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Design and test of a double-nuclear RF coil for ^1H MRI and ^{13}C MRSI at 7T

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Abstract

RF coil operation at the ultrahigh field of 7T is fraught with technical challenges that limit the advancement of novel human *in vivo* applications at 7T. In this work, a hybrid technique combining a microstrip transmission line and a lumped-element L-C loop coil to form a double-nuclear RF coil for proton magnetic resonance imaging and carbon magnetic resonance spectroscopy at 7T was proposed and investigated. Network analysis revealed a high Q-factor and excellent decoupling between the coils. Proton images and localized carbon spectra were acquired with high sensitivity. The successful testing of this novel double-nuclear coil demonstrates the feasibility of this hybrid design for double-nuclear MR imaging and spectroscopy studies at the ultrahigh field of 7T.

Keywords

7 Tesla; ultrahigh field magnetic resonance imaging (MRI); ultrahigh field magnetic resonance spectroscopy (MRS); microstrip transmission line (MTL) resonator; radio-frequency (RF) coil; surface coil; lumped-element L-C loop coil

Introduction

Double-nuclear MR imaging and spectroscopy is useful for attaining morphological and metabolic information in living systems [1-3]. Obtaining magnetic resonance data at ultrahigh magnetic field strengths, e.g., 7T, provides higher signal-to-noise (SNR) and greater spatial and spectral resolution than what can be achieved at lower field strengths [4-16]. Nuclear magnetic resonance (NMR) techniques require RF coils sensitive and efficient

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enough to acquire the minuscule signals after excitation. As magnetic field strength increases, the nuclear precession frequency, i.e. the frequency of MR signals, increases as well [17,18]. Radiation losses increase with higher resonant frequencies, as does the interaction between the coil and the sample [6,11,19,20]. In a double-tuned RF coil configuration, electromagnetic coupling between different nuclear channels may also become problematic. At high and ultrahigh magnetic fields, this coupling issue ultimately leads to diminished MR signal detection efficiency, particularly for non-proton nuclear channels [21-24].

Several design methods have been proposed to address this problem and to gain better performance in double-nuclear MR acquisitions [3,21-23,25-37]. In this work, we design and test a simple coil configuration for double nuclear ^1H imaging and ^{13}C MR spectroscopy at the ultrahigh field of 7T. The design method is based on a hybrid technique using microstrip transmission line resonators [11,20,38-42] for the ^1H channel and regular lumped-element L-C loop resonators for ^{13}C . Our design takes advantage of the fact that microstrip transmission lines (MTLs) generate magnetic fields that are perpendicular to that of a loop coil when the strip conductor and wire loop lie on the same plane. This coil layout theoretically provides intrinsic electromagnetic decoupling between the two nuclear channels. Standard RF bench test and MR imaging experiments have been performed to validate the proposed double-tuned coil design method for both the proton channel and the ^{13}C channel.

Methods

Coil Design

The double-nuclear coil system was comprised of two individual surface coils. A symmetric MTL surface coil was designed for hydrogen MRI at 7T (*Figure 1a*). Adhesive-backed copper tape was used as the strip conductor (12.5 mm \times 141 mm \times 36 μm) and the ground plate (97 mm \times 141 mm \times 36 μm) on a PTFE substrate (97 mm \times 260 mm \times 14.5 mm). The additional length of the PTFE substrate was used as a platform to secure the coaxial cable connections. Fixed and variable capacitors were used to adjust the resonant frequency of the MTL and to minimize reactance and radiative losses through impedance matching. Tuning capacitors were arranged in a symmetric configuration to maintain a symmetric field distribution along the coil. Matching capacitance was split into two capacitors allowing for electric balancing.

A single-turn, segmented, wire-loop surface coil was created for ^{13}C spectroscopy at 7T (*Figure 1b*). Round copper wire (18 AWG, 1.0 mm diameter) was shaped into a rounded-rectangular coil and recessed into the PTFE dielectric substrate by 3 mm. Tuning capacitors were placed symmetrically between the segments of the coil. The segmentation of the wire loop coil reduces the effective electrical length of the wire, providing a more homogenous RF field.

In both coils, single-loop trapping baluns were used to reduce common mode effects. Each balun was tuned to the frequency of the connected coil via a variable capacitor. *Figure 2*

shows the complete coil system with and without the protective PTFE cover sheet (0.3 mm thickness).

Bench Tests

Frequency tuning and impedance matching were performed using a network analyzer (Agilent Technologies, Model E5061A). Bench tests consisted of obtaining reflection and transmission coefficients (S_{11} and S_{21} , respectively) in the unloaded condition.

The S_{11} measurement tests the reflection of RF power sent by the analyzer to the coil, providing information of the energy absorbed by the coil (and the sample) though displaying the energy that has reflected back to the analyzer. The reflection coefficient is used as a measure of coil impedance matching in this study. The transmission coefficient S_{21} was used to measure the electromagnetic coupling between the two coils.

These measurements were then used to calculate the coil efficiency (Q-factor). In this study, Quality factor is defined as

$$Q = \frac{2f_0}{f_2 - f_1} \quad (1)$$

where f_0 is the frequency of the coil resonance, $(f_2 - f_1)$ is the 3dB bandwidth of the S_{11} spectrum.

