

Self-propelled particles that transport cargo through flowing blood and halt hemorrhage

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Delivering therapeutics deep into damaged tissue during bleeding is challenging because of the outward flow of blood. When coagulants cannot reach and clot blood at its source, uncontrolled bleeding can occur and increase surgical complications and fatalities. Self-propelling particles have been proposed as a strategy for transporting agents upstream through blood. Many nanoparticle and microparticle systems exhibiting autonomous or collective movement have been developed, but propulsion has not been used successfully in blood or used *in vivo* to transport therapeutics. We show that simple gas-generating microparticles consisting of carbonate and tranexamic acid traveled through aqueous solutions at velocities of up to 1.5 cm/s and delivered therapeutics millimeters into the vasculature of wounds. The particles transported themselves through a combination of lateral propulsion, buoyant rise, and convection. When loaded with active thrombin, these particles worked effectively as a hemostatic agent and halted severe hemorrhage in multiple animal models of intraoperative and traumatic bleeding. Many medical applications have been suggested for self-propelling particles, and the findings of this study show that the active self-fueled transport of particles can function *in vivo* to enhance drug delivery.

INTRODUCTION

Uncontrolled bleeding occurs in many clinical conditions, including surgical and dental procedures, severe nosebleed, postpartum hemorrhage, trauma, and hemophilia (1–3). The primary concern during severe bleeding is controlling blood loss, but controlling secondary bleeding and infection and promoting tissue repair are also important. These concerns could be addressed by quickly delivering therapeutics, such as coagulants, antifibrinolytics, antimicrobials, or growth factors, to the damaged vasculature (4, 5). However, systemic delivery of these therapeutics via injections or local delivery of these therapeutics via intravascular catheters is often impractical. Delivering agents topically is also limited by biophysical barriers; it is difficult to transport agents against blood flow, especially far enough upstream to reach leaking vessels. We hypothesize that therapeutics formulated into water-reactive particles that release gas to transport themselves can be delivered upstream through blood flow and directly address hemorrhage.

Many particle systems that exhibit active autonomous and collective movement have been developed for broad potential uses (6–12). Chemically driven self-propelling particles, sometimes termed “catalytic microengines,” often rely on gas generation for propulsion, although other mechanisms, such as ultrasound or magnetically driven swimmers, have been used (13, 14). Several limitations have prevented these self-propelling particles from being used to deliver therapeutics *in vivo*. These particles typically propel at velocities many orders of magnitude

slower than blood flow or rely on fuels (often hydrogen peroxide) dispersed in the solution (9, 10). The transport of therapeutics through whole blood by catalytic microengines was recently reported to be unachievable, although noncatalytic self-fueled particles that can transport through gastric fluids have been developed (6, 7, 15). To develop self-fueled particles suitable for transport through blood, we chose materials that react vigorously to produce gas in most aqueous solutions. Calcium carbonate (CaCO_3) is commonly used in antacid tablets and drug formulations, rapidly produces carbon dioxide (CO_2) in acidic solutions, and forms porous microparticles that adsorb protein, making it an ideal substance for self-fueled particles (16). We report that CaCO_3 -based microparticles actively transport through blood and can carry functional protein cargo through wounds and into the vasculature. This is the first report of self-fueled particles being used *in vivo* to transport through blood, and the findings demonstrate that propulsion is a viable mechanism for targeting the delivery of therapeutics into wounds.

RESULTS AND DISCUSSION

When CaCO_3 microparticles were mixed with a solid organic acid, they rapidly traveled through aqueous solutions (Fig. 1A). CaCO_3 particles were mixed with the organic acid protonated tranexamic acid (TXA-NH_3^+) (1:1 molar ratio) and injected into buffered saline solution or whole blood (Fig. 1B). The particles reacted vigorously, rising buoyantly and spreading laterally both below and at the surface within seconds (Fig. 1, C and D). The transport of particles, referred to here as “propulsion,” occurred from a combination of particles rising buoyantly and propelling laterally and the large convection generated by the rapid production of gas bubbles (17). The reaction was self-buffering because much of TXA-NH_3^+ was neutralized as the particles were partially consumed and converted into CO_2 . Propulsion also occurred when other solid organic acids, such as citric acid and malic acid, were substituted for TXA-NH_3^+ (figs. S1 to S3). When CaCO_3 particles were mixed with neutral tranexamic acid (TXA-NH_2), which did not protonate

