ORIGINAL ARTICLE



# Development and validation of a comprehensive model for map of fruits based on enzyme kinetics theory and arrhenius relation

S. Mangaraj • T. K.Goswami • P. V Mahajan

Revised: 1 April 2014 / Accepted: 10 April 2014 / Published online: 14 September 2014 © Association of Food Scientists & Technologists (India) 2014

Abstract MAP is a dynamic system where respiration of the packaged product and gas permeation through the packaging film takes place simultaneously. The desired level of  $O_2$  and  $CO_2$  in a package is achieved by matching film permeation rates for O<sub>2</sub> and CO<sub>2</sub> with respiration rate of the packaged product. A mathematical model for MAP of fresh fruits applying enzyme kinetics based respiration equation coupled with the Arrhenious type model was developed. The model was solved numerically using MATLAB programme. The model was used to determine the time to reach to the equilibrium concentration inside the MA package and the level of  $O_2$  and  $CO_2$  concentration at equilibrium state. The developed model for prediction of equilibrium O2 and CO<sub>2</sub> concentration was validated using experimental data for MA packaging of apple, guava and litchi.

Keywords MAP  $\cdot$  Fruit respiration  $\cdot$  Film permeability  $\cdot$  Modelling  $\cdot$  Shelf life

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# Notations

Ap	Surface area of the packaging film, m <sup>2</sup>
E	Mean relative deviation modulus, %
Ea	Activation energy, kJ $g^{-1}$ mol <sup>-1</sup>
E <sub>ap</sub>	Activation energy of gas transmission rates
1	for O <sub>2</sub> and CO <sub>2</sub> (kJ/kg-mole)
GTR	Gas transmissions rates of films
	$(\text{cm}^3/\text{m}^2 \text{ h } \Delta\text{C})$ at temperature $\text{T}_{\text{abs}}$
GTR <sub>p</sub>	Gas transmission rates pre-exponential
	factor for $O_2$ and $CO_2$ (cm <sup>3</sup> /m <sup>2</sup> h $\Delta C$ )
$K_{m(O2)}$	Michaelis-Menten constant for O <sub>2</sub>
	consumption, % $O_2$
$K_{m(CO2)}$	Michaelis-Menten constant for CO <sub>2</sub>
	evolution, % $O_2$
$K_{i(O2)}$	Inhibition constants for O <sub>2</sub> consumption,
	% CO <sub>2</sub>
$K_{i (CO2)}$	Inhibition constants for CO <sub>2</sub> evolution,
	% CO <sub>2</sub>
R <sub>O2</sub>	Respiration rate, ml $[O_2]$ kg <sup>-1</sup> h <sup>-1</sup>
R <sub>CO2</sub>	Respiration rate, ml $[CO_2]$ kg <sup>-1</sup> h <sup>-1</sup>
Y <sub>O2</sub>	O <sub>2</sub> concentration inside the package
	(cm <sup>3</sup> per cm <sup>3</sup> of air)
Z <sub>CO2</sub>	CO <sub>2</sub> concentration inside the package
	(cm <sup>3</sup> per cm <sup>3</sup> of air)
Т	Storage time in h
$\Delta t$	Time difference between two gas
	measurements
$V_{f}$	Free volume of the respiration chamber
	in ml
W	Weight of the fruit in kg
R	Universal gas constant, 8.314 kJ kg <sup><math>-1</math></sup> mol <sup><math>-1</math></sup> K <sup><math>-1</math></sup>
$R_{CO2}$	Respiration rate, ml $[CO_2]$ kg <sup>-1</sup> h <sup>-1</sup>
R <sub>exp</sub>	Experimental respiration rate, ml kg <sup><math>-1</math></sup> h <sup><math>-1</math></sup>
R <sub>m</sub>	Model parameter of enzyme kinetic

R <sub>pre</sub>	Predicted respiration rate, ml kg <sup><math>-1</math></sup> h <sup><math>-1</math></sup>
$R_{O2}$	Respiration rate, ml $[O_2]$ kg <sup>-1</sup> h <sup>-1</sup>
R <sub>p</sub>	Respiration pre-exponential factor
T <sup>-</sup>	Storage temperature, °C
T <sub>abs</sub>	Storage temperature, K
t	Storage time, h
$\Delta t$	Time difference between two gas
	measurements
$V_f$	Free volume of the respiration chamber, ml
$V_{m (CO2)}$	Maximum respiration rate for $CO_2$
	evolution, ml/kg-h
$V_{m(O2)}$	Maximum respiration rate for O <sub>2</sub>
	consumption, ml/kg-h
$Y_{O2}^{a}$	$O_2$ concentration in the atmospheric air
	(cm <sup>3</sup> per cm <sup>3</sup> of air)
$Z_{CO2}^{a}$	$CO_2$ concentration in the atmospheric air
	(cm <sup>3</sup> per cm <sup>3</sup> of air)
Y <sub>O2</sub> <sup>eq</sup>	Equilibrium/optimum O <sub>2</sub> concentration
	attained in the package
Z <sub>CO2</sub> <sup>eq</sup>	Equilibrium/optimum CO <sub>2</sub> concentration
	attained in the package
Wp	Weight of the fruits in MA package, kg
V <sub>fp</sub>	Free volume in the package, cm <sup>3</sup>
X	Thickness of the film, cm
OTR	Oxygen transmission rates
CTR	Carbon dioxide transmission rates
P <sub>O2</sub>	O <sub>2</sub> permeability of packaging material
	$(\text{cm}^3. \text{ m}^{-2}. \text{ h}^{-1}. \text{ [Conc. diff. of } \text{O}_2 \text{ in})$
	volume fraction] <sup>-1</sup> )
P <sub>CO2</sub>	CO <sub>2</sub> permeability of packaging material
	$(\text{cm}^3. \text{ m}^{-2}. \text{ h}^{-1}. \text{ [Conc. diff. of O}_2 \text{ in})$
	volume fraction] <sup><math>-1</math></sup> )
dY <sub>O2</sub> /dt	Rate of change of O <sub>2</sub> concentration
	$Y_{O2}$ within the package at time 't' of
	storage (cm <sup>3</sup> per cm <sup>3</sup> of air. $h^{-1}$ )
dZ <sub>CO2</sub> /dt	Rate of change of $CO_2$ concentration
	$'Z_{CO2}'$ within the package at time 't'
	of storage (cm <sup>3</sup> per cm <sup>3</sup> of air. $h^{-1}$ )
	respectively