Measurements of resonant frequency shift due to coil loading of small and light samples were obtained by tuning each coil with the phantoms placed on the top surface of the coil assembly, then subsequently removing the phantoms and observing the shift in peak resonant frequency. Any significant shifts would indicate capacitive coupling between the coil and the phantom.

Scanning Parameters

MR data were obtained using the GE 7T whole-body scanner (GE Healthcare, Model MR950). Two phantoms were imaged: a plastic syringe (30 ml) containing 23 ml of ethylene glycol and a plastic syringe (1 ml) containing 0.95 ml of urea. A 2D gradient-recalled echo (GRE) pulse sequence was used for proton imaging (TR = 8.1 ms, TE = 2.8 ms, NEX = 3, $\alpha = 30^\circ$, spatial resolution = 0.31 mm \times 0.31 mm \times 3 mm, matrix size = 256 \times 256).

Ethylene glycol spectroscopic data were acquired using a 2D free-induction decay chemical shift imaging (FID-CSI) pulse sequence (TR = 1000 ms, TE = 2.86 ms, NEX = 8, $\alpha = 90^\circ$, reference chemical shift = 63.4 ppm, sweep width = 5 kHz, time points = 2048, dwell time = 0.2 ms, spatial resolution = 4 mm \times 4 mm \times 30 mm, matrix size = 8 \times 8).

Urea spectroscopic data were acquired using a 2-D FID-CSI pulse sequence (TR = 1000 ms, TE = 3.27 ms, NEX = 8, $\alpha = 90^\circ$, reference chemical shift = 174.3 ppm, sweep width = 5 kHz, time points = 2048, dwell time = 0.2 ms, spatial resolution = 2 mm \times 2 mm \times 5 mm, matrix size = 8 \times 8).

Data Processing

AMIDE software [43] was used to visualize the proton DICOM data and to produce 1D sensitivity profiles across each viewing plane. Raw spectroscopic data were reconstructed through the use of the imaging program, SIVIC [44]. A 9 Hz Lorentzian apodization filter was applied to the raw spectroscopic data prior to spatial and spectral Fourier transformation. Analysis was conducted using the absolute values (magnitude only) of the spectra. The expected MRS peak for ethylene glycol sample was 63.4 ppm, while the expected peak for urea sample was 174.3 ppm.

Results

Bench Tests

The MTL coil performed well as measured by the network analyzer parameter S_{11} . *Figure 3* presents the reflection coefficient graphs for the MTL coil and the wire-loop coil in the unloaded condition. Once the MTL was tuned and properly matched, the coil showed excellent energy deposition with a loss of -52.34 dB at the resonant frequency of 298.60 MHz. The loop coil also performed well with a loss of -49.97 dB at the resonant frequency of 74.95 MHz. Coil efficiency in the unloaded condition as measured by the Q-factor was high with values above 200 for both coils. The results are summarized in *Table 1*.

Coil decoupling was measured through the S_{21} parameter. *Figure 4* displays the transmission coefficient data. Each coil showed a moderately high level of decoupling, with the MTL receiving just -25.66 dB of signal from the loop coil, and the loop coil showing only -17.80 dB of the MTL signal.

The experiment of coil frequency shift with and without small samples (30mL and 0.95mL) was performed independently of the S_{11} and S_{21} measurements above. Results are summarized in *Table 2*. The MTL experienced a slight shift from the tuned frequency of 298.45 MHz with the phantoms on the coil. Upon removal, the resonant frequency shifted $+1.10$ MHz. The wire-loop coil exhibited no noticeable frequency shift in resonant frequency between different conditions.

Proton Imaging

Images of the phantoms were acquired in the axial, coronal, and sagittal planes. Images were then used to generate a 1D sensitivity graph across the mid-line of the largest phantom, the syringe filled with 23 ml of ethylene glycol. *Figure 5* shows this phantom in all three dimensions with corresponding sensitivity graphs. To accentuate signal intensity, a color look-up table (CLUT) was applied through the AMIDE imaging program.

^{13}C Spectroscopy

Figure 6a shows an axial view of the ethylene glycol phantom with an 8×8 grid overlay while *Figure 6b* displays the grid overlay with spectra plotted inside each voxel. The ethylene glycol spectroscopic data were spatially smoothed using a sinc kernel in SIVIC to produce the MRS image shown in *Figure 6c*. These same processing steps were taken with the data from the small urea phantom. *Figure 7a* presents an axial view of the urea phantom.

Figure 7b shows the spectroscopic data for each voxel, and the corresponding interpolated spectral image is shown in *Figure 7c*.

Discussion

Overall, the double-nuclear coil system performed well by every measure. Reflection coefficients showed excellent frequency specificity as indicated by the Q-factors, while transmission coefficients revealed excellent decoupling between coils. The overall efficiency of the wire-loop coil operating at much lower frequency was higher than that of the MTL.

The load frequency shift experiment was conducted to assess the amount of coupling between the sample and the coil, also known as parasitic capacitance, due to the reduction of the resonant frequency when a sample is loaded onto the coil [24]. The MTL experienced a small but significant frequency shift of 1.10 MHz, indicating some level of sample coupling. Since the frequency bandwidth of RF pulses is typically on the order of kHz, this amount of coupling requires retuning the coil when it is loaded and connected to the scanner to prevent a large amount of energy from reflecting back to the system, causing damage. The wire-loop coil performed extremely well during this test. There was no noticeable frequency shift in the loop coil between loading conditions. This may be also due to the small and light imaging samples used for this test.

