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## Transitioning Streaming to Trapping in DC Insulator-based Dielectrophoresis for Biomolecules

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### Abstract

Exploiting dielectrophoresis (DEP) to concentrate and separate biomolecules has recently shown large potential as a microscale bioanalytical tool. Such efforts however require tailored devices and knowledge of all interplaying transport mechanisms competing with dielectrophoresis (DEP). Specifically, a strong DEP contribution to the overall transport mechanism is necessary to exploit DEP of biomolecules for analytical applications such as separation and fractionation. Here, we present improved microfluidic devices combining optical lithography and focused ion beam milling (FIBM) for the manipulation of DNA and proteins using insulator-based dielectrophoresis (iDEP) and direct current (DC) electric fields. Experiments were performed on an elastomer platform forming the iDEP microfluidic device with integrated nanoposts and nanopost arrays. Microscale and nanoscale iDEP was studied for  $\lambda$ -DNA (48.5 kbp) and the protein bovine serum albumin (BSA). Numerical simulations were adapted to the various tested geometries revealing excellent qualitative agreement with experimental observations for streaming and trapping DEP. Both the experimental and simulation results indicate that DC iDEP trapping for  $\lambda$ -DNA occurs with tailored nanoposts fabricated via FIBM. Moreover, streaming iDEP concentration of BSA is improved with integrated nanopost arrays by a factor of 45 compared to microfabricated arrays.

### Keywords

dielectrophoresis; DNA; protein; numerical simulation; trapping condition

## 1. Introduction

Manipulating biomolecules in homogeneous and inhomogeneous fields builds the basis of a variety of analytical separation techniques [1]. Inhomogeneous fields form the basis of gradient techniques, which can be based e.g. on magnetic, electric thermal or centrifugal forces [1,2,3]. Among the gradient techniques, dielectrophoresis (DEP) occurs in an electric field gradient while forces acting on a dipole result in migration upwards or downwards an electric field gradient. This migration phenomenon has recently attracted interest for the application to biomolecules, such as DNA [4,5] and proteins [6,7]. Acting as the dominating force, DEP can be applied for trapping [8,9,10], whereas overlaid with transport mechanisms such as hydrodynamic flow or electroosmotic flow (EOF), DEP can also be employed for separation, sorting and streaming concentration [11,12,13]. Knowledge of all

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transport mechanisms as well as experimental methods to develop suitable microfluidic devices are required to exploit DEP for biomolecules as a routine tool in analytical applications. In this contribution, we investigate micro- and nano-environments to improve our understanding of factors influencing streaming and trapping DEP for DNA and proteins.

The selectivity of DEP is based on the polarizability of biomolecules in a non-uniform electric field. The theoretical basis of DEP for large bio-particles such as cells and the scaling behavior for nanoparticles is well understood [14]. DEP manipulation of bio-particles in the nm scale is challenging since high electric fields are required to achieve sufficiently large forces for DEP trapping competing with diffusion [15] and dissipative electro-thermal forces [16]. Nonetheless, examples for biomolecule manipulation employing DEP have been demonstrated in the past. The first attempts reach back to the work of Washizu [17]. Further improvements demonstrated DEP manipulation with DNA and proteins [5,6,18]. Examples for DNA manipulation by DEP reach from Mbp down to ~40bp [12,16,19,20,21,22,23,24], whereas protein manipulation by DEP has only recently been explored [15,25,26,27,28,29,30,31].

Several experimental approaches have been proposed to create inhomogeneous electric field gradients evoking DEP while realized in microfluidic devices in the majority of cases [32]. Patterned microelectrodes achieve inhomogeneous field gradients, which can be integrated into microfluidic environments [32,33]. Integrating microelectrodes involves disadvantages, such as electrode reactions occurring in the DEP manipulation regions and field gradients localized around the microelectrodes [34,35]. 3-Dimensional glassy-carbon electrodes provide an alternative, as they allow electric fields gradients to be applied homogeneously throughout the entire microchannel depth [36]. Recent advances in the field of DEP have resulted in new approaches for characterizing the behavior of particles using direct current (DC) electric fields. In such approaches, spatial non-uniformities are created by embedding insulating obstacles in the channel to create non-uniform electric field gradients, which was demonstrated for the first time by Lapizco-Encinas et al. [37]. This emerging field of DEP is a 3D system commonly termed DC insulator-based dielectrophoresis (DC-iDEP) or simply insulator-based dielectrophoresis (iDEP). This technique provides several advantages over the traditional AC DEP approaches [30,37]. Insulators are less prone to fouling; that is, they generally retain their function despite surface changes. Further, insulators are robust and chemically inert compared to metallic electrodes avoiding undesired reactions at their surface. Depending on the material of the microfluidic device, electroosmotic flow (EOF) can be used for transporting analyte into the channel thus eliminating external pumps. Furthermore, the fabrication of iDEP devices is simpler as no metal deposition steps are required compared to the electrode based DEP devices. A variety of designs have been proposed and tested to create non uniform electric fields using either single insulating obstacles such as a rectangular posts [38,39,40,41], a triangular hurdle [40], a constriction in the depth of the channel [42], a single microchannel constriction [43], multiple insulating obstacles like insulating post [26,37,44], multiple rectangular blocks [45] or silica microbeads [46]. In addition, modified channel geometries were employed to achieve particle sorting or trapping such as aligned teeth [47], sawtooth channels [48], open-top microstructures [49] or serpentine microchannels [50].