N Number of respiration data points

## Introduction

Modified-atmosphere packaging (MAP) of fresh commodity refers to the technique of sealing actively respiring produce in polymeric film packages to modify the  $O_2$  and  $CO_2$  levels within the package atmosphere. It is often desirable to generate an atmosphere low in  $O_2$  and/or high in  $CO_2$  to influence the metabolism of the product being packaged, or the activity of decay-causing organisms to increase storability and/or shelf life (Kader et al. 1989; Mangaraj et al. 2009). In addition to atmosphere modification, MAP vastly improves moisture retention, which can have a greater influence on preserving quality than  $O_2$  and  $CO_2$  levels (Mangaraj and Tripathi 2013). Furthermore, packaging isolates the product from the external environment and helps to ensure conditions that, if not sterile, at least reduce exposure to pathogens and contaminants (Mahajan et al. 2007).

MAP is a dynamic system during which respiration and permeation occur simultaneously. In a properly designed MAP, after a period of transient state an equilibrium state is established. At equilibrium, the amount of  $O_2$  entering into the package and that of  $CO_2$  permeating out of the package become equal to the amount of  $O_2$  consumed and that of  $CO_2$  evolved by the packaged fruit, respectively (Yam and Lee 1995; Del Nobile et al. 2007). Respiration rate of the commodity, permeability of packaging film, mass of the produce packed inside the package, area of the packaging film, surrounding gas composition, optimum level of  $O_2$  and  $CO_2$ concentration, storage temperature etc. affect the equilibrium gas concentration (Yam and Lee 1995; Jacxsens et al. 2000; Mangaraj et al. 2013a) and they are taken as input parameters for developing mathematical model.

Different mathematical models were developed to describe the mass balance of O<sub>2</sub> and CO<sub>2</sub> concentration inside the package during storage. These model parameters were considered for theoretical design of MAP of commodity. Cameron et al. (1989) employed  $O_2$  depletion method for determining O<sub>2</sub> consumption in a closed system for tomatoes and optimized the package parameters based on the gas exchange model. Christie et al. (1995) proposed a material balance equation that relates the package film permeability and produce metabolism to the in-package gas concentrations. Song et al. (2002) developed a MAP model based on mass balances and the transport phenomenon across the package and solved it numerically using Adams-Moulton's numerical technique. The reasons for choosing the Adams-Moulton's numerically technique in this MAP model is due to the fact that it is useful for the solution of the differential equation to calculate and predict the variation of oxygen and carbon dioxide concentration with time. This method is very accurate for solving the higher order differential equation that form in MAP modeling process.

Rocculi et al. (2006) developed the models applying Michaelis-Menten's equation and Arrehnius's type expression to describe the mass balance of  $O_2$  and  $CO_2$  concentration inside the MA package for minimally processed apple packed in multilayer pouches. Torrieri et al. (2007) studied the effect of temperature, oxygen, red coloration process and postharvest storage time on the respiration rate of fresh-cut Annurca apples for developing suitable MAP. Mahajan et al. (2007) developed software for MAP design of fresh and freshcut produce for selecting suitable packaging materials. Techavises and Hikida (2008) developed a mathematical



Fig. 1 Diagrammatic representation of gaseous exchange in MAP system

model based on Fick's law for predicting O<sub>2</sub>, CO<sub>2</sub>, N<sub>2</sub>, and water vapor exchange in film packaging with macroscopic perforations.

A systematic theoretical design and modeling is needed to establish conditions for the success and benefit of MAP for a particular produce (Exama et al. 1993; Mahajan et al. 2007). Such a design and analysis could provide closely the characteristic of the commodity, film properties and optimized packaging parameters. Simulation of a MAP system is the most appropriate method to allow a correct MAP design and consequently obtain a successful commercial product (Cameron et al. 1989; Makino and Iwasaki 1997; Del Nobile et al. 2007).

Considering these approaches in mind a global model for MA packaging of fruits was proposed. The proposed model coupled to the principle of enzyme kinetics equation that describes the dependence of respiration rate on gas composition, temperature (and eventually time) and models that describes the dependence of packaging material on temperature; with the mass balance equations that describes the gaseous exchange in MAP. Using this model the variation of  $O_2$  and  $CO_2$  inside the MA package and the time to reach equilibrium level could be predicted accurately at any storage temperature.