Proton images generated in each plane showed a significant drop in signal intensity as a function of distance from the conduction strip. The sensitivity of the MTL was limited to a few centimeters around the midline of the main conducting strip. Given the geometry of the MTL and the properties of electromagnetic radiation, this sensitivity profile is exactly what was expected as typical microstrip coil behavior [11,20,40]. However, as demonstrated in literature [8], the field penetration of a microstrip coil can be changed by increasing the substrate thickness of the microstrip transmission line resonator.

The carbon spectroscopic reconstructions revealed excellent sensitivity to the relatively miniscule ^{13}C signal. This was particularly evident in the larger of the two phantoms. Throughout the volume of the sample, peak amplitude corresponded directly with the amount of ethylene glycol in a given voxel. The urea spectroscopic data showed a slight shift in spatial location from the proton image. One way to improve this result would be to increase the resolution of the spectroscopic data. This would entail a substantial increase in acquisition time that was unattainable during this experiment.

Given the specific geometry and size of the prototype coil, a potential application of this coil will be the human calf muscle imaging and spectroscopy in investigating muscle fiber orientation, intramyocellular lipids, congenital myasthenic syndromes, and energy metabolism [45-51]. It can be also used for human extremity $^{13}\text{C}/^1\text{H}$ spectroscopic imaging at the ultrahigh field of 7T.

Conclusion

A simple double-nuclear RF coil using a hybrid method combining microstrip transmission line resonators and lumped-element loop resonators has been developed and investigated

for $^1\text{H}/^{13}\text{C}$ MRI and MRSI at the ultrahigh field of 7T. The prototype of the double-nuclear coil performed well in the aspects of quality factors, imaging coverage, and electromagnetic decoupling between the two nuclear channels, based on bench tests and MRI and MRSI experiments. This design was possible because of the high frequency capability of microstrip resonators and superior decoupling performance resulting from inherently perpendicular fields of the microstrip and the lumped-element loop resonator. This simple and compact double-nuclear coil shows promise for the future where it could be used as array elements in double-tuned RF coil arrays for accelerated imaging and spectroscopic imaging at 7T when appropriate decoupling techniques [52-54] are applied. This could include a planar phased array for human spinal 1H imaging and heteronuclear metabolic imaging, or a cylindrical array for human knee or head double-nuclear MR imaging.

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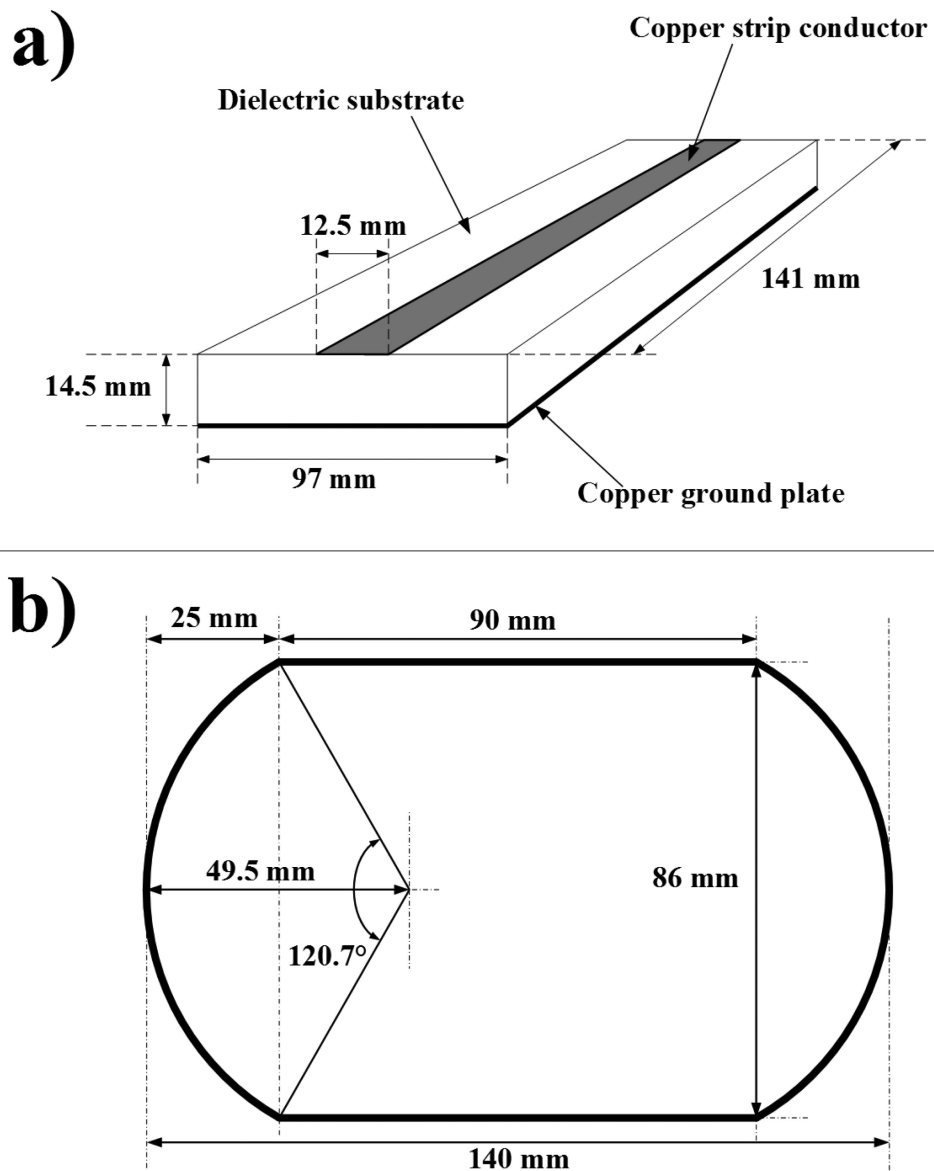