iDEP has been used by several groups [30] including us [12,19,26] to manipulate biomolecules. Exploiting iDEP for separation, pre-concentration or fractionation is particularly favorable in these devices, as the necessary electric field gradients are homogeneous throughout the entire depth of a microchannel. DC-iDEP techniques however result in strong electrokinetic forces and interfere with DEP. Electrokinetic forces result from charged biomolecules, which are consequently transported by electrophoresis (EP). Moreover, EOF arises in the majority of microfluidic environments additionally acting as a

bulk transport mechanism. As a result of electrokinesis, different transport regimes arise in iDEP [13,37]. First, if the DEP component is the dominating transport mechanism, the so-called trapping regime is reached. Molecules transported in the iDEP device are immobilized or trapped at specific locations in the microdevice. This regime is however difficult to achieve for small biomolecules, as large electric field gradients are necessary to evoke strong DEP forces over electrokinetic transport. The second regime refers to streaming DEP, where DEP still influences the transport mechanism. However, electrokinesis is dominating and trapping regions immobilizing particles are now replaced by regions of preferred streaming. This regime results in areas of streaming regions with increased concentration throughout a micropost array. For example, this streaming DEP behavior has recently been demonstrated for a 150 kDa and a 60 kDa protein in a DC iDEP device exhibiting a micropost array [26]. Hence, conditions in which DEP is preferably occurring for biomolecules, i.e. a trapping regime is apparent, are yet to be accomplished in DC iDEP and are important for exploiting DEP in analytical applications for biomolecules.

To achieve larger DEP contribution in DC iDEP, our approach involves the enhancement of electric field gradients to favor DC-iDEP over electrokinetic forces based on a combination of micro- and nanofabrication. It relies on replica molding of a nanostructured device, the master piece, transferring the nanostructure from the negative relief to the elastomeric material. This method is commonly termed soft lithography, and has been applied in similar approaches [51,52,53]. Here, we base the optimization of the master piece on the combination of standard photolithography techniques with focused ion beam milling (FIBM). Etching by FIBM is used for direct (mask free) processing of micro- and nanostructures [54]. However, FIBM has traditionally not been used for insulating substrates. A major problem in ion etching technology is related to the difficulty of calculating and selecting ion beam parameters for obtaining a preset surface geometry, especially in the case of dielectric targets with complex compositions [55,56]. Here, however, we present micro- and nanostructured patterns on SU-8 photoresist combining optical lithography and FIBM serving as the master piece to mold microfluidic devices for DEP manipulation of biomolecules. This approach thus builds on our previously developed iDEP devices obtained from optical lithography. The resulting microfluidic device has feature sizes of  $<1 \mu\text{m}$  well below the feature sizes reported by Shafiee et al. [57] realized in conjunction with deep reactive ion etching, and does not involve tedious multiple process steps such as those developed by Yamahata et. al. [58], Iliescu et. al. [59] and Liao et. al. [31].

With this novel approach, we investigate DC-iDEP for  $\lambda$ -DNA and the protein bovine serum albumin (BSA). We base this study on our previous work in which DC-iDEP streaming of proteins has been observed in an array of triangular microposts [26]. The integration of nanoposts and arrays thereof in the triangular iDEP device geometry was investigated to reveal the improvement in iDEP streaming concentration for DNA eventually leading to DC-iDEP trapping. For BSA, improved streaming concentration was observed. Theoretical considerations using a convection-diffusion model were in excellent agreement with our experimental study for DNA and confirm DC-iDEP trapping in distinct geometries.

## 2. Theory

Dielectrophoresis (DEP) is the migration of polarizable particles under the influence of an inhomogeneous electric field. Depending on the conductivity of the particle and the surrounding medium, the particle can move towards high electric field gradients, known as positive DEP, or away from regions of high electric field gradients as in negative DEP [14,60].

For DC voltages, the DEP force competes with electrokinetic forces in addition to diffusion. Our goal is to employ numerical simulations considering a convection-diffusion model to optimize the microfluidic channel geometries in DC-iDEP and thereby augmenting the dielectrophoretic component of biomolecule transport. For numerical simulations and as below investigated experimentally, we consider a large DNA molecule, namely  $\lambda$ -DNA (48.5 kbp), and the protein BSA.

The flux of particles,  $\vec{J}$ , in a microfluidic channel at steady state  $\left(\frac{\partial c}{\partial t}=0\right)$  according to our convection-diffusion model is defined as:

$$\vec{J} = -D\nabla c + c[\vec{u}_{EK} + \vec{u}_{DEP}] \quad (1)$$

where  $c$  is the concentration of the particles,  $\vec{u}_{EK}$  is the electrokinetic velocity and  $\vec{u}_{DEP}$  is the DEP velocity.  $D$  is the diffusion coefficient, which values  $6.8 \times 10^{-13} \text{ m}^2/\text{s}$  [19] and  $6.1 \times 10^{-11} \text{ m}^2/\text{s}$  [61] for  $\lambda$ -DNA and BSA, respectively.

