

Simultaneous time-temperature-thickness superposition theoretical and statistical modelling of convective drying of guava

Siok Peng Kek · Nyuk Ling Chin · Yus Aniza Yusof

Revised: 15 September 2012 / Accepted: 4 January 2013 / Published online: 22 January 2013
© Association of Food Scientists & Technologists (India) 2013

Abstract Modelling studies of guava drying and quality are presented using theoretical and statistical models by varying temperature from 55 to 75 °C and slice thickness from 3 to 9 mm. The quality of dried fruit was measured for its water activity, colour, vitamin C, and texture. The superposition technique with Midilli-Kucuk model showed efficiency in modelling the drying process with $R^2=0.9991$. The second-order polynomial equations adequately described the quality of dried guava with regression coefficient, $R^2>0.7$. Drying time was a good function of temperature and thickness ($P<0.001$); water activity, colour and vitamin C showed strong dependence on temperature ($P<0.1$); while texture was mainly influenced by its thickness ($P<0.005$). The optimum drying temperature of 70 °C at slice thickness of 6 mm was determined using the desirability function method. Simultaneous modelling using the theoretical and statistical drying models provides information on water diffusion and evaporation with the drying responses and factors.

Keywords Guava · Modelling · Drying · Optimisation · Time-temperature superposition technique

Introduction

The aim of modelling is to establish a quantitative relationship between independent and dependent variables using mathematical and statistical methods in characterising how one variable affects the other (Huang et al. 2001). The disadvantage of a statistical model is that it derives

relationship between variables based on conventional linear regression techniques *e.g.* the simple and multiple regressions. Although these models are useful in investigating the possible effects of certain variable (Rahman 2005), they lack in providing understanding on its process mechanisms. In theoretical models, mathematical models are established using laws, theorems, principles, and assumptions about the phenomena which provide more information about the process variables.

The thin-layer drying models proposed for evaluating drying behaviour are reported as theoretical (Fick's second law of diffusion), semi-theoretical and empirical in fruit drying studies which include apple (Sacilik and Elicin 2006), strawberries (Akpınar and Bicer 2006), kiwifruits (Kaya et al. 2010) and a range of tropical fruits, like chempedak (Chong et al. 2008a), salak (Ong and Law 2009) and litchi (Janjai et al. 2010). The semi-theoretical model which is derived from Fick's second law is the most commonly adapted to predict drying kinetics of food materials. They often give good estimation by incorporating lump sum values of other effects into the model parameters (Ong and Law 2009). They are simpler and do not need assumptions of sample geometry, mass diffusivity and conductivity. While the empirical models contain parameters that have no physical meaning as they neglect the fundamentals of the drying process (Akpınar and Bicer 2006), the semi-theoretical models have limitations of reporting drying time for specific drying conditions.

The superposition technique is applicable to model the complex drying data into a single master curve which incorporates a large number of variables for prediction of drying kinetics. This time-temperature superposition technique (TTST) is also known as the reduced parameters technique which is used in modelling of rheological behaviour of polymeric materials and fluid food (Steffe 1996; Chin et al. 2009). TTST was used to model the effect of air temperature and slice

S. P. Kek · N. L. Chin (✉) · Y. A. Yusof
Department of Process and Food Engineering,
Faculty of Engineering, Universiti Putra Malaysia,
43400 UPM Serdang, Selangor, Malaysia
e-mail: chinnl@eng.upm.edu.my

thickness on drying kinetics of tomato slices and Avishan leaves at different temperatures and velocities (Khazaei et al. 2008b; Khazaei et al. 2008a). The use of TTST in modelling could reduce model constants and enhance the fitted semi-theoretical model to be a single and general model which represents the overall drying kinetics of a dried fruit.

The objective of this research was to model guava fruit drying using both theoretical and statistical models to obtain a qualitative understanding of the drying process and quantitative evaluation of product evolution to desired quality attributes for ease of control in a food drying process and optimisation. The effect of temperature and slice thickness on the drying kinetics of dried guava was investigated through TTST modelling. The optimum drying condition to produce dehydrated products with low water activity, high vitamin C retention, attractive colour, and acceptable texture for minimum processing time was determined using response surface methodology (RSM) with aim of producing dried guava to be used as dried fruit ingredients (Myers et al. 2009).

Materials and methods

Materials

Fresh guava fruits (*Psidium guajava*; Kampuchea cultivar Vietnam, GU8) were obtained from Kampung Pelegong, Labu, Negeri Sembilan, Malaysia. Guava fruits are widely planted for fresh consumption and it is one of the top tropical fruits rich in vitamin C content. The initial moisture content of guava slices was determined by heating in a convection oven (UM500, Memmert GmbH, Schwabach, Germany) at 105 °C for 48 h following the AOAC method, 931.04 (AOAC 1990). Guava samples were kept in refrigerator at 10 °C to maintain its maturity before use and they were in the range of 8.0±0.2 °Brix.

Drying process

Guava samples were cut vertically into quarters and its core with seeds removed. Each fruit slice was then cut horizontally to their axis into three different thicknesses of 3, 6, and 9 mm with top surface area of 20 mm×20 mm, measured to ±0.02 mm using a digital caliper (Mitutoyo, Japan) from the white fleshy part of guava fruit. The guava slices were placed in stainless steel petri dishes and dried at temperature of 55, 65, or 75 °C in a convection oven. Samples were removed at various intervals and weighed, before returning to the oven to continue drying. The weight loss of samples was determined using an electronic balance (Ross B204-S, Mettler Toledo, Swiss). Weighing interval of 15 min was used during the first hour drying, 30 min the following next 2 h, and a 60 min' interval until the calculated final moisture

content of the guava reached approximately 20 % (w.b.). Each run was performed in an identical manner and replicates of four were obtained from the same batch of fruits.

Determination of effective diffusivity and activation energy

The guava slices were assumed in the form of infinite slab and the analytical solution of the Fick's second law is given as (Crank 1975):

$$\frac{M_t - M_e}{M_0 - M_e} = MR = \frac{8}{\pi^2} \sum_{i=1}^{\infty} \frac{1}{(2i-1)^2} \exp \left[-\frac{(2i-1)^2 \pi^2 D_{eff} t}{4h^2} \right] \quad (1)$$

where MR is the dimensionless moisture ratio, M_t is the moisture content at any time, t (g water/g dry solids), M_e is the equilibrium moisture content, M_0 is the initial moisture content, D_{eff} is the effective diffusivity, h is the thickness of the guava slice (mm) where drying occurs from only one side, and i is a positive integer.

Thus, for sufficiently long drying time, Fick's second law is simplified and expressed in a logarithmic form as shown in Eq. (2) with its dimensionless moisture ratio (MR) simplified to M_t/M_0 due to relatively small M_e compared to M_t or M_0 (Doymaz 2009; Sacilik and Elicin 2006).

$$\ln \left(\frac{M_t}{M_0} \right) = \ln \frac{8}{\pi^2} - D_{eff} \left(\frac{\pi^2}{4h^2} \right) t \quad (2)$$

The effective diffusivity of dried guava was calculated from the slope of the logarithm form of simple diffusion model from Eq. (2).

$$Slope = -D_{eff} \left(\frac{\pi^2}{4h^2} \right) \quad (3)$$

The effective diffusivity, as a function of the drying temperature, was correlated by an Arrhenius-type equation where activation energy was determined.

$$D_{eff} = D_0 \exp \left(-\frac{E_a}{RT_{abs}} \right) \quad (4)$$

D_0 is the Arrhenius diffusivity constant, E_a is the activation energy (kJ/mol), R is the universal gas constant (8.314 J/mol K), and T_{abs} is the absolute temperature in Kelvin.

The effective diffusivity was also reported as a function of the drying temperature and sample thickness in the Arrhenius-type equation using multiple regression analysis (Panchariya et al. 2002; Khazaei et al. 2008b).

$$D_{eff} = (\alpha_0 h^{\alpha_1}) \exp \left(-\frac{\alpha_2}{T_{abs}} \right) \quad (5)$$

where T_{abs} is the absolute temperature, h is the slice thickness (mm), α_0 , α_1 , and α_2 are constants.

Model development

Theoretical modelling

A 3² factorial design experiment with drying temperatures of 55, 65 and 75 °C and slice thickness of 3, 6 and 9 mm which gave a total of 9 runs was conducted for drying kinetics studies. The experimental data of drying curves, *MR(t)* was fitted to the selected semi-theoretical thin layer drying models shown in Table 1. In selecting the best suited model describing the drying process of guava, curve fitting was performed by computing the sum square errors (*SSE*) and minimising it with the least square method using Microsoft Excel SOLVER tool (Microsoft Office Professional 2007, USA). The generalised reduced gradient (GRG2) nonlinear optimisation code was adopted in determining the model constants, *a*, *b*, *c*, *k* and *n*.

