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Optical sensing of analytes in aqueous solutions with a multiple surface-plasmon-polariton-wave platform

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The commonly used optical sensor based on surface plasmon-polariton wave phenomenon can sense just one chemical, because only one SPP wave can be guided by the interface of a metal and a dielectric material contained in the sensor. Multiple analytes could be detected and/or the sensing reliability for a single analyte could be enhanced, if multiple SPP-wave modes could be excited on a single metal/dielectric interface. For that to happen, the partnering dielectric material must be periodically non-homogeneous. Using a chiral sculptured thin film (CSTF) as that material in a SPP-wave platform, we show that the angular locations of multiple SPP-wave modes shift when the void regions of the CSTF are infiltrated with a fluid. The sensitivities realized in the proof-of-concept experiments are comparable to state-of-research values.

S traddling the boundary of two materials, a surface wave is a delicate phenomenon. Any alteration in the constitution of either of the two partnering materials will alter the characteristics of the surface wave, which makes this phenomenon highly suitable for sensing applications. An electromagnetic surface wave commonly used for optical sensing of chemical and biochemical analytes¹⁻³ in a host of research settings spanning chemistry, physics, life sciences, engineering, food science, agriculture, forensic science, pharmaceuticals, and pathology is the surface-plasmon-polariton (SPP) wave. The propagation of an SPP wave is guided by the interface of a metal and a dielectric material^{4,5}. Microscopically, the SPP wave results from the interaction of free electrons in the metal and polaritons in the dielectric material to form quasiparticles called plasmon-polaritons that propagate along the interface.

Optical techniques requiring just a prism of high refractive index, as demonstrated by Otto⁶ and Kretschmann and Raether⁷, made the excitation of SPP waves so inexpensive that SPP-wave-based optical sensors became commonplace by the early 1990s. In one commonly used configuration, a metal thin film with a thickness on the order of a few tens of nanometers is deposited onto the hypotenuse of a $45^{\circ}-90^{\circ}-45^{\circ}$ prism, and air is the partnering dielectric material. When monochromatic light is incident on one of the slanted faces of the prism such that the magnetic field of light is directed tangentially to that face (i.e., the light is *p* polarized), and the angle of incidence on the prism/metal interface θ is such that no transmission of optical energy occurs across the metal (because θ exceeds the critical angle for a fictitious prism/air interface), most of the light is reflected through the other slanted face of the prism. The balance is absorbed. When the absorptance is plotted against θ , a peak indicates the excitation of an SPP wave guided by the metal/air interface.

Suppose that air is replaced by a fluid such as water. Then, the *p*-polarized plane wave has to arrive at a higher angle of incidence in order to excite the SPP wave¹⁰. The increase in the value of θ is the basis of numerous commercially available SPP-wave-based sensors⁸ capable of label-free and real-time detection of a huge variety of analytes^{1,2}.

The chief disadvantage of these commercially available SPP-wave-based sensors is that they are limited to detecting one analyte at a time, since only one SPP wave of a specific frequency can be guided by a metal/dielectric interface. Spatial arrays of multiple sensors are needed to detect multiple analytes simultaneously. If multiple SPP-wave modes could be guided at a specified frequency by a metal/dielectric interface, multiple channels per sensor will become available to sense multiple analytes. Alternatively, the sensing of one analyte could be done reliably through those multiple channels. Both of these possibilities motivated the work presented here.

During the last five years, theory has demonstrated that multiple SPP-wave modes can indeed be guided by the interface of a metal and a dielectric material, provided that the dielectric material is periodically non-homogeneous normal to the interface⁹⁻¹¹. Characteristics such as phase speed, attenuation rate, and spatial profiles of the

electromagnetic fields are different from one SPP-wave mode to another, but all have the same frequency. Furthermore, the excitation of multiple SPP-wave modes along the interface of a metal and a periodically non-homogeneous dielectric material at a single frequency has been experimentally demonstrated¹²⁻¹⁵.

In Refs. 9-15, the periodically non-homogeneous dielectric material is either an isotropic rugate filter¹¹ or a sculptured thin film (STF) that is periodically non-homogeneous along its thickness direction^{9,10,12-15}. STFs are a class of nano-engineered, unidirectionally non-homogeneous, and anisotropic thin films that can be fabricated using a variety of physical vapor deposition (PVD) techniques^{16,17}. Typically, a collimated vapor flux is directed toward a substrate which is rocking and/or rotating in a low-pressure vacuum chamber¹⁷. One type of STF is a sculptured nematic thin film (SNTF) that is fabricated by rocking the substrate about an axis that is tangential to the substrate plane. Another type of STF is a chiral STF (CSTF) which is fabricated when the substrate is rotated at a constant rate about an axis which passes normally through it. Both metal/SNTF13 and metal/CSTF interfaces^{12,14,15} have been experimentally shown to support the propagation of multiple SPP-wave modes at a single frequency.