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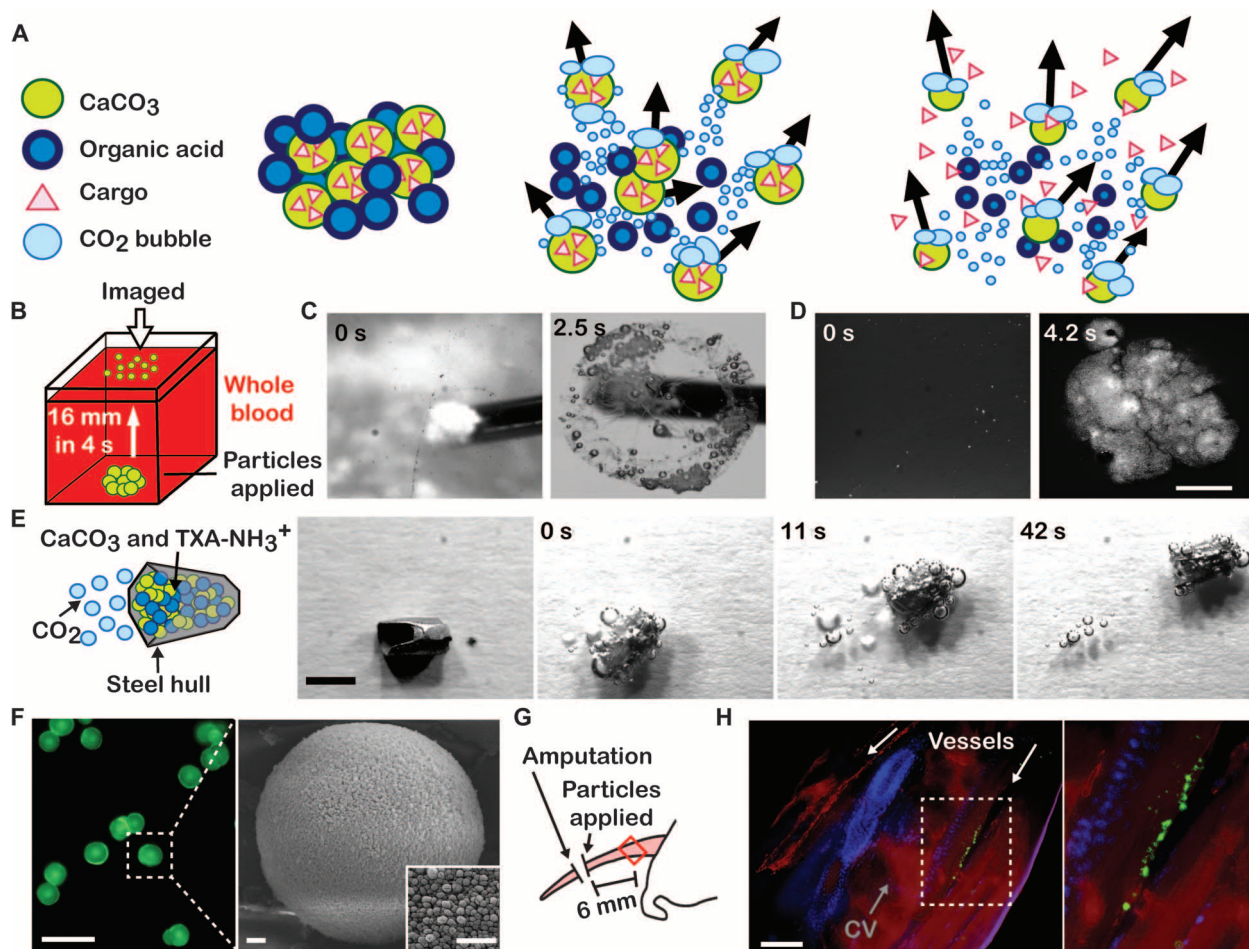


Fig. 1. CaCO_3 particles combined with an organic acid travel through aqueous solutions. (A) Schematic showing CaCO_3 particles releasing CO_2 and propelling themselves and their cargo when placed in water. (B) Schematic showing how particle movement was measured in buffer and whole blood. (C and D) Images of particles appearing at the surface of a buffered solution (C) and whole blood (D). Scale bars, 2 mm. (E) Schematic and images of a steel hull propelled by CaCO_3 and TXA-NH_3^+ . Scale bar, 2 mm. (F) Images of immobilized CaCO_3 particles containing a fluorescently tagged cargo, FITC-dextran. Scale bars, 30 μm (green fluorescent particles) and 0.5 μm (scanning electron micrographs). (G) Schematic showing a mouse tail being amputated and treated with propelling CaCO_3 particles. Red rectangle denotes the field of view in (H). (H) Histological section of a treated tail showing particles located 6 mm inside the tail, blood vessels, and caudal vertebrae (CV). Fluorescence staining shows actin (red), nuclei (blue), and CaCO_3 particles (green). Scale bar, 200 μm .

carbonate, they did not propel. Similar to other types of gas-releasing fuels used in propelled particles, this CO_2 -releasing mixture could be incorporated into a larger object and propel it (9, 10, 18). A 10-mg steel hull containing the fuel propelled at 0.2 mm/s despite having a mass 10 times greater than that of the fuel (Fig. 1E).

Porous CaCO_3 microparticles capable of adsorbing molecular cargos were prepared by controlled precipitation through the addition of aqueous Na_2CO_3 to aqueous CaCl_2 (16). The particles had spherical geometries with an average diameter of 10 μm (Fig. 1F). Nonporous particulates of CaCO_3 and Na_2CO_3 also propelled but could not load high concentrations of cargo (Fig. 2A and figs. S1 to S3). To initially test whether porous microparticles could propel and carry fluorescent cargos through blood in vivo, we applied them to a site of bleeding in a mouse model of hemorrhage. A portion of the mouse tail was amputated, and propelling microparticles containing fluorescent nanoparticles or fluorescein isothiocyanate (FITC)-dextran were applied.

Histological sections of the intact tail showed fluorescent particles up to 1 cm deep in the vasculature, confirming transport and delivery through blood in vivo (Fig. 1, G and H). Propelled particles transported through blood vessels and colocalized with red blood cells past the surface of the tail wound (fig. S4). When nonpropelling CaCO_3 microparticles were tested, particles were not found past the surface of the tail. Because of the multiple mechanisms of propulsion and the complex nature of blood flow in wounds, particles were not expected to maintain their velocity in a single direction. No signs of pain or distress were observed even when particles and TXA-NH_3^+ were injected intravenously, and the histological analysis of lung tissues showed no difference from controls, suggesting that major embolism or severe toxicity did not occur (fig. S5). However, additional work is required to rigorously evaluate safety and toxicity for specific applications. Although the propulsion of catalytic microengines in blood was previously considered unachievable (6, 7), our results show that generating gas from particles can achieve this.

