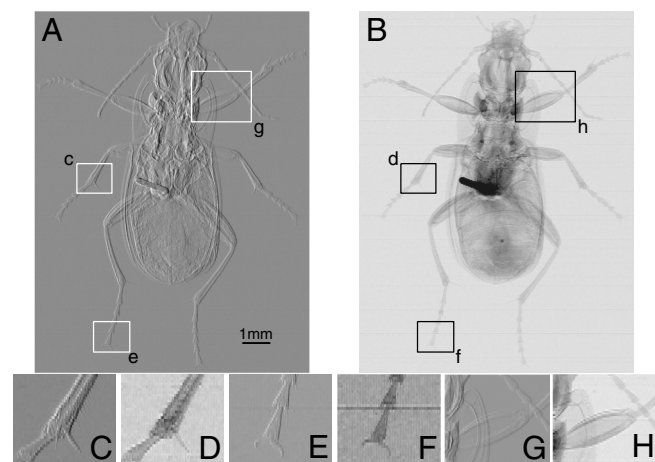


in the *SI Text*. The beams incident upon the detector aperture are approximately Gaussian, even when an absorption gradient is present. Yet, the entire beam is shifted due to a phase gradient and so phase sensitivity is not lost. In this case, only two images are required to retrieve sample phase and absorption. If, however, a point source is employed in the presence of strong absorption gradients it may be necessary to acquire more than two images. This is because we have developed a method to correct the measured phased gradient in the presence of strong absorption gradients as is also shown in the *SI Text*.

**Image of a Ground Beetle.** The very high sensitivity of the technique is demonstrated by images of a ground beetle in Fig. 4. These images were acquired using a Rigaku 007HF X-ray tube generator operated at 35 kVp/25 ma with a rotating Mo target. Theoretical calculation and experimental measurement confirmed the source FWHM as 60  $\mu\text{m}$ . A wide field CAXPCI setup was employed with an 85  $\mu\text{m}$  pixel size Anrad SMAM flat panel detector. Grating  $A_2$  had a pitch of 83.5  $\mu\text{m}$  and an opening of  $P = 20 \mu\text{m}$ .  $A_1$  had a pitch of 66.8  $\mu\text{m}$  and an opening of  $W = 12 \mu\text{m}$ . The gratings were manufactured by Creatv Microtech (Potomac, Maryland). Images were taken at eight subpixel positions to increase spatial resolution.

The DP image is in general sharper and reveals substantially more detail than the absorption image. Many fibrils visible in the DP image are invisible in the absorption image. Nearly all details are better defined in the differential phase (DP) image than the absorption image. The crucial aspect of the images in Fig. 4 is that details are present in the DP image that are significantly smaller than  $P$  and the grating pitch, thus demonstrating what we know from theory, that the method's sensitivity is indeed not constrained by either of these quantities.

**Phantom Images.** We also performed phantom measurements using a number of filaments described in the caption of Fig. 2 to verify the accuracy of the technique. The first set of images were acquired using the same system as that used to image the ground beetle with the exception that a presample aperture,  $A_1$ , of pitch 134  $\mu\text{m}$  and  $W = 16 \mu\text{m}$  was used to reduce the effect of



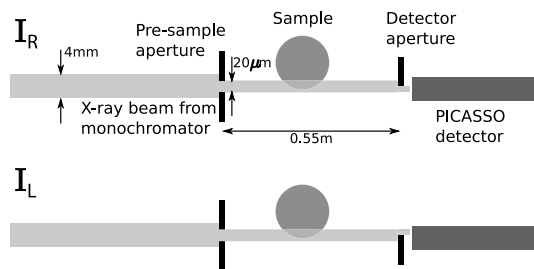
**Fig. 4.** Differential phase and absorption images of a ground beetle. (A) The DP image ( $\phi'$ ) for a ground beetle. (B) The absorption image ( $\exp(-2k\mu)$ ) of the ground beetle. The smaller images along the lower part of the figure are blown up versions of the boxed regions in A and B. In both cases the image contrast has been saturated slightly to enhance the visibility. Note also that the highly absorbing region near the center of the beetle is a metal pin. (C and D) Small hairs attached to the leg are visible on the DP contrast image (C), yet completely invisible in the absorption image (D). Other fine details are much better defined in the DP image. (E and F) Structure and fine details are much better resolved in the DP image (E). (G and H) Internal structure of over laying features are much better defined in the DP image (G).

pixel spillover on the acquired images (23). This means that every second column of pixels was ignored. Subsequently, 16 subpixel images are required to obtain the same spatial resolution as the image of the ground beetle.

The phantom images reveal a number of important properties of the technique. Firstly, DP images can be obtained for highly as well as weakly absorbing materials. For example, the raw profiles of the titanium filament in Fig. 2C show very little phase contrast yet an accurate phase profile is still extracted. Further, accurate DP profiles are also obtained for the polyetheretherketone (PEEK) filaments that are weakly absorbing. The use of a polychromatic source makes it difficult to quantitatively verify the experimental results as is the case for most polychromatic imaging techniques. The concept of effective energy has been used previously (15), however, this is an unreliable approach for broad spectra because a given spectrum will result in different effective energies for samples of different thickness and/or composition. This problem is shared by all polychromatic imaging techniques, such as X-ray computed tomography (24), for example. We have, however, plotted the extracted DP profile for titanium along with the theoretical profile calculated using the effective energy, taking into account the distribution of  $\delta(E)$  and  $\beta(E)$  for titanium, the estimated source spectrum and a filament of 125  $\mu\text{m}$  nominal radius. This demonstrates agreement between theory and experiment and, in particular, that accurate phase retrieval may be performed with spatially incoherent sources.