Any STF is porous, with porosity ranging from 10% to 90%, depending on the material evaporated and the substrate dynamics^{17,18}. When the porous regions of an STF are infiltrated with a fluid, its optical characteristics change^{19,20}. Theory has shown²¹ that when a periodically non-homogeneous STF would be incorporated in an SPP-wave-based sensor, multiple SPP-wave modes allowed at a single frequency would enhance sensing capabilities significantly.

In this communication, we report experimental evidence of this theoretical result. We show that a multiple SPP-wave platform exemplified by a metal/CSTF combination in the commonly used prism-coupled configuration supports the propagation of three distinct SPP-wave modes at a single frequency. When infiltrated with water or a sucrose solution, the number of SPP-wave modes reduces to two. The angles of incidence of the absorptance peaks are different on infiltration by the different fluids. As a consequence, our work opens up two research avenues for SPP-wave-based sensors: (i) more reliable sensing of a single analyte, and (ii) simultaneous sensing of multiple analytes.

Results

Figure 1 shows the cross-sectional image of an SPP-wave platform incorporating the interface of a thin aluminum film and a lanthanum-fluoride CSTF on a silicon substrate. This substrate was chosen in order to obtain cross-sectional images on a field-emission scanning electron microscope (FE-SEM). The CSTF displays periodic and non-homogenous chiral morphology. The average film thickness is 1.27 μ m which is in good agreement with a 1.20- μ m-thick film as indicated by an *in-situ* quartz crystal monitor during thin-film deposition. The CSTF is three periods thick, each period being ~400 nm.

Several replicates of this platform (labeled A) along with several replicates of another platform (labeled B) containing a four-period-thick CSTF were deposited on dense flint glass substrates for optical sensing experiments. The period was maintained as ~400 nm. Lanthanum fluoride was chosen because it is insoluble in water and has a bulk refractive index ($n_{LaF3} = 1.601$) higher than that of water ($n_{H2O} = 1.333$) but lower than that of dense flint glass of type SF11 ($n_{SF11} = 1.778$) at room temperature and 1 atm pressure²². For the prism-coupled configuration, a dense flint glass prism was affixed to the dense flint glass substrate with an index-matching liquid ($n_{iml} = 1.785$).



Figure 1 | Multiple SPP-wave platform for optical sensing. High-resolution cross-section FE-SEM image of platform A containing a three-period CSTF made by directing a collimated vapor of LaF₃ at an angle $\chi_{\nu} = 15^{\circ}$ to the plane of a substrate rotating at about 0.06 rpm at 6.5 × 10⁻⁶ Torr base pressure. The period of the CSTF is ~400 nm. Underneath is a 30-nm-thick film of Al that had been deposited on a stationary silicon substrate at 1.5×10^{-5} Torr base pressure and $\chi_{\nu} = 90^{\circ}$. The silicon substrate was used in order to obtain this image; otherwise, a dense flint glass (SF11) substrate was used for optical sensing experiments in the prism-coupled configuration. Platform B is similar except that the CSTF has four periods, each ~400 nm thick.

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The prism-coupled configuration is shown in Fig. 2 when a fluid infiltrates and lies atop the CSTF. The reflectance of *p*-polarized light at 472.44 THz was measured using a photodetector as a function of the angle $\theta = 45^{\circ} + [\sin^{-1}(n_{\rm SF11}^{-1}\sin\phi)]$, where ϕ is the angle between the direction of the incident light and the normal to the slanted face of the prism on which light is incident. This measurement was made for uninfiltrated platforms as well as for platforms in which the CSTF was infiltrated with deionized water ($n_{\rm H2O} = 1.333$), 0.183 M aqueous solution of sucrose ($n_{0.183} = 1.340$)²³, and a 0.367 M aqueous solution of sucrose ($n_{0.367} = 1.351$)²³. After checking that transmission of optical energy into air beyond the CSTF does not occur in the range of θ investigated, the absorptance can be obtained by subtracting the reflectance from unity. An absorptance peak is then manifested as a reflectance dip.

