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# **Design of a Breast Phantom for Quantitative Magnetic Resonance Imaging**

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# **Abstract**

**Purpose—**We present a breast phantom designed to enable quantitative assessment of measurements of  $T_1$  relaxation time, apparent diffusion coefficient (ADC), and other attributes of breast tissue, with long-term support from a national metrology institute.

**Materials and Methods—**A breast phantom was created with two independent, interchangeable units for diffusion and  $T_1/T_2$  relaxation, each with flexible outer shells. The  $T_1$  unit was filled with corn syrup solution and grapeseed oil to mimic the relaxation behavior of fibroglandular, and fatty tissues respectively. The diffusion unit contains plastic tubes filled with aqueous solutions of polyvinylpyrrolidone (PVP) to modulate the apparent diffusion coefficient (ADC). The phantom was imaged at 1.5 T and 3.0 T using MRI scanners and common breast coils from multiple manufacturers to assess  $T_1$  and  $T_2$  relaxation time and ADC values.

**Results—**The fibroglandular mimic exhibited target  $T_1$  values on 1.5 T and 3.0 T clinical systems (25–75 percentile range: 1289 to 1400 ms and 1533 to 1845 ms respectively) across all bore temperatures. PVP solutions mimicked the range of ADC values from malignant tumors to normal breast tissue (40 % PVP median:  $633 \times 10^{-6}$  mm<sup>2</sup>/s to 0 % PVP median:  $2231 \times 10^{-6}$  $\text{mm}^2$ /s) at temperatures 17 °C to 24 °C. The interchangeable phantom units allowed both the diffusion and  $T_1/T_2$  units to be tested on the left and right sides of the coil to assess any variation.

**Conclusions—This phantom enables**  $T_1$  **and ADC measurements, fits in a variety of clinical** breast coils, and can serve as a quality control tool to facilitate the standardization of quantitative measurements for breast MRI.

# **Keywords**

breast MRI; apparent diffusion coefficient; relaxation; tissue mimic; phantoms; quality control

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# **INTRODUCTION**

Breast cancer is one of the three most common cancers in women and the second leading cause of cancer deaths in women in 2014 (1). Magnetic resonance imaging (MRI), with quantitative sequences is increasingly employed for breast cancer diagnosis, staging and monitoring. Several clinical trials that use these MRI techniques to assess treatment are currently underway (2, 3).

To assess the efficacy of breast cancer treatment, it is clinically important to understand the sources of variability in breast MRI, such as fat suppression, variations in the left and right sides of the coil, and image distortion, so that observed changes in patients can be interpreted correctly. Breast MRI measurements, particularly those used in multi-centered treatment trials, should be standardized using reliable methods for quality control. In fact, standardized acquisition parameters, quality control protocols and data reporting have been previously recommended (4). In addition, a critical step toward image quality assurance is through the use of a standard reference object or phantom.

An ideal breast phantom should have the following attributes: (a) ability to simulate the heterogeneous distribution of fat and fibroglandular tissue in the breast to test fat suppression techniques; (b) design for quantitatively evaluating standard proton spin relaxation time  $(T_1, T_2)$ , and diffusion protocols in breast MR imaging; (c) compatibility with commonly used breast coil types; (d) ability to assess variation in the left and right sides of the coil; and (e) ability to measure image distortion (5). In an effort to develop a new breast phantom, we evaluated phantoms presented in the literature. We found that these phantoms were either incompatible with some breast coil types (6), or unable to assess diffusion MRI (7).

In this work, we present a new breast phantom that is designed and fabricated to enable quantitative assessment of measurements of  $T_1$  relaxation time, apparent diffusion coefficient (ADC), and other attributes of breast tissue, with long-term support from a national metrology institute.

