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Spurious cross-frequency amplitude-amplitude coupling in nonstationary, nonlinear signals

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Abstract

Recent studies of brain activities show that cross-frequency coupling (CFC) play an important role in memory and learning. Many measures have been proposed to investigate the CFC phenomenon, including the correlation between the amplitude envelopes of two brain waves at different frequencies — cross-frequency amplitude-amplitude coupling (AAC). In this short communication, we describe how nonstationary, nonlinear oscillatory signals may produce spurious cross-frequency AAC. Utilizing the empirical mode decomposition, we also propose a new method for assessment of AAC that can potentially reduce the effects of nonlinearity and nonstationarity and, thus, help to avoid the detection of artificial AACs. We compare the performances of this new method and the traditional Fourier-based AAC method. We also discuss the strategies to identify potential spurious AACs.

Keywords

cross-frequency coupling; amplitude-amplitude coupling; empirical mode decomposition; phase-amplitude coupling; modulation index

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1. Introduction

Various physical and physiological systems generate seemingly irregular outputs such as heart rate, motor activity, and brain activity that display complex oscillations/fluctuations over a range of frequencies [1-2]. These fluctuations are not simply caused by random external influences but possess intrinsic dynamic patterns that are of relevance to health [3-8]. Many recent studies have revealed cross-frequency coupling (CFC) in these complex fluctuations in which interactions occur between rhythms at different frequencies either within the same signals or in different signals [9]. CFC is of particular interest in the studies of brain activities because they are indicative of information propagation across different brain regions for specific neurophysiological functions [10-14]. There are three types of CFCs: phase synchronization (phase-phase CFC), phase-amplitude coupling (PAC), and amplitude-amplitude coupling (AAC). Most CFC studies have been mainly focused on the development and application of phase/frequency synchronization [15-18] and PAC [19-21]. However, few studies were conducted to validate/test the analytical tools for assessment of AAC despite the evidence for the physiological importance of AAC [22].

In this brief communication, we show that signals with nonstationary, nonlinear oscillations can lead to spurious AAC. The difficulties in identifying AAC while avoiding artifacts lie within the two required steps in assessing AAC: (1) extracting oscillatory components with varying amplitude, and (2) quantifying the coupling between the amplitudes of a pair of oscillatory components. To illustrate the difficulties, we test a previously used AAC method that is based on spectral analysis or Fourier transform [22]. In addition, we propose a new analytical tool for the assessment of AAC that is based on the empirical mode decomposition (EMD) — a decomposition that can better extract nonlinear and nonstationary oscillatory components from noisy signals [23-30]. We examine and compare the performances of the two methods using synthetic signals without AAC that are nonstationary and nonlinear as often observed in EEG recordings. The goal of this study is to illustrate certain pitfalls in AAC measures and to provide certain simulation results that can guide for appropriate result interpretation in AAC studies of real physiological data.

2. Methods

2.1. Assessment of AAC

2.1.1. Spectral cross-frequency comodulation analysis (SCFCA)—To assess AAC in local field potentials, the SCFCA was previously proposed and used to calculate the correlations [31] between the spectral power time series for all pairs of frequencies [22]. Briefly, for a signal, the method involves two steps (Diag. 1A): (1) multitaper spectral analysis is performed to obtain spectrum in sliding windows (window size = 3s; step size = 0.1s; taper number = 9) and to construct time \times frequency spectrograms (frequency resolution = 2Hz); and (2) cross-correlation is calculated for each pair of two power density time series at two frequencies to obtain an amplitude–amplitude power comodulogram. We note that the time and frequency resolutions of the SCFCA are determined by the selected parameters of the Fourier transform and filtering. For instance, with 3 s for the window size of each spectrum, it is not possible to identify the coupling between the amplitudes of two

oscillatory components that only occurs at frequencies much greater than $> 1/3\text{Hz}$ (Supplemental Figure 1).