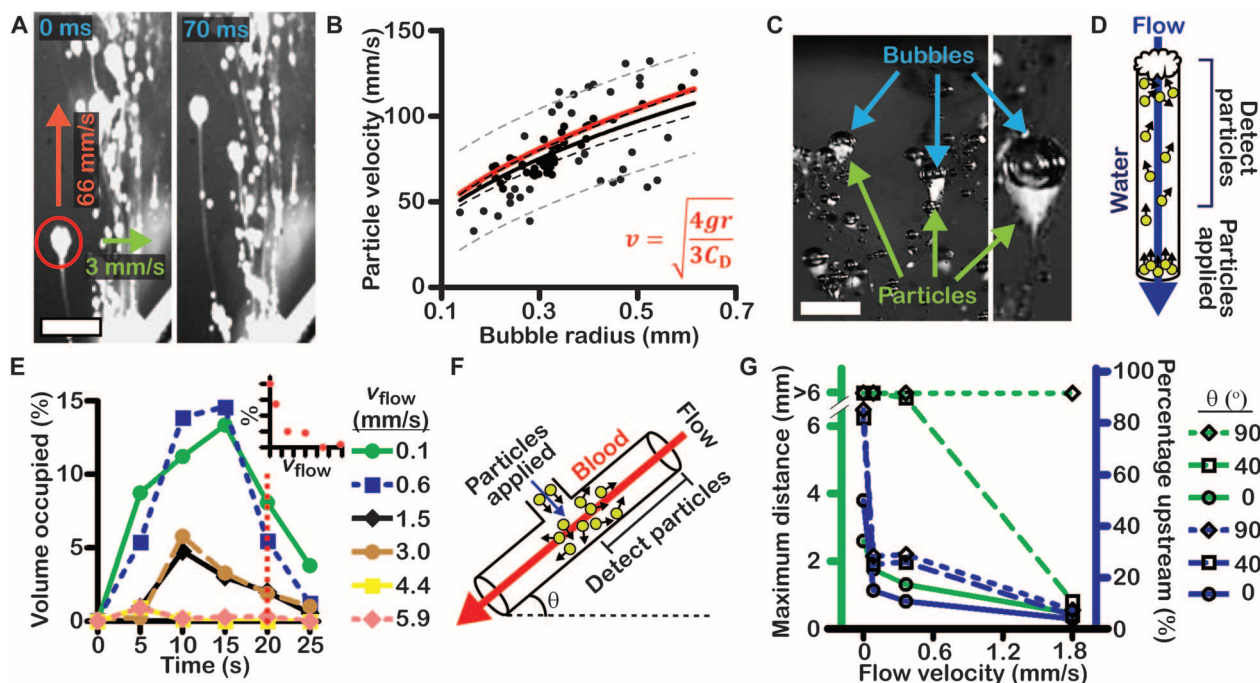


Fig. 2. CaCO_3 particles travel upstream and at high velocities through stagnant and flowing solutions. (A) Images of CaCO_3 particles transporting upward through a stagnant acidic solution. (B) Particle velocity increased as a function of the volume of attached bubbles. The red line denotes the velocities of bubbles predicted by a model equating buoyant and drag forces. The black solid line denotes a one-half power regression of the data. Dashed lines denote the 99% confidence band (black) and 90% prediction band (gray) of regression. (C) Images of particles carried upward by CO_2 bubbles. (D) Schematic showing how propulsion of particles with TXA-NH_3^+ through flowing water was measured. (E) The particles traveled against flow velocities of up to 3 mm/s. (Inset) Fraction of particles that accumulated for each flow velocity at 20 s. (F) Schematic showing how propulsion of particles through a channel of flowing whole blood was measured at three angles. (G) Maximum distances that particles traveled upstream through flowing and stagnant blood at various angles. Scale bars, 2 mm.

To understand the range of potential applications for propelling CaCO_3 particles, we measured the velocities of particles in stagnant and flowing solutions (Fig. 2). CaCO_3 particles were injected at the bottom of a container containing an aqueous organic acid, and particle trajectories were imaged (Fig. 2A). Particles usually reacted as aggregates with a diameter (mean \pm SD) of 0.4 ± 0.2 mm, breaking apart into individual particles as they traveled (figs. S1 and S2). Particles had upward velocities of 71 ± 23 mm/s and lateral velocities of 3.6 ± 3.5 mm/s, among the fastest reported for self-propelling particles (9, 10). This upward velocity of particles mimics the gravitic movement used by some microorganisms to propel upward against gravity (19). Particle velocity increased with bubble volume (Fig. 2B). Images showed that CaCO_3 particles were attached to the bottom of CO_2 bubbles and were buoyantly carried upward as they reacted (Fig. 2C). When particles were intentionally clumped together into larger, heavier aggregates, they sank and propelled laterally with similar horizontal velocities of ~ 3 mm/s (fig. S3). These results may imply that other gas-releasing self-propelled particles of low density may rise buoyantly if the reaction rate is high and large bubbles are produced.

The forces expected to cause upward transport were considered: the buoyant force of CO_2 bubbles and the drag force opposing motion (Supplementary Materials). The buoyant force F_{buoy} is given by $F_{\text{buoy}} = \rho g V$, where ρ is the density of the aqueous solution, g is the acceleration due to gravity, and V is the bubble volume. The CO_2 bubbles were modeled as oblate spheroids. The Reynolds number for this system ranges between 1 and 100; therefore, the drag force F_{drag} is approxi-

mated by $F_{\text{drag}} \approx \frac{1}{2} \rho A v^2 C_D$, where A is the frontal area of the bubble, v is the upward velocity, and C_D is the coefficient of drag. Equating F_{buoy} to F_{drag} gives $v \approx (4gr/3C_D)^{1/2}$, where r is the bubble radius. Despite simplifying assumptions and deriving them from first principles, this relationship is remarkably consistent with the observed particle velocities and bubble radii, successfully predicting the one-half power regression of the data within 10% (Fig. 2B). The model does not describe many important aspects of the behavior of particles in flowing solutions or wounds (such as turbulent or pulsating flow) or in heterogeneous solutions (such as blood) (20).