## Materials and methods

## Respiration rate model

The Michaelis-Menten type equation based on principle of enzyme kinetics with uncompetitive type of inhibition, wherein  $CO_2$  does not bind with the enzyme but reacts with enzyme substrate complex (Lee and Wicker 1991), was the model fitted to the experimental respiration data (Peppelenbos and Leven 1996; Mangaraj and Goswami 2011a, b). The relevant enzyme kinetics models are shown Eqs. (1) and (2).

$$R_{O2} = \frac{V_{m(O2)} \times Y_{O2}}{k_{m(O2)} + \left\{1 + ([Z_{CO2}])/k_{i(O2)}\right\}Y_{O2}}$$
(1)

$$R_{CO2} = \frac{V_{m(CO2)} \times Y_{O2}}{k_{m(CO2)} + \left\{1 + \left([Z_{CO2}]/k_{i(CO2)}\right)\right\}Y_{O2}}$$
(2)

The temperature dependence of the model parameters of the above Michaelis-Menten equations was quantified using an Arhhenius model (Mangaraj and Goswami 2008).

$$R_{\rm m} = R_{\rm p} \exp\left[\frac{E_{\rm a}}{R \times T_{\rm abs}}\right] \tag{3}$$

Model for gas transmission rates

The gas transmission rates (OTR/CTR) of polymeric film are temperature dependent and hence Arrhenius-equations of the following type were fitted to the experimental data to depict the relationship of GTR with temperature (Exama et al. 1993).

$$GTR = GTR_{p}exp\left[\frac{-E_{aGTR}}{RT_{abs}}\right]$$
(4)

Table 1	1	Activation energy	and pre	e-exponential	factor o	f An	rhenius-type e	quation	for c	lifferen	t mode	l parameters	of uncompeti	itive i	nhib	itior
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Arrhenius parameter	V <sub>m (O2)</sub>	V <sub>m (CO2)</sub>	k <sub>m (O2)</sub>	k <sub>m (CO2)</sub>	k <sub>i (O2)</sub>	$k_{i\;(\rm CO2)}$
Apple						
$E_a$ (kJ/g-mole)	30.06	25.10	20.45	11.88	-20.23	-16.84
$R_p (ml [O_2] kg^{-1} h^{-1})$	$5.2 \times 10^{6}$	$9.1 \times 10^{5}$	$3.8 \times 10^{4}$	$1.7 \times 10^{3}$	$1.7 \times 10^{-3}$	$9.2 \times 10^{-3}$
Guava						
E <sub>a</sub> (kJ/g-mole)	27.89	26.69	14.58	18.02	-17.54	-16.40
$R_p (ml [O_2] kg^{-1} h^{-1})$	$3.7 \times 10^{6}$	$1.9 \times 10^{6}$	$4.5 \times 10^{3}$	$1.4 \times 10^{4}$	$5.0 \times 10^{-3}$	$7.0 \times 10^{-3}$
Litchi						
E <sub>a</sub> (kJ/g-mole)	42.24	39.45	17.76	16.36	-18.17	-10.44
$R_p (ml [O_2] kg^{-1} h^{-1})$	$2.59 \times 10^{9}$	$6.17 \times 10^{8}$	$2.33 \times 10^{4}$	$9.19 \times 10^{3}$	$2.9 \times 10^{-3}$	$1.1 \times 10^{-1}$

## Design variables in MAP

The variables involved in the MA package design are: the surrounding gases composition  $(Y_{O2}{}^a \text{ and } Z_{CO2}{}^a)$ , temperature (T), O<sub>2</sub> consumption rate and CO<sub>2</sub> production rate (R<sub>O2</sub> and R<sub>CO2</sub>), the optimum gas composition to be attained in the package (Y<sub>O2</sub> $^{eq}$  and Z<sub>CO2</sub> $^{eq}$ ), weight of the fruits in package (W<sub>p</sub>), surface area of the packaging film (A<sub>p</sub>), free volume of the package (V<sub>fp</sub>), thickness of the film (x), gas transmission rates of film to O<sub>2</sub> and CO<sub>2</sub> (OTR and CTR). The ultimate aim of this design was to select suitable films for a 1±0.1 kg fill weight so that the equilibrium concentrations of O<sub>2</sub> and CO<sub>2</sub> are reached within shortest possible time and these concentrations lie within the range required for maximum shelf life of stored fruits (Das 2005; Mangaraj et al. 2009; Mangaraj et al. 2011). The package size of 1±0.1 kg was considered based on survey conducted at the local market.

Target level of MA package air composition for fruits

The recommended level of gas concentration in CA/MA storage of apple, guava and litchi for maintaining quality and extending shelf-life are 1–3 and 3–5 %; 2–5 and 2–5 %; 3–5 and 3–5 % O<sub>2</sub> and CO<sub>2</sub>, respectively (Mangaraj and Goswami 2009a, b; Singh and Pal 2008; Shivakumar et al. 2007) with N<sub>2</sub>. On the basis of preliminary investigations and the sub-optimal package air composition it was found appropriate for designing the optimal MA packages for apple, guava and litchi with target air composition of 3 %O<sub>2</sub> and 3 % CO<sub>2</sub>; 5 %O<sub>2</sub> and 4 % CO<sub>2</sub>; 5 %O<sub>2</sub> and 5 % CO<sub>2</sub> in N<sub>2</sub>, respectively.