Uninfiltrated platforms. Figure 3 presents typical plots of the reflectance vs. θ for platforms A and B. Pronounced reflectance dips for platform A are located at $\theta = 34.94^{\circ}$, 37.09° , 39.61° , and 43.06° whereas similar dips for platform B are located at $\theta = 34.94^{\circ}$, 38.51° , 41.39° , and 43.06° . The angular locations of the leftmost ($\theta = 34.94^{\circ}$) and the rightmost dips ($\theta = 43.06^{\circ}$) coincide extremely well, which is a strong indication that both represent two distinct SPP-wave modes¹¹⁻¹⁴ that are strongly localized to the metal/CSTF interface on the CSTF side. Theoretical understanding¹³ allows us to conclude that the fields of both SPP-wave modes die out inside the CSTF within a distance of no more than three periods from the metal/CSTF interface. These dips are marked by '1' and '3' in Fig. 3.

The two reflectance dips labeled '2', the one for platform A located at $\theta = 39.61^{\circ}$ and the one for platform B at $\theta = 38.51^{\circ}$, do not coincide and are 1.1° apart. Either these reflectance dips represent a single SPP-wave mode that is not as strongly localized to the metal/ CSTF interface as the ones labeled '1' and '3', or they represent a waveguide mode²⁵. A waveguide mode would extend over the entire thickness of the partnering dielectric material and its location on the θ axis would change with that thickness²⁵. In contrast, the location of an SPP-wave mode could vary as that thickness increases up to a certain threshold, but not beyond it²⁴.

In order to resolve the nature of the reflectance dips labeled '2' in Fig. 3, we computed the propagation constants of different waveguide modes in a homogeneous dielectric slab of refractive index n_{hds} bounded by a perfect electric conductor on one face and air on the other. Since the penetration of electromagnetic fields in a metal cannot occur significantly beyond the skin depth in that metal, and the skin depth for thin-film aluminum is about 30 nm, the replacement of the metal by a perfect conductor simplifies analysis. The



Figure 3 | Measured reflectance plots for uninfiltrated platforms. Reflectance measured as a function of θ at 472.44 THz of platforms A (red solid line) and B (blue dashed line). The incident light is *p* polarized and the CSTFs are uninfiltrated. The reflectance dips indicating the excitation of an SPP-wave mode are identified by '1', '2', and '3'.

refractive index n_{hds} was estimated as the average of n_{LaF3} and $n_{air} = 1.0$, with the reasonable assumption that both lanthanum fluoride and air are present in the CSTF in equal volumetric proportions. The propagation constants were divided by the wavenumber in the prism material to obtain the sines of angles that are analogous to θ .

We calculated that waveguide modes should occur at $\theta \sim 37.1^\circ$, 43.6°, and 46.7° in platform A. Evidence of the first waveguide mode $(\theta \sim 37.1^\circ)$ is indeed available as a moderate reflectance dip in Fig. 3, but the other two waveguide modes appear to have been excited very weakly, if at all, in the prism-coupled configuration. Waveguide modes could appear at $\theta \sim 36.5^\circ$, 41.9°, 45.2°, and 46.6° in platform B. Evidence of the first waveguide mode $(\theta \sim 36.5^\circ)$ is available as a very shallow dip and of the second waveguide mode $(\theta \sim 41.9^\circ)$ as a strong dip in Fig. 3, the remaining two waveguide modes being extremely weakly excited if at all. We conclude therefore that the dips marked '2' represent a single SPP-wave mode that is localized to the metal/CSTF interface within a distance exceeding at least three periods inside the CSTF²⁴.

Thus, Fig. 3 shows that *p*-polarized light at 472.44 THz launched three SPP-wave modes in the SPP-wave platform investigated, thereby qualitatively confirming earlier experimental^{12,14,15} and theoretical^{10,24} research.



Water-infiltrated platforms. When the air inside and atop the CSTF is replaced by a fluid of a refractive index greater than that of air,

Figure 2 | Schematic of prism-coupled configuration. The CSTF/metal/substrate platform is affixed to a prism made of the same material as the substrate with an index-matching liquid. Light incident on one slanted face at angle ϕ is incident on the prism/metal interface at angle θ . This figure shows that the fluid containing the analyte completely infiltrates and lies atop the CSTF.

theory indicates that a change in the optical properties of the partnering dielectric material seriously affects the SPP-wave phenomenon²¹. Indeed, the angle of incidence required to excite the (sole) SPP-wave mode is known to increase with increase in the refractive index of the fluid infiltrating a homogeneous, isotropic partnering dielectric material¹.