# **METHODS**

#### **Phantom Design**

The initial phantom prototype was guided by several design elements: 1) interspersed fibroglandular and adipose breast tissue elements extending over anatomically-representative distances in the anterior-posterior, superior-inferior, and medial-lateral directions to test fat suppression techniques; 2) adherence to *in vivo* physiologic ranges for both  $T_1$  relaxation and ADC values; 3) physical compatibility with commonly used clinical breast MRI coils; 4) repeated elements in both the left and right sides of the coil; and 5) geometric structures for measuring image distortion.

The breast phantom was created as two distinct, interchangeable units: one for diffusion and geometric distortion evaluation and one for  $T_1/T_2$  relaxation evaluation, which are connected via a polycarbonate "backboard" (Figure 1). Both phantom units consist of a flexible outer

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silicone shell (Durometer 10A, dimensions: 15.0 cm height and 12.5 cm diameter) to allow easy positioning in many coil geometries, and rigid polycarbonate internal components to ensure precise geometry and separation between materials. The interchangeable nature allows the phantom units to be imaged in both the left and right sides of a typical clinical breast coil. The polycarbonate backboard ensures rigid, reproducible spacing between the two breast phantom units, and it allows the phantom unit position to be adjusted in the medial-lateral plane for a better fit in breast coils.

In vivo measurements of the  $T_1$  and  $T_2$  relaxation times and ADC properties of fibroglandular, adipose, benign tumor and malignant tumor tissues we compiled from the literature are given in Table 1 (8–11). To mimic the  $T_1$  relaxation time of fibroglandular tissue, the bulk solution is 35 % weight-by-weight (w/w) corn syrup (ACH Food Companies, Inc, Cordova, TN) in deionized water. Grapeseed oil (Sovena USA, Rome, NY) was used to mimic both the chemical shift from water and the  $T_1$  and  $T_2$  relaxation times of adipose tissue in the breast. Polyvinylpyrrolidone (PVP, average mol. wt. 40,000 Da, Sigma-Aldrich, St. Louis, MO) was used to control the diffusion of water (12, 13). PVP concentrations of 0, 10, 14, 18, 25 and 40 % w/w are included to mimic the diffusion properties of fibroglandular and tumor tissues (Table 1) at bore temperature. The 10, 14, and 18 % w/w PVP tubes are for determination of ADC measurement resolution, to decipher the sensitivity of ADC measurements to distinguish benign and malignant lesions. The differences between the expected ADC values of 10 and 18 % w/w PVP are similar to the differences between benign and malignant tumors:  $1610 \pm 330 \times 10^{-6}$  mm<sup>2</sup>/s compared to  $1250 \pm 290 \times 10^{-6}$  $mm^2/s(9)$ .

The diffusion phantom unit, shown in Figure 2 A–C, contains 16 plastic sample tubes (4 large, 12 small), aligned in the anterior-posterior direction, containing the PVP solutions. Adipose tissue mimic tubes are also included to test the efficacy of fat suppression techniques in ADC sequences. The large tubes in the diffusion phantom unit measure 12.5 cm long and 1.4 cm inner diameter (Falcon 15 mL Conical Tube); the small tubes are 8.7 cm long and 1.0 cm in outer diameter (Wheaton 5 mL Int RB CryoElite Tube). The diffusion phantom unit also contains two perpendicular polycarbonate plates, bisecting the phantom in the axial and sagittal orientations that are designed for assessing image distortions and resolution, respectively. The axial plate contains a grid of circles on 2.0 cm center-to-center spacing in both the anterior-posterior and right-left directions, with four anterior-posterior rows of four to six, 1.0 cm diameter circles (Figure 1 A). The sagittal plate contains circular features with diameters ranging from 0.1 cm to 1.5 cm that can be used to measure resolution accuracy (Figure 1 B and Figure 2 C).

The  $T_1$  relaxation phantom unit as shown in Figure 2 D–F consists of four closed cylindrical compartments, alternately filled with adipose or fibroglandular tissue mimics (14). Each compartment contains a layer of polypropylene spheres (1.8 cm inner diameter), filled with a variety of tissue mimics described in Table 2. The two larger, more posterior layers each contain nine internal spheres (Figure 2 E, F), and the two smaller, anterior layers each contain three internal spheres.