# Development of MAP model for fruits

Respiration of the fruits and the gas permeation through the packaging film takes place simultaneously during MA packaging. In general, the relative humidity in the internal package atmosphere is higher than the external atmosphere. Hence some amount of water vapor may permeate out of the package, depending upon the WVTR of the polymeric film. The mathematical modeling of gaseous exchange for respiratory gases ( $O_2$  and  $CO_2$ ) has been attempted here. The diagrammatic representation of the gaseous exchange in MAP is shown in Fig. 1.

The concept is that once the fruit is sealed inside the package the  $O_2$  and  $CO_2$  concentration gradients develop due to the fruit respiration and the polymeric film serves as the regulator of  $O_2$  flow into the package and the flow of  $CO_2$  out of the package. At a given temperature and for a considerably small length of transient period, the rates of  $O_2$  consumption ( $R_{O2}$ ) and the rate of  $CO_2$  evolution ( $R_{CO2}$ ) of the packaged fruits depend greatly on  $O_2$  concentration ( $Y_{O2}$ ) and CO<sub>2</sub> concentration ( $Z_{CO2}$ ). Considering that there is no gas stratification inside the packages and that the total

Parameters for Arrhenious	Polymeric	: films with t	heir thickness	10												
equations	BOPP-30	д	BOPP-45	п	PVC-25 μ		PVC-35 µ	1	PVC-50 µ	_	LDPE-40	ц	LDPE-60	ц	PVDC-40	ユ
	OTR	CTR	OTR	CTR	OTR	CTR	OTR	CTR	OTR	CTR	OTR	CTR	OTR	CTR	OTR	Ú

Activation energy and pre-exponential factor of Arrhenius-type equation for selected polymeric films

Table 2

 $2.94 \times 10^{9}$ 

 $1.54 \times 10^{8}$ 

 $6.38 \times 10^{12}$ 

 $3.34 \times 10^{11}$ 

 $8.51 \times 10^{12}$ 

 $5.52 \times 10^{11}$ 

53.991.58×10<sup>13</sup>

 $9.90 \times 10^{11}$ 

 $2.18 \times 10^{13}$ 

 $1.57 \times 10^{12}$ 

 $1.22 \times 10^{13}$ 

49.65 $9.52 \times 10^{11}$ 

 $2.06 \times 10^{14}$ 

 $1.55 \times 10^{11}$ 

 $1.34 \times 10^{12}$ 

 $7.58 \times 10^{10}$ 

 $GTR_p (cm^3/m^2 h \Delta C)$ 

Ea (kJ/g-mole)

66.84

52.96

53.36

50.09

51.65

53.84

51.89

51.40

50.82

46.84

54.38

51.40

54.01

51.61

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pressure is constant (Mahajan et al. 2007; Mangaraj et al. 2011), the differential mass balance equations that describe the  $O_2$  concentration changes in a package containing respiring product are:

Rate of  $O_2$  entry into package space—Rate of  $O_2$  consumed by product

= Rate of  $O_2$  accumulation inside package space

That is, 
$$A_p P_{O2} (Y_{O2}^a - Y_{O2}) - W_p R_{O2} = V_{fp} \left( \frac{dY_{O2}}{dt} \right)$$
 (5)

$$\operatorname{Or}\left(\frac{\mathrm{d}Y_{\mathrm{O2}}}{\mathrm{d}t}\right) = -\left(\frac{W_{\mathrm{p}}}{V_{\mathrm{fp}}}\right)R_{\mathrm{O2}} + \left(\frac{A_{\mathrm{p}}P_{\mathrm{O2}}}{V_{\mathrm{fp}}}\right)\left(Y_{\mathrm{O2}}^{\mathrm{a}} - Y_{\mathrm{O2}}\right) \quad (6)$$

Similarly, the  $\mathrm{CO}_2$  concentration changes in a package can be written as,

Rate of CO<sub>2</sub> generated by the fruits—Rate of CO<sub>2</sub> leaving out of the package space

= Rate of accumulation  $CO_2$  inside package space That is,

$$W_{p}R_{CO2} - A_{p}P_{Co2}(Z_{CO2} - Z_{CO2}^{a}) = V_{fp}\left(\frac{dZ_{CO2}}{dt}\right)$$
 (7)

$$Or\left(\frac{dZ_{CO2}}{dt}\right) = \left(\frac{W_p}{V_{fp}}\right)R_{CO2} - \left(\frac{A_p P_{CO2}}{V_{fp}}\right) \left(Z_{CO2} - Z_{CO2}^a\right)$$
(8)

The Eqs. 6 and 8 were coupled to the enzyme kinetics models that describes the dependence of respiration rate on gas composition, temperature (and eventually time) i.e. Eqs. 1, 2 and 3 and models that describes the dependence of packaging film on temperature, i.e. Eq. 4 constitute the basic of development MAP models. Now substituting the Eqs. 1, 2, 3 and 4 appropriately in Eqs. 6 and 8 we have:

$$\left(\frac{\mathrm{d}Y_{02}}{\mathrm{d}t}\right) = -\left(\frac{\mathrm{W}_{\mathrm{p}}}{\mathrm{V}_{\mathrm{fp}}}\right) \times \left\langle \frac{\left(\mathrm{R}_{\mathrm{pvmO2}} \times \exp\left[\frac{-\mathrm{E}_{\mathrm{avmO2}}}{\mathrm{R} \times \mathrm{T}_{\mathrm{abs}}}\right]\right) \times \mathrm{Y}_{02}}{\left(\mathrm{R}_{\mathrm{pvmO2}} \times \exp\left[\frac{-\mathrm{E}_{\mathrm{akmO2}}}{\mathrm{R} \times \mathrm{T}_{\mathrm{abs}}}\right]\right)\right) + \left\{1 + \left[\left[Z_{\mathrm{CO2}}\right] \left(\mathrm{R}_{\mathrm{pkiO2}} \times \exp\left[\frac{-\mathrm{E}_{\mathrm{akiO2}}}{\mathrm{R} \times \mathrm{T}_{\mathrm{abs}}}\right]\right)\right]\right\} \times \mathrm{Y}_{02}}\right) + \left(\frac{\mathrm{A}_{\mathrm{p}} \times \left(\mathrm{OTR}_{\mathrm{p}} \times \exp\left[\frac{\mathrm{E}_{\mathrm{aOTR}}}{\mathrm{R}\mathrm{T}_{\mathrm{abs}}}\right]\right)}{\mathrm{V}_{\mathrm{fp}}}\right) \times \left(\mathrm{Y}_{\mathrm{fp}}^{\mathrm{a}} - \mathrm{Y}_{\mathrm{O2}}\right)$$

$$(9)$$

Table 3 Equilibrium concentration of  $O_2$  and  $CO_2$  predicted by the model and experimental observations for apple (PCG-LFR-1), guava (PCG-LFR-3) and litchi (PCG-LFR-5) packages

MA package fill w	eight of 1.00 kg					
Temperature (°C)	$Y_{O2}^{\text{eq-pre}} (\%)$	$Y_{02}^{eq-exp}$ (%)	Z <sub>CO2</sub> <sup>eq-pre</sup> (%)	Z <sub>CO2</sub> <sup>eq-exp</sup> (%)	t <sup>eq-pre</sup> (h)	t <sup>eq-exp</sup> (h)
Apple						
10	3.11	3.17	3.53	3.74	60.00	66.00
15	3.14	3.22	3.51	3.68	54.00	58.00
20	3.31	3.24	3.59	3.74	46.00	50.00
25	3.30	3.17	3.90	4.17	40.00	42.00
Guava						
10	4.97	5.20	2.91	3.34	24.00	26.00
15	4.86	5.13	2.97	3.45	22.00	24.00
20	4.82	5.00	2.93	3.39	18.00	20.00
25	5.11	5.27	2.86	3.27	16.00	16.00
Litchi						
10	4.93	5.16	3.32	3.96	44.00	48.00
15	5.01	5.24	3.20	3.75	40.00	42.00
20	4.90	5.19	3.14	3.63	30.00	28.00

$$\left(\frac{dZ_{CO2}}{dt}\right) = \left(\frac{W_{p}}{V_{fp}}\right) \times \left\langle \frac{\left(R_{pvmCO2} \times exp\left[\frac{-E_{avmCO2}}{R \times T_{abs}}\right]\right) \times Y_{O2}}{\left(R_{pkmCO2} \times exp\left[\frac{-E_{akmCO2}}{R \times T_{abs}}\right]\right) + \left\{1 + \left[\left[Z_{CO2}\right] \left(R_{pkiCO2} \times exp\left[\frac{-E_{akiCO2}}{R \times T_{abs}}\right]\right)\right]\right\} \times Y_{O2}}\right) - \left(\frac{A_{p} \times \left(CTR_{p} \times \left[\frac{E_{aCTR}}{RT_{abs}}\right]\right)}{V_{fp}}\right) \times \left(Z_{CO2} - Z_{CO2}^{a}\right) \times \left(Z_{CO2} - Z_{CO2}^{a}\right)}\right) + \left\{1 + \left[\left[Z_{CO2}\right] \left(R_{pkiCO2} \times exp\left[\frac{-E_{akiCO2}}{R \times T_{abs}}\right]\right)\right\} + Y_{O2}\right) + \left(1 + \left[Z_{CO2}\right] \left(R_{pkiCO2} \times exp\left[\frac{-E_{akiCO2}}{R \times T_{abs}}\right]\right)\right) + \left(1 + \left[Z_{CO2}\right] \left(R_{pkiCO2} \times exp\left[\frac{-E_{akiCO2}}{R \times T_{abs}}\right]\right)\right) + \left(1 + \left[Z_{CO2}\right] \left(R_{pkiCO2} \times exp\left[\frac{-E_{akiCO2}}{R \times T_{abs}}\right]\right)\right) + \left(1 + \left[Z_{CO2}\right] \left(R_{pkiCO2} \times exp\left[\frac{-E_{akiCO2}}{R \times T_{abs}}\right]\right)\right) + \left(1 + \left[Z_{CO2}\right] \left(R_{pkiCO2} \times exp\left[\frac{-E_{akiCO2}}{R \times T_{abs}}\right]\right)\right) + \left(1 + \left[Z_{CO2}\right] \left(R_{pkiCO2} \times exp\left[\frac{-E_{akiCO2}}{R \times T_{abs}}\right]\right)\right) + \left(1 + \left[Z_{CO2}\right] \left(R_{pkiCO2} \times exp\left[\frac{-E_{akiCO2}}{R \times T_{abs}}\right]\right)\right) + \left(1 + \left[Z_{CO2}\right] \left(R_{pkiCO2} \times exp\left[\frac{-E_{akiCO2}}{R \times T_{abs}}\right]\right)\right) + \left(1 + \left[Z_{CO2}\right] \left(R_{pkiCO2} \times exp\left[\frac{-E_{akiCO2}}{R \times T_{abs}}\right]\right)\right) + \left(1 + \left[Z_{CO2}\right] \left(R_{pkiCO2} \times exp\left[\frac{-E_{akiCO2}}{R \times T_{abs}}\right]\right)\right) + \left(1 + \left[Z_{CO2}\right] \left(R_{pkiCO2} \times exp\left[\frac{-E_{akiCO2}}{R \times T_{abs}}\right]\right)\right) + \left(1 + \left[Z_{CO2}\right] \left(R_{pkiCO2} \times exp\left[\frac{-E_{akiCO2}}{R \times T_{abs}}\right]\right)\right) + \left(1 + \left[Z_{CO2}\right] \left(R_{pkiCO2} \times exp\left[\frac{-E_{akiCO2}}{R \times T_{abs}}\right]\right)\right) + \left(1 + \left[Z_{CO2}\right] \left(R_{pkiCO2} \times exp\left[\frac{-E_{akiCO2}}{R \times T_{abs}}\right]\right)\right) + \left(1 + \left[Z_{CO2}\right] \left(R_{pkiCO2} \times exp\left[\frac{-E_{akiCO2}}{R \times T_{abs}}\right]\right)\right) + \left(1 + \left[Z_{CO2}\right] \left(R_{pkiCO2} \times exp\left[\frac{-E_{akiCO2}}{R \times T_{abs}}\right]\right)\right) + \left(1 + \left[Z_{CO2}\right] \left(R_{pkiCO2} \times exp\left[\frac{-E_{akiCO2}}{R \times T_{abs}}\right]\right)\right) + \left(1 + \left(R_{cO2}\right) \left(R_{pkiCO2} \times exp\left[\frac{-E_{akiCO2}}{R \times T_{abs}}\right]\right)\right)$$