The dependence of the drying rate constant, *k* selected from the best fitted model on drying temperature and slice thickness variables was then described in the Arrhenius-type model using multiple regression analysis (Panchariya et al. 2002; Khazaei et al. 2008b):

$$k = (\alpha_0 h^{\alpha_1}) \exp\left(-\frac{\alpha_2}{T_{abs}}\right) \tag{6}$$

where *T_{abs}* is the absolute temperature, *h* is the slice thickness (mm), α_0 , α_1 , and α_2 are constants.

Time-temperature-thickness superposition

A total of nine average drying curves sharing the same data for theoretical modelling were superposed by shifting along the abscissa to form a master curve in two steps of shifting. The drying curves, *MR(t)* of three slice thickness at common drying temperature were first shifted horizontally on the log (time) axis to a reference slice thickness of 6 mm to obtain the dimensionless time-thickness shift factors, *a_{h,i}*:

$$\log a_{h,i} = \log t_R - \log t_i \tag{7}$$

where *t_R* = time at reference thickness and *t_i* = time at other thickness for each moisture ratio ranging between 0.1 and 0.8. At reference thickness, $\log a_{h,R}=0$, where *a_h* at

Table 1 Common semi-theoretical models applied to the drying curves of guava slices

| No. | Model name | Model equation |
|-----|---------------------|---|
| 1 | Newton | <i>MR</i> = exp(- <i>kt</i>) |
| 2 | Page | <i>MR</i> = exp(- <i>ktⁿ</i>) |
| 3 | Henderson and Pabis | <i>MR</i> = <i>a</i> exp(- <i>kt</i>) |
| 4 | Logarithmic | <i>MR</i> = <i>a</i> exp(- <i>kt</i>) + <i>c</i> |
| 5 | Two term | <i>MR</i> = <i>a</i> exp(- <i>k₁t</i>) + <i>b</i> exp(- <i>k₂t</i>) |
| 6 | Midilli-Kucuk | <i>MR</i> = <i>a</i> exp(- <i>ktⁿ</i>) + <i>bt</i> |

reference is 1. When *t_R* = *t·a_h*, where the quantity *t·a_h* is known as the reduced or pseudo time, *t'* (Khazaei et al. 2008b), the horizontal shifting with average *a_h* forms one master curve *MR(t')* for each drying temperature.

Subsequently, the three developed temperature master curves were shifted to a reference temperature of 65 °C to construct a single master curve with the average temperature shift factor of *a_T* following Eq. (7). The final master curve *MR(t'')* where *t''=t·a_h·a_T* was used to estimate moisture ratio of guava slices at temperature of 55–75 °C and thickness of 3–9 mm. The final single master curve was fitted to all six semi-theoretical models (Table 1) to obtain the best fitted universal moisture ratio master curve as a function of time, temperature and thickness, *MR(t,T,h)*.

Statistical modelling

Response surface methodology (RSM) was used to design the experiment and determine the adequate model for dried guava quality analysis using Minitab Statistical Software (Version 15, Minitab Inc., USA). A face-centred central composite design was chosen to evaluate the relationship of drying temperature and slice thickness as independent variables, *X* to the dependent responses, *Y* which included the drying time, water activity, colour, vitamin C, and texture of dried guava. The complete design consisted 13 sets of test conditions including five replicates of the centre point (Table 2) which shared the same data for 9 experimental runs conducted for theoretical modelling.

Second-order polynomial model equation (Eq. (8)) was defined and fitted for each response from the experimental data.

$$Y = \beta_0 + \beta_1 X_1 + \beta_2 X_2 + \beta_{11} X_1^2 + \beta_{22} X_2^2 + \beta_{12} X_1 X_2 \tag{8}$$

Y indicates the estimated response, β_0 , β_1 , β_2 , β_{11} , β_{22} , and β_{12} are constant coefficients where β_0 is a constant, β_1

Table 2 Face-centred central composite design matrix used to evaluate the effects of processing variables (uncoded) on quality properties of guava slices

| Runs | Temperature (°C) | Thickness (mm) |
|-----------------|------------------|----------------|
| 1 | 75 | 3 |
| 2 | 65 | 9 |
| 3 | 55 | 6 |
| 4 | 55 | 3 |
| 5 ^a | 65 | 6 |
| 6 ^a | 65 | 6 |
| 7 ^a | 65 | 6 |
| 8 | 55 | 9 |
| 9 ^a | 65 | 6 |
| 10 | 65 | 3 |
| 11 ^a | 65 | 6 |
| 12 | 75 | 6 |
| 13 | 75 | 9 |

^acentre point

and β_2 are coefficients for linear terms, β_{11} and β_{22} are coefficients for quadratic terms, and β_{12} is the coefficient for interaction terms. X_1 and X_2 are the uncoded values of the independent variables of drying temperature ($^{\circ}\text{C}$) and slice thickness (mm), respectively.

Quality parameters

Water activity

The water activity of the dried samples was determined using a water activity meter (FA-st, GBX, Bourge de Peage, France). Each water activity measurement was based on the average values of three measurements.

Colour analysis

The colour of the samples was measured using UltraScan PRO Spectrophotometer (Hunter Associates Laboratory, Inc., VA, U.S.A.). The colour was expressed in terms of L (lightness), a (redness) and b (yellowness) according to the Hunter Lab colour scale. The total colour change (ΔE) is calculated from the L , a , and b values.

$$\Delta E = \sqrt{(L_i - L_f)^2 + (a_i - a_f)^2 + (b_i - b_f)^2} \quad (9)$$

where i and f indicates the initial colour values of fresh samples and final colour values of dried samples respectively.

Texture analysis

Texture Profile Analysis (TPA) was used to determine the texture of the samples by using a texture analyser (TA-XT_{plus}, Stable Micro Systems, Surrey, U.K.). Samples were placed horizontally at the centre of platform. Two compression cycles were performed on samples with a 2.0 mm diameter cylinder stainless steel probe at strain 50 % of sample height with 5 s between cycles. The pre-test speed was 1.0 mm/s, test speed was 5.0 mm/s, post-test speed was 5.0 mm/s, and the trigger force was 5 g. Hardness, springiness, cohesiveness, and chewiness of the samples were computed from each TPA curve using the texture analyser software macro (TEE 32 Stable Micro System, UK). The textural measurement was based on the average values from the four samples slices for each combination of drying temperature and slice thickness.

Vitamin C analysis

The vitamin C contents of samples were determined with a standard vitamin C measurement (Boyer 1986). Each sample was weighed and ground in a porcelain mortar with 25 ml of the metaphosphoric acid 4 % solution, HPO_3 .

The liquid extract was poured into 100 ml volumetric flask and the solid residual was again ground with 25 ml of the HPO_3 solution. Total volume of liquid extract was made up to 100 ml with HPO_3 solution. The solution was filtered and 10 ml of the filtrate was transferred into an Erlenmeyer flask. The filtrate was titrated with 2,6-Dichlorophenolindophenol solution until a distinct rose-pink colour persisted for 10 to 20 s. Each measurement was based on the average values of three determinations. 10 ml of HPO_3 solution was also titrated as blank.

Statistical analysis

The goodness of fit of the proposed semi-theoretical models was evaluated with the coefficient of determination (R^2), reduced chi-squared (χ^2), and root mean square error (RMSE) which was calculated as follow:

$$R^2 = 1 - \frac{SSE}{SST} \quad (10)$$

$$\chi^2 = \frac{\sum_{i=1}^N (MR_{exp,i} - MR_{pre,i})^2}{N - n} \quad (11)$$

$$RMSE = \left[\frac{1}{N} \sum_{i=1}^N (MR_{pre,i} - MR_{exp,i})^2 \right]^{1/2} \quad (12)$$

where SSE is the sum of square error, SST is the total corrected sum of squares, $MR_{exp,i}$ is the i^{th} experimentally observed moisture ratio, $MR_{pre,i}$ is the i^{th} predicted moisture ratio, N is the number of observations and n is the number of constants. R^2 was the primary criterion for selecting best fitted model with minimum SSE (Walpole et al. 2002).

The statistical models were tested for their adequacy by performing analysis of variance (ANOVA) to test the significance of the model. The suitability of the second-order polynomial function was judged by the associating it with probability (P value) and R^2 . The optimisation response variables were performed by using response optimiser option of MINITAB (Version 15) with the desirability function technique.