The combined electrokinetic velocity results from EOF and electrophoresis as follows:

$$\vec{u}_{EK} = \mu_{EK} \vec{E} = (\mu_{EOF} + \mu_{DEP}) \vec{E} \quad (2)$$

Here,  $\mu_{EOF}$  is the electroosmotic mobility,  $\mu_{EP}$  the electrophoretic mobility and  $\vec{E}$  the electric field. The electroosmotic mobility in the employed microchannels in a dynamic or a static coating procedure of the tri-block-copolymer F108 has been determined to be  $0.53 \times 10^{-8} \text{ m}^2/\text{Vs}$  [62] and  $1.5 \times 10^{-8} \text{ m}^2/\text{Vs}$  [63], respectively. We note that the static coating procedure was employed for proteins, whereas the dynamic coating procedure was used for DNA. The electrophoretic mobility of  $\lambda$ -DNA (48.5 kbp) was previously determined as  $-3.5 \times 10^{-8} \text{ m}^2/\text{Vs}$  [12]. In the case of BSA, we consider that  $\mu_{EP}$  is considerably smaller than  $\mu_{EOF}$  and of opposite sign. This is reasoned because our experimental observations reflected a strong cathodic EOF, confirming that electrophoresis counteracts electroosmosis only to a marginal extent. Therefore, we conducted simulations using an overall electrokinetic mobility of  $-3.0 \times 10^{-8} \text{ m}^2/\text{Vs}$  for  $\lambda$ -DNA and  $1.5 \times 10^{-8} \text{ m}^2/\text{Vs}$  for BSA considering only  $\mu_{EOF}$  contribution in equation (2).

The DEP velocity results from the equilibrium of DEP and drag forces and is described as [14,60]:

$$\vec{u}_{DEP} = \mu_{DEP} \nabla E^2 \quad (3)$$

where  $\mu_{DEP}$  is the dielectrophoretic mobility. This  $\mu_{DEP}$  is the ratio of a particle's polarizability,  $\alpha$ , and its friction coefficient,  $f$  with  $\mu_{DEP} = \frac{\alpha}{f}$  [14]. Using the Einstein relation, we can determine the friction coefficient [64]:

$$f = \frac{kT}{D} \quad (4)$$

where  $k$  is the Boltzmann constant and  $T$  the temperature. Thus, one can obtain  $\mu_{DEP}$  for a biomolecule from known  $\alpha$  and  $f$ . For a  $\lambda$ -DNA molecule,  $\alpha$  amounts in  $3.10 \times 10^{-29} \text{ F/m}^2$  as previously reported by Regtmeier et al. [19]. Therefore, we calculate a positive  $\mu_{DEP}$  for  $\lambda$ -DNA of  $2.61 \times 10^{-21} \text{ m}^4/\text{sV}^2$  with the diffusion coefficient for  $\lambda$ -DNA as noted above. For

the case of BSA, we assume a positive  $\mu_{DEP}$  of  $8.6 \times 10^{-24} \text{ m}^4/\text{sV}^2$  as employed in our previous study [26].

Using COMSOL 4.2a software, we solve equation (1) at steady state. This model is useful to predict the concentration profile along a channel when the electrokinesis dominates over DEP, which is known as streaming behavior [13,30]. However, under trapping conditions

where DEP forces dominate over electrokinesis, accumulation arises and  $\frac{\partial c}{\partial t} \neq 0$  [65]. Thus, under accumulation conditions, the steady-state condition via the convection-diffusion model cannot be found. Hence, we analyze the condition of trapping by calculating the electric field and  $\nabla E^2$  in our microfluidic channel as previously described [66,67,68]. In the case of trapping, the particle migration is strongly governed by DEP and the direction of the flux perpendicular to  $\vec{E}$  is null. It follows:

$$\vec{J} \cdot \vec{E} = 0 \quad (5)$$

Substituting for  $\vec{J}$  and omitting the diffusion term we write:

$$c[\mu_{EK} \vec{E} + \mu_{DEP} \nabla E^2] \cdot \vec{E} = 0 \quad (6)$$

and

$$-\frac{\mu_{DEP} \nabla E^2}{\mu_{EK} E^2} \cdot \vec{E} = 1 \quad (7)$$

Equation (7) is useful to determine the trapping condition, i.e. the situation in which DEP dominates and accumulation is observed. When  $\mu_{DEP} / \mu_{EK} < 0$ , the condition of trapping is defined as:

$$\frac{\mu_{DEP} \nabla E^2}{\mu_{EK} E^2} \cdot \vec{E} > 1 \quad (8)$$

Thus, from numerical simulations, we would expect the DEP trapping to occur when this condition is satisfied in a specific microfluidic design in the case of  $\lambda$ -DNA. If equation (8) reveals values smaller than unity, DEP streaming behavior is apparent. Consequently, when equation (8) is satisfied in a specific design, we plot these values for a nanostructured design. If however streaming DEP is predicted from numerical simulations for a specific nanostructured design, we further compute the concentration distribution obtained by solving equation (1) in the steady-state.

We explore different geometries varying in shape and dimensions as shown in Figure 1-b. Triangular microposts as shown in Figure 1a-c are fabricated by optical lithography. Using FIBM, we fabricate three different nanopost geometries in between the posts: a single circular post, an array of circular posts and a rectangular post, as shown in Figure 1-b.

### 3. Materials and Methods

#### 3.1 Chemicals

Double-stranded 48.5kbp  $\lambda$ -phage DNA was obtained from Fermentas Inc. Alexa Fluor 488 labeled BSA and YOYO-1 iodide (excitation maximum 491 / emission maximum 509 nm)

was acquired from Invitrogen (NY, USA).  $\text{Na}_2\text{HPO}_4$ ,  $\text{KH}_2\text{PO}_4$ , poly(ethyleneglycol)-block-poly(propyleneglycol)-block-poly(ethylene glycol) (Pluronic F108) and 3-[(3-cholamidopropyl)dimethylammonio]-1-propanesulfonate (CHAPS) were purchased from Sigma-Aldrich. Deionized water (Millipore, USA) was used for all buffers. Sylgard 184, composed of the silicone elastomer base and the curing agent for poly(dimethylsiloxane) (PDMS), was purchased from KR Anderson (AZ, USA). The negative photoresist SU-8 2007 and the developer were obtained from Microchem.