2.1.2. Intrinsic mode amplitude-amplitude coupling (IMAAC)—Strong evidence indicates that, as compared to the Fourier transform, the empirical mode decomposition (EMD) can better extract nonlinear and nonstationary oscillations [32]. Thus, we introduce a new EMD-based method for the assessment of AAC. This method, namely, intrinsic mode amplitude-amplitude coupling (IMAAC), involves the following steps (Diag. 1B; Fig. 1). (1) The EMD is used to extract oscillatory components of a signal at different frequencies with each component (intrinsic mode function: IMF) representing true fluctuations in the raw data over a narrow band of frequencies. To avoid the mixed mode (i.e., specific signal may not be separated into the same IMFs every time) [33], we propose to use noised-enhance ensemble EMD (EEMD) with the noise level of 20% (where noise level 20% represents a standard deviation of 20%) and 400 realizations [34]. In addition, we use the updated version of the EMD algorithm that is proposed by Wang et al. and can be <1000 times less time consuming than the original EMD [35]. To avoid potential mode splitting (i.e., an oscillatory component is divided into different IMFs) [36], an orthogonal checking is performed and split modes are combined [32]. Briefly, each sequentially pairing IMFs are combined recursively if their inner product is larger than 0.3 (Fig. 1A-C). (2) The instantaneous amplitudes (or envelope) and frequencies of all IMFs are obtained using the Hilbert transform (Fig. 1B). (3) The interaction between the envelopes of each pair of IMFs is quantified (see details below) and used as the modulation index (MI) of the two IMFs (Fig. 1D) that will be assigned to a frequency-frequency plane at the frequency coordinates based on the cycle-by-cycle frequencies of the two IMFs. Finally, the AAC comodulogram is obtained by averaging all MIs (i.e., from all pairs of IMFs) in the frequency-frequency plan in each $2\text{Hz} \times 2\text{Hz}$ region that indicates the AAC level (Fig. 1E).

To assess the ACC interaction or MI between two IMFs (e.g., IMF 1 and IMF2 in Fig. 1B), the simple way would be to calculate the cross-correlation coefficient of their envelopes (e.g., Envelope 1 for IMF 1 and Envelope 2 for IMF 2 in Fig. 1B). However, one of the drawbacks in this approach (as well as in the SCFCA) is that the cross correlation analysis assumes stationary signals (note that IMF envelopes are not necessarily stationary) [37-41]. To address the concerns, we propose an alternative way to calculate the MI by investigating the couplings between the two envelopes at different frequencies. Specifically, the EEMD is used to decompose the envelope of the IMF at a lower frequency (e.g., Envelope 2 for IMF 2 in Fig. 1B). For each resultant envelope's IMF at a frequency lower than that of the IMF (e.g., 10 Hz for IMF 2 in Figure 1C), its phase modulation on the envelope of the other IMF (i.e., Envelope 1) is assessed to yield a phase-amplitude coupling (PAC) index (Fig. 1D). All PAC indices (e.g., for different IMFs of Envelope 2 in Fig. 1C) are then weight-averaged (i.e., weighted based on the standard deviations of the envelope's IMFs) to obtain the MI between the two IMFs.

To determine the statistical significance of each MI, we apply a shuffling procedure in which individual cycles of the two IMFs are permuted randomly [42]. The process is repeated 100 times and MI is calculated for each realization. The mean and standard deviation of the 100

MIIs of the surrogate data are used to z-score the original MI. Those measurements which did not exceed a significance level of $p = 0.05$ were eliminated.

The proposed new AAC method is implemented using Matlab and the code is available upon request (<http://in.ncu.edu.tw/mzlo/drLo.html> or <https://sleep.med.harvard.edu/research/labs/112/Medical+Biodynamics+Program+MBP>).

