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Relaxor-PbTiO₃ Single Crystals for Various Applications

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Abstract

Piezoelectric materials lie at the heart of electromechanical devices. Applications include actuators, ultrasonic imaging, high intensity focused ultrasound, underwater ultrasound, nondestructive evaluation transducer, pressure sensors, and accelerometers, to name a few. In this work, the advantages and disadvantages of relaxor-PbTiO₃-based single crystals are discussed, based on the requirements (figure of merit) of various applications, with emphasis on recent developments of the shear properties of single crystals as a function of temperature and applied fields.

I. Introduction

Relaxor-PbTiO₃ (PT) single crystals, including Pb(Mg_{1/3}Nb_{2/3})O₃-PT (PMNT) and Pb(Zn_{1/3}Nb_{2/3})O₃-PT (PZNT), have been extensively studied, because of their high piezoelectric coefficients, >1500 pC/N, high electromechanical coupling factors, > 0.9, and high usable strain levels, far outperforming the state-of-art of polycrystalline Pb(Zr, Ti)O₃ (PZT) ceramics, as shown in Table I [1]–[7]. These crystals have been commercialized and employed in medical ultrasonic imaging transducer applications [1], [9], [10]. In addition, the cryogenic properties of relaxor-PT single crystals were reported to be superior to their polycrystalline counterparts, with piezoelectric coefficients being on the order of ~70% of their room temperature values at –150°C, whereas polycrystalline ceramics possess much lower values, being only 30% of the original data [11], [12], which have been demonstrated for actuator or ultrasonic motor applications at cryogenic temperature [13]–[15]. Another advantage of relaxor-PT single crystals is their strong anisotropic characteristics. Because of the symmetry of crystals, many modes can be obtained by “domain engineering” [16], [17], giving rise to optimized piezoelectric properties with different vibration modes. Table II gives the summary of various vibration modes in single crystals with rhombohedral phase [1], [18], when the crystals were poled along [001] direction, 4mm symmetry was formed

with 4R engineered domain configuration, in which the highest longitudinal piezoelectric coefficient d_{33} was observed to be on the order of ~ 2000 pC/N, whereas mm2 macroscopic symmetry was induced when the crystals were poled along [011] direction, with 2R engineered domain configuration, in which the highest lateral piezoelectric coefficient d_{32} was obtained and found to be on the order of -1780 pC/N. In contrast, single-domain state 1R, with macroscopic symmetry 3m, was achieved when rhombohedral crystals were poled along their spontaneous polarization direction [111], leading to ultrahigh shear piezoelectric coefficient d_{15} , on the order of ~ 3700 pC/N. Of particular significance is that electromechanical coupling factors for both extensional (longitudinal and lateral) and transverse vibration modes were found to be on the order of ~ 0.9 , promising for broad bandwidth transducer applications. However, these crystals were found to possess low coercive fields ($E_C \sim 2$ to 3 kV/cm), low mechanical quality factors ($Q \sim 75$), and Curie temperatures $T_C \sim 130^\circ\text{C}$ to 170°C , restricting their acceptance in numerous applications. Furthermore, they are limited by their low ferroelectric rhombohedral-to-tetragonal phase-transition temperature T_{RT} , on the order of 60°C to 100°C , because of the strongly curved morphotropic phase boundary (MPB), as shown in Table I [1]. Thus, extensive effort has been put into the development of new ferroelectric crystal systems with expanded temperature and field usage ranges [1], [2]. To separate the crystal systems, the previously mentioned PMNT and PZNT binary single crystals were categorized as first-generation relaxor-PT crystals, whereas crystals with higher T_C/T_{RT} and E_C values are categorized as second-generation relaxor-PT crystals, which may include, but are not limited to ternary systems with a PMN end member, such as $\text{Pb}(\text{In}_{0.5}\text{Nb}_{0.5})\text{O}_3$ -PMN-PT (PIN-PMN-PT) [19]–[26] and PMN-PT-PbZrO₃ (PMN-PZT) [27]–[29] ternary crystals, with E_C and T_{RT} values being on the order of ~ 5 kV/cm and 90°C to 150°C , greatly expanding their potentials for transducer applications [1]. In addition, for high-power applications, low dielectric loss and mechanical loss are desirable for reducing heat generation. Based on these requirements, third-generation crystals have been explored by adding a small amount of acceptor dopants to tailor the crystal's electromechanical parameters to specific device needs, such as manganese-modified PMNT-based crystals, with greatly improved mechanical quality factors [1], [30]–[33]. The property comparison for the three generations of relaxor-PT single crystals is also shown in Table I.

From a viewpoint of material, different figures of merit (FOMs) have been considered for various applications. For example, actuator applications require large piezoelectric strain coefficient with large nonhysteretic strain level to achieve large displacements under an external drive field, whereas transducer applications need an FOM of electromechanical coupling factor and dielectric permittivity to achieve broad bandwidth and high sensitivity. Low dielectric loss is important for devices operating at off-resonance frequency, accounting for low heat generation [34], whereas mechanical loss is critical for devices operating at resonance frequency because the acoustic power output is closely associated with the mechanical quality factor [35]. In addition, high coercive field is necessary for applications under high drive condition, which will improve the field stability and simplify the device design (for example, dc bias may be required to stabilize the poling status of PMNT crystals for transducer applications, because of their low coercive fields) [1], [9], [33], [36]–[38]. For all applications, ferroelectric materials with high Curie temperatures are

desirable for the following reasons: first, ferroelectric crystals with higher Curie temperatures are found to possess expanded temperature usage range with less-temperature-dependent properties; second, ferroelectric crystals with higher Curie temperatures have larger coercive field [2]. Fig. 1 gives a schematic diagram showing the material properties related to electromechanical device performance.