Verification of models

Experimental data for quality attributes and drying kinetics were obtained by conducting an independent set of experiment following the optimum conditions found. The experimental value was compared with the predicted from the optimised model by calculating the percentage error (Eq. (13)) to determine the adequacy of the drying kinetics and response surface models. The percentage

error, *PE* which is lower than 10 % indicates a good fit (McLaughlin and Magee 1998).

$$PE(\%) = \left(\frac{m_{exp} - m_{pre}}{m_{exp}} \right) * 100 \tag{13}$$

where m_{exp} is experimental value and m_{pre} is predicted value.

Results and discussion

Drying characteristics of dried guava

The initial moisture content of the fresh guava slices was 91.31 ± 0.59 % wet basis (w.b.) and it was dried until approximately 20.36 ± 1.05 % (w.b.) or about 0.2564 ± 0.0165 g water/g dry solids to achieve an edible form. Rapid drying to the range of 15–20 % moisture was suggested to minimise the time for Maillard browning (DeLong 1992; Sagar and Suresh 2010). Figure 1 shows the variation in drying rate as a function of moisture content. There was an initial transient state at the beginning of the drying process, where fresh guava slices at ambient needed some time to reach the set oven temperature before drying starts and the drying rate increased. It was also observed that the drying rate decreased continuously with decreasing moisture content or increasing drying time. Since fresh guava is high in moisture content, there was only the falling-rate period during the drying process (Bakshi and Singh 1980). The only falling-rate period proved that diffusion has pre-dominantly governed the moisture movement in the samples. This observation was in agreement with previous work on bananas (Nguyen and Price 2007), guava and papaya (Hawllader et al. 2006). Figure 1 illustrates that the higher the temperature and the thinner the material, the higher the drying rate due to high evaporation rate of moisture transfer from the surface to heated air and the reduced distance for the moisture travels in thinly slices. It was observed that the surface area to volume ratio is bigger for thin slices which increased the

exposure of samples to heated air. The calculated surface area to volume ratio for the 3, 6 and 9 mm samples are 0.87:1, 0.53:1 and 0.42:1, respectively. This has resulted the highest drying rates and least drying time for guava slices with smallest thickness of 3 mm at drying temperature of 75 °C. A thinner sample slice and higher drying temperature give a greater drying rate and shorter drying period, as reported in drying of apple slices (Sacilik and Elicin 2006) and chempedak (Chong et al. 2008a). No significant difference of drying rates between slice thickness of 6 and 9 mm as the curves were closed to each other in this study.

Effective diffusivity and activation energy

The effective moisture diffusivity, D_{eff} is an important mass transport property that refers to the rate of moisture movement in solids where water diffuses from inner regions (where moisture content is higher) to surface regions (with lower moisture content). The process of water evaporating off at the surface with sufficient heat supplied is accounted as the drying rate (Derossi et al. 2011). Lee and Kim (2009) and Nguyen and Price (2007) are in agreement that D_{eff} increases with temperature for the radish and banana samples studied respectively due to a rapid initial rate of moisture evaporation. However, with sample thickness, Lee and Kim (2009) reported that D_{eff} increased with reducing sample thickness while Nguyen and Price (2007) found otherwise. From the values of effective diffusivity tabulated in Table 3 for guava slices, D_{eff} increased about two times greater with every 3 mm increase in slice thickness, similar trend to those reported in Nguyen and Price (2007). Side diffusion of moisture migration might present in thick slabs which enhanced the diffusion defying assumptions of one-directional diffusion from inside to the surface of the slabs known as the edge effect. For the thinner slabs, a high temperature could have resulted a fast surface hardening where it slows down the drying rates and lowers the effective diffusivity.

Fig. 1 Effects of different slice thickness of guava slices at **a** 55 °C, **b** 65 °C and **c** 75 °C on drying rates given as means ± standard error ($n=4$)

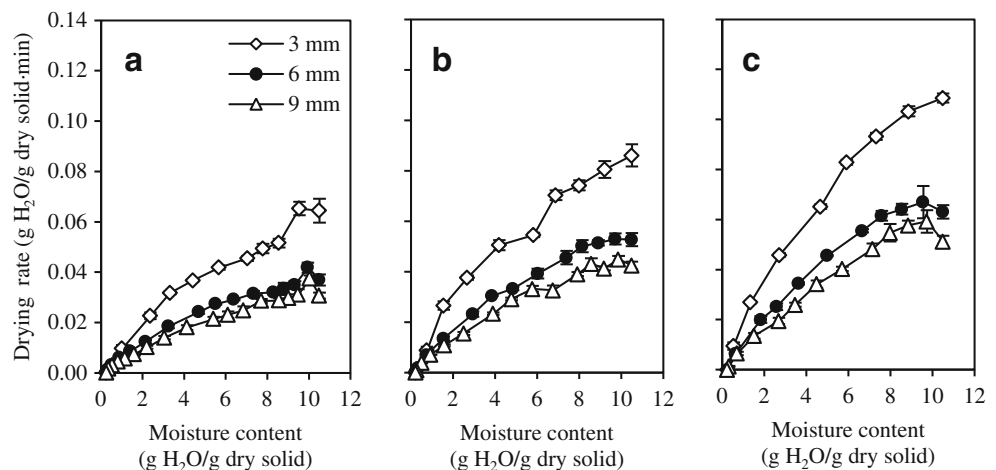


Table 3 Effective diffusivity, D_{eff} and constant diffusivity, D_o for different thickness and temperatures

| Thickness (mm) | Temperature (°C) | D_{eff} (m ² /s) | D_o (m ² /s) |
|----------------|------------------|-------------------------------|---------------------------|
| 3 | 55 | 5.139E-10 | 8.174E-05 |
| | 65 | 7.624E-10 | |
| | 75 | 1.021E-09 | |
| 6 | 55 | 1.312E-09 | 4.918E-05 |
| | 65 | 1.918E-09 | |
| | 75 | 2.395E-09 | |
| 9 | 55 | 2.357E-09 | 1.000E-04 |
| | 65 | 3.418E-09 | |
| | 75 | 4.338E-09 | |

The effective diffusivities of guava slices found were from 5.139×10^{-10} to 4.338×10^{-9} m²/s which is within the general range of 10^{-11} – 10^{-8} m²/s for 82 % of food materials (Marinos-Kouris and Maroulis 1995; Erbay and Icier 2009). The effect of temperature and thickness on effective diffusivity was tested with two-way analysis of variance (ANOVA). The effective diffusivity increased significantly when both drying temperature ($P=0.04$) and slice thickness ($P=0.003$) increased and the diffusivity of guava slices was a strong function of temperature and thickness. A multiple linear regression analysis was used to express the effective diffusivity, D_{eff} as a function of temperature, T and thickness, h following Eq. (5). High correlations between effective diffusivity with temperature and thickness in Eq. (14) verify that water diffusion is affected by both these factors. This water diffusion coefficient model for guava slices provides useful information through the diffusion rate in explaining the drying kinetics upon the conditions within the material.

$$D_{eff} = 7.465 \times 10^{-6} h^{1.351} \exp\left(-\frac{3621}{T_{abs}}\right) \quad (R^2 = 0.9972) \quad (14)$$

The activation energy, E_a is important in describing the sensibility of D_{eff} with temperature (Erbay and Icier 2009). The calculated activation energy using Eq. (4) was 32.63, 28.67, and 29.02 kJ/mol for guava thickness 3, 6, and 9 mm, respectively. These activation energy values are in the range of 15–40 kJ/mol for various food (Rizvi 1986). The greater value of activation energy for thickness 3 mm means more sensibility of effective diffusivities to temperature (Erbay and Icier 2009).

Drying models

Table 4 shows the goodness of fit of six common drying models and the Midilli-Kucuk model was the best model to represent the thin layer drying behaviour of guava slices at different drying temperatures and slice thickness based on

the criteria of the highest R^2 , lowest χ^2 and $RMSE$. Generally, R^2 , χ^2 , and $RMSE$ varied between 0.9982 and 0.9998, 3.048×10^{-5} and 2.726×10^{-4} , and 0.00434 and 0.01453, respectively. Figure 2 shows that the experimental moisture ratio was excellently fitted with the Midilli-Kucuk model which describes the drying kinetics of guava adequately.