Figure 1. Diagrams of each RF resonator. a) Microstrip transmission line resonator tuned to the proton precession frequency of 298 MHz. PTFE was used as the dielectric substrate. b) Wire-loop resonator tuned to the carbon-13 precession frequency of 75 MHz. The rounded rectangular shape allowed a larger field of view with less wire than a rectangular coil.

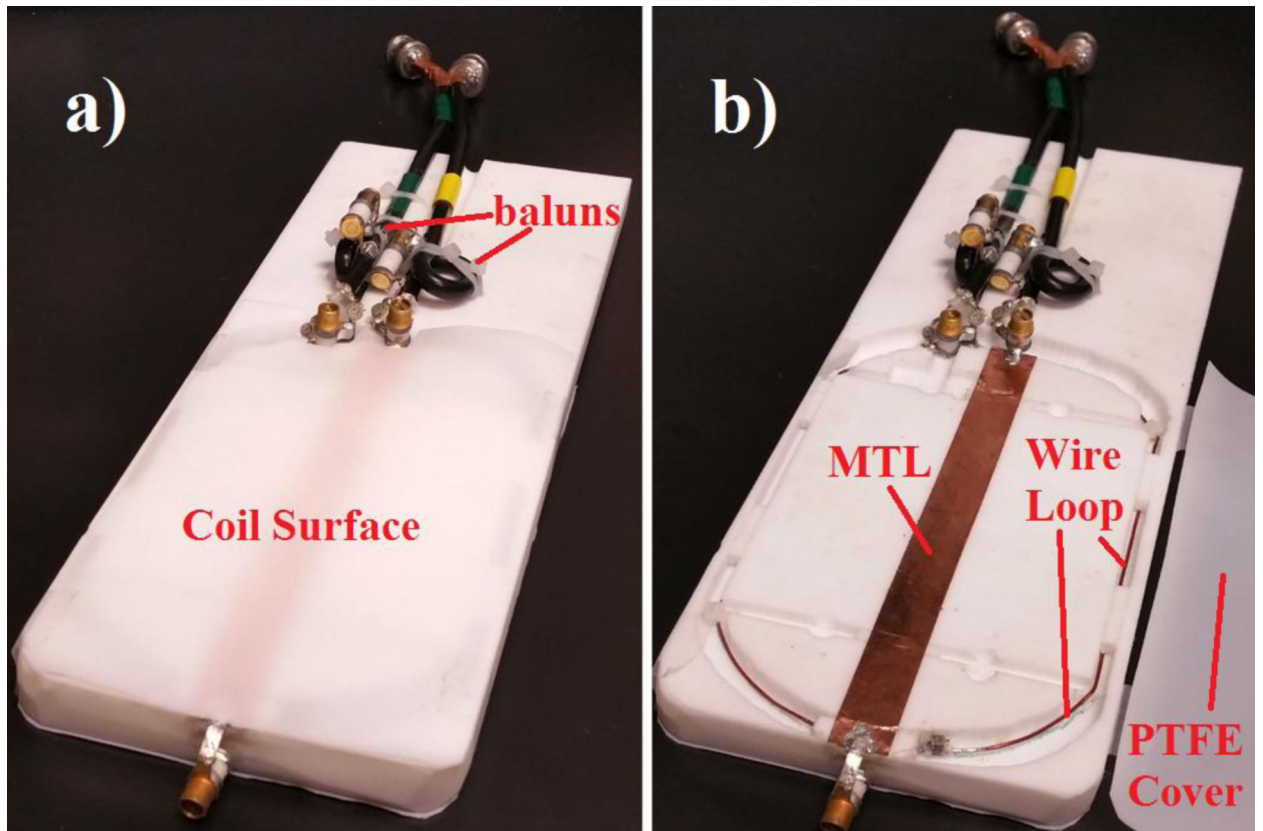


Figure 2. Images of constructed double-nuclear coil system. a) Coil system with PTFE cover sheet over the resonators. b) Coil system with the PTFE cover sheet moved aside. The wire coil is 3 mm below the plane of the strip conductor and secured with plastic zip-ties.