Until now, piezoelectric investigations for relaxor-PT-based crystals have been mainly focused on their extensional behavior, whereas limited attention was paid to the transverse (shear) piezoelectric property for electromechanical applications. In this work, the advantages and disadvantages of the three generations of ferroelectric relaxor-PT crystals are discussed with respect to various electromechanical applications. Recent developments of shear properties, including thickness shear and face shear vibration modes, were investigated based on different crystal compositions/phases and poling directions.

II. Experimental

Relaxor-PT single crystals, including PMNT, PIN-PMN-PT and Mn:PIN-PMN-PT crystals were grown using the modified Bridgman method. The as-grown crystal boules are typically 3 inches in diameter and 5 inches in length [1]. The crystals were oriented along various crystallographic directions, [001], [011], and [111], and made into different samples with geometries following the IEEE standard on piezoelectricity [39]. The samples were vacuum sputtered with gold thin films as electrodes on the side faces and poled at electric fields of 10 to 20 kV/cm, depending on their respective coercive fields. For samples poled along their spontaneous polarization, the poling condition was selected to be 5 kV/cm electric field and above their Curie temperature, and then field cooled down to room temperature, to avoid the cracks induced in single-domain state [40]. For thickness-shear samples, the electrodes on the side faces were removed after poling, and subsequently re-electroded on the large faces vertical to the original electrode planes. The capacitance, resonance, and anti-resonance frequencies for different vibration modes are measured using a multi-frequency LCR meter (HP4284A, Agilent Technologies Inc., Santa Clara, CA) and HP4194A impedance-phase gain analyzer, respectively, from which, the dielectric permittivity, elastic constant, electromechanical coupling factor, piezoelectric coefficient, and mechanical quality factor can be calculated.

III. Applications (Advantages and Disadvantages of Relaxor-PT Crystals)

As shown in Table I, PMNT first-generation single crystals were found to possess high dielectric and electromechanical properties, exhibit great benefit over poly-crystalline ceramics; however, their low T_C , T_{RT} , and E_C are the main concerns for practical applications, thus, second- and third-generation relaxor-PT single crystals with comparable piezoelectric properties have been developed, with enhanced T_{RT} , E_C , and Q_m , which greatly expand the temperature and field usage ranges, potential for various electromechanical applications.

For medical ultrasound imaging applications, including single-element and phased-array structures, 1–3 and 2–2 crystal/epoxy composites have been extensively studied, because of the high electromechanical coupling factors, with values of longitudinal $k_{33} > 0.90$ and

sliver $k_{33}' > 0.80$, respectively, both much higher than that of thickness $k_t \sim 0.60$, as shown in Fig. 2. Furthermore, the composites are found to possess the advantage of lower acoustic impedance, being about 12 to 20 MRayls, much smaller than single crystals (~ 30 MRayls), which will benefit the matching of the transducers to the human body (~ 3 to 5 MRayls) [41]. However, recent experimental data for PMNT crystal/epoxy 1–3 composites (piezoelectric composite- micromachined ultrasound transducer PC-MUT) operating at high frequencies > 20 MHz exhibited a large decrease in electromechanical coupling, with values being less than 0.80 [42], [43], showing a strong scaling effect and leading to the question of the origin of property degradation at high frequencies [44], [45]. Besides medical imaging transducers, other applications, including underwater acoustic transducers, nondestructive evaluation (NDE) transducers, piezoelectric actuators, and sensors are also benefit from the high extensional piezoelectric properties of relaxor-PT crystals [1]. Recently, single crystals with shear vibration mode drew attention for low-frequency acoustic transducer applications, because of the ultrahigh elastic compliance and piezoelectric coefficients (listed in Table II).

Schematic figures of the various thickness shear mode crystal samples are shown in Fig. 3 [31], [46], including the standard crystal cut A: $[111]/(1-10)$ (the first $[hkl]$ is the poling direction and the second (hkl) is the electroding surface), which is rhombohedral phase and shows single domain state 1R; other crystal cuts, B: $[110]/(-110)$ and C: $[110]/(001)$ are rhombohedral and/or orthorhombic crystal samples with domain structures 2R or 1O after the poling process; D: $[001]/(110)$ and E: $[001]/(100)$ are tetragonal crystal samples with a 1T domain state. The bottom figure shows the piezoelectric deformation of the thickness shear vibration. Of particular significance for $[011]$ -poled rhombohedral crystals is the large face shear vibration that can be achieved in $Z_t \pm 45^\circ$ -cut samples, which incorporates two extensional lateral modes, as shown in Fig. 4 [46]–[50], with the piezoelectric deformation of the face shear vibration given in bottom figure. The benefit of this mode is that the resonance is associated with the length of the sample and not the thickness, thus further reducing the device dimensions for a given frequency when compared with thickness shear.