The values of the Midilli-Kucuk model constants, a , k , n , and b are listed in Table 4. The drying rate constant, k increases with the increase in drying temperature and decrease of slice thickness. This indicated that higher temperature and smaller thickness enhanced the driving force of heat and mass transfer. However, a , b and n values did not show any clear trends as they may have depended on additional processing conditions. Similar findings on the model constants are reported in Khazaei et al.'s (2008b) work on tomato drying. Hence, the drying rate constant, k (min⁻¹) is correlated by the Arrhenius-type equation model as given in Eq. (15):

$$k = 5932h^{-0.6073} \exp\left(-\frac{4589}{T_{abs}}\right) \quad (R^2 = 0.9304) \quad (15)$$

By inserting function k (Eq. (15)) into the 4-term variables Midilli-Kucuk model, it allows the moisture ratio's expression to be reduced to a 3-term variable model known as the single model which is expressed as a function of drying time, drying temperature, and slice thickness (Eq. (16)), with constants $a=0.9915$, $n=1.198$ and $b=-1.930 \times 10^{-5}$ fitted using data obtained from entire experimental data.

$$MR(t, T, h) = 0.9915 \exp(-kt^{1.198}) + (-1.930 \times 10^{-5}) t \quad (R^2 = 0.9962, \chi^2 = 4.493 \times 10^{-4}, \& RMSE = 0.02092) \quad (16)$$

In general, the drying rate, dM/dt , drying rate constant, k , and effective diffusivities, D_{eff} of this guava drying study increased with drying temperature. The effective diffusivities increased with sample thickness, which also seem to give a lower drying rate (Fig. 1) and drying rate constant (Table 4). Although the effective diffusivity increased in thick guava slices, it did not manage to increase the drying rate, and this may be due to the reasons of insufficient heat to evaporate off the moisture that gathered at the surface in shorter period and the effect of lower surface-volume ratio in thicker samples. This was found similar to reports by Falade and Solademi (2010) and Khazaei et al. (2008b) on drying of sweet potato and tomato with no explanations given. In addition, the drying rate and drying rate constant can also be expressed as a function of effective diffusivities and thickness. Following the liquid diffusion theory (Geankoplis 2003), by rearranging and differentiating Eq. (2), the drying rate can be written as $\frac{dM}{dt} = \frac{\pi^2 D_{eff} M}{4h^2}$. When the slope in Eq. (3) was compared with the slope of Henderson and Pabis's Eq. in Table 1, the drying rate constant could be expressed as $k = \frac{\pi^2 D_{eff}}{4h^2}$ (Erbay and Icier

Table 4 Statistical parameters and model constants of semi-theoretical models for modelling the drying kinetics of guava slices

| Name of model | Statistical parameters and model constants | Various temperature-thickness combinations | | | | | | | | | | | | Master-curve 55–75 °C | Optimal condition 70 °C |
|----------------------------|--|--|------------|------------|------------|------------|------------|------------|------------|------------|------------|------------|------------|--------------------------|----------------------------|
| | | 55 °C | | | | 65 °C | | | | 75 °C | | | | | |
| | | 3 mm | 6 mm | 9 mm | 3 mm | 6 mm | 9 mm | 3 mm | 6 mm | 9 mm | 3 mm | 6 mm | 9 mm | | |
| Newton | R^2 | 0.9902 | 0.9890 | 0.9932 | 0.9855 | 0.9891 | 0.9910 | 0.9850 | 0.9873 | 0.9925 | 0.9897 | 0.9927 | 0.9897 | 0.9927 | |
| | χ^2 | 1.228E-03 | 1.407E-03 | 8.603E-04 | 1.753E-03 | 1.360E-03 | 1.153E-03 | 1.895E-03 | 1.521E-03 | 9.245E-04 | 1.205E-03 | 8.978E-04 | 1.205E-03 | 8.978E-04 | |
| Page | <i>RMSE</i> | 0.03366 | 0.03632 | 0.02851 | 0.03972 | 0.03543 | 0.03280 | 0.04104 | 0.03719 | 0.02921 | 0.03456 | 0.02869 | 0.03456 | 0.02869 | |
| | R^2 | 0.9977 | 0.9988 | 0.9994 | 0.9978 | 0.9989 | 0.9993 | 0.9988 | 0.9993 | 0.9997 | 0.9988 | 0.9995 | 0.9988 | 0.9995 | |
| Henderson and Pabis | χ^2 | 3.095E-04 | 1.584E-04 | 7.789E-05 | 2.982E-04 | 1.497E-04 | 8.934E-05 | 1.767E-04 | 8.645E-05 | 3.618E-05 | 1.452E-04 | 6.237E-05 | 1.452E-04 | 6.237E-05 | |
| | <i>RMSE</i> | 0.01618 | 0.01177 | 0.00832 | 0.01545 | 0.01126 | 0.00880 | 0.01172 | 0.00841 | 0.00553 | 0.01195 | 0.00721 | 0.01195 | 0.00721 | |
| Logrithmic | R^2 | 0.9922 | 0.9921 | 0.9953 | 0.9887 | 0.9922 | 0.9938 | 0.9882 | 0.9914 | 0.9954 | 0.9925 | 0.9950 | 0.9925 | 0.9950 | |
| | χ^2 | 1.065E-03 | 1.087E-03 | 6.290E-04 | 1.534E-03 | 1.052E-03 | 8.469E-04 | 1.698E-03 | 1.147E-03 | 6.242E-04 | 8.798E-04 | 6.771E-04 | 8.798E-04 | 6.771E-04 | |
| Two term | <i>RMSE</i> | 0.03002 | 0.03084 | 0.02365 | 0.03503 | 0.02984 | 0.02709 | 0.03634 | 0.03064 | 0.02298 | 0.02941 | 0.02375 | 0.02941 | 0.02375 | |
| | R^2 | 0.9961 | 0.9976 | 0.9988 | 0.9976 | 0.9979 | 0.9981 | 0.9980 | 0.9979 | 0.9984 | 0.9974 | 0.9982 | 0.9974 | 0.9982 | |
| Midilli-Kucuk ^a | χ^2 | 5.906E-04 | 3.568E-04 | 1.702E-04 | 3.778E-04 | 3.126E-04 | 2.821E-04 | 3.449E-04 | 3.066E-04 | 2.316E-04 | 3.062E-04 | 2.655E-04 | 3.062E-04 | 2.655E-04 | |
| | <i>RMSE</i> | 0.02131 | 0.01703 | 0.01191 | 0.01626 | 0.01551 | 0.01502 | 0.01516 | 0.01493 | 0.01335 | 0.01720 | 0.01411 | 0.01720 | 0.01411 | |
| Midilli-Kucuk ^a | R^2 | 0.9922 | 0.9921 | 0.9953 | 0.9887 | 0.9922 | 0.9938 | 0.9882 | 0.9914 | 0.9954 | 0.9925 | 0.9950 | 0.9925 | 0.9950 | |
| | χ^2 | 1.302E-03 | 1.268E-03 | 7.189E-04 | 2.045E-03 | 1.286E-03 | 1.001E-03 | 2.377E-03 | 1.475E-03 | 7.629E-04 | 8.953E-04 | 8.463E-04 | 8.953E-04 | 8.463E-04 | |
| Midilli-Kucuk ^a | <i>RMSE</i> | 0.03002 | 0.03084 | 0.02365 | 0.03503 | 0.02984 | 0.02709 | 0.03634 | 0.03064 | 0.02298 | 0.02941 | 0.02375 | 0.02941 | 0.02375 | |
| | R^2 | 0.9982 | 0.9994 | 0.9997 | 0.9989 | 0.9995 | 0.9996 | 0.9996 | 0.9998 | 0.9998 | 0.9991 | 0.9997 | 0.9991 | 0.9997 | |
| Midilli-Kucuk ^a | χ^2 | 3.048E-04 | 1.004E-04 | 4.090E-05 | 1.958E-04 | 9.103E-05 | 5.708E-05 | 9.054E-05 | 3.478E-05 | 2.726E-05 | 1.028E-04 | 4.844E-05 | 1.028E-04 | 4.844E-05 | |
| | <i>RMSE</i> | 0.01453 | 0.00868 | 0.00564 | 0.01084 | 0.00794 | 0.00647 | 0.00709 | 0.00470 | 0.00434 | 0.00964 | 0.00568 | 0.00964 | 0.00568 | |
| Midilli-Kucuk ^a | k (min ⁻¹) | 2.592E-03 | 1.348E-03 | 1.579E-03 | 4.402E-03 | 2.493E-03 | 1.943E-03 | 5.779E-03 | 3.308E-03 | 3.206E-03 | 2.436E-03 | 3.861E-03 | 2.436E-03 | 3.861E-03 | |
| | n | 1.217 | 1.230 | 1.163 | 1.185 | 1.195 | 1.197 | 1.201 | 1.198 | 1.164 | 1.200 | 1.165 | 1.200 | 1.165 | |
| Midilli-Kucuk ^a | a | 0.9821 | 0.9839 | 0.9899 | 0.9920 | 0.9911 | 0.9901 | 0.9952 | 0.9964 | 0.9987 | 0.9898 | 0.9949 | 0.9898 | 0.9949 | |
| | b (min ⁻¹) | -2.218E-05 | -2.660E-05 | -2.284E-05 | -1.853E-04 | -5.936E-05 | -2.735E-05 | -2.048E-04 | -9.348E-05 | -2.856E-05 | -4.144E-05 | -3.690E-05 | -4.144E-05 | -3.690E-05 | |

^a best fitted model

2009). Both equations show that the drying rate and drying rate constant are inversely proportional to the square of the thickness (Mittal 1999) which supported that thickness could give low drying rates and drying rate constants.