Numerical analysis

Simultaneous solution of above differential equations would give variation of  $O_2$  concentration,  $Y_{O2}$  (volume fraction),  $CO_2$  concentration,  $Z_{CO2}$  (volume fraction) as a function of time, t (h). The typical functional relationship for  $R_{O2}$  and  $R_{CO2}$  as a function of  $Y_{O2}$  and  $Z_{CO2}$  is carried out numerically, using Adams numerical method, which is based on Taylor's formula (Piskunov 1981).

The estimated values of respiration model parameters  $R_p$  and  $E_a$  for  $O_2$  consumption and  $CO_2$  evolution, along with the weight of fruits ( $W_p$ ) constitute the product parameters. The GTR<sub>p</sub>,  $E_{aOTR}$  and  $E_{aCTR}$  of selected films were used as film parameters. Total surface area of film package ( $A_p$ ) and the package head space ( $V_{fp}$ ) served as input for package parameters, whereas, initial in-pack  $O_2$  and  $CO_2$  concentration ( $Y_{O2}$ ,  $Z_{CO2}$ ) and outside atmosphere ( $Y_{O2}^a$  and  $Z_{CO2}^a$ ) served as environment parameters. As the MA package initially contained air, initial  $O_2$  and  $CO_2$  ( $Y_{O2}$  and  $Z_{CO2}$ ) concentration were taken as 21 % (0.21 cm<sup>3</sup>/cm<sup>3</sup> of air) and 0.03 % (0.0003 cm<sup>3</sup>/cm<sup>3</sup> of air) respectively.

# MA Packaging of selected fruits

Apple, guava and litchi of medium size harvested at commercial maturity were collected from the orchard and numberlabeled for MA packaging (Mangaraj and Goswami 2009c). Five types of packages (PKG-LFR1, PKG-LFR2, PKG-LFR3, PKG-LFR4 and PKG-LFR5) of required size i.e.  $24 \times 19$  cm for apple;  $19 \times 19$  cm for guava and  $28 \times 22$  cm for litchi for  $1\pm0.1$  kg fill weight were developed. Fruits were packaged and heat sealed. Impulse time was adjusted for different films for obtaining a clean seal. Silicon rubber septums were glued to the packages to facilitate gas sampling. The MA packages were labeled marked and kept in the incubator for subsequent storage study at 10, 15, 20 and  $25^{\circ}$ C (Mangaraj et al. 2005; Mangaraj et al. 2012a, b; Mangaraj et al. 2013b).

The samples of package air were analyzed on Gas Chromatograph (Mangaraj and Goswami 2009a, b) for determining the variation of  $O_2$  and  $CO_2$  concentration in the package with time. The equilibrium concentration of  $O_2$  ( $Y_{O2}^{eq}$ ) and  $CO_2$  ( $Z_{CO2}^{eq}$ ) were subsequently determined. From the mathematical model of gaseous

exchange in MAP, the values of  $Y_{O2}$ ,  $Z_{CO2}$ ,  $Y_{O2}^{eq}$ ,  $Z_{CO2}^{eq}$  and  $t_{eq}$  were predicted by employing MATLAB Programme. The predicted and the experimental values of  $Y_{O2}$ ,  $Z_{CO2}$ ,  $Y_{O2}^{eq}$ ,  $Z_{CO2}^{eq}$  and  $t_{eq}$  were compared for validation of the developed model.