The same trend has been theoretically found for the metal/CSTF interface²¹. But there is one difference. As the refractive index of the fluid increases towards the refractive index of the skeleton material of the CSTF, the number of SPP-wave modes must tend to unity. This is because the infiltrated CSTF becomes isotropic and homogeneous when the two refractive indexes equal each other²⁶.

Figure 4 presents typical plots of the reflectance vs. θ for platforms A and B infiltrated by deionized water. Pronounced reflectance dips for platform A are located at $\theta = 49.65^{\circ}$ and 52.17° , and for platform B at $\theta = 48.98^{\circ}$, 51.52° , and 53.04° . These data indicate a potential reduction in the number of SPP-wave modes as well as shifts to greater angles of incidence to excite those modes.

Although both reflectance dips for platform A are located on the θ axis within a degree of at least one reflectance dip for platform B, the underlying causes for these reflectance dips still need to be ascertained. Therefore, we repeated the analysis for the propagation constants of different waveguide modes in a homogeneous dielectric slab of refractive index n_{hds} bounded by a perfect electric conductor on one face and water on the other. The refractive index n_{hds} was estimated this time as the average of n_{LaF3} and n_{H2O} , with the assumption that water completely filled the pores of the CSTF. Again, the propagation constants were divided by the wavenumber in the prism material to obtain the sines of angles that are analogous to θ .

Waveguide modes should occur at $\theta \sim 51.4^{\circ}$ and 55.9° in platform A. Neither of these two are easy to find in Fig. 4, indicating that the reflectance dips at $\theta = 49.65^{\circ}$ and 52.17° are indicative of the excitation of two SPP-wave modes.

Waveguide modes should occur at $\theta \sim 49.4^{\circ}$, 53.3° , and 55.2° in platform B. The leftmost one cannot be seen in Fig. 4, the middle one is strongly present, and the rightmost one has a shallow existence. Accordingly, the strong reflectance dips at $\theta = 48.98^{\circ}$ and 51.52° represent the excitation of two SPP-wave modes. Because their locations on the θ axis are about 0.7° less than those for platform B, we conclude that both of these SPP-wave modes are localized to the metal/CSTF interface within a distance exceeding at least three periods inside the CSTF²⁴. The dips are marked by '1' and '2' in Fig. 4.

Sucrose-solution-infiltrated platforms. Replicates of the platforms used for the water-infiltration experiments were used for the next two sensing experiments. In the first of these two experiments, a 0.183 M aqueous solution of sucrose $(n_{0.183} = 1.340)$ infiltrated



Figure 4 | Measured reflectance plots for water-infiltrated platforms. Reflectance measured as a function of θ at 472.44 THz of platforms A (red solid line) and B (blue dashed line). The incident light is *p* polarized and water infiltrates and lies atop the CSTF. The reflectance dips indicating the excitation of an SPP-wave mode are identified by '1' and '2'.

and lay atop platform A. In the second, a 0.367 M aqueous solution ($n_{0.367} = 1.351$) was used instead. The thicker platform B was not used because the viscosity of the solutions could prevent them from reaching the pores close to the interface.

Figure 5 presents typical plots of the reflectance vs. θ for platform A when a sucrose solution infiltrates and lies atop the three-period CSTF. The plot for water-infiltrated platform A is also provided in this figure for comparison. Both SPP-wave modes '1' and '2' shift to higher values of θ with increase in sucrose content from 0 to 0.367 M (and hence the increase in the refractive index of the infiltrant fluid from 1.333 to 1.351). This figure is the main result of this communication, as it completely validates the theoretical prediction²¹ of multiple SPP-wave modes available for optical sensing at the interface of a metal and a dielectric material that is a periodically non-homogeneous normal to the interface.

Sensitivity. Let $\theta(n_{infil},m)$ denote the angle of incidence for a reflectance dip indicating the excitation of the SPP-wave mode labeled $m \in \{1,2\}$ in Fig. 5. Then, a sensitivity with respect to water infiltration can be defined as

$$\rho(n_{infil},m) = \frac{\theta(n_{infil},m) - \theta(n_{H2O},m)}{n_{infil} - n_{H2O}}.$$
 (1)

The sensitivity values for both sucrose solutions and for both SPPwave modes from Fig. 5 are tabulated in Table 1.