Master curve

Drying curves in Fig. 2 show a similar trend for the different thicknesses and temperatures. This suggests that the master-curve technique could be used to obtain a general drying kinetics model describing the drying behaviour of guava slices. With the reference of 6 mm slice thickness, the master curve for each temperature was obtained (Fig. 3) through the average time-thickness shifting factors, a_h (Table 5) which combines the effect of the drying time and slice thickness into a single value of reduced time t' . Time-thickness shift factor, a_h was regressed into the Arrhenius-type equation as a function of thickness, h (mm) and temperature, T_{abs} (K).

$$a_h = 4.0h^{-0.6216} \exp\left(-\frac{57.29}{T_{abs}}\right) \quad (R^2 = 0.9880) \quad (17)$$

Master curves in terms of $t \cdot a_h$ in Fig. 3 were shifted again to drying temperature of 65 °C, acting as the reference to generate a single master curve (Fig. 4) of moisture ratio as a function of reduced time t'' . The relationship between temperature shift factor a_T and temperature, T (°C) was determined as follow:

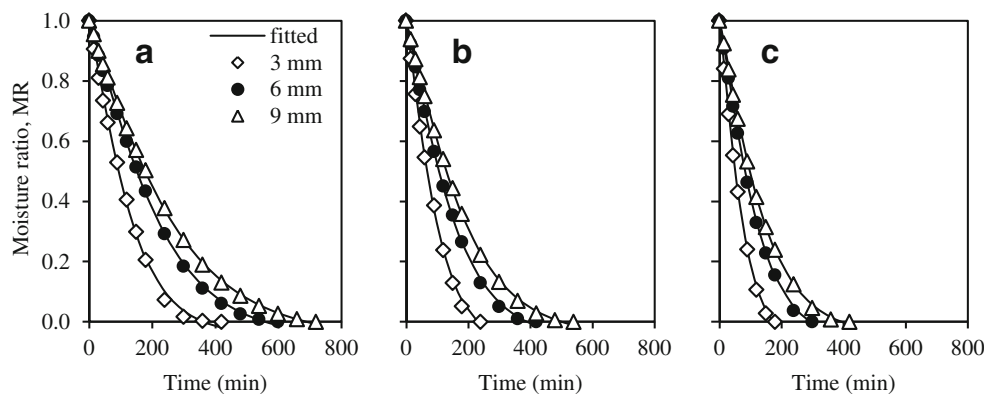
$$a_T = 0.02888T - 0.8847 \quad (R^2 = 0.9995) \quad (18)$$

The final master curve was fitted with the selected semi-theoretical models in Table 1 in order to derive a relationship between moisture ratio, drying time, drying temperature, and slice thickness. The master curve that combines drying time, temperature, and thickness was best fitted with the Midilli-Kucuk model (Table 4).

$$MR(t'', T, h) = 0.9898 \exp\left[-2.436 \times 10^{-3}(t'')^{1.2}\right] - 4.144 \times 10^{-5}(t'') \quad (R^2 = 0.9991, \chi^2 = 1.028 \times 10^{-4}, \& RMSE = 0.009964) \quad (19)$$

where $t'' = t \cdot a_h \cdot a_T$

Fig. 2 Moisture ratio as a function of drying time for different slice thickness for temperatures at **a** 55 °C, **b** 65 °C and **c** 75 °C and fitted with the Midilli-Kucuk model



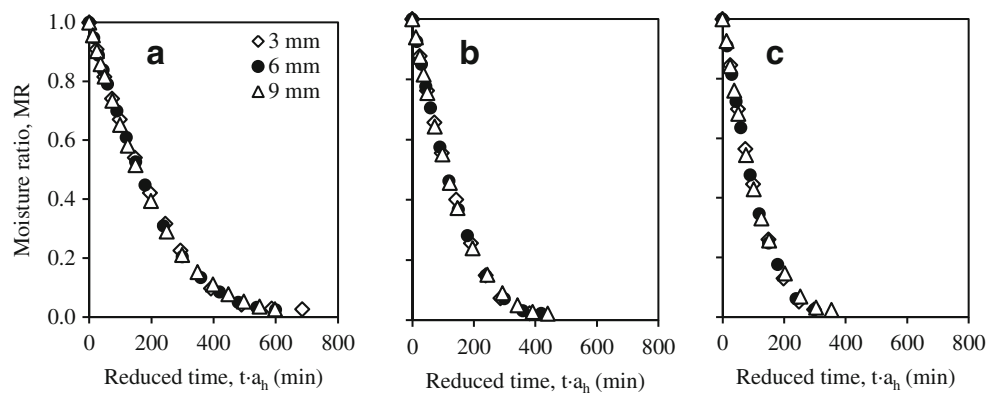
A comparison between R^2 for the master curve fitted with Midilli-Kucuk model for Eq. (19) generated using the superposition technique and the single model in Eq. (16) shows that the superposition technique has higher accuracy in predicting the moisture ratio of guava slices. The results indicated that curve shifting based on the time-temperature-thickness superposition technique is applicable in the drying process to predict the moisture ratio.

Statistical model for product quality

Table 6 lists the coefficients for the response surface equations in uncoded units with indication of significance through its P -value. All the response models were statistically significant at $P < 0.1$ with acceptable R^2 values ($R^2 > 0.7$) and non-significant lack-of-fit. The coefficient of determination, R^2 was used to validate each of the models and explained the overall predictive capability of the model. Granato et al. (2010) stated that the value of $R^2 \geq 70\%$ was considered good for sensory, colorimetric and physico-chemical results. The regression models for the quality attributes of dried guava were fitted adequately with the second-order polynomial model. A close observation on the effect of temperature and thickness on the quality attributes of dried guava showed that water activity, colour and vitamin C were significantly affected by the temperature ($P < 0.1$); while thickness had more influence on hardness and chewiness ($P < 0.005$). The combined effect of drying temperature and slice thickness on any response are visualised by the three dimensional surface plots for the fitted model as the function of these two independent variables in Fig. 5.

Drying time is an external condition that affects fruit quality directly and indirectly. Prolonged exposure to drying environment causes degradation of fruit properties. Apart from displaying moisture distribution through the drying curve plot, the statistical model fitting of drying time shows a strong function of drying temperature and slice thickness where it was significantly affected by all the model terms ($P < 0.05$) as shown in Table 6. Figure 5(a) shows that drying time increased with decreasing drying temperature from 75 °C to

Fig. 3 Master-curves fitted with Midilli-Kucuk model showing moisture ratio versus reduced time with reference thickness of 6 mm at temperatures **a** 55 °C, **b** 65 °C and **c** 75 °C



55 °C, and increasing slice thickness. With a reference of drying time for thickness 3 mm as basis, the drying time increased by 42.9 %, 75.0 %, and 66.7 % for 6 mm thickness, 71.4 %, 125 %, and 133 % for 9 mm at drying temperatures of 55 °C, 65 °C, and 75 °C, respectively.

Water activity (a_w) is referred for food stability and safety control as it is very much linked to microbial growth, rates of deteriorative reactions and chemical/physical properties (Jangam and Mujumdar 2010). Water activity of fresh guava was as high as 0.954 ± 0.002 but after drying, it reduced significantly to a range of 0.45–0.55 (Fig. 5(b)). Despite these small variations of water activities was due to minor variances in the final moisture content of dried guava at the end of drying, these hot air-dried guava are safe for storage as they achieved the minimum level of below 0.62 for storage to prohibit microbial growth (Patkai 2006; Jangam and Mujumdar 2010). Beauchat (1981) and Fellows (1988) also reported that $a_w = 0.60$ was the lowest limit for growth of osmophilic or xerophilic yeast and fungi for dried fruit with 15–20 % water. Water activity of dried guava was significantly affected ($P < 0.10$) by temperature and the quadratic of temperature model terms (Table 6).