2.2. Synthetic signals

To test the performances of the SCFCA and IMAAC, we apply the two methods to a series of simulated nonstationary oscillatory signals with different degrees of nonlinearity. To generate nonlinear waveforms, we construct each cycle by stitching the half-cycle waveforms of two sinusoidal functions with the same amplitudes but not necessarily same periods (Fig. 2A). The degree of nonlinearity/asymmetry is determined by the ratio of the periods of the two sinusoids (p_2/p_1). We also use the sawtooth waves as an extreme case for asymmetric/nonlinear oscillations (Fig. 2B). In this study, all oscillatory cycles by default have the same frequency ($f_1 = 10$ Hz). To introduce nonstationarities, we assign a random value between 0 and 4 to the amplitude of each cycle for Type 1 signals (Fig. 3). For each synthetic signal, the sampling frequency is 600 Hz, data length is 100 s, and there is a white-noise component with the noise level of 10% (i.e., SD of the white noise is 10% of that of the oscillatory component).

3. Results

We study and compare the SCFCA and IMAAC results by applying them to nonstationary oscillatory signals without AAC. For the signals with linear oscillations (period ratio $p_1/p_2 = 1$), SCFCA results show certain artificial AACs between components at frequencies close to $f_1 = 10$ Hz (Fig. 4B). These artifacts in the SCFCA results are due to the blurred peak in the spectral densities that is induced by the nonstationary oscillation (i.e., unstable amplitude) (Fig. 4A). When the waveforms become nonlinear ($p_2/p_1 > 1$), more significant spurious AACs appear between f_1 (10Hz) and its harmonic frequencies (e.g., 20Hz, 30Hz, and 40Hz) as well as between those harmonic frequencies (Fig. 4D). These artifacts are clearly caused by the nonlinearity in the waveforms that leads to power densities at harmonic frequencies (Fig. 4C). As the degree of nonlinearity or asymmetry (characterized by p_2/p_1) increases, the power densities spread to higher harmonic frequencies, resulting in more strong artificial AACs between the harmonics over a wider range of frequencies (Fig. 4E-G). When the asymmetric waveform is sawtooth with the shape edge, spurious AACs become so strong and appear between all pairs of fundamental and harmonic frequencies (Fig. 4H).

As compared to the SCFCA, nonstationarity and nonlinearity have less impact on the IMAAC. For all simulated symmetric or asymmetric oscillations with p_2/p_1 between 1 and 9, the IMAAC avoids detection of spurious AAC because the EMD allows a reliable extraction of the 10-Hz oscillations with unstable amplitude (Fig. 5A-C, 5E-G). Only for sawtooth, artificial AACs appear in the IMACC results (Fig. 5H). These spurious AACs occur because the sharp edges in the sawtooth waveforms induce artificial oscillations in all high-frequency components (higher than f_1) at the same time locations (Fig. 5D).

4. Discussions

In this short communication we demonstrate that nonlinear oscillations with nonstationary amplitude may produce spurious cross-frequency amplitude-amplitude coupling. By applying a previously proposed AAC measure (i.e., derived from the SCFCA based on the correlations between spectral powers) to a series of nonlinear oscillatory signals at a fixed frequency (i.e., frequency is constant), we find that nonstationarity alone can induce artificial AACs at frequencies close to the fixed frequency. Nonlinearity has more impacts on the AAC measure. Even a slight nonlinearity in the waveform can induce strong spurious AACs over a wide range of frequencies. The reason for the failure of the method is that the Fourier transform assumes sinusoidal oscillations with constant amplitudes. Even for oscillations at a fixed frequency, the spectral power will spread into a region close to the frequency. Moreover, the Fourier transform constructs a nonlinear waveform using sinusoids not only at the fundamental frequency but also at harmonic frequencies. Thus, although there are no high-frequency oscillations in the original data, the spectrum can have significant powers at high (harmonic) frequencies that are proportional to the power density at the fundamental frequency [43]. As a consequence, when the amplitude of nonlinear oscillations varies (i.e., nonstationary oscillations), spurious AACs appear. We note that the similar Fourier-related limitations can also lead to spurious phase synchronization [44,45].

To overcome the limitations of the Fourier transform, we propose the IMAAC that is based on the empirical mode decomposition (EMD). The new method has a much better performance than the Fourier-based method in terms of avoiding spurious AACs. The advantage comes from the ability of the EMD in extracting/separating oscillations from a noisy signal without losing the amplitude information. The IMAAC is also suitable for nonlinear oscillations to certain degree, e.g., no spurious AACs even when the ascending segment is nine times long of the descending segment in an asymmetric cycle.