Over the limited range (1.333 to 1.351) of the refractive index of the infiltrant fluid tested, the sensitivity is \sim 80 deg/RIU. This figure is about three times higher than the one predicted theoretically for a multiple-SPP-wave platform incorporating a titanium-oxide CSTF²¹. Most likely, the lanthanum-fluoride CSTF used in our experiments is more porous than the titanium-oxide CSTF involved in theoretical prediction.

In the absence of a CSTF, only one SPP-wave mode can propagate guided by a metal/air or a metal/fluid interface at a given frequency. For a single-SPP-wave platform comprising a SF11 prism, a SF11 substrate, and a metal film made of either gold or silver, the dynamic sensitivity

$$\rho_{dyn}(n_{infil}, 1) = \frac{d\theta(n_{infil}, 1)}{dn_{infil}}$$
(2)

cannot exceed 85 deg/RIU at 472.44 THz²⁷. However, Table 1 yields the ratios



Figure 5 | Measured reflectance plots for sucrose-solution-infiltrated platform A. Reflectance measured as a function of θ at 472.44 THz of platform A when an aqueous solution of sucrose infiltrates and lies atop the three-period CSTF. The incident light is *p* polarized. The blue solid line is for the 0 M solution, the red dashed line is for the 0.183 M solution, and the black dashed-dotted line is for the 0.367 M solution. The reflectance dips indicating the excitation of the two SPP-wave modes are identified by '1' and '2'.

Table 1 | Sensitivities $\rho(n_{0.183}, m)$ asnd $\rho(n_{0.367}, m)$ for the mth SPPwave mode in Figure 5

m	n _{infil} (RIU)	$\theta(n_{infil},m) - \theta(n_{H2O},m)$ (deg)	ho (deg/RIU)
1	1.340	0.55	78.57
	1.351	1.54	85.55
2	1.340	0.44	62.85
	1.351	1.68	93.33

$$\frac{\theta(n_{0.367}, 1) - \theta(n_{0.183}, 1)}{n_{0.367} - n_{0.183}} = 90 \text{ deg/RIU and}$$
$$\frac{\theta(n_{0.367}, 2) - \theta(n_{0.183}, 2)}{n_{0.367} - n_{0.183}} = 112.7 \text{ deg/RIU}$$

for platform A. Thus, the use of a CSTF has not only delivered multiple SPP-wave modes, each capable of being used for sensing, but also equal or better sensitivity in the prism-coupled configuration²⁷. Further enhancement for commercial purposes would require careful selection of the prism material, the metal, and the CSTF material, as theoretical studies have already shown for single-SPP-wave platforms²⁷. Moreover, the use of a lensing system after the laser-diode module would allow simultaneous measurements for a range of angles θ , and the replacement of the photodetector by an array of charge-coupled device (CCD) sensors would speed up the measurement process²⁸.

Discussion

A multiple SPP-wave-based optical sensor with a single metal/dielectric interface has been demonstrated and confirms previous theoretical predictions, the partnering dielectric material being a chiral sculptured thin film. Improvement in performance will come from optimizing the vapor flux angle during the fabrication of the CSTF. Whereas a CSTF with a high value of χ_{ν} would have very little porosity and therefore very little sensitivity, a CSTF with a very low value of χ_{ν} would be so porous as to be fragile. Although only one analyte (i.e., sucrose) was used in the proof-of-concept experiments reported here, the occurrence of multiple SPP-wave modes is exploitable for both more reliable sensing of a single analyte and multi-analyte sensing, using regression analysis²⁹.

More reliable sensing of a simple analyte is possible using Taylor expansions of the shifts $\theta(n_{\text{infil}}, m) - \theta(n_{\text{H20}}, m)$ with respect to $n_{\text{infil}} - n_{\text{H20}}$ for each *m*, as has been shown for a sensor based on a class of electromagnetic surface waves guided by the interface of two dielectric materials³⁰. The reference infiltrant need not be H₂O.

For sensing multiple analytes, layers of different recognition materials will have to be implanted at different depths into the CSTF, care being taken that the implantation depths are such that one of the multiple SPP-wave modes has a maximal electric field at that depth²⁴ in order to perturb the angular location of the reflectance dip significantly. This could be done by short-term co-deposition of a recognition material in addition to one chosen for fabricating the CSTF³¹. Properly chosen recognition materials would impart specificity of sensing.

Furthermore, as not only *p*-polarized light but also *s*-polarized light can excite SPP-wave modes guided by the interface of a metal and a periodically non-homogeneous dielectric material^{9,10,13}, further avenues for multi-analyte sensing are now available for investigation.