Colour is the key of attractiveness and directly affects consumers' acceptance on foods. High colour change indicates the dried samples are far different from fresh fruit. Figure 5(c) shows that total colour change (ΔE) of guava

slices decreased when temperature and thickness decreased. Higher temperature and longer drying times were observed to degrade colour much due to the natural fruit pigment losses and non-enzymatic browning reactions. Highest colour change occurred when drying at the highest temperature of 75 °C for the longest duration of 420 min. The colour change during drying is mainly caused by chemical and biochemical reactions of the surface characteristics of food (Perera 2005). Pott et al. (2005) also found noticeable colour change towards the red hue and caused by browning reaction when high air temperatures and excessive drying times were applied on dried mango slices.

Vitamin C is an essential nutrient for human. Being a water soluble and a most labile component among all vitamins contained in foods, it is highly sensitive to heat and can be degraded greatly when heat is applied for a given residual moisture content of fruit (Hawllader et al. 2006). Due to its perishable characteristics, removing moisture is desired to enable storage for a longer time with minimum loss of nutrients. Statistical analysis shows that vitamin C is strongly affected by temperature ($P = 0.001$). Figure 5(d) illustrates that maximum vitamin C content was retained at 65 °C. The

Table 5 Average thickness shift factors, a_h and temperature shift factors, a_T for guava slices of 3, 6, and 9 mm dried at temperatures of 55, 65, and 75 °C

| Temperature (°C) | a_h | | | a_T |
|------------------|----------------------|---|------|-------|
| | Slice thickness (mm) | | | |
| | 3 | 6 | 9 | |
| 55 | 1.63 | 1 | 0.83 | 0.70 |
| 65 | 1.59 | 1 | 0.82 | 1 |
| 75 | 1.66 | 1 | 0.84 | 1.28 |

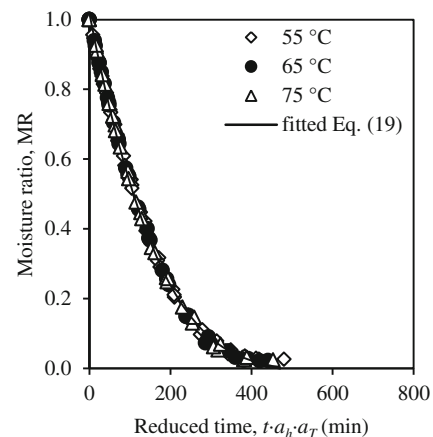


Fig. 4 Master curve fitted with Midilli-Kucuk model showing time-temperature-thickness superposition for guava slices

Table 6 Coefficient of the regression model equations for drying time and quality properties of guava slices

| Coefficient | Drying time (min) | Water activity | Colour change | Vitamin C (mg/100 g) | Hardness (g) | Springiness | Cohesiveness | Chewiness (g) |
|---------------------|-------------------|---------------------|---------------------|----------------------|---------------------|---------------------|---------------------|---------------------|
| β_0 | 2335.34 | -1.55145 | 117.518 | -6300.13 | 5619.96 | -0.090994 | 0.379917 | 2392.60 |
| β_1 | -59.41**** | 0.06449** | -2.692* | 210.71**** | -108.11 | 0.036426 | 0.022700 | -24.12 |
| β_2 | 109.51**** | 0.02418 | -3.707 | 27.00 | -798.81**** | -0.075578 | -0.088611 | -541.18**** |
| β_{11} | 0.37**** | -0.00047* | 0.018 | -1.57**** | 0.45 | -0.000254 | -0.000190 | -0.08 |
| β_{22} | -2.53**** | 0.00273 | 0.087 | 0.26 | 19.56** | 0.004180 | 0.002333 | 9.31 |
| β_{12} | -0.50** | -0.00103 | 0.061* | -0.68 | 11.67**** | -0.000117 | 0.000433 | 7.80**** |
| R^2 | 0.9969 | 0.7275 | 0.8534 | 0.8734 | 0.9691 | 0.8630 | 0.6862 | 0.9126 |
| P (lack of fit) | – | 0.927 ^{ns} | 0.787 ^{ns} | 0.258 ^{ns} | 0.747 ^{ns} | 0.863 ^{ns} | 0.606 ^{ns} | 0.681 ^{ns} |
| P (overall model) | < 0.0005**** | 0.057* | 0.008*** | 0.005*** | < 0.0005**** | 0.006*** | 0.088* | 0.001**** |

β_0 the estimated constant regression coefficient

β_1 and β_2 the estimated linear regression coefficient of drying temperature and slice thickness, respectively

β_{11} and β_{22} the estimated quadratic regression coefficient of drying temperature and slice thickness, respectively

β_{12} the estimated interaction regression coefficient of drying temperature and slice thickness

* $P < 0.10$, ** $P < 0.05$, *** $P < 0.01$, **** $P < 0.005$; ^{ns} not significant ($P > 0.5$)

lowest vitamin C retention (419.21 mg/100 g) occurred in samples dried at 75 °C with 9 mm thickness, lower than those dried at 55 °C.

Changes in texture of dried food are due to modification of microstructure or more generally due to case hardening or crust formation. Hardness is defined as the peak force on the first compression and is used to investigate case hardening in dried fruit; while, chewiness refers to the energy required to masticate a solid food product (Bourne 2002). Both attributes, the hardness and chewiness are desirable in dried fruit to obtain good mouth-feel. Hardness and chewiness have a similar trend where they increase with drying temperature and slice thickness (Fig. 5(e) & (h)). They are also significantly affected by thickness (Table 6). Increase of hardness at high temperature is due to the formation of a hard impermeable skin on the sample surface, which is known as case hardening or crust formation (Fellows 1988). Increase of hardness leads to increase of chewiness at high drying temperature as chewiness is also defined as a function of hardness. However, less hard and chewy product was found for the combination of 75 °C temperature and 3 mm thickness. It is noticeable that hardness of thin slices would only increase minimally due to thinner crust formation caused by a rapid drying rate even though it has been dried at high temperature (Achanta and Okos 1996). Perera (2005) reported that most air-dried products suffers collapse of structure, having firmer textures and increasing in chewiness, which can be undesirable to the customer. Chong et al. (2008b) explained that hardness in dried samples is due to depolymerisation of cell wall constituents such as occurrence of pectin after the exposure to heat during drying. Similar results was noted for hot-air dried chempedak where both hardness and

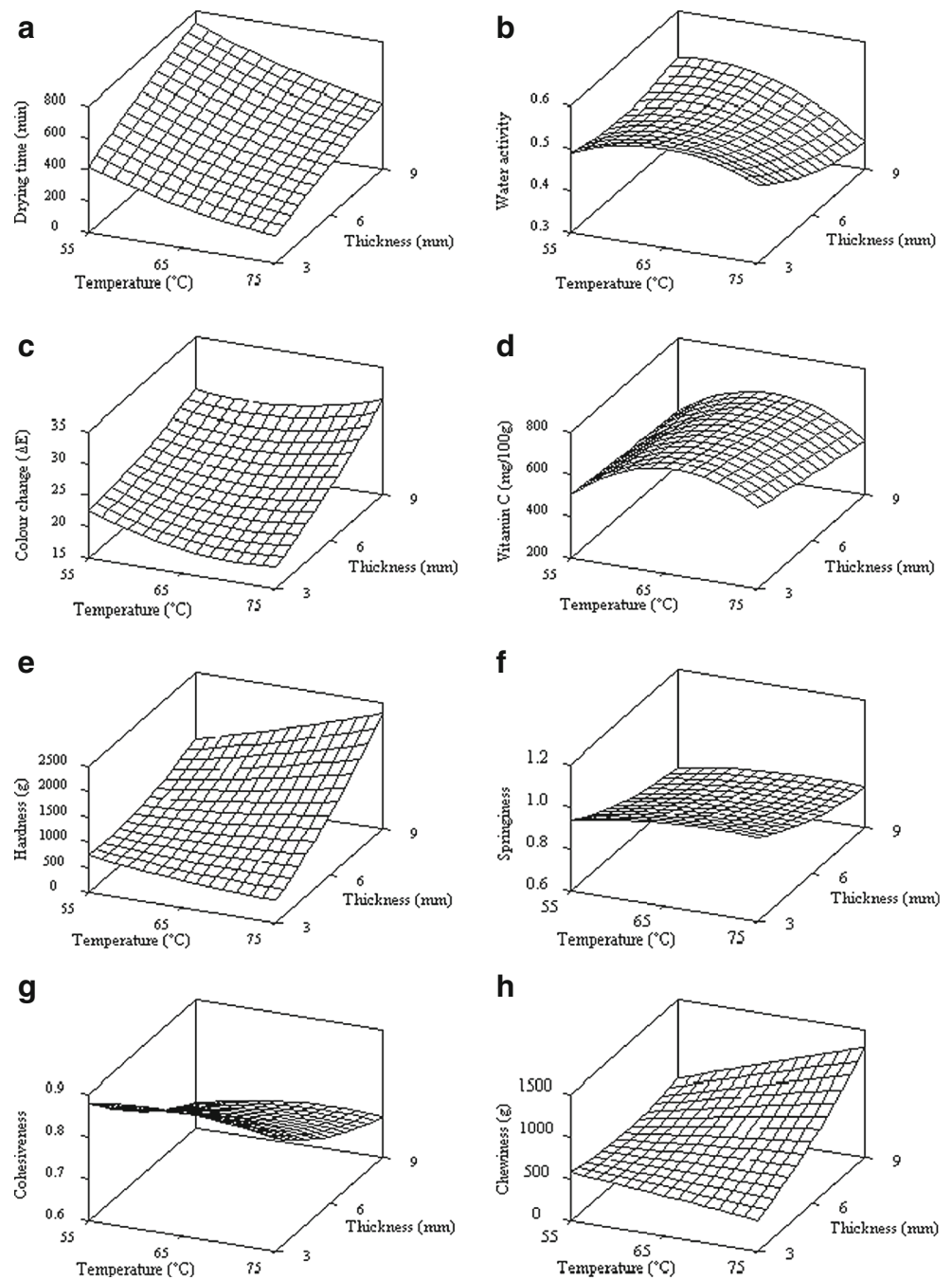
chewiness values increased and springiness decreased with increase of drying temperatures (Chong et al. 2008a).