Table III summarizes the thickness shear properties for various crystals with different domain configurations and compared with commercial PZT polycrystalline ceramics. It is evident that high shear piezoelectric coefficients and elastic compliances can be easily achieved in crystals with single-domain states, such as 1R and 1O, which will benefit the broad bandwidth transducer applications (high electromechanical coupling) at low operational frequency range (large elastic compliance). In addition, the high shear elastic compliance (low frequency constant) of single crystals results in small parts for the same frequency compared with polycrystalline ceramics, allowing miniaturization of the transducers or sensors. However, there are problems for the usage of shear vibration modes, including the temperature instability of dielectric and piezoelectric properties; low allowable drive field stability because the working direction is vertical to the poling direction in the thickness-shear mode; low mechanical quality factor, which is very important for high-power application and cross-talk effects, etc. [1]. Furthermore, large shear properties have been observed in crystals with a single-domain state, however; as a single-domain material, it is subject to cracking from the large electric-field-induced strain/stress during the poling process [1], [40], which can be avoided in multi-domain states. As listed in Table III, large

shear d_{15} and elastic s_{55}^E values, being on the order of ~ 3350 pC/N and 208 pm²/N, respectively, were obtained in engineered domain configuration 2R, with the advantage of no cracking during the poling process.

In the following, the details addressing these issues are discussed, to optimize material properties for transducer applications.

A. Scaling Effect

Fig. 5 shows the electromechanical properties of relax-or-PT crystal/epoxy 1–3 composites as a function of sample thickness. For comparison, the longitudinal coupling factors (k_{33}) of the monolithic PMNT and PIN-PMN-PT samples were calculated by the equation

$k_{33} = \sqrt{1 - (\epsilon_{33}^S / \epsilon_{33}^T)}$ and plotted as a function of sample thickness. In addition, the reported coupling factors for PMNT/epoxy 1–3 composites were included in Fig. 5 [42], [43]. Note that the corresponding resonance frequencies on the top x-axis of Fig. 5 were calculated from the frequency constants by assuming ~ 1000 Hz·m for both monolithic and 1–3 composites samples. From Fig. 5, the monolithic PMNT crystals were found to exhibit a decreasing trend in coupling (k_{33}) with decreasing sample thickness, because of the degradation of the free dielectric permittivity [44], [45]. The 20 MHz PIN-PMN-PT/epoxy 1–3 composites were found to maintain higher electromechanical coupling factors, being on the order of 0.80, when compared with 20-MHz PMNT composites, with coupling being only 0.74. The observed scaling effect is reported to be associated with the ferroelectric domain size; the large domains will be clamped by the surface boundary when the physical size of the samples becomes of the same order as the domain size. This can be confirmed by the domain observations, in which the domain size of PMNT crystals was found to be on the order of 10 to 20 μm , whereas it is only about 1 μm for PIN-PMN-PT crystals, showing a large advantage of the ternary system [44], [45]. To confirm the role of domain size on the dielectric and piezoelectric properties in ultrathin samples, a field-cool poling approach was applied to PMNT crystals, for which significantly smaller domain sizes, being on the order of ~ 5 μm , were achieved; consequently, the dielectric permittivity and piezoelectric coefficient were greatly improved, from 3000, 1300 pm/V to 5600, 2200 pm/V, respectively [51].

B. Temperature Stability

The thermal stability of dielectric and piezoelectric properties is very important for most electromechanical applications. In general, the dielectric and piezoelectric response of relax-PT ferroelectric crystals exhibit relatively large temperature variation, because of the multiple ferroelectric–ferroelectric phase transitions lying in or near the temperature range of -50°C to 100°C [1], [2]. Based on thermodynamic analysis of perovskite single crystals, the temperature dependence of the transverse dielectric permittivity is strongly related to the ferroelectric phase transitions. Fig. 6 shows the temperature dependent dielectric permittivity variation of 1O single-domain-state crystals, where the variation of dielectric K_{11} was found to be on the order of 30 000 ppm/ $^\circ\text{C}$, because of the curved orthorhombic to tetragonal phase boundary, whereas variation of dielectric K_{22} was found to be on the order of 1500 ppm/ $^\circ\text{C}$, much flatter than that of K_{11} [26]. This phenomena can be explained by the

fact that the orthorhombic to rhombohedral phase boundary is vertical and not related to the temperature variation [1], [40], [52]. Correspondingly, the shear piezoelectric coefficient d_{24} was found to maintain a similar value until the T_{OT} transition temperature, being less than 6%, much less than the variation of d_{15} in the same temperature range, which was found to be on the order of $\sim 180\%$. As expected, the longitudinal coefficient d_{33} along [111] direction for crystals with 3O engineered domains, which is closely associated with d_{24} in the 1O single-domain state, was found to show temperature-independent behavior, yet with a high value of ~ 900 pC/N; thus, it is promising for applications in which high temperature stability is demanded [1].