### 3.2 Device Fabrication

A schematic of the microfluidic device is shown in Figure 1-a. All channels were 2  $\mu\text{m}$  high, 100  $\mu\text{m}$  wide and 1 cm long. A combination of photolithography and FIBM was used to fabricate a master, from which a PDMS mold was formed. First, the master relief of SU-8 photoresist (2 $\mu\text{m}$  thickness) was patterned via photolithography on a silicon wafer using standard photolithography. This wafer was coated with a 20nm Cr layer using Cressington 308R Evaporator (Ted Pella, Inc., USA). After that, FIBM was used to mill the nanostructures as shown in Figure 1-b with a Nova 200 (FEI Company, USA). A current of 3 nA was used to mill the patterns. Characteristic dimensions of resulting posts are listed in Table 1 and defined in Figure 1-b. From this master wafer, a PDMS mold was formed resulting in channel cross sections of 2 $\mu\text{m}$   $\times$  100  $\mu\text{m}$ . Figure 1 c–d shows scanning electron microscopy images of the obtained master wafer and the resultant PDMS nano-posts respectively. Reservoir holes with a diameter of 2mm were punched at corresponding positions in the PDMS mold. Finally, the micro/nano structured PDMS mold was  $\text{O}_2$ -plasma activated under vacuum (PDC-001 Harrick Plasma, Harrick, USA). Simultaneously, a cleaned glass slide was treated with  $\text{O}_2$ -plasma under similar conditions. The glass slide and PDMS mold were assembled directly after plasma activation.

### 3.3 Dielectrophoresis Experiments

Phosphate buffer (10 mM) was diluted with water to obtain a conductivity of 0.01 S/m resulting in pH=8.1. Before the experiment, PDMS channels and reservoirs were filled with 250 $\mu\text{M}$  F108 in phosphate buffer at 0.01 S/m for 10min under a low potential of 100 V. Next, 40pM  $\lambda$ -DNA in phosphate buffer containing YOYO-1 in a base pair ratio of 1:10 was added to one of the reservoirs. Potentials of 1500 V and 3000 V were employed to manipulate DNA by DEP.

Fluorescently labeled BSA was used in the same buffer as  $\lambda$ -DNA. However, the coating strategy was different. The channel was filled with 250 $\mu\text{M}$  F108 in buffer solution and incubated over night. Subsequently, the buffer was exchanged with a solution of 3mg/mL of CHAPS. Next, 7 nM BSA was added in one of the reservoirs and a potential of 1500 V was applied to manipulate BSA by DEP.

The DEP behavior of labeled DNA and BSA was observed by fluorescence microscopy on an inverted fluorescence microscope (IX 71, Olympus, USA) with filter sets for YOYO-1 and Alexa Fluor 488 fluorescence and a 60 $\times$  objective (LUC Plan, Olympus, US). Fluorescence intensity was recorded with a CCD-Camera (Quantum 512SC, Photometrics, USA) at 100 ms exposure time. Image J software (version 1.43) was used for the data analysis. We analyzed the increase of intensities at either streamline or trapping areas at which biomolecules concentrated as obtained from the recorded images with the concentration factor R, which is given in equation 9:

$$R = \frac{I_M - I_{\text{PDMS}}}{I_C - I_{\text{PDMS}}} \quad (9)$$

where  $I_M$  refers to the maximum intensity for either streamline or trapping areas at applied potential,  $I_{PDMS}$  to the background intensity of PDMS outside the channel and  $I_C$  to the intensity of the channel filled with analyte prior to the application of potential.

#### 4. Results and Discussion

Three different geometries were used as schematically depicted in Figure 1-b to improve DC-iDEP concentration of DNA and proteins. We base this study on our previous work in which streaming DEP with proteins has been demonstrated. Hence, we use a well-characterized triangular micro-post array and study the improvement of iDEP with the integration of nanoposts by FIBM. We report the fluorescence distribution from the experimental work using the combined micro- and nanostructured device, reflecting the DNA and protein concentration, as well as the concentration profile obtained by numerical simulations using the above described convection-diffusion model.

Figure 2 summarizes the experimental and numerical simulation studies for  $\lambda$ -DNA. In the case of triangular microstructures (no nanoposts), experimental results reveal streaming DEP along the triangular posts at 3000 V as shown in Figure 2-a. This streaming behavior for microposts leads to an increase in DNA concentration in regions close to the center of the microposts and can be assigned to biomolecules exhibiting positive DEP [26]. We thus refer to positive streaming behavior along the micro and nanopost arrays. This behavior is in accordance with previous simulations for streaming in the case of positive biomolecule DEP and observed positive DEP for similar buffer ionic strength and pH [12,19]. Note that negative streaming DEP would deplete regions that are concentrated in positive streaming DEP [26].