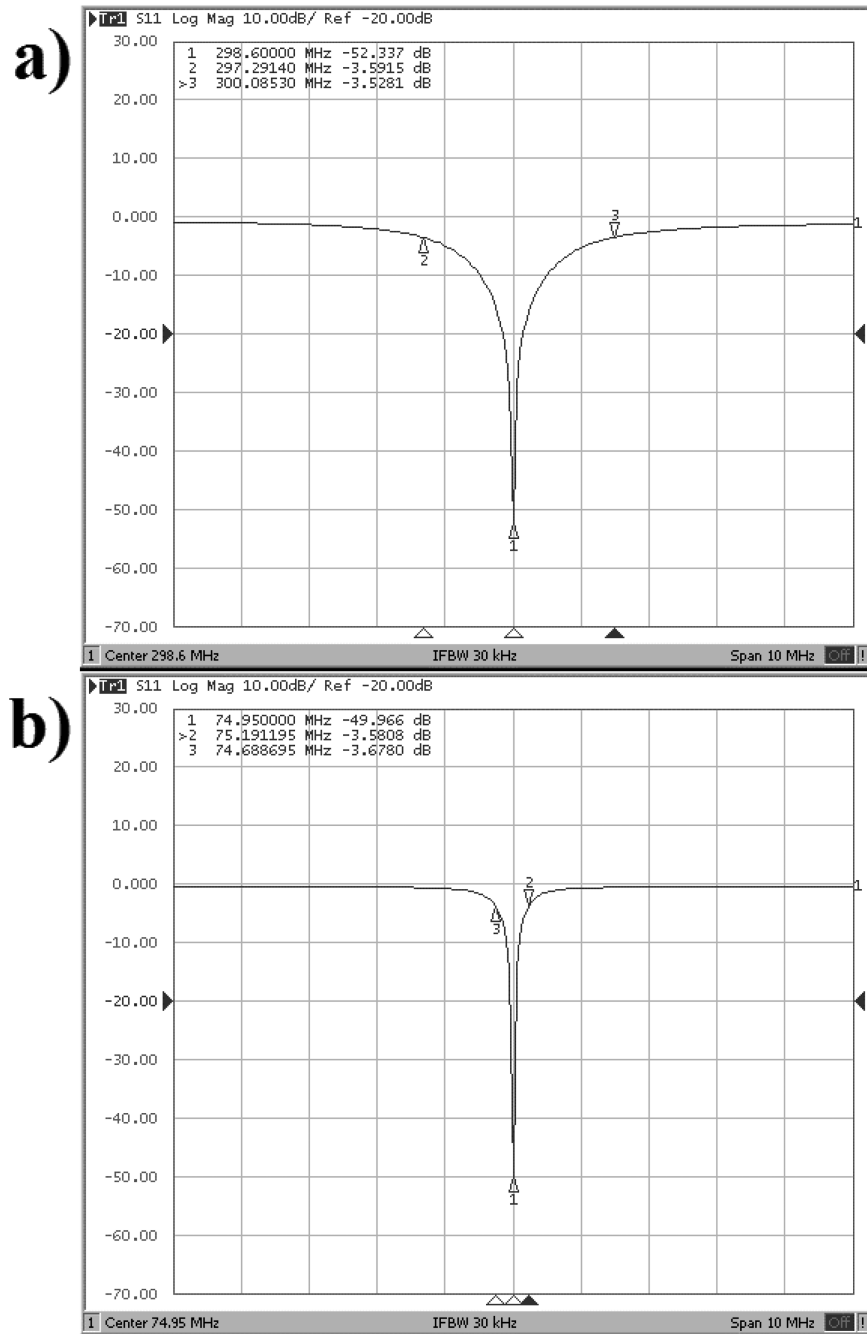


Figure 3. Reflection coefficient graphs of each coil in the coil unloaded condition. a) Results from the hydrogen microstrip coil. b) Results from the carbon wire-loop coil. The scale in both graphs along the x-axis is 1 MHz per square, and along the y-axis each box represents 10 dB per square.