To determine whether the particles were capable of transporting upstream against blood flow, we mixed CaCO_3 and TXA-NH_3^+ together and applied them to an aqueous solution flowing through a glass capillary at velocities between 0.06 and 5.9 mm/s (Fig. 2D). Particles applied at the bottom of the tube traveled upward, and the fraction of the tube occupied by particles and accompanying bubbles was measured (Fig. 2E). The propelling particles successfully opposed flow velocities of up to 3.0 mm/s. Fluorescence images showed that fluorescent CaCO_3 particles reached the top of the flowing solution (fig. S6). To determine the flow velocity of blood through which particles could travel, we injected them into a stream of whole blood in a microfluidic channel (Fig. 2, F and G). The maximum distance that particles traveled through flowing and stagnant blood was measured. In stagnant blood oriented perpendicular to gravity, particles traveled to a maximum distance of 3.9 mm at a velocity of 0.54 mm/s (movie S1). Through blood flowing at 0.4 mm/s, a large portion of particles consistently traveled

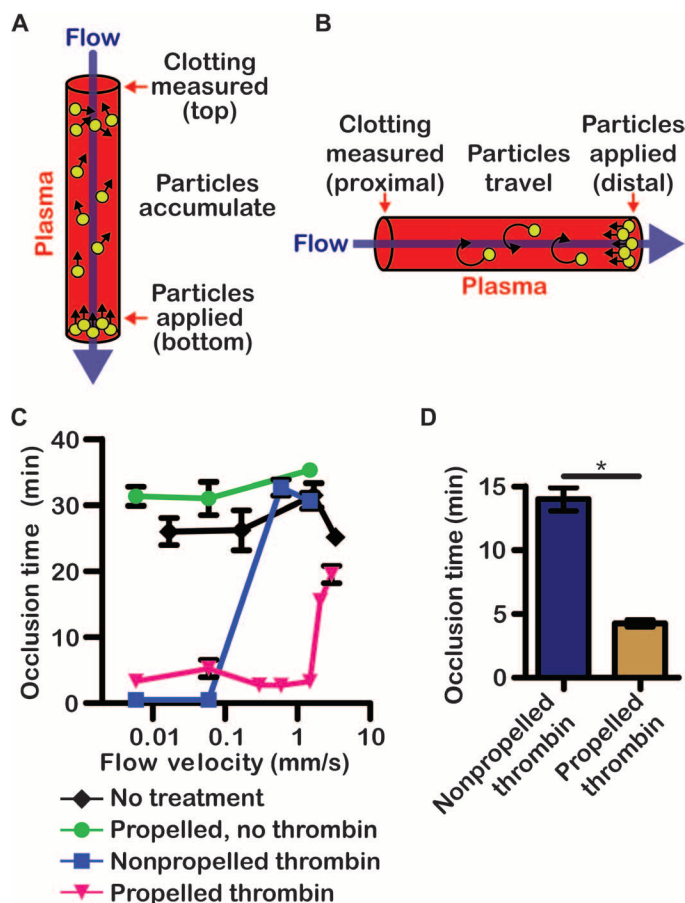


Fig. 3. Propelled thrombin clots flowing blood plasma and halts severe hemorrhage. (A and B) Schematic of clotting and occlusion of flowing blood plasma ex vivo in vertical (A) and horizontal (B) orientations. (C and D) Clotting of flowing human plasma ex vivo by thrombin-loaded particles at various flow rates in a vertical orientation (C) and at 0.13 mm/s in a horizontal orientation (D). $n = 3$. $*P < 0.05$. Error bars indicate SEM.

upstream at various angles relative to gravity. When the flow was 1.8 mm/s and parallel to the direction of gravity, 13% of particles propelled upstream to a maximum distance of 6 mm. Particles were capable of transporting over a distance of 1 m upstream through blood (fig. S7). Physiological flow velocities are about 1 mm/s in capillaries and up to 10 to 100 mm/s in larger arteries but are variable and can be much lower in wounds when bleeding originates from these vessels (21). On the basis of these values, CaCO_3 particles appear capable of propelling through flow velocities present in wounds and small vessels, but likely not against blood flowing through large arteries. This may help contain the particles near wound sites and prevent them from entering the systemic circulation.

The ability to transport molecular cargos through blood could address an unmet need for materials that effectively halt severe bleeding. Bleeding can be minimized with antifibrinolytics (such as tranexamic acid) or with intravascular catheters that embolize the vasculature (22). However, when vessels cannot be targeted with catheters or when bleeding must be stopped immediately, more traditional approaches are attempted. The wound can be packed with dressings or powders containing gelatin, modified cellulose, or zeolites (23, 24). Intraoper-

atively, thrombin can be applied topically, in solution, or with gelatin (25, 26). However, these methods are not highly effective during severe bleeding or when external blood loss originates inside a cavity (24).

To create propelling particles that clot blood, we adsorbed thrombin (a serine protease that activates the coagulation system and directly cleaves fibrinogen) onto porous particles. Particles were loaded with 0.9 μmol of active thrombin per gram of CaCO_3 , of which about 0.6 μmol was loosely bound and could be removed upon washing with low-stringency buffer (fig. S8A). These thrombin-loaded particles, added alone or combined with either TXA-NH_3^+ (“propelled thrombin”) or TXA-NH_2 (“nonpropelled thrombin”), rapidly clotted blood, and the activities of thrombin in propelled and nonpropelled formulations were similar (fig. S8). Tranexamic acid can contribute to the stabilization of clots by inhibiting clot lysis, although this process occurs much slower than clot initiation by thrombin. To test whether the propelled thrombin particles could clot flowing plasma, we applied the particles to the bottom of a glass capillary tube where plasma flowed between 0.006 and 3.4 mm/s (Fig. 3A). A microfluidic system was used to control the flow of plasma and to detect occlusion of flow through the capillary tube (fig. S9). The propelled thrombin occluded flow at velocities about 10 times faster than nonpropelled thrombin. At a physiologically relevant flow velocity of 3 mm/s, the particles propelled upward against flow, accumulated high in the tubing, and initiated clotting (Fig. 3C). Nonpropelled thrombin only occluded flow at very slow velocities (up to 0.06 mm/s) and showed no difference from controls at velocities of 0.6 mm/s and above, where the background occlusion times were 30 min. Without propulsion, thrombin was able to form a clot at the exit of the tubing, but it was easily pushed out and was unable to permanently occlude flow. Thrombin clotted flowing plasma four times faster when it was adsorbed onto propelled particles compared to when it was nonadsorbed and mechanically mixed with the particles; however, both of these gas-generating formulations clotted faster than thrombin adsorbed on nonpropelled particles (fig. S8). In a separate experiment, when plasma was flowed perpendicular to gravity at 0.125 mm/s, propulsion still significantly decreased time to occlusion, which occurred in 4 min with propelled thrombin but took 14 min with nonpropelled thrombin (Fig. 3, B and D). Together, these results show that thrombin initiates clotting faster when propelled because it is delivered upstream both by direct transport (as cargo loaded onto the propelled particles) and likely by the convective effects of gas generation.