## **Results and discussions**

## MAP modelling and analysis

With the objective of meeting MAP requirements of fruit the polymeric high, medium and low barrier hydrophilic films namely, low density polyethylene (LDPE), biaxially oriented polypropylene (BOPP), polyvinyl chloride (PVC), polyvinyledene chloride (PVDC) were procured from Reliance Food Industry, Kolkata considering various film characteristics (Exama et al. 1993; Mangaraj et al. 2009; Costa et al. 2011). Two different films were combined through the tailoring of film laminates to bring the gas transmission requirement of the laminates close to the required values (Mangaraj et al. 2012a, b; Mangaraj and Tripathi 2013, a, ba,b). Three types of film packages i.e. PCG-LFR-1 (BOPP-30  $\mu$ +PVC-50  $\mu$ ) for apple; PCG-LFR-3 (BOPP-45 µ+PVC-25 µ) for guava; and PCG-LFR-5 (BOPP-30  $\mu$ +PVC-25  $\mu$ ) for litchi of package size 24 cm×19 cm; 19 cm×19 cm and 28 cm 22 cm, respectively were chosen for experimental validation of proposed MAP model (Mangaraj et al. 2012a, b; Mangaraj and Tripathi 2013, a, b). The activation energy and pre-exponential factor of Arrhenius-type equation for different model parameters of enzyme kinetics of uncompetitive inhibition is presented in Table 1; moreover the activation energy and pre-exponential factor of Arrheniustype equation for selected polymeric films is given in Table 2. These values were used for validating the developed global MAP model (Mangaraj and Goswami 2008, 2011a. b).

In this study a generalized global model was developed and verified against the MAP storage study data for apple, guava and litchi for  $1\pm0.1$  kg fill weight. The output obtained from this model was compared with the experimental data and used for predicting the equilibrium level of O<sub>2</sub> and CO<sub>2</sub> in MA packaging of different commodity carried out by some researchers. Equilibrium concentrations of O2 and CO2 in MA packages

The predicted as well as experimental values of Y<sub>02</sub><sup>eq</sup>,  $Z_{CO2}^{eq}$  and  $t_{eq}$  for various MA packages for  $1\pm0.1$  kg fill weight at different storage temperatures have been presented in Table 3. The profile of package air composition with time predicted by the modelling of gaseous exchange in MAP for the packages PCG-LFR-1, PCG-LFR-3 and PCG-LFR-5 for apple, guava and litchi, respectively at 15°C has been depicted in Fig. 2. Most of the packages have established equilibrium at such levels of O<sub>2</sub> and CO<sub>2</sub>, which were fairly close to the target levels. The predicted and experimental values of Y<sub>02</sub><sup>eq</sup>, Z<sub>C02</sub><sup>eq</sup> were found to be higher than the target levels for all the MA packages. There was good agreement between predicted as well as experimental values of Y<sub>02</sub><sup>eq</sup> and Z<sub>CO2</sub><sup>eq</sup>. The experimental values of  $Y_{O2}^{eq}$  varied between 3.10–3.31 % (0.031–0.033 cm<sup>3</sup> per cm<sup>3</sup> of air); 5.00–5.37 % (0.05–0.054 cm<sup>3</sup> per cm<sup>3</sup> of air); 4.95-5.28 % (0.049-0.053 cm<sup>3</sup> per cm<sup>3</sup> of air) whereas those of  $Z_{CO2}^{eq}$  varied between 3.34–4.17 %  $(0.0334-0.0417 \text{ cm}^3 \text{ per cm}^3 \text{ of air}); 3.14-3.72 \%$  $(0.0314-0.0372 \text{ cm}^3 \text{ per cm}^3 \text{ of air}); 3.56-4.20 \%$ (0.0356-0.0420 cm<sup>3</sup> per cm<sup>3</sup> of air) for all types of MA packages for apple, guava and litchi, respectively at all the reference temperature levels. The equilibrium O<sub>2</sub> and CO<sub>2</sub> concentration obtained from the model was verified against the experimental data for MA packages of fruits. The mean relative deviation moduli between the equilibrium concentration of O<sub>2</sub> and CO<sub>2</sub> as predicted by the developed model and that obtained through experiments were found to be in the range of 5.92-8.6 % and 7.14-9.35 %, respectively. This indicated that, the developed model is in good agreement with the experimental data. The experimental as well as predicted variation of O2 and CO2 levels in MA packages PCG-LFR-3 at 15°C storage temperatures has been shown in Fig. 3. During steady state period, the experimental values of O<sub>2</sub> and CO<sub>2</sub> were found to be nearly constant for an extended period of storage. By and large all types of MA packages have established dynamic equilibrium state without causing any unfavorable deviation from the target levels of O2 and CO2 at all the reference storage temperatures.

## Equilibrium time



Fig. 2 (a, b, c): Predicted variation of  $O_2$  and  $CO_2$  with time by the model in MA packed apple, guava and litchi at 15°C

34–80 h; 10–34 h and 24–56 for all types of MA packages for apple, guava and litchi, respectively at all the reference storage temperatures as given in Table 3. The mean relative deviation moduli for the equilibrium time as predicted by the developed model and that obtained through experiments were found to be 7.77, 7.17 and 2.47 % for apple, guava and litchi, respectively. This indicated that, the developed model is in good



Fig. 3 Experimental and predicted variation in package air composition with time for guava (PCG-LFR-3) at 15°C storage temperatures

agreement with the experimental data. There was some deviation of experimental values from the predicted ones. The development of guasi-equilibrium conditions and the variations in the free volume in the package (V<sub>fp</sub>), because of the varying fill weight, were probably the cause of such deviations in equilibrium time  $(t_{eq})$ values. In fact, small variations in V<sub>fp</sub> are always possible in a flexible package. Hence, it is unrealistic to expect a constant value of V<sub>fp</sub> in the flexible packages. It has been seen that the variation in O2 affects both  $R_{O2}$  and  $R_{CO2}$  significantly. With the variation in  $R_{O2}$ and R<sub>CO2</sub>, the O<sub>2</sub> consumption as well as the CO<sub>2</sub> evolution of the package varies which in turn affects  $O_2$  and  $CO_2$  level in the internal atmosphere of the package. Thus, as O2 decreases, RCO2 reduces which in turn reduces CO<sub>2</sub> in the internal atmosphere of the package.