C. Drive Field Stability

Ferroelectrics exhibit nonlinear properties under high drive field, because of the interfaces' (domain wall and/or phase boundary) motion [1], [53], [54]. The piezoelectric and dielectric responses of relaxor-PT single crystals generally increase with increasing drive field up to a threshold value, above which, the samples will be depolarized and lose their piezoactivity. The threshold value is closely related to the respective coercive field of ferroelectrics, which is on the order of 2 to 10 kV/cm for relaxor-PT crystals, depending on the phase and composition. In the case of thickness-shear vibrations, the allowable drive field is much lower than coercive field, because the working direction of thickness shear is perpendicular to the poling direction [33]. As listed in Table IV, the field stability ratios (allowable drive field level divided by coercive field) of pure relaxor-PT single crystals were found to be on the order of $\sim 40\%$, less than half of the coercive field, regardless of crystal systems and different thickness-shear vibrations. However, for the acceptor (Mn) modified relaxor-PT single crystals, internal bias was found to be on the order of 0.6 to 1.2 kV/cm, leading to the enhanced allowable drive field, with field stability ratio increasing to $>65\%$, much higher than that of pure counterparts [33]. Furthermore, it should be noted that drive field stability of relaxor-PT crystals can also be enhanced by applying the uniaxial stress to crystals [55]. Of particular significance is that the field stability ratio of the face-shear vibration mode, being on the order of 100%, greatly expands the usage range for high-power applications, which is due to the fact that the working direction is along the poling direction in face shear vibration [48].

D. Mechanical Quality Factor

High-power applications, such as high-intensity focused ultrasound (HIFU), NDE, and underwater acoustic transducers, not only require high allowable drive field, also need high mechanical quality factor Q_m , which will efficiently increase the vibration velocity and decrease the heat generation under high drive condition at resonance frequency. In ferroelectrics, the Q_m was mainly affected by the existence of domain wall motion and polarization rotation, where the polarization rotation angle was found to play an important role in the determination of Q_m value in relaxor-PT crystals, because of the inherent anisotropic characteristics [1]. From Table III, the Q_m values for thickness-shear vibration modes were found to be very low, being on the order of ~ 30 for relaxor-PT single-crystal systems. For comparison, the mechanical Q_m was reported to be on the order of >1000 for longitudinal vibration mode in single-domain crystals. This is because the polarization rotation angle for thickness shear vibration in single-domain state is 90° , whereas the angle

is 0° for longitudinal vibration [1]. To improve the mechanical Q_m , acceptor dopant was employed to modify relaxor-PT crystals, analogous to “hard” PZT ceramics; however, although large improvement was found for the longitudinal vibration (Q_m increases to >800), limited success was achieved for thickness-shear vibration. Of particular importance is that the new face shear vibration, as shown in Fig. 4, taking advantage of the working direction being the same to the poling direction and the small polarization rotation angle ($\sim 35.3^\circ$), exhibited higher mechanical Q_m , being on the order of >100 , further increased to >200 for Mn-modified crystals, significantly higher than those values of thickness-shear vibrations, as given in Table V [46], [48].

E. Cross-Talk

For an ideal sensor application, the sensors only give an output when they are loaded (such as force, pressure, or acceleration) along their sensitivity axis, and the load normal to that axis should not produce any output. However, real sensors may give an output also to a force normal to their sensitive axis, which will have significant influence on the accuracy of the measurement results; this is called cross-talk [56]. For example, thickness-shear piezoelectric d_{16} , being on the order of -1700 pC/N, was observed in crystals with 1R single-domain state, strongly cross-talks with piezoelectric d_{15} . Thus, it is desirable to reduce or eliminate the cross-talk effect in practical applications. It was reported that d_{16} can be eliminated by rotating the sample around the x -axis with an angle of $\alpha = \arctan(-d_{16}/d_{15})$ [49], [57]. Other approaches to obtain thickness shear samples without cross-talk include the utilization of domain configurations other than 1R single-domain state, such as 1T and 1O/2R, with macroscopic symmetries of 4mm and mm2, respectively, where the d_{16} value is zero. It should be noted that for face-shear vibration, cross-talk from extensional vibrations d_{31} or d_{32} can be eliminated by rotating the sample along Z -axis with angle of $\alpha = \arctan(d_{31}/-d_{32})$ or $\alpha = \arctan(-d_{32}/d_{31})$, without sacrificing the large d_{36} [58].

IV. Summary

The advantages and disadvantages of relaxor-PT single crystals for transducer applications were discussed in this paper. The second-generation ternary PIN-PMN-PT single crystals were found to possess a higher usage temperature range and coercive field; of particular important is the small domain size, being on the order of ~ 1 μm , exhibiting less scaling effect and promising for ultrahigh frequency transducer applications. The enhanced coercive field and the existence of internal bias for third-generation Mn:PIN-PMN-PT crystals improved the field stability ratio greatly when compared with their pure counterparts, allowing high drive condition. Specifically, face-shear vibration was found to possess large drive field stability and high mechanical Q_m , in addition to the high piezoelectric coefficient and elastic compliance. Furthermore, the controlling dimension of face shear is the length direction, instead of the thickness, making face-shear vibration a promising candidate for compact, low-frequency and high-power transducer applications.

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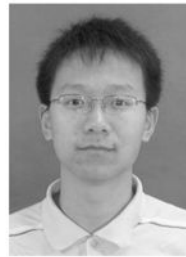
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Biographies



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Thomas R. ShROUT is Professor of Materials and Senior Scientist at The Pennsylvania State University. He received B.S. and Ph.D. degrees in ceramic science from The Pennsylvania State University in 1976 and 1981, respectively. Prior to joining the faculty at Penn State, Dr. ShROUT was with Sprague Electric Co. and AVX Co. He was a recipient of the Ikeda Memorial Award in Ferroelectrics in 2005, the IEEE Ferroelectrics Recognition Award in 2006, the Electroceramics Bridge Building Award in 2009, and distinguished lecturer (IEEE-UFFC) in 2007–2008. He is a fellow of the American Ceramic Society and IEEE-UFFC. He was senior VP of Ferroelectrics, IEEE-UFFC from 2006 to 2009. He holds 19 patents and has coauthored more than 300 papers in the area of electronic single crystals and ceramics with an emphasis on processing property relationships.