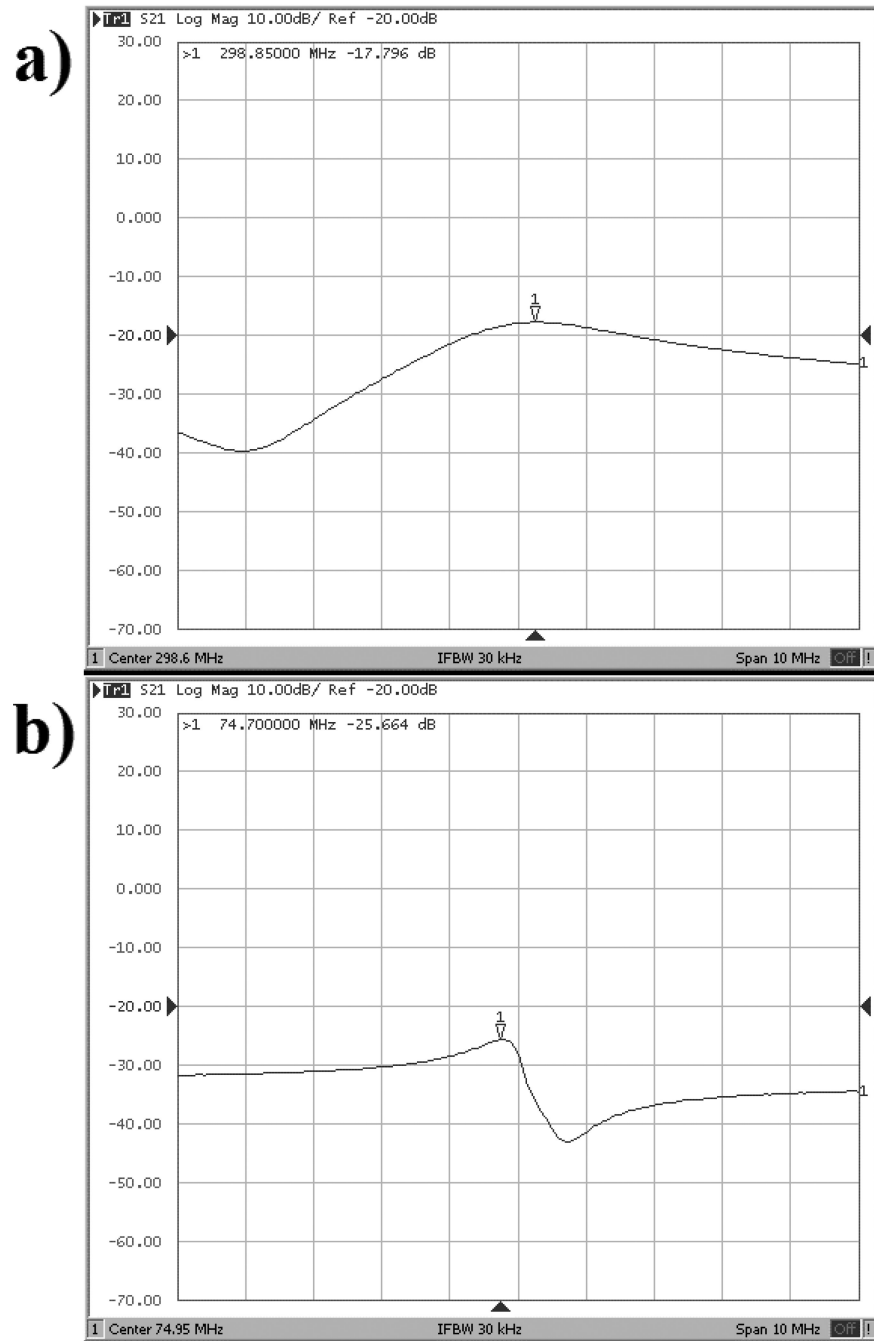


Figure 4. Transmission coefficient graphs of each coil in the coil unloaded condition. a) Results from the hydrogen microstrip coil. b) Results from the carbon wire-loop coil. The scale in both graphs along the x-axis is 1 MHz per square, and along the y-axis each box represents 10 dB per square.

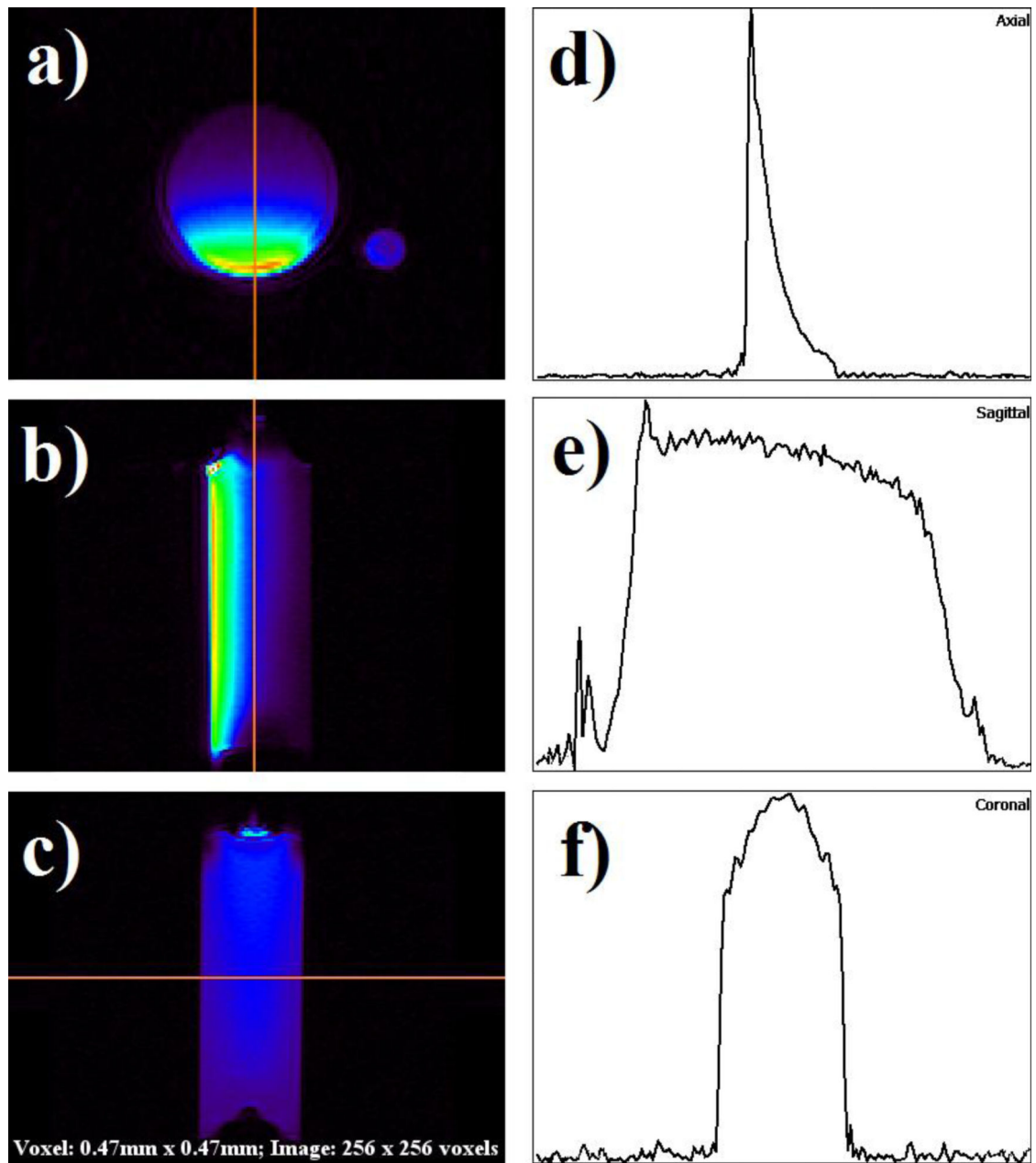


Figure 5.