### **Reference Measurements**

The  $T_1$  and diffusion phantom units were imaged on a small-bore 1.5 T pre-clinical MRI system (Agilent Technologies, Santa Clara, CA) to generate reference values and to measure the effect of temperature on the  $T_1$ ,  $T_2$ , and ADC of the different mimic materials. Components were imaged at clinically relevant bore temperatures: 17.91, 19.07, 20.16 and 22.11 °C ( $\pm$ 0.01 °C). The temperature control set-up consists of two, concentric cylinders with an outer fill of proton-MR invisible solution (Fluorinert FC-43, 3M, St. Paul, MN) and an inner fill of deionized water. Samples are placed in the inner compartment. The outer compartment is connected to a temperature-controlled circulator (PolyScience 9102, Niles, IL), which is filled with Fluorinert. The temperature change in the inner compartment is driven by the change in the Fluorinert that is circulating in the outer fill. Temperature is measured continuously using an MRI-compatible fiber-optic probe (OTP-M, OpSens, Québec, Canada) located centrally in the inner compartment.  $T_1$  relaxation time was measured using a spin-echo inversion recovery (IR) sequence with TR/TE 10,000/14.75 ms and inversion times (TI) 50, 75, 100, 125, 150, 250, 500, 1000, 1500, 2000, and 3000 ms. T<sub>2</sub> relaxation time was measured using a spin-echo multiple echo time sequence with TR 5000 ms and echo times 15, 20, 40, 80, 160, 320, and 640 ms. ADC was measured using a spinecho sequence with TR/TE 10,000/33.64 ms and b-values 0, 100, 600 and 900 s/mm<sup>2</sup> . For all experiments, field of view (FOV) was 150 mm<sup>2</sup>, matrix size was  $256 \times 256$ . Quantitative analysis to determine  $T_1$ ,  $T_2$ , and ADC was performed using software (PhantomViewer) developed at the National Institute of Standards and Technology (14) using standard python toolboxes including LMFIT (15). Mean and standard deviation of the model fit are reported.

Phantom mimic solutions were also assessed at 3.0 T using an NMR spectrometer. Aliquots of each solution were transferred into standard 5 mm NMR tubes. A fiber optic temperature probe was positioned in each NMR tube so that the sensing element was in the middle of the RF coil. Each sample was equilibrated to 20.00  $^{\circ}$ C (standard deviation  $\pm$ 0.03  $^{\circ}$ C) for at least 15 minutes and was continuously monitored during the acquisition of relaxometry data.

Inversion recovery and Carr-Purcell-Meiboom-Gill (CPMG) experiments were performed to measure  $T_1$  and  $T_2$  relaxation times, respectively (16, 17). Each experiment sampled 20 different inversion/decay times. Inversion times (TI) ranged from 0.005 s to 15 s, and the nominal  $\tau_{cp}$ , the time from a 180° refocusing pulse to the resultant echo, was 1 ms. The maximum length of the Carr-Purcell echo train varied according to the sample, but ranged from 0.486 s to 20.3 s. Time-domain data were Fourier transformed, the areas of the resonance peaks were plotted as a function of TI or echo train duration, and fit to exponential recovery and decay curves, respectively.

A spin-echo sequence was performed on the adipose and fibroglandular tissue mimic to replicate the  $T_2$  measurements made on the 1.5 T pre-clinical MRI system. Single echoes were acquired with a variable TE starting at 15 ms and increasing in 15 ms increments to 195 ms. Initial amplitude of the free induction decay was plotted as a function of TE and fit to an exponential decay.