It is important to note that the IMACC eventually fails when nonlinearity becomes too strong, i.e., as occurred to sawtooth waveforms with sharp edges [46,47]. This is expected because EMD cannot preserve spikes or shape edges in IMFs despite its tolerance to nonlinearity. A previous study has demonstrate that sharp edges also affect the detection of another type of CFC, leading to spurious PACs [48]. Currently, there is still no reliable AAC methods that can handle data with spikes or shape edges. Though the co-existence of AACs at harmonics of a certain frequency in the AAC comodulogram can be a ‘warning’ sign for spurious AACs, the most reliable approach to identify the effects of sharp edge is still checking the raw data [22]. However, it may be time consuming if sharp edges are not present in all cycles and all cycles must be visually examined one by one. Our simulations indicate that checking the EMD-derived IMFs of raw data and their instantaneous amplitudes (or envelopes) may be an easier way to identify shape edges. Specifically, sharp edges (or spikes) will lead to peaks in the amplitude envelope of the IMF at the frequency of the oscillation with the shape edges, i.e., the envelope oscillates at the same frequency (intra-wave variations); and the same sharp edges (or spikes) will generate high-amplitude oscillations at the relatively same time location in all IMFs at higher frequencies (Fig. 6A). Such intra-wave variations with simultaneous appearances of high-amplitude oscillations in

multiple IMFs are normally absent in signals with real AACs (Fig. 6B, 6D) and can be easily visualized, thus providing a great hint for spurious AACs (Fig. 6C).

The main purpose of this short communication is to demonstrate the difficulties in avoiding the detection of spurious AAC in nonstationary, nonlinear oscillatory signals. The proposed IMACC appears more resilient to effects of nonstationarity and nonlinearity as compared to the Fourier-based AAC measure. Note that our results are based on the examinations using one type of nonstationarities (i.e., random amplitude) and one type of nonlinearities (i.e., asymmetry). It is important for the follow-up studies to test and compare the new and traditional AAC measures using different types of nonstationarities such as unstable frequency and different types of nonlinearities such as logistic map and duffing oscillator. Moreover, in addition to cross-frequency coupling between certain frequencies, other types of couplings that do not depend on specific frequency oscillations may be present in physical and physiological systems [49,50]. Checking how nonlinearity and nonstationary affect different coupling measures is warranted in future studies.

Supplementary Material

Refer to Web version on PubMed Central for supplementary material.

Acknowledgments

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Highlights

1. Nonstationary oscillations can induce spurious amplitude-amplitude coupling (AAC).
2. Nonlinear waveform can induce spurious AAC.
3. The EMD-based AAC method performs better than the Fourier-based AAC method.