Similar results were observed when a single circular post is included in between the triangular posts, as shown in Figure 2-b, where streaming behavior is maintained. The DNA iDEP streaming behavior further changed significantly for integrated nano arrays of circular posts and an integrated rectangular post as demonstrated in Figures 2-c and d. In these two geometries, the characteristic profile of streaming DEP reduces significantly. We attribute this change to a transition from streaming to trapping DEP in the nanopost regions, as apparent in Figure 2-c, caused by larger DEP forces. Figure 2-c shows an even larger concentration around the nanopost, suggesting even stronger iDEP trapping. It is noteworthy that DEP trapping behavior was achieved for both the nanopost array and the rectangular nanopost geometry at half the electric field applied in comparison to Figure 2a (microposts only). Therefore, we note that trapping conditions were obtained at lower applied potentials through the integration of the nanoposts.

Table 2 summarizes the experimentally obtained concentration factor  $R$  as well as numerically calculated maximum  $\nabla E^2$  values for the studied geometries. As shown in Table 2, a  $\sim 1.3$ -fold increase of fluorescence intensity is observed with the circular nano post compared to the triangular microposts, indicating an improvement of DNA streaming concentration. In the case of the circular nanopost array, the fluorescence intensity is further enhanced at the regions of the nanoposts by  $\sim 5$ -fold. This is augmented to  $\sim 30$ -fold for the rectangular case.

To further characterize this nanostructure-dependent DEP behavior, we carried out numerical simulations to reveal the acting  $\nabla E^2$  (see Table 2) and concentration distribution in the iDEP channel solving equation (1), for cases in which the trapping condition (8) was not satisfied. Figure 1-e shows the  $\nabla E^2$  exemplarity for rectangular nanopost. Note that the highest gradients are in between the triangular posts and the corners of the rectangular nanopost which is similar to the other nanopost geometries. Figures 2-(e-g) show the

concentration profiles at steady-state for the case of  $\lambda$ -DNA and varying geometry. For triangular posts, we observe that our simulations match qualitatively well with our experimental results. They reflect the regions of streaming concentration obtained in experiments and show the concentration enhancement accordingly.

Next, we compare the experimental results for the single circular post compared to the numerical simulation. From Table 2, we calculate an enhancement of  $\nabla E^2$  by 77% at 1500 V compared to the triangular microarrays, indicating a larger DEP force. Moreover, Figure 2-f shows a change in the position of the concentration profile, which is also observed experimentally in Figure 2-b. Although the streaming regime is maintained similarly to the case of triangular microposts, the concentration distribution is now located not only along the triangular posts but also around the single circular post. Numerical simulations reflect this effect demonstrating concentration along the microposts but also along the circular post (Figure 2-f).

In the case of the circular nanopost array, simulation results suggest that streaming behavior is still apparent but the shift of largest concentration to the nanopost regions is more pronounced (Figure 2-g). Table 2 also shows a higher  $\nabla E^2$  value; hence, we attribute a larger DEP component to this nanopost array geometry even though streaming DEP is still dominating in simulations. However, experimental results (Figure 2-c) indicate DEP trapping at 1500 V. This discrepancy between simulation and experimental work may arise from irregularities in the FIBM process as well as from interactions of DNA molecules with posts or entanglement of DNA molecules at the nanopost regions that are not captured by simulations.

We further analyze the case of the rectangular nanopost. In this case, we plot the trapping regions according to equation (7) (see Figure 2-h) since equation (1) cannot be solved for the steady-state to obtain the concentration distribution. In Figure 2-h, the areas in which trapping occurs are represented by red colors (i.e. equation (8) is valid). Although this region is a very localized on a length scale of 100 nm, we suspect this area is sufficient to trap DNA molecules with persistence lengths of 50 nm [69,70]. Note that the experimentally observed trapping regions are much larger which we attribute to the molecular extension of the large  $\lambda$ -DNA molecules. Moreover, the rectangular nanopost increases the maximum  $\nabla E^2$  by  $\sim 2.5$  orders of magnitude (see Table 2), confirming largely augmented DEP forces. Our detailed study thus reveals conditions under which larger DNA molecules can be trapped by DC-iDEP.

Finally, we investigated the improvement of iDEP-based concentration for proteins. Experimentally, we employed the protein BSA and compared to numerical simulations with adapted parameters (see theory section). Figure 3-a presents the iDEP streaming concentration of BSA, obtained with the nanopost array. We note that iDEP streaming is expected as  $\mu_{DEP}$  for proteins is three orders of magnitude lower than for DNA ( $8.6 \times 10^{-24} \text{ m}^4/\text{V}^2\text{s}$  for protein vs  $2.61 \times 10^{-21} \text{ m}^4/\text{V}^2\text{s}$  for DNA). Further, a concentration factor of 11 is obtained as shown in Table 2. This is a factor of  $\sim 45$  more intense than observed in our previous work using only triangular microstructures [26]. Although numerical simulations in this geometry show an improved concentration by adding the nanopost array, the concentration factor according to the numerical simulation is only  $\sim 5\%$  for the nanoposts array vs.  $\sim 2\%$  for the microtriangular posts, see Figures 3 b–c. These differences in quantitative concentration between the numerical simulations and experimental may arise from irregularities in the FIBM process leading underestimated electric field gradients. Deviations in the estimation of  $\mu_{DEP}$ , which was adapted to our previous study on DEP for an immunoglobulin G molecule [18,26] for BSA, are an additional uncertainty factor. We note that protein DEP is still little understood and factors contributing to  $\mu_{DEP}$  are very



likely to change for different proteins. Moreover, particle deformation and particle-particle interaction are additional factors that are not captured in our model and may contribute to the discrepancy in experimental observations and computations. Nonetheless, our theoretical study allows predicting changes in streaming iDEP of proteins due to variation in the device geometry.