The self-propelling particles were tested for their ability to halt hemorrhage in two murine models. First, in a model of amputation, mouse tails were transected 8 mm from the tip, causing severe hemorrhage (27). Propelled or nonpropelled thrombin particles were applied for 30 s at the site of amputation, and bleeding was monitored for 10 min in warm saline. Control mice were not treated after the amputation. The propelled thrombin significantly decreased bleeding time compared to the other groups (Fig. 4A and fig. S10). Among mice that received propelled thrombin, seven of nine (78%) stopped bleeding during the observation. In contrast, in the groups that received nonpropelled thrombin and no treatment, only three of nine (33%) and two of eight (25%) mice stopped bleeding, respectively. During a single-dose test for toxicity that lasted 3 days, all treated mice remained healthy. Compared to untreated mice, they showed no signs of distress or tissue necrosis and no increase in the infiltration of inflammatory cells in histological sections of the tail (fig. S11).

The transport of particles in spatially unconfined systems is mostly upward as a result of buoyant rise. If the transport of particles in wounds

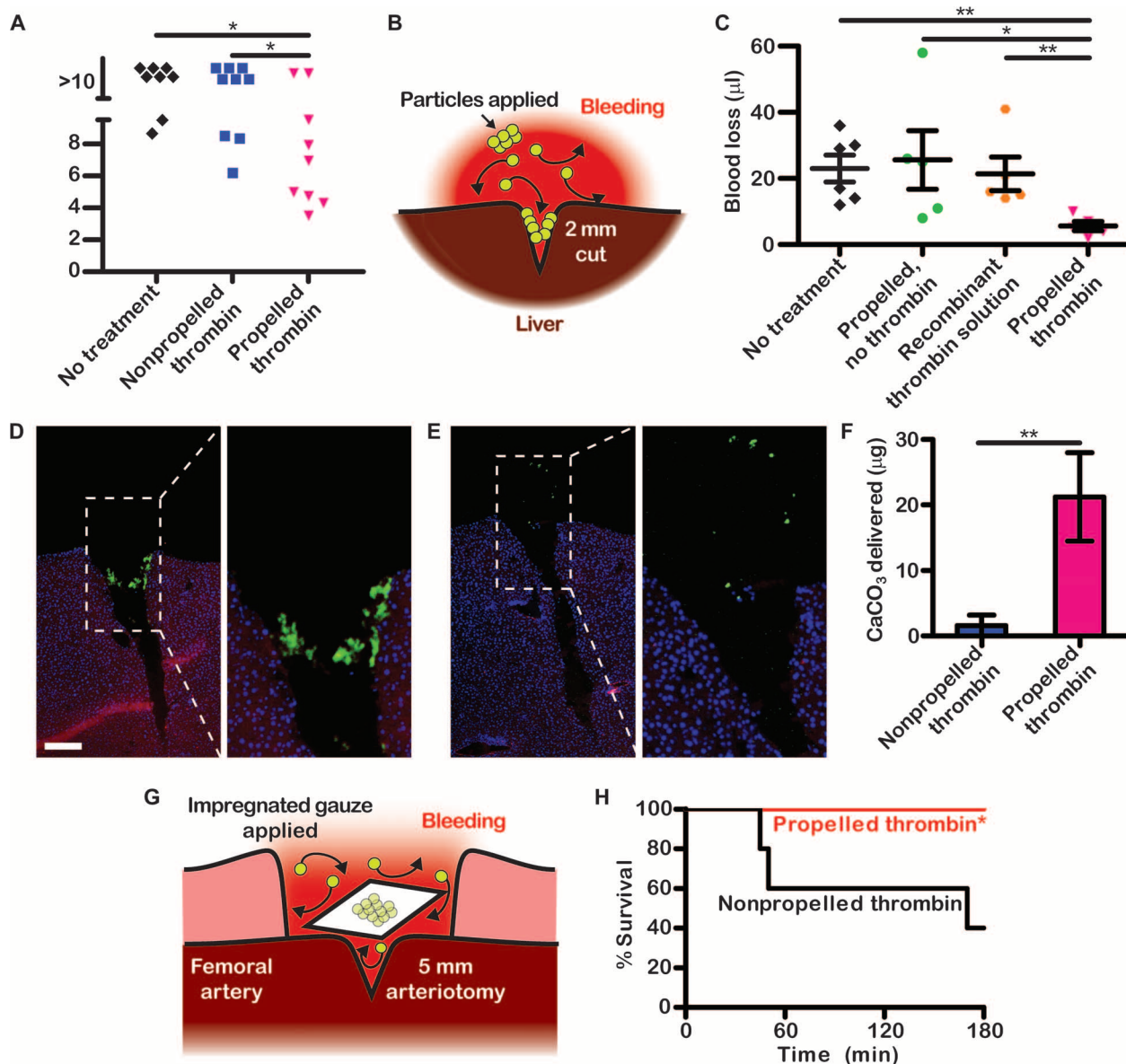


Fig. 4. Propelled thrombin is delivered deep into wounds and halts hemorrhage in vivo. (A) Bleeding times in vivo after the tails of mice were amputated. (B) Schematic showing a mouse liver punctured and treated with propelled thrombin. (C) Volume of blood loss in a separate cohort of mice after their livers were punctured and treated. (D and E) Histological sections of livers treated with propelled thrombin (D) or nonpropelled thrombin (E). Fluorescence staining shows actin (red), nuclei (blue), and CaCO₃ particles (green). Scale bar, 200 μm . (F) Mass of CaCO₃ delivered to sites of liver puncture. (G) Schematic showing a pig's punctured femoral artery being treated with gauze impregnated with propelled thrombin. (H) Survival of pigs after treatment. $n = 5$. * $P < 0.05$, ** $P < 0.01$. Error bars indicate SEM.

only occurred upward, it could potentially limit the use of particles to very specific clinical scenarios where bleeding is in the direction of gravity. To test whether propelled thrombin could be efficacious in a wide variety of wound geometries, including wounds with an unfavorable orientation relative to gravity where transport by convection and lateral propulsion would play a role, we used a second murine model and a porcine model. In the second murine model of hemorrhage, particles were applied to punctured livers. Mice were laid supine, incisions were made to the median lobe of each liver, and bleeding occurred opposite the direction of gravity (Fig. 4B). Wounds received

propelled thrombin, a clinically used solution of recombinant thrombin, propelled particles without thrombin, or no treatment. Propelled thrombin significantly decreased blood loss compared to the other groups (Fig. 4C).