Reduction in  $CO_2$  level tends to retrieve  $R_{CO2}$  slightly. However, the amount of reduction in CO2 due to decrease in  $O_2$  is greater than the amount of retrieved. As such, with the decrease in O<sub>2</sub> level CO<sub>2</sub> level also decreases, though by small amounts. Thus, though the equilibrium condition for CO<sub>2</sub> level appears to be approaching earlier than that of O<sub>2</sub> level but in true sense,  $CO_2$  level becomes stable only when  $O_2$  level attains equilibrium (Fig. 2 and 3). It implies that the equilibrium for both, O<sub>2</sub> and CO<sub>2</sub> is attained simultaneously in MA packaging. Also, in view of the fact that O<sub>2</sub> level has more pronounced effect on respiration rates than CO<sub>2</sub> level, the equilibrium time (teq) for O2 level assume greater importance. The single equilibrium time  $(t_{eq})$ approach advocated in this study is in agreeance with the study of (Rocculi et al. 2006; Torrieri et al. 2007; Gonzalez-Buesa et al. 2009; Tariq et al. 2009; Mangaraj et al. 2011).

Validation of model with other's work

Mahajan and Goswami (2001) has developed enzyme kinetics respiration model for red delicious apple. Using the values of model parameters the activation energy and respiration pre-exponential factor for  $O_2$  consumption and  $CO_2$  evolution was obtained. Substituting these values in Eqs. 9 and 10, with area of packaging film  $(A_p)$  as 0.11 m<sup>2</sup>, mass of apple  $(W_p)$  of 1.00 kg, void volume of the package  $(V_{fp})$  of 1,000 cm<sup>3</sup> the variation



Fig 4 a Plot between  $O_2$  and  $CO_2$  with time for red delicious apple b Plot between  $O_2$  and  $CO_2$  with time for tomato c Plot between  $O_2$  and  $CO_2$  with time for button mushroom

of  $O_2$  and  $CO_2$  with time plot was obtained (Fig. 4a). It shows that (Fig. 4a) the model has achieved an equilibrium concentration of 6 % O<sub>2</sub> (0.06 cm<sup>3</sup> per cm<sup>3</sup> of air) and 4 % CO<sub>2</sub> (cm<sup>3</sup> per cm<sup>3</sup> of air) at 40 h and remains in equilibrium for 100 h. Geeson et al. (1985) conducted MA packaging study with tomato of weighing 390 g using 15 µ polyvinylchloride film having void volume of 550 cm<sup>3</sup> at a temperature of 10 °C. The equilibrium concentration of O<sub>2</sub> (4 %) and CO<sub>2</sub> (10 %) achieved inside the film package in 200 h using the developed model (Fig. 4b). Similarly, Rai and Paul (2007) worked on design and modelling of gaseous exchange in MAP for button mushrooms. They stored mushrooms of weight 500 g inside a 57 µLDPE film having a void volume of 545 cm<sup>3</sup> and area of packaging film of 0.11 m<sup>2</sup> at a temperature of 15 °C. They recorded the variation of O2 concentration and CO2 concentration with time inside the MA package. They found that  $O_2$ concentration decreased and CO<sub>2</sub> concentration increased inside the package as the storage period progressed (Fig. 4c). The model suggested, that the dynamic equilibrium attained at 2 % oxygen and 4 % carbon dioxide level (Fig. 4c) and it maintained till 96 h of packaging. The mean relative deviation modulus for equilibrium gas concentration and time as predicted by the developed model and experimental values varied in the range of 4.7-8.5 % and 3.9-6.4 %, respectively indicating the good predictability of the developed MAP model.

# Conclusions

A mathematical model for MA packaging of apple, guava and litchi applying enzyme kinetics based respiration equation coupled with the Arrhenious model was developed. The model was used to determine the time to reach to the equilibrium concentration inside the MA package and the level of O<sub>2</sub> and CO<sub>2</sub> concentration at equilibrium state. The equilibrium O2 and CO2 concentration obtained from the model was verified against the experimental data for MA packages of fruits. The mean relative deviation moduli between the equilibrium concentration of O<sub>2</sub> and CO<sub>2</sub> as predicted by the developed model and that obtained through experiments were found to be in the range of 5.92-8.60 % and 7.14-9.35 %, respectively for apple, guava and litchi fruits. This indicated that, the developed model is in good agreement with the experimental data. There were some deviations of equilibrium time between the predicted and experimental values may be attributed to the development of quasi-equilibrium conditions and the variations in the free volume in the package due to the varying fill weight. In fact, small variations in free volume are always possible in a flexible package. It has been seen that the equilibrium time for both,  $O_2$  and  $CO_2$  attained simultaneously in MA packaging. The model has been used for predicting the equilibrium level of  $O_2$  and  $CO_2$  in MA packaging of different commodity carried out by some researchers. These results further strengthen the model for its validation and wide application for fresh fruits and vegetables.

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