Material Parameter		Performance
• High Piezoelectric Coefficient	$(s = dV)$	High Strain (Actuator)
• High Electromechanical Coupling (Electrical \leftrightarrow Mechanical)	$\left(k_{ij}^2 = \frac{d^2}{\epsilon S} \right)$	Bandwidth & Sensitivity (Transducer)
• Dielectric Permittivity	(Cap $\propto \epsilon_0 K$)	Electrical Impedance Matching
• Low Electrical & Mechanical Loss ($\tan\delta$, mechQ)	$P = \omega E^2 k^2 \epsilon Q$ $(P_{disp} = \omega E^2 \epsilon \tan\delta)$	Acoustic Power (Power dissipated)
• Transition Temperature	T_C , MPB	Temperature usage range Temperature dependence

Fig. 1.
Relationship between material property and device performance.

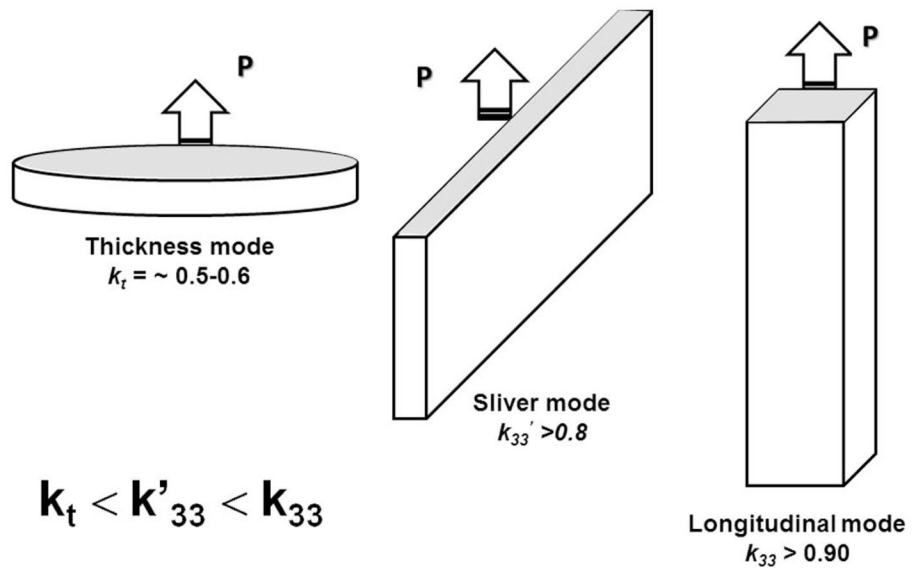


Fig. 2. The comparison of the electromechanical coupling for thickness, sliver, and longitudinal single-crystal samples.