## 5. Conclusions

We conducted a thorough experimental and numerical study revealing parameters that improve iDEP-based concentration of  $\lambda$ -DNA and the protein BSA. While streaming DEP is observed in micropost arrays, the integration of nanoposts leads to an increase in concentration when a single circular nanopost is embedded due to the DEP enhancement. Moreover, when a nanopost array with closer spacing of posts or a rectangular nanopost is integrated, iDEP trapping is observed under DC conditions experimentally. These larger DEP components are shown through increased  $\nabla E^2$  resulting from numerical simulations in the tested nanostructures. Moreover, numerical simulations according to a convection-diffusion model predict the concentration increase due to iDEP streaming in reasonable agreement with experimental observations. Discrepancies in the on-set of trapping between experiment and simulation remain for the nanopost array, which we attribute to the fact that the molecular structure of DNA is not adequately captured in our model as well as additional phenomena such as particle-particle interaction and particle deformation. Furthermore, we revealed that the integration of a rectangular array leads to iDEP trapping under DC conditions in excellent agreement with the trapping condition obtained theoretically.

While we predicted a DEP force for BSA is three orders of magnitude lower than for  $\lambda$ -DNA streaming behavior in the nanopost array is increased as observed experimentally and predicted by numerical simulation. Although there is a quantitative discrepancy with numerical simulations compared with experimental results, simulations predict an enhancement in concentration in the nanostructure array which was confirmed experimentally. In summary, our study provides details on the improvement of nanostructures for iDEP trapping under DC conditions. The results also reveal that iDEP trapping will require largely improved  $\nabla E^2$  and further down-scaled geometries to achieve protein trapping under DC conditions. Compared to existing approaches for protein DEP, our approach involves a simple elastomer molding process to produce iDEP devices. We anticipate downscaling to dimensions lower than 100nm suitable for protein trapping by iDEP will be achieved in the future with improved FIBM.

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## Glossary

<b>EOF</b>	Electroosmosis
<b>DEP</b>	Dielectrophoresis
<b>iDEP</b>	insulator-based Dielectrophoresis
<b>FIBM</b>	Focused Ion Beam Milling

## Biographies

*Fernanda Camacho-Alanis* earned her Ph.D. degree in Electrical Engineering in 2010 from the University of Virginia completing her thesis on the fabrication of molecular electronic devices on semiconductor substrates. She received her Master's degree as well as her BS from the National University of Mexico, Mexico City. Ms. F. Camacho-Alanis won an Award for Excellence in Scholarship as well as the Graduate Research Award at University of Virginia in 2009. She is currently a Postdoc in the Department of Chemistry and Biochemistry Arizona State University working in the area of microfluidics.