# **Clinical Imaging Techniques**

 $T_1$ ,  $T_2$  relaxation times and ADC values of the phantom components were measured on commercially available systems at 1.5 T (Signa, GE Healthcare, Milwaukee, WI) using an open, bilateral, 8-channel breast coil (Hologic (formerly Sentinelle Medical), Toronto, Ontario), and at 3.0 T (Verio, Siemens AG Medical Solutions, Erlangen, Germany) using an open, bilateral, 16-channel breast coil (Hologic (formerly Sentinelle Medical), Toronto, Ontario). All imaging was done in the axial orientation.  $T_1$  relaxation measurements were made using 3D variable flip angle (VFA) methods with flip angles: 5, 8, 15, 22, and 43 degrees. At 1.5 T, TR/TE was 16.7/4.0 ms with 2 averages, slice thickness 2 mm, field of view 400 mm<sup>2</sup> and pixel size 1.56 mm<sup>2</sup>. At 3.0 T, TR/TE was 16.0/2.6 ms with 1 average, slice thickness 1 mm, field of view 340 mm<sup>2</sup> and pixel size 0.89 mm<sup>2</sup>. T<sub>2</sub> relaxation measurements were made using 2D variable echo time (VTE) methods using the same slice thickness and spatial resolution as the  $T_1$  VFA measurements. At 1.5 T, TR was 2000 ms and the echo times were 8.34, 16.68, 25.03, 33.37, 41.72, 50.06, 58.40, and 66.75 ms. At 3.0 T, TR was 4000 ms, and the echo times were 11.6, 23.2, 34.8, 46.4, 58.0, 69.6, 81.2 and 92.8 ms. ADC measurements were performed using single-shot echo-planar imaging (EPI) and four b-values: 0, 100, 600 and 800 s/mm<sup>2</sup>, with anterior/posterior frequency-encode direction and bandwidth 1953 Hz. At 1.5 T, TR/TE was 7500/70.4 ms, slice thickness 2 mm, field of view 400 mm<sup>2</sup>, and pixel size  $1.56$  mm<sup>2</sup>. At 3.0 T, TR/TE was  $14100/88$  ms, slice thickness 2 mm, field of view 399 mm<sup>2</sup>, and pixel size 2.63 mm<sup>2</sup>.

#### **Clinical Image Analysis**

Clinical image analysis consisted of the creation of image maps and selection of the regions of interest (ROIs). We used software developed in the IDL programming environment (Exelis Visual Information Solutions, Boulder, CO) at the University of California San Francisco (18). To allow for better visualization and to ensure that ROIs could be drawn on a sufficient number of slices, axial images were interpolated in the slice direction to yield isotropic voxels and then resampled to the coronal orientation. Interpolation and resampling were not necessary for diffusion-weighted images, because the tubes in the diffusion phantom unit were sufficiently visible in the original axial orientation.

 $T_1$  maps for VFA acquisitions were computed using the method for spoiled gradient steady state acquisitions (19, 20). In brief, the signal  $S_i$  acquired at a flip angle  $a_i$  is a function of the  $T_1$ , TR and equilibrium magnetization  $M_0$ :

$$
S_i = M_0 \sin \alpha_i \frac{1 - E_1}{1 - \cos \alpha_i E_1} \tag{1}
$$

where  $E_1 = e^{-TR}/T_1$ . Since signal is acquired at different flip angles, the T<sub>1</sub> can be determined by transforming the VFA signal equation into the linear form  $Y_i = mX_i + b$ ,

$$
\frac{S_i}{\sin \alpha_i} = E_1 \frac{S_i}{\tan \alpha_i} + M_0 (1 - E_1)
$$
 (2)

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and then extracting T<sub>1</sub> from the slope  $m = E_1$  as follows (19, 20):

 $T_1 = -\frac{TR}{\ln(m)}$  (3)

Voxels with non-physiological  $T_1$  values (less than 0 or greater than 10 s) were excluded prior to computing summary statistics (mean, median, etc.). ADC maps were generated by fitting the equation:

$$
lnS_b = lnS_0 - b \, ADC \quad (4)
$$

using a linear least-squares approach, where  $S_b$  and  $S_d$  are the diffusion-weighted and nondiffusion-weighted signals respectively, and  $b$  is the diffusion sensitizing factor.