In a separate cohort of mice, livers were analyzed histologically after fluorescent nanoparticles had been incorporated into CaCO₃. Because of the substantial sample variability in blood loss and tissue damage in tail wounds, accumulation of particles was rigorously quantified using this liver puncture model of bleeding (28). Ten times more particles were localized in the liver wound with propelled thrombin than with

nonpropelled thrombin (Fig. 4, D to F). Enhanced transport and delivery downward into the wounds occurred because the reaction of ~100,000 particles and the resulting local convection rapidly distributed them throughout the blood and wound.

To test whether self-propelling particles could prevent death from catastrophic bleeding, we used a porcine model of traumatic femoral artery hemorrhage (29). The femoral arteries of pigs were surgically exposed, and punch holes 5 mm in diameter were inflicted to induce rapid high-pressure arterial bleeding (Fig. 4G). Without hemostatic intervention at the bleeding site, pigs quickly died of hemorrhagic shock ($n = 0$ of 5; 0% survival at 3 hours). Alternatively, when a gauze containing propelled thrombin was packed above the bleeding artery, there was 100% (5 of 5) survival, whereas only 40% (2 of 5) of pigs survived to 3 hours when they were treated with a gauze containing nonpropelled thrombin (Fig. 4H and fig. S12). The propelled and non-propelled thrombin gauzes were identical formulations, except that the propelled sample contained TXA-NH₃⁺, whereas the nonpropelled sample contained TXA-NH₂ and did not produce CO₂. No external pressure was applied after packing, and CO₂ freely escaped the wounds.

CONCLUSION

We have developed a simple self-fueled particle system for delivering cargo through flowing aqueous solutions. This system is functional; the propelled particles delivered a coagulation enzyme and halted bleeding in three animal models of severe hemorrhage. The efficacy seen in these models demonstrates that gas generation can effectively transport particles throughout blood in diverse scenarios. This material may be particularly useful in treating external or intraoperative bleeding that originates internally, such as in the uterus, sinus, gastrointestinal tract, or abdomen, where traditional topical agents are less effective. In this work, we focused on delivering coagulants because bleeding is an important health problem, with trauma being the leading cause of death in young people worldwide and with postpartum hemorrhage being one of the leading causes of death in mothers during childbirth (30, 31). This system may have far-reaching applications for the delivery of therapeutics other than coagulants to sites of injury and hemorrhage. CaCO₃ adsorbs biomolecules nonspecifically; therefore, a wide range of therapeutics can be loaded and propelled. CaCO₃ particles are also scalable to submicrometer diameters and larger quantities (32). The by-products of the reaction, including CO₂, are inert and soluble in blood. Initial applications in drug delivery may include locally distributing therapeutics in complex vascular geometries when injected via drug-eluting intravascular catheters or transporting therapeutics through blood and into exposed tissue during surgery, such as tumor resection. Numerous medical applications have been suggested for self-propelling particles, and the findings from this study provide evidence that these applications may be achieved.

MATERIALS AND METHODS

Additional methods for the supplementary data can be found in the Supplementary Materials.

Preparing propulsion reagents

To generate porous CaCO₃ microparticles, a solution of Na₂CO₃ (0.33 M in 50 ml of water) was quickly added to a rapidly stirring solution of

CaCl₂ (0.33 M in 50 ml of water) (16). Precipitated CaCO₃ microparticles were collected by centrifugation at 3000g for 10 min and washed with deionized water. To make fluorescent microparticles loaded with FITC-dextran or dark-red fluorescent (660/680) polystyrene nanoparticles (200 nm), the fluorescent agent was added to the CaCl₂ solution before precipitation at 50 μM for FITC-dextran (4 kDa) or at 0.2 mg/ml for nanoparticles. To generate TXA-NH₃⁺, concentrated HCl was added to 0.5 M TXA-NH₂ until the pH reached 4.3, and then the solid TXA-NH₃⁺ was collected after lyophilization. To adsorb thrombin onto the particles, the particles were suspended at 10% (w/v) in a solution of bovine thrombin (447 μM) buffered with 10 mM Hepes. The suspension was incubated at 4°C for 1 hour. The particles were purified by centrifugation at 10,000g for 5 min and lyophilized. To obtain mixtures capable of propelling, the CaCO₃ particles were then added to TXA-NH₃⁺ at an equal molar ratio.

Measuring the velocities of CaCO₃ particulates and porous CaCO₃ microparticles

We tested the velocities of both porous CaCO₃ microparticles and CaCO₃ particulates as obtained from the manufacturer. Particle velocities were measured after injection into 1 M citric acid at 16 mm below the surface. Particles were imaged at time intervals of 35 ms. Particulates and porous microparticles were separately mixed with TXA-NH₃⁺ (1:1 molar ratio), yielding mixtures that propelled when injected into solutions with neutral pH. Propelling mixture was injected similarly into phosphate-buffered saline containing 50 mM sodium citrate (PBS-citrate), heparinized and citrated whole blood, or a solution of washed and concentrated red blood cells in PBS-citrate. Citrate was used to prevent blood clotting upon addition of Ca²⁺ and to prevent precipitation of calcium phosphate. The surface of the blood or buffer was imaged, and the time at which the particles were observed at the surface was recorded to calculate the average upward velocity of the mixture. The steel hull was made of a 2-mm piece of an 18-gauge steel needle that was closed at one end. About 1 mg of the CaCO₃/TXA-NH₃⁺ mixture was loaded into the hull and submerged in an aqueous solution containing 1.5 M citric acid, 33% glycerol (v/v), and bovine serum albumin (16.4 mM).