Table 6 shows that springiness and cohesiveness were not significantly affected by both process variables. Thinly dried guava was found to be more elastic due to its high springiness. Figure 5(f) and (g) show that springiness and cohesiveness have reduced slightly when the size of the dried fruit was thicker with small deviations when temperature increased. Hardening indicates a decrease of fruit elasticity (Sirisomboon et al. 2000) and a high value of hardness results in lower springiness.

Optimisation of dried guava attributes

Optimum conditions to hot air dried guava were determined by specifying the goal for each response. It was targeted to obtain minimum drying time, water activity, colour change and maximum vitamin C and to achieve 1,761 g of hardness and 407 g of chewiness by referring to the texture attributes of commercial dried guava with moisture content about 0.036 g water/g dry solid (Chong et al. 2009). Minimisation of drying time reflects the reduction of heat exposure and energy consumption of the drying operation whilst also minimising the degradation of product quality. The texture attributes of commercially dried guava samples reported in Chong et al. (2009) was used as reference because of its Malaysian variety and it was inappropriate to target the texture attributes as maximum or minimum where the desired mouth-feel of dried guava for product acceptance was important. Springiness and cohesiveness attributes were excluded in the optimisation since they are not significantly affected by temperature and thickness.

Fig. 5 Effects of drying temperature and slice thickness on **a** drying time, **b** water activity, **c** colour change, **d** vitamin C, **e** hardness, **f** springiness, **g** cohesiveness, and **h** chewiness



The composite desirability value of the optimum solution was 0.6192 for the optimised temperature 70 °C and thickness 6 mm. The values of responses at the optimum condition are given in Table 7. The desirability of hardness was much lower at 0.4715 and this could be resulted by the different moisture content between the commercial products (0.036 g water/g dry solid) and experimental samples (0.2564±0.01654 g water/g dry solid). The commercial product is known to be added with accepted food additives that gives variances to hardness. However, it was acceptable to set 1,761 g of hardness and 407 g of chewiness as target

in optimisation because they were in the range of texture for dried guava produced in this research.

Verification of the optimised drying

The adequacy of the statistical model equations for predicting optimal response attributes were tested by drying guava of 6 mm thickness at 70 °C. Table 7 shows the model verification results. The final moisture content of dried guava was 19.99±1.35 % (w.b.) after drying for 360 min. The percentage errors from Eq. (13) for water activity,

Table 7 Process variables, responses optimisation, desirability, and experimental value for the responses at optimum condition

| Variables | Goal | Lower | Target | Upper | Predicted | Desirability | Experimental |
|----------------------|----------|---------|----------|----------|-----------|--------------|------------------|
| Factors | | | | | | 0.6192 | |
| Temperature (°C) | in range | 55 | in range | 75 | 70 | | 70 |
| Thickness (mm) | in range | 3 | in range | 9 | 6 | | 6 |
| Responses | | | | | | | |
| Drying time (min) | minimum | 180 | 180 | 720 | 357 | 0.6718 | 360 |
| Water activity | minimum | 0.367 | 0.367 | 0.547 | 0.452 | 0.5259 | 0.481±0.006 |
| Colour change | minimum | 17.51 | 17.51 | 30.16 | 22.18 | 0.6305 | 23.85±3.76 |
| Vitamin C (mg/100 g) | maximum | 395.03 | 687.72 | 687.72 | 624.66 | 0.7652 | 704.72±59.43 |
| Hardness (g) | target | 429.253 | 1761.000 | 2330.810 | 1057.189 | 0.4715 | 1501.406±508.025 |
| Chewiness (g) | target | 396.636 | 407.000 | 1341.038 | 686.142 | 0.7011 | 756.944±255.022 |

colour change, vitamin C, hardness and chewiness are 6.03 %, 7 %, 11.36 %, 29.59 %, and 9.35 %. The predicted values were found mostly in the range of experimental value. Although the percentage error of hardness was 29.59 %, the experimental value of hardness of 1501.4 g at optimum drying temperature, 70 °C and slice thickness, 6 mm was comparable to the hardness of the commercially dried guava, which was 1,761 g reported by Chong et al. (2009).

The drying curve for this optimum drying condition was also fitted with all the semi-theoretical models in Table 1 where the Midilli-Kucuk model was also best fitted model (Table 4) with $R^2=0.9997$. In fitting this data to the single model (Eq. (16)) and the master curve fitted Midilli-Kucuk model (Eq. (19)) as shown in Fig. 6, the master curve fitting was slightly better with $R^2=0.9995$, $\chi^2=9.138 \times 10^{-5}$, $RMSE=0.007805$, versus the single model $R^2=0.9973$, $\chi^2=4.106 \times 10^{-4}$, $RMSE=0.01755$. The predicted effective diffusivity calculated from Eq. (14) of $2.196 \times 10^{-9} \text{ m}^2/\text{s}$ was very close to the experimentally found diffusion coefficient, $2.303 \times 10^{-9} \text{ m}^2/\text{s}$.

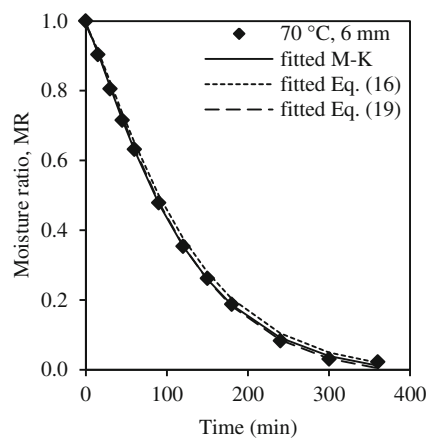


Fig. 6 Moisture ratio as a function of drying time for optimal condition at 70 °C with 6 mm guava slices and fitted with Midilli-Kucuk model (M-K), single model (Eq. (16)) and master curve fitted with Midilli-Kucuk model (Eq. (19))

The percentage error, PE for the effective diffusivity was 4.65 % with no significant difference between the predicted and experimental values.

Conclusions

Theoretical and statistical models have been established simultaneously in relating the drying kinetics and quality attributes of dried guava through the determination and comparison of drying rates, drying rate constants, effective diffusivity at different drying temperature, time and guava thickness. Elevated air temperature and thin slices resulted in higher drying kinetics. Effective diffusivity was enhanced by increasing drying temperature and thickness. The Midilli-Kucuk model has described the thin layer drying behaviour of guava slices where the superposition technique showed high accuracy in predicting the moisture ratio of guava slices conveniently. The statistical modelling is important in predicting drying responses including drying time, water activity, colour change, vitamin C content, and texture of sample and subsequently used for drying process optimisation. Drying time presented a strong dependence on both drying temperature and sample thickness; temperature had more significant effect on water activity, colour and vitamin C ($P<0.091$) while increasing slice thickness caused an increase in hardness and chewiness ($P<0.004$). The theoretical drying kinetics and constants of the optimised drying at 70 °C for 6 mm slices are useful in reflecting the drying mechanisms of a practical drying process.