The comparison between extracted and theoretical DP is, however, much clearer when a near-monochromatic source is used. This is why we also made measurements of the same filaments using the SYNchrotron Radiation for MEDical Physics bending magnet beam line of the Elettra synchrotron radiation facility in Trieste, Italy. The beamline is described in more detail elsewhere (25, 26); we give here only the details relevant to the experiment. The sample stage was located, in the experimental room, approximately 20 m from the apparent X-ray source, which has a dimension of  $0.280 \times 0.080 \text{ mm}^2$ . This results in a usable beam of dimension approximately  $120 \times 4 \text{ mm}^2$ . A channel-cut Si (1,1,1) crystal monochromatizes the beam to nominal photon energy 20 keV with a fractional bandwidth of 0.2%. The DP image is extracted using the point source alternative in Eq. 13 and the experimental setup was quite different to that used in the laboratory as shown in Fig. 5. A single pair of slits was used to shape a beam 20  $\mu\text{m}$  high and 120 mm wide. A single edge was placed in front of the detector to obtain the  $I_L$  and  $I_R$  images. A photon counting, linear array silicon microstrip detector known as PICASSO was employed (27). The detector works in the so-called “edge-on” configuration and provides an array of 2,368 pixels 50  $\mu\text{m}$  wide and 300  $\mu\text{m}$  high. An important property of the PICASSO detector is that it exhibits negligible pixel cross-talk between pixels. In this setup the image must be scanned through the beam to acquire an image.

We present DP images of PEEK and Ti filaments in Fig. 2F as these are the lowest and highest absorbing filaments, respectively,



**Fig. 5.** Synchrotron experimental setup. The beam extends 120 mm into the page and an image is generated by scanning the object vertically through the beam. The diagram is not to scale.

imaged using the laboratory setup. The refractive index of PEEK and Ti were obtained from ref. (28) as  $\delta = 7.15 \times 10^{-7}$ ,  $\beta = 2.74 \times 10^{-10}$ , and  $\delta = 21.9 \times 10^{-7}$ ,  $\beta = 346 \times 10^{-10}$ , respectively, at photon energy 20 keV. The plots show an excellent agreement between experiment and theory in both cases.

## Discussion

It is important to clarify what we mean by an incoherent source. Coherence can be formally defined using the theory of coherence (29), however, this is not necessary for our purposes. For practical purposes, spatial coherence is characterized completely by the focal spot size and temporal coherence by the spectral width of the source. We say that our method is incoherent because the transverse coherence length ( $z_{so}\bar{\lambda}/\text{FWHM}$ ), where  $\bar{\lambda}$  is the mean wavelength and FWHM is that of the source focal spot, is of the order of  $1 \mu\text{m}$  at the presample aperture (30). Yet, the presample aperture pitch and opening are at least an order of magnitude greater than this and so spatial coherence impacts negligibly on image formation. The main limitation on focal spot size is that the projected focal spot size should not exceed  $P$ . Thus, the focal spot FWHM should satisfy  $\text{FWHM} < Pz_{so}/z_{od}$ . For the laboratory setup this required  $\text{FWHM} < 80 \mu\text{m}$ . This is to ensure that the majority of photons not absorbed by the sample are recorded in  $I_L$  or  $I_R$ . The limit on source spectral width is set purely by the thickness of the apertures as these need to remain strongly absorbing. CAXPCI still works if the apertures are partially absorbing (21), however, the accuracy of the quantitative phase and absorption information is compromised. Because the technique doesn't depend upon interference there are no source spectral width limitations, in fact, a broad spectrum eliminates artifacts from the images that could appear due to diffraction by the presample aperture if a monochromatic source were employed. Thus, the quantitative CAXPCI method requires neither spatial nor temporal coherence thus allowing conventional laboratory source without aperturing or filtering to be used. A further strength of the method is its ability to be constructed from commercially available sources and detectors. The apertures, being relatively coarse, are able to be produced to enable imaging over a large field of view. There has, however, been a perception that imaging using coarse gratings to achieve a large field of view comes at the expense of sensitivity and spatial resolution. Fortunately this is not the case as demonstrated in Figs. 2 and 4. Conventionally, the spatial resolution of X-ray imaging systems is determined by the pixel size as is indeed the case with CAXPCI. However, as the detector aperture effectively redefines the

pixel size we can achieve higher spatial resolution by dithering or scanning the object by subpixel increments. The final image may be reconstructed without the need for a deconvolution step. The sensitivity of the technique is not compromised either because the edge illumination principle (18) is the key to contrast generation—a subtly different mechanism to that employed in grating interferometry.

Another advantage of using relatively coarse apertures is insensitivity to misalignment of the apertures. We have developed an automated system that allows the apertures to be aligned to within precision of the stages to align the apertures. We have found that the factor which limits the quality of the alignment is in fact defects in the manufacture of the mask.

## Conclusion

We have presented a means of performing quantitative DP imaging using commercially available X-ray tube generators and detectors. We believe this is a unique example of where quantitative X-ray phase imaging has been performed with an unapertured and unfiltered incoherent source. Only two raw images are required thus making the technique compatible with applications where acquisition time and radiation dose are critical. The technique thus also paves the way for X-ray phase tomography, compatible with applications outside of specialized laboratories. The pitch of the apertures is sufficiently large to allow an alignment tolerance consistent with use outside the laboratory. Furthermore, the field of view of the system may be increased easily as masks with linear dimensions in the tens of centimeters are already commercially available. This would enable the system to fully utilize the field of view of detectors currently used clinically and industrially. We have also shown that even though we employ a nonmicrofocal, unapertured and unfiltered X-ray tube generator with large-scale apertures, we still achieve high DP sensitivity and spatial resolution. It is thus reasonable to suggest that the quantitative technique could in the future lead to much safer quantitative X-ray phase medical imaging.

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