Proton images and line intensity profiles in each plane. A rainbow color lookup table has been used to accentuate signal intensity. (a) Axial view. (b) Sagittal view. (c) Coronal view. (d) Intensity profile across axial view image. Left to right corresponds with bottom to top in a). (e) Intensity profile across sagittal image. Left to right corresponds with top to bottom in b). (f) Intensity profile across coronal image. The line profile is in the same direction as c).

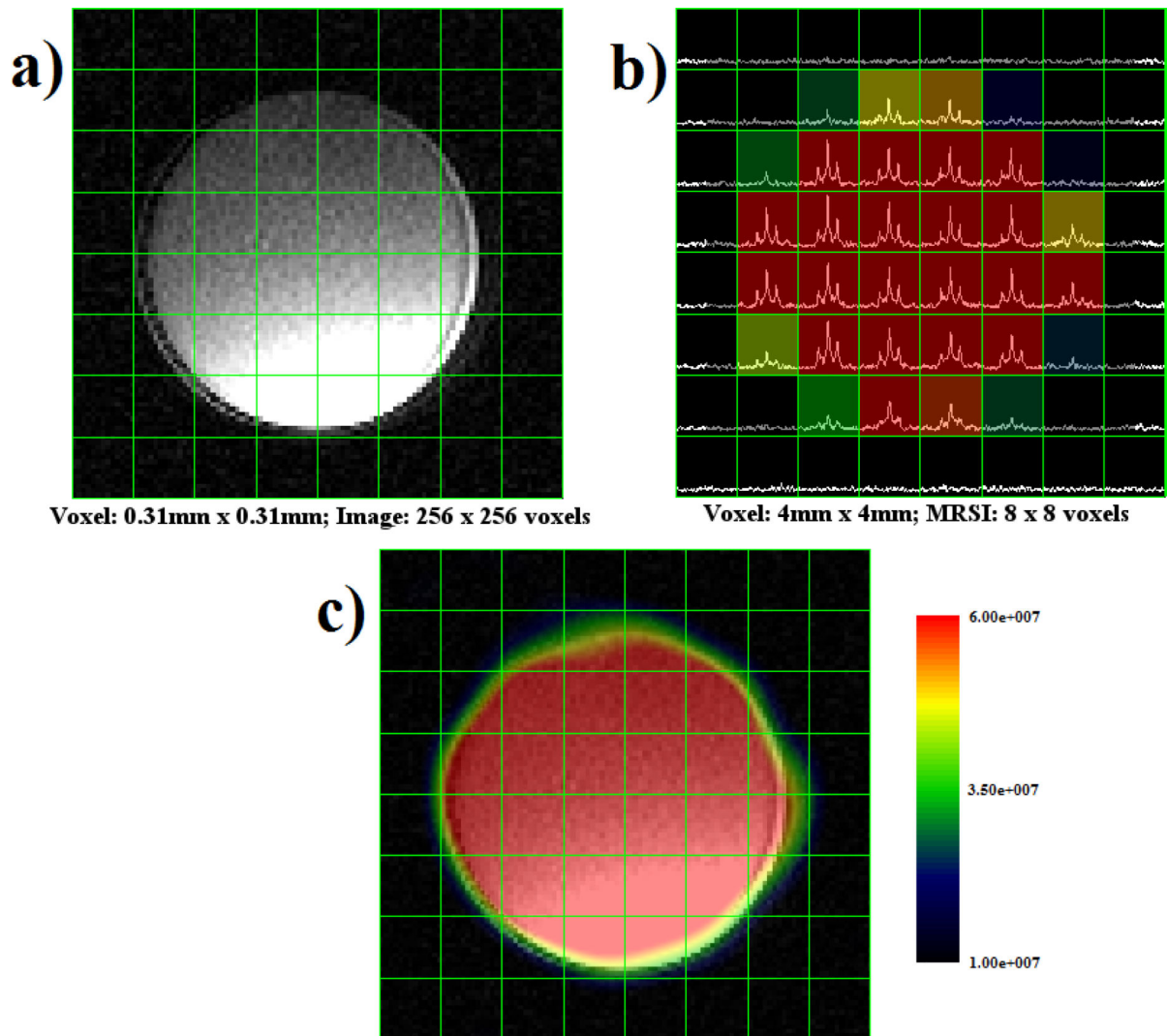


Figure 6. Montage of ethylene glycol image and spectroscopic data. (a) Proton MRI with 8×8 grid overlay. (b) MRS data presented in each voxel, with peaks corresponding to ^{13}C chemical shift. (c) MRSI generated from spatial and spectral data representing ethylene glycol concentration. The color overlay was spatially smoothed using a sinc kernel in SIVIC.