Measuring the propulsion of CaCO₃ microparticles against flow using microfluidics

An *in vitro* microfluidic system was used to assess the particles' ability to propel through flowing water. Water containing 0.1% Tween-20 was flowed, using a syringe pump, at velocities between 0.06 and 5.9 mm/s. The solution was fed through a microfluidic device made of polydimethylsiloxane (PDMS), which contained a "Y-shaped" junction. At the ends of the junction, polytetrafluoroethylene tubing connected the device to glass capillaries (10 cm long, internal diameter of 0.8 mm). The propelled particle mixture was applied at the end of one of the capillaries, and the transit and accumulation of particles and bubbles were imaged over the length of the capillary. The cross-sectional area of particles and bubbles was recorded for 30 s in the region 4 to 7 cm upstream of the site of particle application (Fig. 2E).

To determine the ability of particles to propel against flowing whole blood, citrated whole blood was flowed at velocities between 0 and 1.8 mm/s through a PDMS microfluidic channel positioned at 0°, 40°, and 90°. At 90°, the channel was parallel to the direction of gravity. Blood was flowed downward while the movement of particles upstream was measured. Particles were injected into the middle of the channel via

a catheter, and the movement of particles and bubbles was imaged by optical microscopy. In experiments testing propulsion in horizontal devices, steps were taken to minimize any error in leveling. The microscope stage was leveled using a spirit level. The microfluidic devices were flat because the silicon wafer templates were also flat. The glass capillaries used in the clotting experiments were flat. To further minimize systematic errors in leveling and unintended irregularities in device construction, the devices were rotated by 180° in a plane normal to gravity between measurements. Velocities and displacements of particles were quantified in both directions, and these measurements were averaged. The maximum distance that particles traveled against flow and the fraction of particles that traveled against flow were measured. The microfluidic channel extended 6 mm past the injection site; thus, 6 mm was the maximum distance traveled by particles in this experiment.

Measuring flow and occlusion times in an in vitro bleeding model using microfluidics

Citrated human blood plasma was recalcified by adding calcium-rich saline (40 mM CaCl₂ and 90 mM NaCl) to plasma (1:3 volumetric ratio). Recalcified blood plasma was flowed through glass capillaries (10 cm long, internal diameter of 0.8 mm) coated with poly-L-lysine (PLL), and the propelling particles (20 mg) were applied to the end of one of the capillaries. The capillaries were coated with 0.01% PLL for 1 hour and dried for 1 hour at 60°C; PLL enhanced the adhesion of the clot to the capillary and increased background occlusion times. Plasma was held in plastic syringe reservoirs and flowed into the capillaries via polyethylene tubing. Particles (20 mg) containing combinations of CaCO₃, thrombin, and TXA-NH₃⁺ were applied while plasma was flowing through. A microfluidic system loaded with oil was used upstream of the syringes of plasma to control flow rates through the capillaries and to detect occlusion of the capillaries with clotted blood plasma. The oil contained 10% PFO (1H,1H,2H,2H-perfluoro-1-octanol), which was used as surfactant. The movement of tracer particles was monitored with optical microscopy to determine when occlusion and clotting occurred. Times of clot initiation were compared between groups using Mann-Whitney *U* test.

Analyzing bleeding times in a mouse model of amputation and hemorrhage

All procedures involving animals were approved by the University of British Columbia Animal Care Committee and performed in accordance with the guidelines established by the Canadian Council on Animal Care. BALB/c mice weighing 20 to 25 g were anesthetized via isoflurane inhalation. Tails were transected 8 mm from the tip and then subjected to either no treatment or treatment with either nonpropelled thrombin or propelled thrombin particles for 30 s (thrombin $\sim 1.8 \times 10^{-5}$ mg/g, CaCO₃ 0.5 mg/g, and tranexamic acid 0.5 mg/g; $\sim 1,000,000$ particles). Bleeding was recorded over a 10-min observation period while the tails were immersed in citrated saline. Because some mice did not stop bleeding during the 10-min observation, total time clotted was plotted for each treatment group (fig. S10). For example, each mouse that did not stop bleeding had a total time clotted of zero. To determine the statistical significance of bleeding time, total time clotted was compared using Mann-Whitney *U* test.

Quantifying blood loss in a mouse model of liver puncture and hemorrhage

Livers were accessed via a transverse incision about 3 cm in length. Two lacerations, each 2 mm long and 2 mm deep, were made on each liver

using a 2-mm ophthalmic knife. Blood loss was quantified from each laceration independently. Blood was collected on preweighed filter papers immediately after injury until bleeding stopped. Filter papers (~ 2 cm by 2 cm) were arranged to line the site of puncture before incision. Each laceration bled for 30 s before either the CaCO₃ mixture (2 to 3 mg) or a freshly reconstituted recombinant thrombin solution (20 μ l) was applied (thrombin $\sim 1.8 \times 10^{-6}$ mg/g, CaCO₃ 0.05 mg/g, and tranexamic acid 0.05 mg/g; $\sim 100,000$ particles). The particles (in powder form) were applied to this liver model of bleeding, whereas no pressure was applied. The particles freely moved through blood in any direction. Blood losses were compared by Mann-Whitney *U* test. To confirm that changes in filter paper mass correlated with the volumes of blood soaked, known volumes of fresh blood were soaked onto preweighed filter papers (fig. S13).

To measure the delivery of propelled CaCO₃ into the sites of liver injury, the livers of a separate cohort of mice were accessed and similarly injured. Immediately after injury, 2 to 3 mg of propelled or non-propelled CaCO₃ microparticles ($\sim 100,000$ particles) containing dark-red fluorescent nanoparticles and thrombin were applied. Once bleeding stopped, the livers were collected. Histological sections were viewed with an epifluorescence microscope, and the amount of fluorescent nanoparticles was quantified using ImageJ software. Fluorescent intensities were compared to a standard containing a known mass of the particles to calculate the mass of CaCO₃ delivered to each wound.