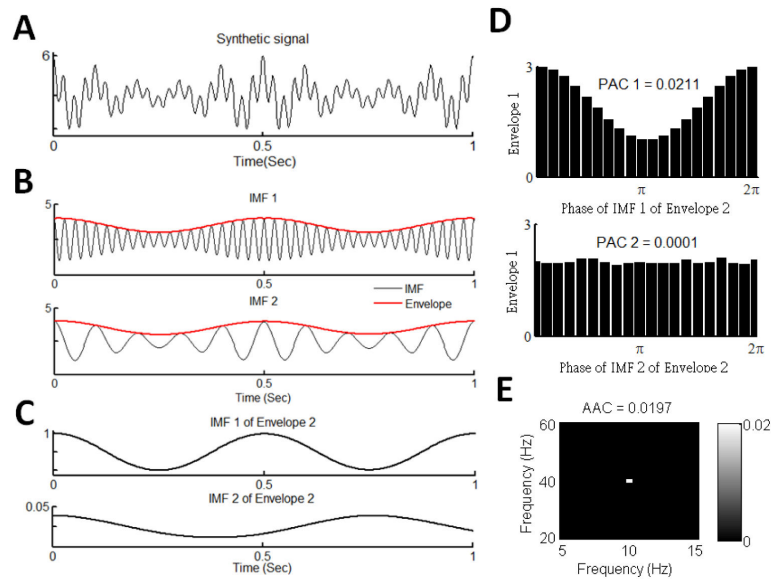


Fig. 1. Demonstration of the intrinsic mode amplitude-amplitude coupling (IMAAC) analysis. (A) A synthetic signal with 10-Hz and 40-Hz oscillations whose amplitudes are simultaneously modulated by a 2-Hz sinusoidal wave. (B) Two intrinsic mode functions (IMFs) of the signal in A and their instantaneous amplitudes (envelopes). IMFs are obtained using EEMD. IMF1 and IMF2 are the 40-Hz and 10-Hz oscillatory components in the raw data, respectively. The envelope of each IMF is obtained using the Hilbert transform, i.e., Envelope 1 for IMF 1 and Envelope 2 for IMF 2. (C) Two IMFs of Envelope 2 in B. The first IMF corresponds to the 2-Hz oscillation. (D) The phase-amplitude distribution (PA distribution) between the first IMF (2Hz) and second IMF of Envelope 2 (phase) and Envelope 1 (amplitude). (E) The modulation indices (MIs) is calculated based on the PA distributions in D, and the MI between the IMF 1 and IMF 2 is weight-averaged according to the standard deviations (SD) of Envelope 2's IMFs (see C). The MI will be assigned to a frequency-frequency plane at the coordinate 10 Hz x 40 Hz because the frequencies of IMF 1 and IMF 2 in all cycles are 40 Hz and 10 Hz, respectively.

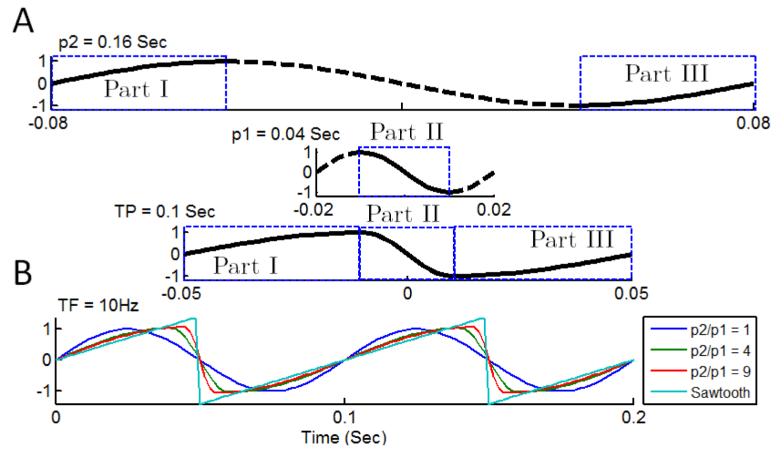


Fig.2.

Construction of nonlinear waveforms with different degrees of asymmetry. (A) An example of asymmetric wave (target period (TP) = 0.1 sec) is created using two sinusoidal waves. We use Part I (from $[-\pi/2, 0]$) and Part II (from $[-\pi, -\pi/2]$) for the one with period 2 (p_2) = 0.16 sec, and Part II in the other one with period 1 (p_1) = 0.04 sec. (B) We fix TP as 0.1 sec (or target frequency (TF) = 10 Hz) and change the period ratio (p_2/p_1) to control the degree of asymmetry. The sawtooth wave is the extreme case of asymmetric wave.

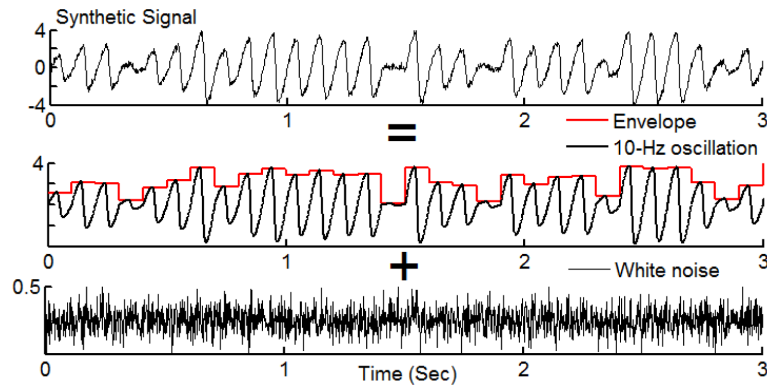


Fig.3.