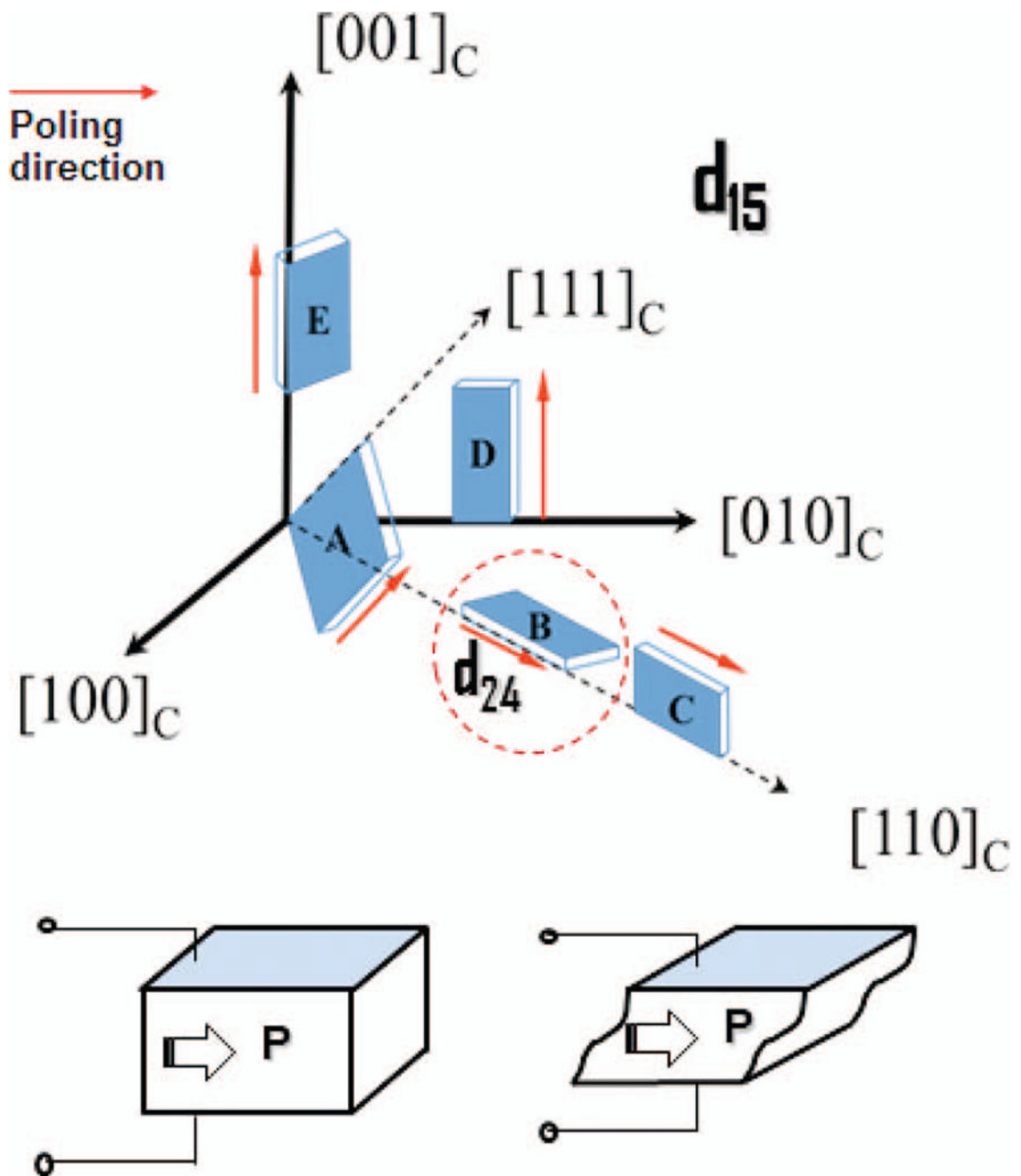


Fig. 3.
 (top) Schematic figure of the various thickness-shear mode samples of relaxor-PT crystals (adapted from [33]) and (bottom) the related thickness-shear piezoelectric deformation. The arrows represent the poling direction.

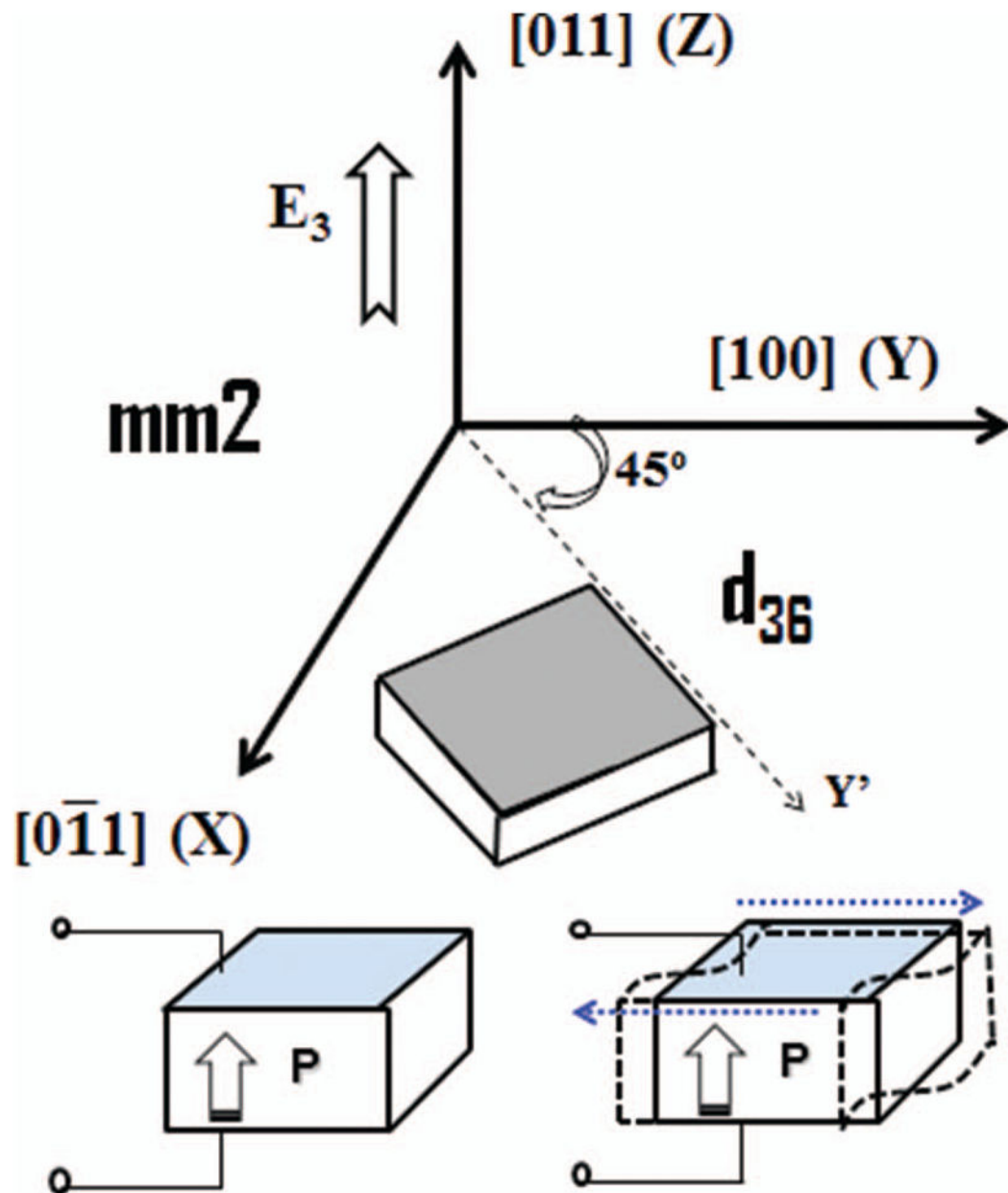


Fig. 4. (top) Schematic of $Z_t \pm 45^\circ$ -cut sample and (bottom) related face-shear piezoelectric deformation. The arrow represents the poling direction (adapted from [46]).