Porcine model of lethal traumatic hemorrhage

To prepare a gauze loaded with CaCO₃ and adsorbed thrombin, 8 g of CaCO₃ microparticles was suspended in 8 ml of glycine-buffered saline (GBS) (40 mM glycine and 171 mM NaCl, pH 7.2) containing human thrombin (0.06 mg/ml; specific activity ~ 4000 U/mg) and incubated on ice for 20 min. The suspension was diluted with an additional 8 ml of GBS, poured onto 3-g strips of Kerlix gauze, and lyophilized. To prepare a propelled or nonpropelled thrombin gauze, these dressings were combined with 3-g strips of Kerlix gauze containing either TXA-NH₃⁺ (4.7 g) or TXA-NH₂ (4.7 g), respectively (CaCO₃ ~ 267 mg/kg, tranexamic acid 157 mg/kg, and human thrombin 1.67×10^{-2} mg/kg). The doses of CaCO₃ and tranexamic acid reflected the maximum amount of material that could be loaded onto the gauze. The dose of thrombin was similar to the therapeutic doses of commercially available thrombin products. Gauzes were trimmed to standard length and width using a gauze template, which was previously found to tightly pack the bleeding wound cavity.

A modified porcine bleeding model developed by the U.S. military to test topical hemostatic agents was used in these experiments (26). After induction of anesthesia with inhaled isoflurane, the left femoral artery and vein were cannulated for arterial blood pressure monitoring and administration of resuscitation fluids (fig. S14). The injury site was prepped by a 4-cm skin incision on the right hindlimb to access the femoral artery, which remained exposed while the adductor muscles were kept intact. The exposed artery was bathed in 2% lidocaine to dilate and prevent vasospasm after injury. The artery was clamped proximally and distally, and a 5-mm biopsy punch was used to create an arteriotomy on the anterior wall of the artery. The clamps were removed to allow for 30 s of free bleeding. Bleeding wounds were packed with the selected gauze to tightly fill the wound cavity. Compression and repacking of wounds were not performed. At 3.5 min after the onset of hemorrhage, all animals received one bolus of hydroxyethyl starch solution (15 ml/kg, Hextend; Hospira Inc.) infused

over 15 min. Lactated Ringer electrolyte solution (Hospira Inc.) was infused as needed (3 ml/kg/min up to a maximum of 100 ml/kg/min) to achieve or maintain a mean arterial pressure (MAP) of ≥ 60 mmHg. Animals were observed for 3 hours, and blood was collected using pre-weighed gauze. Blood loss and MAP were measured serially. Animals were euthanized under anesthesia if they survived to 3 hours or if the arterial pressure waveform was lost, indicating loss of cardiac activity.

SUPPLEMENTARY MATERIALS

Supplementary material for this article is available at <http://advances.sciencemag.org/cgi/content/full/1/9/e1500379/DC1>

Materials and Methods

- Fig. S1. Velocities of CaCO₃ particulates and porous microparticles.
 Fig. S2. Imaging CaCO₃ particulates in acidic solution.
 Fig. S3. Large carbonate particles propel horizontally but not upward.
 Fig. S4. Histological analysis of mouse tails treated with propelling CaCO₃ microparticles.
 Fig. S5. Mice remain healthy after intravenous injection of particles.
 Fig. S6. Bubbles traveling upstream carry CaCO₃ microparticles.
 Fig. S7. Measuring the maximum distance traveled by propelled particles through flowing whole blood.
 Fig. S8. Thrombin can be immobilized on CaCO₃ particles and clot stagnant plasma.
 Fig. S9. Full apparatus used to detect occlusion of flowing blood plasma.
 Fig. S10. Alternative representations of data in Fig. 4.
 Fig. S11. Histological sections of two treated tails at different distances from the site of amputation.
 Fig. S12. Inguinal crease on a pig after treatment with propelled thrombin gauze.
 Fig. S13. Quantification of blood loss after mouse liver puncture.
 Fig. S14. Blood loss and MAP in a porcine model of lethal femoral artery hemorrhage.
 Movie S1. Transport of CaCO₃ particulates in 1 M citric acid.

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Acknowledgments: We thank C. Haynes, L. Ho, E. García, S. Novakowski, the UBC Animal Care Services, and the UBC Animal Resource Unit for helpful suggestions, as well as the UBC Bioimaging facility and Wax-it Histology Services for their help in imaging and preparing samples. **Funding:** This work was funded by the Canadian Institutes of Health Research (grants MOP-119426 and MSH-130166), Grand Challenges Canada (grant 0098-01), Natural Science and Engineering Research Council (grant 418652-2012), and Canadian Foundation for Innovation (grant 31928). N.J.W. was supported in part by the National Center for Advancing Translational Sciences (NCATS) (grant KL2 TR000421), a component of the NIH. The views expressed in this article are those of the authors and do not necessarily represent the official views of the NCATS or the NIH. **Author contributions:** J.R.B., C.J.K., J.H.Y., M.H.T., A.K., A.L., L.S.M., T.F.B., and N.J.W. conceived the hypotheses, methods, and applications; J.R.B., J.H.Y., M.H.T., A.K., X.W., A.E.S., E.B.L., D.C., A.L., and J.Q.Z. performed the experiments; J.R.B., C.J.K., J.H.Y., M.H.T., A.K., A.L., and J.M.P. analyzed the data; J.R.B., C.J.K., and J.H.Y. wrote the manuscript; and all authors discussed results and commented on the manuscript. **Competing interests:** A patent application for the work reported in this article has been filed. **Data and materials availability:** Data will be made available upon request by emailing ckastrup@msl.ubc.ca.

Submitted 16 April 2015

Accepted 24 June 2015

Published 2 October 2015

10.1126/sciadv.1500379

Citation: J. R. Baylis, J. H. Yeon, M. H. Thomson, A. Kazerooni, X. Wang, A. E. St. John, E. B. Lim, D. Chien, A. Lee, J. Q. Zhang, J. M. Piret, L. S. Machan, T. F. Burke, N. J. White, C. J. Kastrup, Self-propelled particles that transport cargo through flowing blood and halt hemorrhage. *Sci. Adv.* **1**, e1500379 (2015).