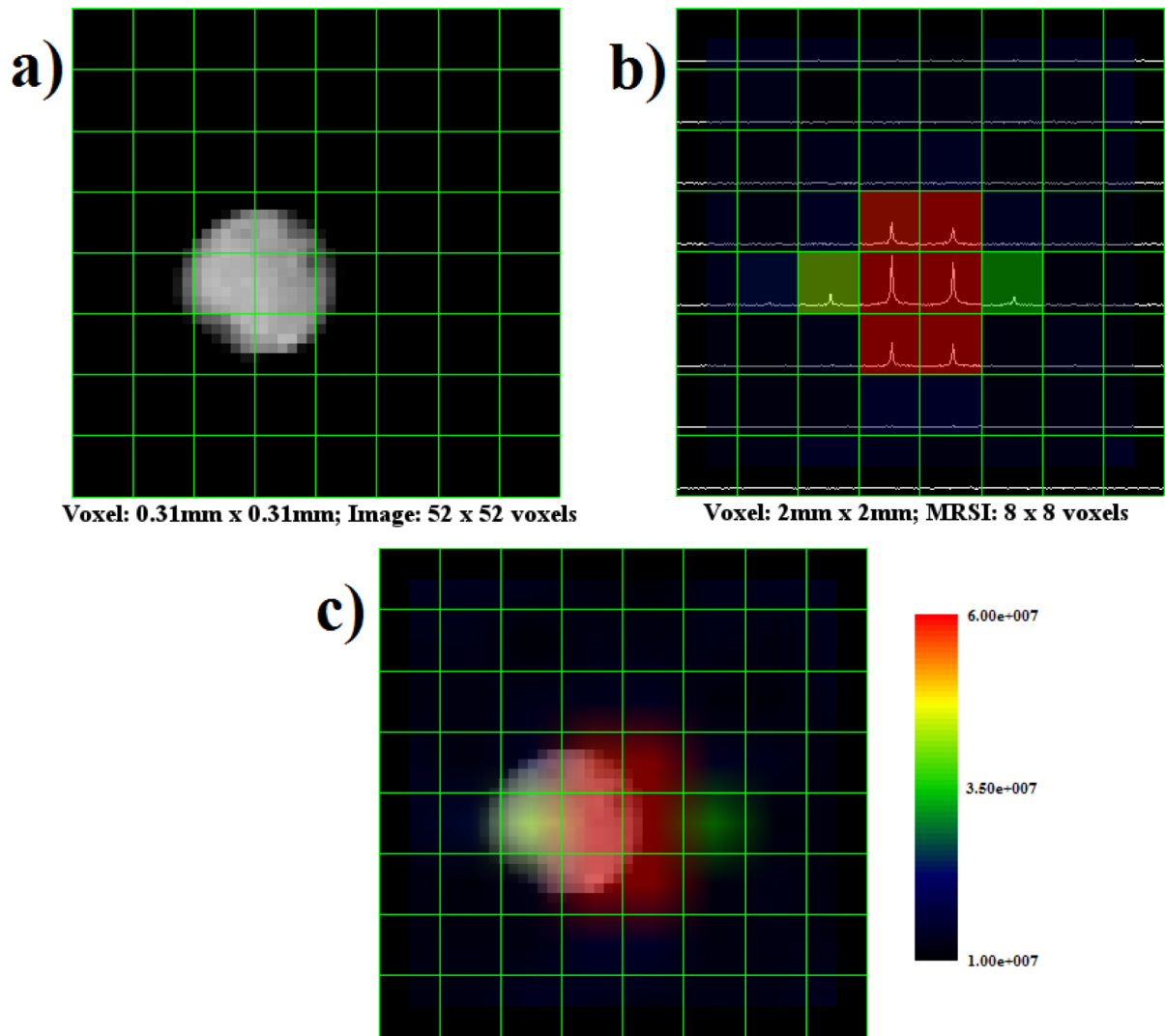


Figure 7. Montage of urea image and spectroscopic data. a) Proton MRI with 8×8 grid overlay. b) MRS data presented in each voxel, with peaks corresponding to ^{13}C chemical shift. c) MRSI generated from spatial and spectral data representing urea concentration. Note the small spatial shift between image and spectroscopic data. The color overlay was spatially smoothed using a sinc kernel in SIVIC.

Table 1

Electrical characteristics of microstrip transmission line coil (^1H) and wire loop coil (^{13}C).

Coil	Condition	f (MHz)	BW (MHz)	S_{11} (dB)	S_{21} (dB)	Q
^1H MTL	Empty	298.60	2.79	-52.34	-25.66	213.75
^{13}C Loop	w/ 30mL Ethylene glycol	74.95	0.5	-49.97	-17.80	298.31

f = Resonant Frequency, BW = Bandwidth, S_{11} = Reflection Coefficient, S_{21} = Transmission Coefficient, Q = Quality Factor.

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Table 2

Frequency shifts of microstrip transmission line (^1H) and wire loop coil (^{13}C) with the small samples.

Coil	Condition	f (MHz)	BW (MHz)	S_{11} (dB)	Q
^1H MTL	Empty (unloaded) with small samples (30mL Ethylene glycol)	299.55	3.16	-23.50	189.85
		298.45	3.44	-43.77	173.66
		-1.10	0.28	-20.28	-16.18
^{13}C Loop	Empty (unloaded) with small samples (0.95mL urea)	74.95	0.51	-42.26	292.46
		74.95	0.51	-40.17	292.46
		0	0	2.10	0