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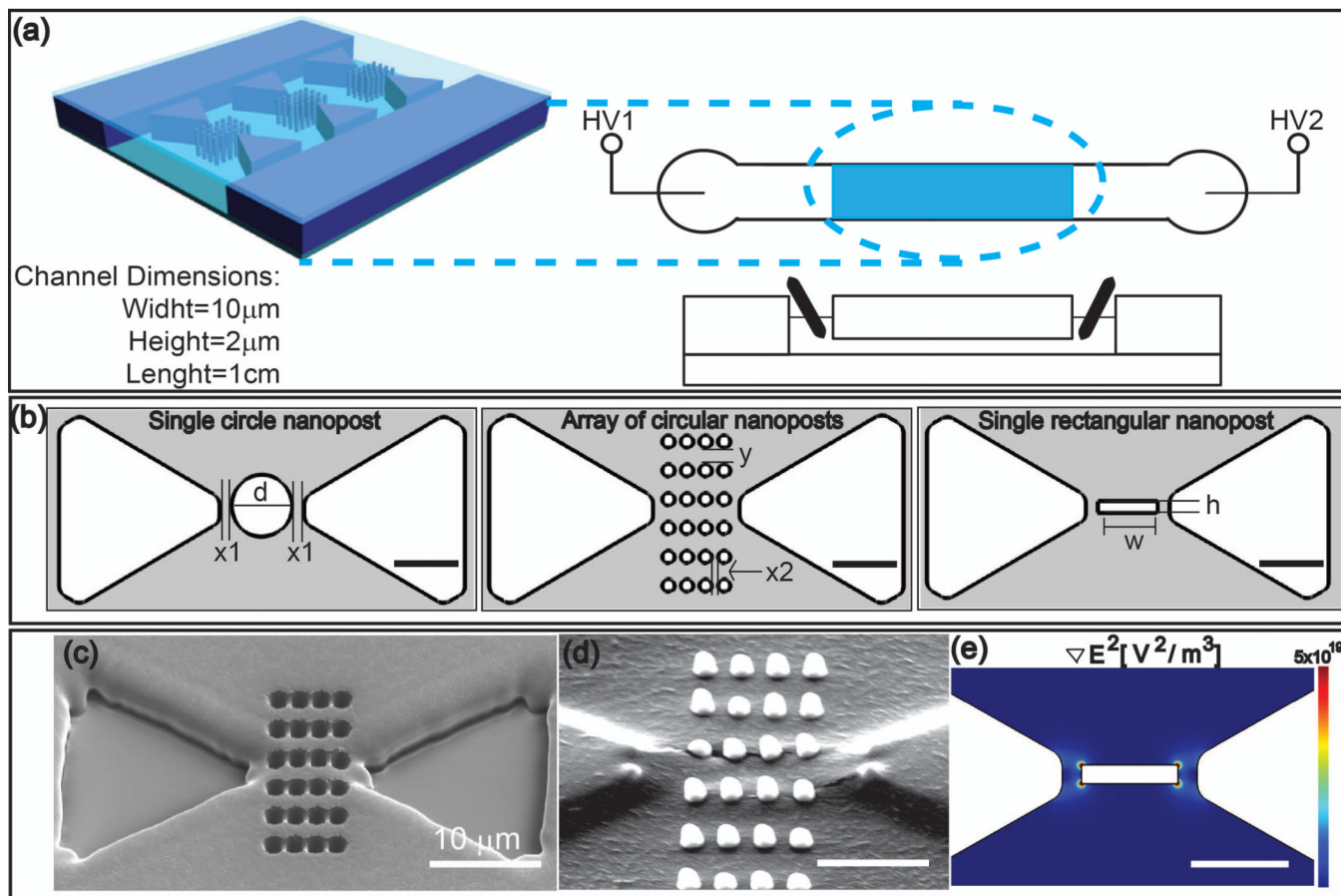
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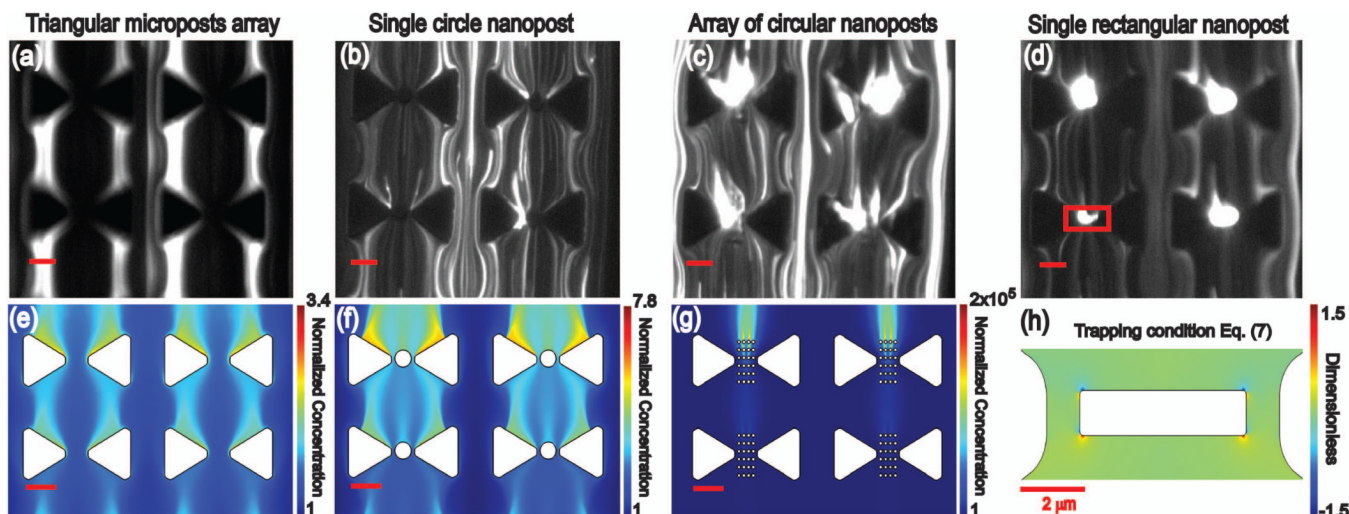
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**Figure 1.**

a) Schematic of the microfluidic device (not to scale): The upper right part shows a schematic top view with shaded areas indicating the position of the micropost array. The lower right part shows a cross section along the longitudinal axis with electrodes integrated in the reservoirs. The enlargement on the left shows a triangular micropost array with an integrated nanopost array. For simplicity, only one nanopost array per row is shown. b) Dimensions of the constrictions for a circular post in between triangles (left), circular array in between triangles (middle), and rectangular post in between triangles (right); detailed dimensions are found in Table 1. c) SEM image of the master piece after FIBM and optical lithography. d) Corresponding PDMS mold using the master piece in (c) images with SEM. The height of the circular post array is  $\sim 2 \mu\text{m}$ . e)  $\nabla E^2$  is shown exemplarily for a rectangular nanopost design. The scale bar is 5  $\mu\text{m}$  unless indicated in the figure.