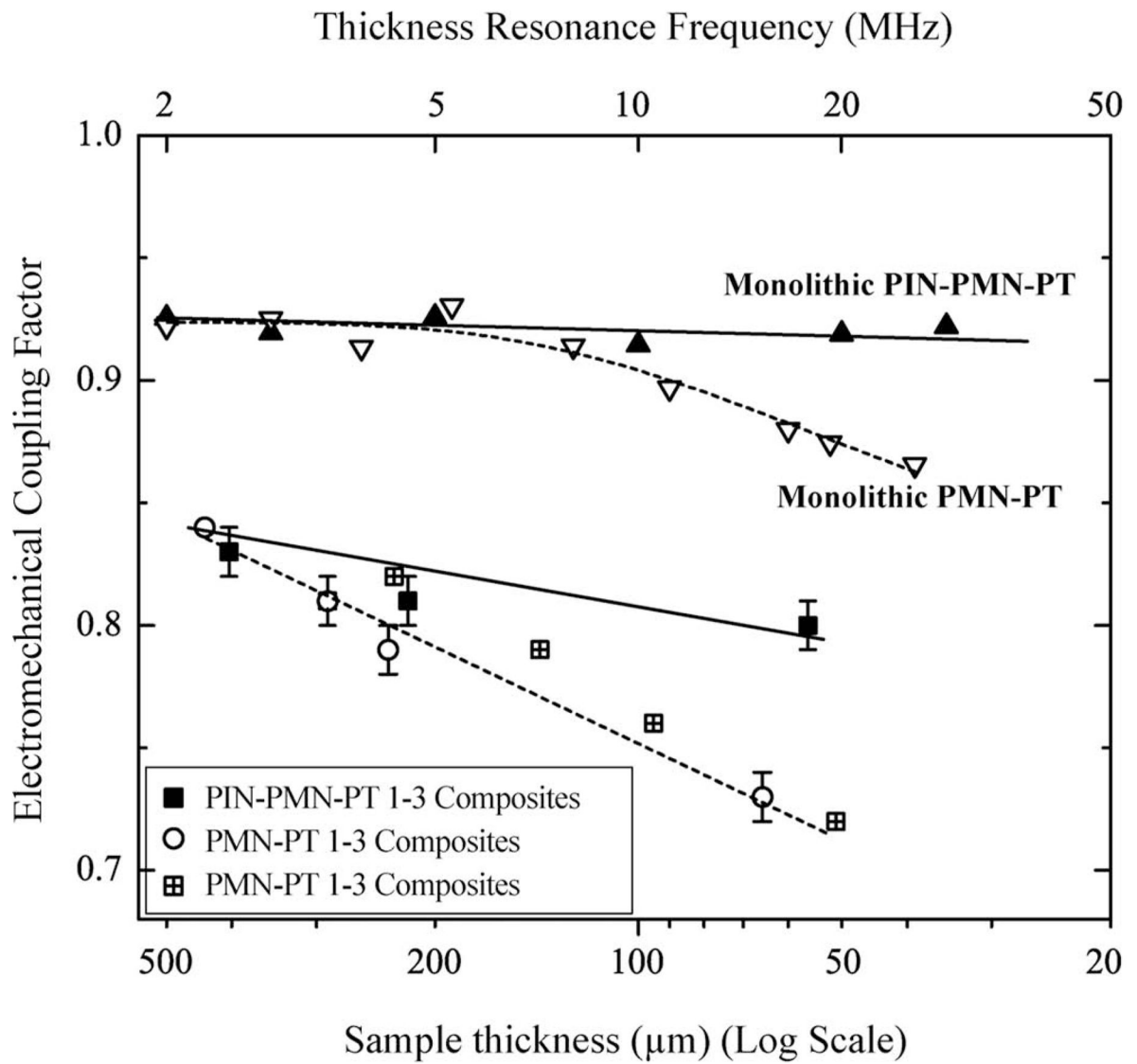


Fig. 5. Electromechanical coupling factor for monolithic and crystal/epoxy 1-3 composites as a function of sample thickness and corresponding ultrasound frequency (after [44] copyright © 2010, the American Institute of Physics).