Nomenclature

| | |
|--------------|--|
| a, b, c, n | model constants |
| a_h | dimensionless time-thickness shift factor |
| a_T | dimensionless time-temperature shift factor |
| D_{eff} | effective diffusivities (m^2/s) |
| D_o | constant in Arrhenius equation (m^2/s) |

| | |
|-----------------|---|
| E_a | activation energy (kJ/mol) |
| h | slice thickness (mm) |
| k | drying rate constant (min^{-1}) |
| M_0 | initial moisture content (g water/g dry solids) |
| M_e | equilibrium moisture content (g water/g dry solids) |
| M_t | moisture content at any time (g water/g dry solids) |
| $M = M_t - M_e$ | free moisture content at any time (g water/g dry solids) |
| MR | moisture ratio (dimensionless) |
| PE | percentage error (%) |
| R | universal gas constant 8.314 (J/mol K) |
| R^2 | coefficient of determination |
| $RMSE$ | root mean square error |
| t | time (s or min) |
| t', t'' | reduced or pseudo time (min) |
| T | temperature ($^{\circ}\text{C}$) |
| T_{abs} | absolute temperature (K) |
| X_1, X_2 | independent variables of temperature and thickness in RSM |
| Y | dependent responses in RSM |
| ΔE | colour change |

Greek letters

| | |
|----------|-----------------------|
| α | constants |
| β | constant coefficients |
| χ^2 | reduced chi-squared |

Subscripts

| | |
|------------|--------------|
| <i>exp</i> | experimental |
| <i>pre</i> | predicted |

References

- Achanta S, Okos MR (1996) Predicting the quality of dehydrated foods and biopolymers- research needs and opportunities. *Drying Technol* 14:1329–1368
- Akpınar EK, Bicer Y (2006) Mathematical modeling and experimental study on thin layer drying of strawberry. *Int J Food Eng* 2(1):1–16
- AOAC (1990) Official Method of Analysis. No. 931.04. Association of Official Analytical Chemists, Washington, DC
- Bakshi AS, Singh RP (1980) Drying characteristics of parboiled rice. In: Mujumdar AS (ed) *Drying'80*. Hemisphere Publishing Company, Washington DC
- Beauchat LR (1981) Microbial stability as affected by water activity. *Cereal Food World* 25(7):345–349
- Bourne M (2002) Food texture and viscosity-concept and measurement, 2nd edn. Academic, UK
- Boyer RF (1986) Modern experimental biochemistry. The Benjamin/Cummings Publishing Company, Inc., Menlo Park
- Chin NL, Chan SM, Yusof YA, Chuah TG, Talib RA (2009) Modelling of rheological behaviour of pummelo juice concentrates. *J Food Eng* 93:134–140
- Chong CH, Law CL, Cloke M, Abdullah LC, Wan Daud WR (2009) Drying models and quality analysis of sun-dried ciku. *Drying Technol* 27:985–992
- Chong CH, Law CL, Cloke M, Hii CL, Abdullah LC, Wan Daud WR (2008a) Drying kinetics and product quality of dried chempedak. *J Food Eng* 88:522–527
- Chong CH, Law CL, Cloke M, Luqman CA, Wan Daud WR (2008b) Drying kinetics, texture, colour, and determination of effective diffusivities during sun drying of chempedak. *Drying Technol* 26:1286–1293
- Crank J (1975) Mathematics of diffusion, 2nd edn. Oxford University Press, London
- DeLong D (1992) How to dry food. The Berkley Publishing Group, New York
- Derossi A, Severini C, Cassi D (2011) Mass transfer mechanisms during dehydration of vegetable food: traditional and innovative approaches. In: El-Amin M (ed) *Advanced topics in mass transfer*. InTech, Croatia
- Doymaz I (2009) An experimental study on drying of green apples. *Drying Technol* 27:478–485
- Erbay Z, Icier F (2009) A review of thin layer drying of foods: theory, modeling, and experimental results. *Crit Rev Food Sci Nutr* 50:441–464
- Falade KO, Solademi OJ (2010) Modelling of air drying of fresh and blanched sweet potato slices. *Int J Food Sci Technol* 45:278–288
- Fellows P (1988) Food processing technology. Ellis Horwood Ltd. & VCH, Chichester
- Geankoplis CJ (2003) Transport processes and separation principles (include unit operation), 4th edn. Prentice Hall PTR, Upper Saddle River
- Granato D, Bigaski J, Castro IA, Masson MI (2010) Sensory evaluation and physicochemical optimization of soy-based desserts using response surface methodology. *Food Chem* 121(3):899–906
- Hawladar MNA, Perera CO, Tian M, Yeo KL (2006) Drying of guava and papaya: impact of different drying methods. *Drying Technol* 24:77–87
- Huang Y, Whittaker AD, Lacey RE (2001) Automation for food engineering: food quality quantization and process control. CRC Press, Taylor & Francis Group, New York
- Jangam SV, Mujumdar AS (2010) Basic concepts and definition. In: Jangam SV, Law CL, Mujumdar AS (eds) *Drying of foods, vegetables and fruit*, vol 1., pp 1–30
- Janjai S, Precoppe M, Lamlert N, Mahayothee B, Bala BK, Nagle M, Muller J (2010) Thin-layer drying of litchi (*Litchi chinensis* Sonn.). *Food Bioprod Process* 89:194–201
- Kaya A, Aydin O, Kolayh S (2010) Effect of different drying conditions on the vitamin C (ascorbic acid) content of Hayward kiwifruits (*Actinidia deliciosa* Planch). *Food Bioprod Process* 88:165–173
- Khazaei J, Arabhosseini A, Khosrobeygi Z (2008a) Application of superposition technique for modeling drying behaviour of Avishan (*Zataria multiflora*) leaves. *Trans ASABE* 51(4):1383–1393
- Khazaei J, Chegini G-R, Bakhshiani M (2008b) A novel alternative method for modeling the effects of air temperature and slice thickness on quality and drying kinetics of tomato slices: superposition technique. *Drying Technol* 36:759–775
- Lee JH, Kim HJ (2009) Vacuum drying kinetics of Asian white radish (*Raphanus sativus* L.) slices. *LWT—Food Sci Technol* 42:180–186
- Marinos-Kouris D, Maroulis ZB (1995) Transport properties in the drying of solids. In: Mujumdar AS (ed) *Handbook of industrial drying*, 2nd edn. Marcel Dekker, New York, pp 113–160
- McLaughlin CP, Magee TRA (1998) The determination of sorption isotherm and the isosteric heats of sorption for potatoes. *J Food Eng* 35:267–280

- Mittal GS (1999) Mass diffusivity of food products. *Food Rev Int* 15 (1):19–66
- Myers RH, Montgomery DC, Anderson-Cook CM (2009) *Response surface methodology: process and product optimization using designed experiments*, 3rd edn. John Wiley and Sons, Inc., New York
- Nguyen M-H, Price WE (2007) Air-drying of banana: influence of experimental parameters, slab thickness, banana maturity and harvesting season. *J Food Eng* 79:200–207
- Ong SP, Law CL (2009) Mathematical modeling of thin layer drying of salak. *J Appl Sci* 9(17):3048–3054
- Panchariya PC, Popovic D, Sharma AL (2002) Thin-layer modelling of black tea drying process. *J Food Eng* 52:349–357
- Patkai G (2006) Fruit as an ingredient in a fruit product. In: Hui YH (ed) *Handbook of fruits and fruit processing*, 1st edn. Blackwell Publishing, USA, pp 217–230
- Perera CO (2005) Selected quality attributes of dried foods. *Drying Technol* 23:717–730
- Pott I, Neidhart S, Muhlbauer W, Carle R (2005) Quality improvement of non-sulphited mango slices by drying at high temperatures. *Innov Food Sci Emerg Technol* 6:412–419
- Rahman MS (2005) Dried food properties: challenges ahead. *Drying Technol* 23:695–715
- Rizvi SSH (1986) Thermodynamic properties of food in dehydration. In: Rao MA, Rizvi SSH (eds) *Engineering properties of foods*. Marcel Dekker, New York, pp 190–193
- Sacilik K, Elicin AK (2006) The thin layer drying characteristics of organic apple slices. *J Food Eng* 73:281–289
- Sagar VR, Suresh KP (2010) Recent advances in drying and dehydration of fruits and vegetables: a review. *J Food Sci Technol* 47(1):15–26
- Sirisomboon P, Tanaka M, Akinaga T, Kojima T (2000) Evaluation of the textural properties of Japanese pear. *J Texture Stud* 31:665–677
- Steffe JF (1996) *Rheological methods in food process engineering*, 2nd edn. Freeman Press, MI
- Walpole RE, Myers RH, Myers SL, Ye K (2002) *Probability and statistics for engineers and scientists*, 7th edn. Prentice Hall, NJ