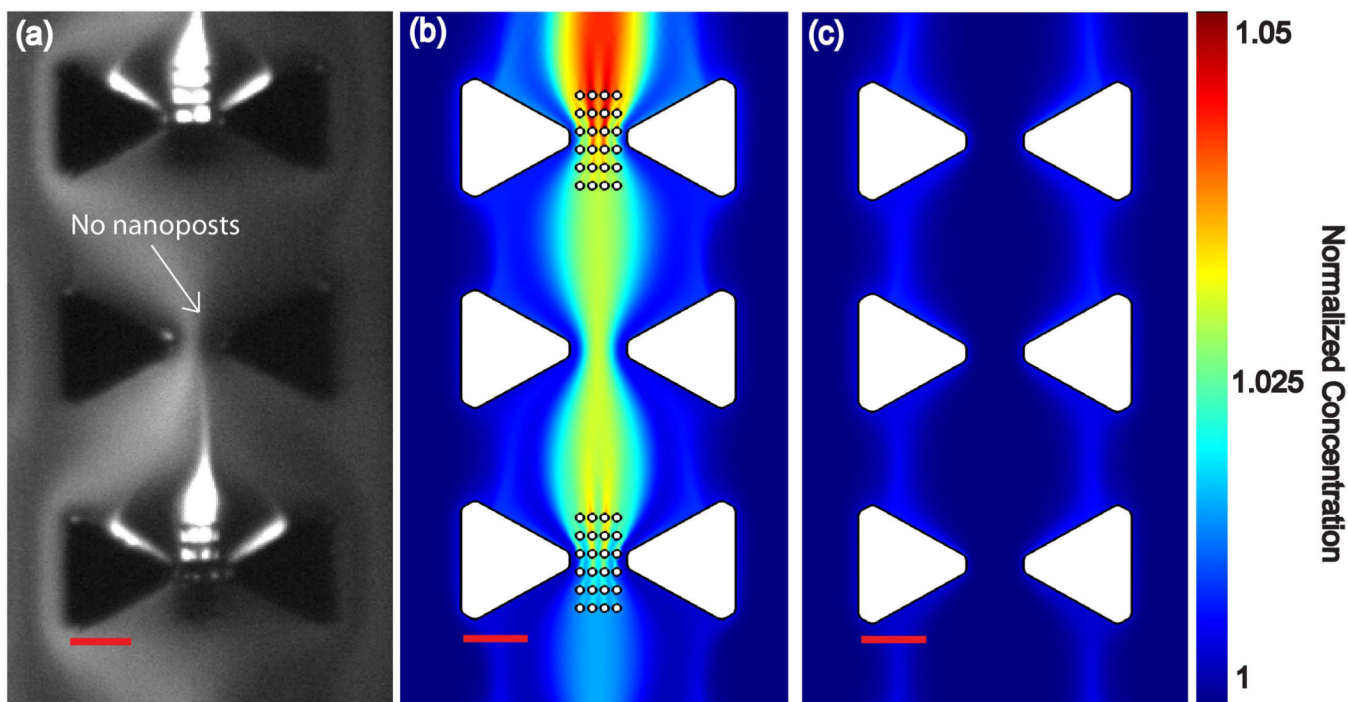


**Figure 2.**

Experimental results and numerical simulations for triangular microposts as well as the combination of micro- and nanostructures under DC-iDEP of  $\lambda$ -DNA. The flow direction in all cases is from bottom to top. Scale bar is  $10\mu\text{m}$  unless indicated in the figure. The applied potential was 1500 V except for Figures a) and e) which were performed at 3000 V.

Figure a–d. Fluorescence microscopy snapshots obtained from video microscopy imaging. a) triangular microposts, b) single circular nanopost, c) array of circular nanoposts and d) single rectangular nanopost, the red rectangle marked in this figure is zoom for figure 2-h. Note that a) and b) indicate streaming iDEP while c) and d) figures indicate iDEP trapping. Figure e–g. Simulation results under streaming regime. The concentration profile is plotted solving equation (1). e) triangular microposts f) a single circular nanopost, g) array of circular nanoposts post, and d) a single rectangular post.

Figure h. Equation (7) is plotted in the accumulation regime for the case of the rectangular nanopost, in the area indicated with the rectangle in figure 2-d. Note that the trapping condition is met for values  $>1$  (red colors) according to eq. (8).



**Figure 3.**

a) Experimental observation of streaming iDEP of BSA using the circular nanopost array in between the triangle microposts. Note that every other facing triangle was processed with a nanopost array. b) Concentration distribution obtained by numerical simulation solving eq. 1, qualitatively matching the experimental results. c) Concentration distribution obtained by numerical simulation without nanoposts solving eq. 1. The color scale for the concentration applies to both b and c. Scale bar is  $10\mu\text{m}$ .



**Table 1**

Dimensions of posts in the microfluidic channel as indicated in Figure 1-b.

Geometry	d ( $\mu\text{m}$ )	x1( $\mu\text{m}$ )	x2( $\mu\text{m}$ )	y( $\mu\text{m}$ )	w( $\mu\text{m}$ )	h ( $\mu\text{m}$ )
Circular posts	2.5	1	NA	NA	NA	NA
Circular array of posts	1	0.75	0.5	2.3	NA	NA
Rectangular posts	NA	1	NA	NA	5	1

**Table 2**

Maximum  $\nabla E^2$  obtained by numerical simulations within different geometries and concentration factor R from experimental results for  $\lambda$ -DNA at 1500 V/cm unless indicated.

(n.d. = not determined, n.a.=not applicable)

Geometry	$\nabla E^2$ max. [V <sup>2</sup> /m <sup>3</sup> ]	R for DNA	R for BSA	$R_{\text{nm-posts}}/R_{\text{Triangles}}$ for $\lambda$ -DNA at 1500 V
Triangular array of microposts	$9.4 \times 10^{16}$	$35 \pm 3.5$	0.24 <sup>**</sup>	n.a.
Triangular array of microposts <sup>*</sup>	$3.8 \times 10^{17}$	$87 \pm 5.2$	n.d.	n.a.
Circular nanopost	$6.9 \times 10^{18}$	$46 \pm 6.9$	n.d.	1.3
Circular array of nanoposts	$2.0 \times 10^{18}$	$173 \pm 29.4$	$11 \pm 0.9$	5
Rectangular nanopost	$5.2 \times 10^{19}$	$039 \pm 145$	n.d.	30

\* at 3000 V

\*\* from reference at 3000 V [26]