A synthetic signal with nonstationary, nonlinear oscillations. Nonlinear waveforms are created based on the prototype in Fig. 2 with $p_2/p_1 = 4$. The amplitude of each cycle is a random number in the range of 0-4. The frequency of all cycles is 10 Hz. The synthetic signal also has a component of Gaussian white noise with the standard deviation equal to 10% of the oscillatory component.

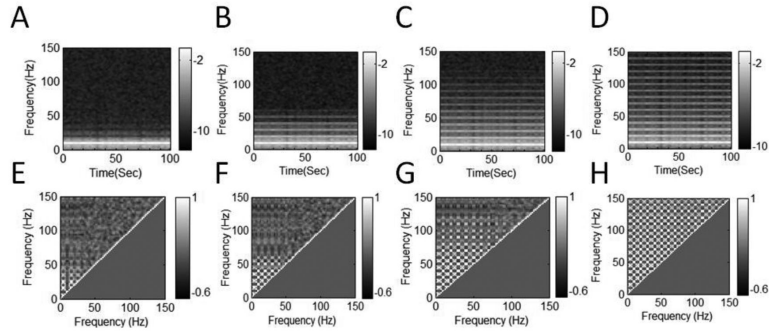


Fig.4.

SCFCA results of synthetic signals with asymmetric 10-Hz oscillation and nonstationary envelope. (A-D) Multitaper power spectra (PS) and (E-H) AAC comodulograms (AACCs) for signals with different degrees of asymmetry: (A, E) $p_2/p_1 = 1$, (B, F) $p_2/p_1 = 4$, (C, G) $p_2/p_1 = 9$, and (D, H) sawtooth. AACCs are obtained from cross-frequency correlation of PS in (A-D). For all signals, the nonstationary envelope is the same as shown in Fig. 3. The nonlinearity associated with the asymmetrical waveform leads to powers at harmonics, the nonstationarity causes the smearing of power densities at the fundamental and harmonic frequencies.

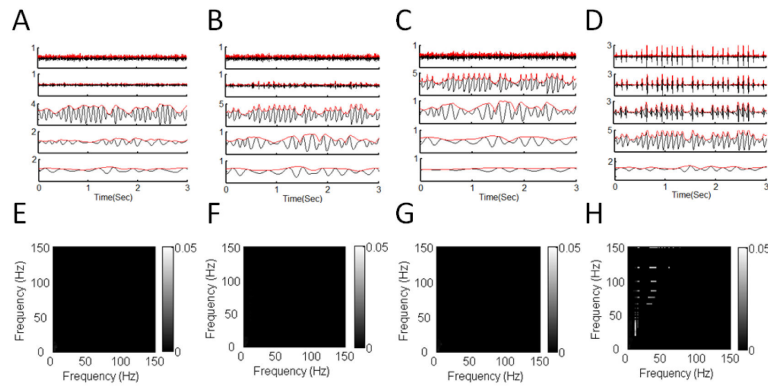


Fig.5. IMACC results of the synthetic signals with asymmetric oscillation and nonstationary envelope. (A-D) IMFs (black lines) and their instantaneous amplitudes or envelopes (red lines), and (E-H) AACC of the same signals used in Fig. 4. (A, E) $p_2/p_1 = 1$, (B, F) $p_2/p_1 = 4$, (C, G) $p_2/p_1 = 9$, and (D, H) sawtooth.