In closing, let us mention the imaging SPP-wave sensor in which broadband light is used in place of monochromatic light and the photodetector is replaced by an array of CCD or CMOS sensors. With only one SPP-wave mode launched at a specific frequency, the multi-frequency data is optically manipulated to measure n_{infil} correct to five decimal digits²⁸. Incorporation of the multiple-SPPwave platform is expected to enhance the capabilities of imaging SPP-wave sensors as well.

Methods

Deposition of aluminum. A dense flint glass (SF11) substrate (Swiss Jewel Co., Philadelphia, PA, USA) was cleaned in an ultrasonic bath of ethanol for five min and blow-dried with a nitrogen gun before being positioned onto a substrate holder required for thin-film deposition. The substrate holder and the substrate were placed in a low-pressure evaporation chamber in which the resistive-heating PVD technique was employed. At a base pressure of 1.5×10^{-5} Torr, 35 A current was passed



Figure 6 | Custom-built machine used to perform all experiments with uninfiltrated or infiltrated platforms. This custom-built machine incorporates a prism-coupled configuration at its apex. As the stepper motor rotates the turnbuckle-style screw, the angle of incidence of the 472.44 THz *p*-polarized beam on one slanted face of the prism changes and the appropriate voltage readings from an oscilloscope (not shown) connected to the photodetector are recorded.

through a tungsten basket housing an aluminum pellet. The aluminum vapor flux was directed towards the substrate until a 30-nm-thick film was produced. The deposition rate monitored using a quartz crystal monitor (Inficon, Bad Ragaz, Switzerland) *in situ* was kept fixed at 0.4 \pm 0.02 nm s⁻¹.

Deposition of CSTF. The low-pressure chamber was opened after the aluminum film had been deposited, was loaded with a notched boat containing LaF3 powder (Phelly Materials, Upper Saddle River, NJ, USA), and then evacuated again. When the base pressure of 6.5×10^{-6} Torr was reached, a computer-controlled stepper motor tilted the aluminum-coated substrate about an axis tangential to the substrate plane to a fixed angle $\chi_v = 15^\circ$. Then, a current was passed through the notched boat and increased in increments of 5 A until reaching 95 A in order to generate a LaF3 vapor flux. The deposition rate was kept fixed at 0.4 \pm 0.02 nm s⁻¹ while a second computer-controlled stepper motor continuously rotated the substrate holder about an axis which passes normally through it in a clockwise manner when viewed from the vapor source in increments of 18° with a 48-s pause between successive increments. Twenty 18° steps were needed to complete the deposition of one structural period of thickness $2\Omega = 400$ nm. After the deposition of either three or four periods of the CSTF, the platform was allowed to reach room temperature before the evaporation chamber was exposed to atmosphere. The platform was placed in a low-pressure desiccator for 24 h before its reflectance spectrum was collected.

Optical measurements. The dense flint glass substrate in the platform was affixed to the hypotenuse of a $45^{\circ}-90^{\circ}-45^{\circ}$ dense flint glass prism (Edmund Optics, Barrington, NJ, USA) with one drop of an index-matching liquid (Cargille Laboratories, Cedar Grove, NJ, USA). The assembly was then placed onto a custom-built machine shown in Fig. 6. The machine has an incidence arm and reflection arm. A low-power 472.44 THz laser-diode module (ThorLabs, Newton, NJ, USA) followed by a linear polarizer was positioned as the light source on the incidence arm. The intensity of light received by a PDA36A photodetector (ThorLabs, Newton, NJ, USA) on the reflection arm was measured using a TDS 2024B oscilloscope (Tektronix, Beaverton, OR, USA). Dividing the intensity of the reflected light by that of the incident light delivered the reflectance.

As the angle between the two arms was changed, the angle ϕ was increased from -20° to 30° in steps of 0.02°.

For measurements in which the CSTF was infiltrated, a drop of the solution (water, or water containing sucrose) was put on top of the CSTF.

Electron microscopy. An FEI Nova NanoSEM 630 (Hillsboro, OR, USA) fieldemission scanning electron microscope was used to image the morphology of the CSTFs.

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Author contributions

S.E.S. and D.P.P. fabricated all thin films and jointly designed and fabricated the custom-built machine which was used for all optical measurements used in this investigation. S.E.S. made all optical measurements. A.L. conducted the waveguide mode analysis and supervised the research. S.E.S. and A.L. were primarily responsible for writing this manuscript.

Additional information

Competing financial interests: The authors declare no competing financial interests.

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