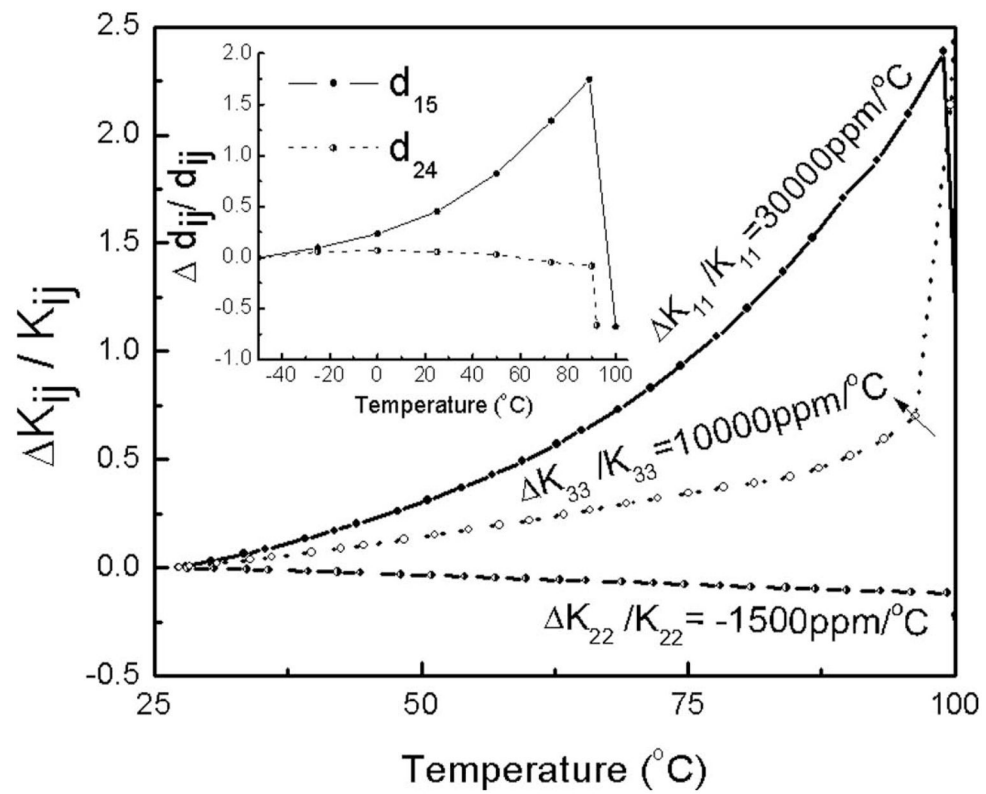


Fig. 6. Dielectric permittivity variation as a function of temperature for [011]-poled single-domain crystals; the small inset shows the shear piezoelectric variation as a function of temperature (after [26] copyright © 2011, the American Institute of Physics).

TABLE I

Property Comparison of Single Crystals and Polycrystalline Ceramics.

	T_C (°C)	T_{RT} (°C)	K	loss	d_{33} (pC/N)	k_{33}	s_{33}^E (pm ² /N)	E_C (kV/cm)	Q_m
Generation I	135	95	5400	0.004	1540	0.91	60.0	2.3	120
Generation II	191	125	4400	0.004	1510	0.92	69.0	5.0	180
Generation III	193	128	3810	0.002	1340	0.92	62.4	5.0	700
PZT5H	193	/	3400	0.02	600	0.75	20.7	7.0	70
PZT5A	365	/	1700	0.02	370	0.71	18.8	18	70
PZT4	328	/	1300	0.004	290	0.70	14.9	14	500
PZT8	300	/	1000	0.004	230	0.64	14.6	18	1000

Ceramics data are from [8].

TABLE II

Piezoelectric Property Comparison for Relaxor-PT Crystals With Various Vibration Modes.

Vibration mode	ϵ_i/ϵ_0	d_{ij} (pC/N)	k_{ij}	s_{ij}^E (pm ² /N)
Longitudinal $ij = 33$ [001]	6000	2000	0.90	93.0
Lateral $ij = 32$ [011]	4500	-1780	0.90	100
Shear $ij = 15$ [111]	8130	3700	0.93	220

Data are from [1], [46].

TABLE III

Shear Mode Property Comparison for Single Crystals and Polycrystalline Ceramics.

	d_{15} (pC/N)	d_{24} (pC/N)	s_{55}^E (pm ² /N)	Q
Rhom 1R	3700	3700	220	~30
Rhom 2R	3350	160	208	~40
Orthor 1O	4550	4100	316	~30
Tetra 1T	2350	2350	55	~30
PZT4	500	500	39	~70
PZT8	330	330	32	~160
PZT5A	580	580	48	~15
PZT5H	740	740	44	~15

Data are from [1], [46].

TABLE IV

Drive Field Stability of Shear Vibration for Relaxor-PT Single Crystals, (PIN: PIN-PMN-PT; PIN-Mn: Mn:PIN-PMN-PT).

Material	Vibration	E_C (kV/cm)	Allowable drive field (kV/cm)	Field stability ratio (%)
PMNT	d_{15} (2R)	2.5	1.0	40
PIN	d_{15} (2R)	5	2.0	40
PIN	d_{24} (1O)	5	2.0	40
PIN-Mn	d_{15} (2R)	7.3	5.0	68
PIN-Mn	d_{24} (1O)	4.5	3.0	65
PIN	d_{36} (2R)	5	5.0	100

Data are from [33], [46].

TABLE V

Piezoelectric Face Shear Properties for Single Crystals With Rhombohedral Phase (PIN-Mn: Mn:PIN-PMN-PT).

	d_{36} (pC/N)	k_{36}	s_{66}^E (pm ² /N)	Q_{36}
PMNT (low PT)	1730	0.78	129	200
PMNT (high PT)	2800	0.83	225	150
PIN-Mn (low PT)	1810	0.80	166	500
PIN-Mn (high PT)	2270	0.82	230	300

Data are from [46]. Mechanical Q s were measured using $4 \times 4 \times 1$ mm devices.