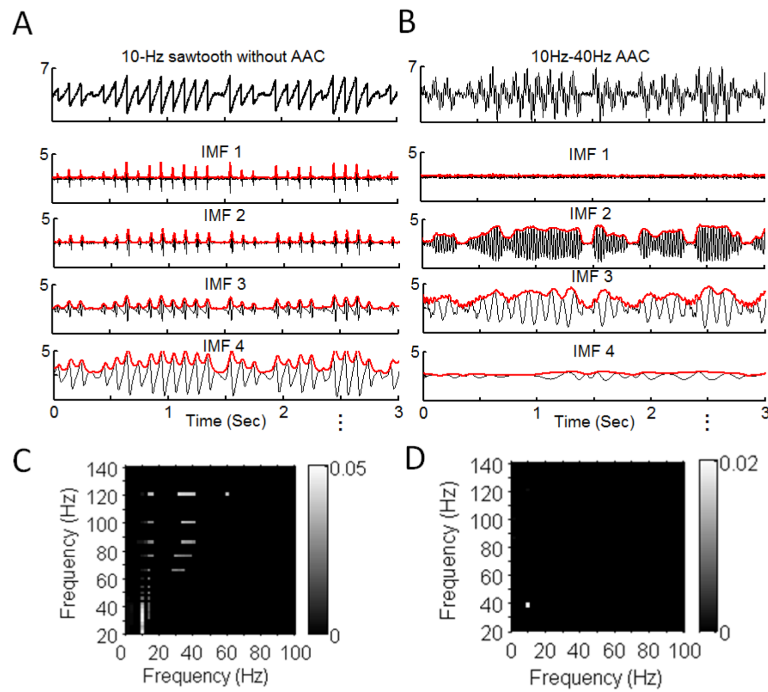
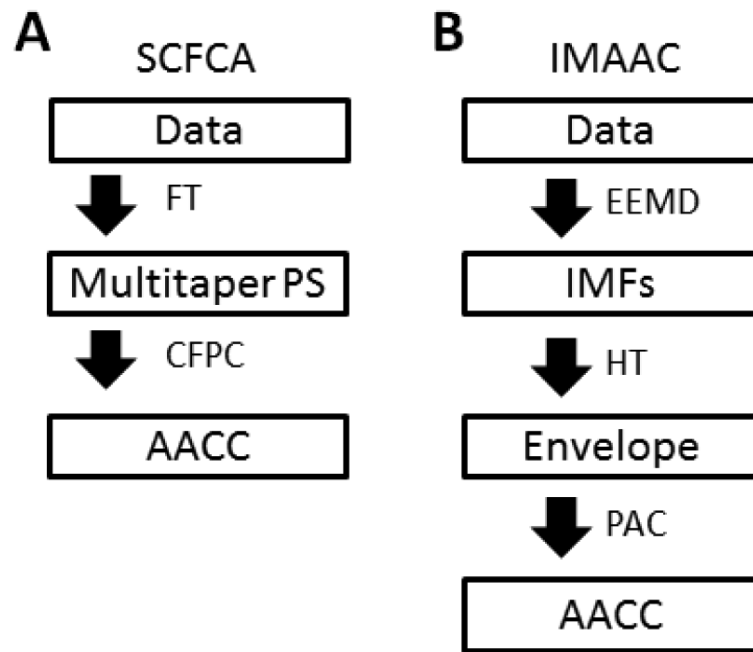


Fig.6. Comparison of IMAAC results for signals with spurious and true AACs. (A, B) IMFs and (C, D) AACC of (A) a sawtooth wave (10 Hz) without AAC and (B) a synthetic signal with AAC between two sinusoids (10 Hz and 40 Hz). In both signals, the amplitudes of oscillations are modulated by the same arbitrary nonstationary amplitude.

**Diag. 1.**

The procedures of the two methods for the assessment of cross-frequency amplitude-amplitude coupling. (A) The spectral cross-frequency comodulation analysis (SCFCA). (B) The intrinsic mode amplitude-amplitude coupling (IMAAC). FT: Fourier transform; PS: power spectrum; CFPC: cross-frequency power correlation; AACC: amplitude-amplitude coupling comodulogram; EEMD: ensemble empirical mode decomposition method; IMF: intrinsic mode function; HT: Hilbert transform; PAC: phase-amplitude coupling;