ROIs were created manually. For each of the four layers of the  $T_1$  phantom unit, a 10 mm diameter circle (approximated as a polygon with 24 vertices) was placed within each sphere on the five contiguous slices centered on the slice with the greatest cross-sectional area for that sphere. All five such two-dimensional (2D) ROIs were then stacked into a multi-slice, cylindrical ROI. Multi-slice ROIs were similarly generated for the background of all four layers. ROIs for the background were identical to ROIs for the spheres in shape and size and were drawn on the same slices as the spheres' ROIs.

ROIs for the diffusion phantom unit were rectangles measuring approximately 70 mm by 3 mm for the four large tubes and 55 mm by 2 mm for the 12 small tubes. ROIs for the large tubes were created on the three contiguous slices centered on the slice with the greatest cross-sectional area of the tubes, while ROIs for the smaller tubes were created on the two contiguous slices with the greatest cross-sectional area of the tubes in each slice. These 2D ROIs were subsequently stacked into multi-slice, rectangular cuboid ROIs. In some data sets, the geometry of the tubes was distorted due to echo planar imaging (EPI) artifacts. For those data sets, ROIs were rotated at angles ranging from −5 to +5 degrees to ensure that the ROIs were circumscribed within the tubes.

To assess geometric distortion, we defined each hole based on pixel intensity, calculated the center of each defined hole, and measured center-to-center distances between all holes in the Right/Left (R/L) and Anterior/Posterior (A/P) directions. We report the average center-tocenter distance across a row or column.

# **RESULTS**

#### **Phantom Design and Tissue Mimics**

The small-bore MRI and NMR spectrometer measurements revealed that the fibroglandular mimic material (35 % corn syrup by mass water) was within the range of in vivo  $T_1$  values from literature at 1.5 T and 3.0 T, but the  $T_2$  relaxation time measured at 1.5 T was more than four times longer than the targeted in vivo  $T_2$  (10) (Tables 1–3).

For an adipose tissue mimic, grapeseed oil possessed an ideal combination of  $T_1$  and  $T_2$ relaxation times along with an appropriate chemical shift (Tables 2 and 3). Using a spectral fat suppression method, signal from the grapeseed oil and the silicone outer shell were suppressed when compared to corresponding  $T_1$ -weighted images acquired without fat suppression (Figure 3).

The measured ADC values for the PVP samples included in the breast diffusion phantom unit spanned the literature reported range of ADC values for malignant and benign breast masses and lesions as well as for normal tissue (Table 2) (9).

The interchangeable phantom units allow both the diffusion and  $T_1/T_2$  unit to be tested on the left and right sides of the coil to assess any variation. The flexible silicone outer shell allowed the phantom units to easily fit into the commonly used, commercially available breast coils that were tested.

#### **Clinical Imaging Assessment**

The  $T_1$  values of the fibroglandular mimic material measured with 3D VFA method were slightly higher than the targeted in vivo  $T_1$  values at 1.5 T and 3.0 T (Figure 4 A), and they were higher than the IR-measured  $T_1$  reference values (1.5 T: 1141  $\pm$  46 ms, 3.0 T: 1230  $\pm$  34.6 ms). The T<sub>2</sub> relaxation times measured at 1.5 T and 3.0 T (Figure 4 B) were much longer than the targeted in vivo  $T_2$  time of 54 to 63 ms. The grapeseed oil  $T_1$  measured with 3D VFA method at 1.5 T and 3.0 T (Figure 4 A) were just below the IR-measured reference  $T_1$  values (1.5 T: 236  $\pm$  42 ms, 3.0 T: 297  $\pm$  6.3 ms). The grapeseed oil  $T_2$  relaxation times measured at 1.5 T and 3.0 T (Figure 4 B) were much longer than the targeted in vivo  $T_2$  time of 53 ms.

The PVP samples in the diffusion phantom closely approximated the range of ADC values from malignant tumors to normal breast tissue (Figure 5). ADC measurements of PVP were consistent across the MRI system/breast coil configurations tested and matched the range of ADC reference measurements. Representative diffusion weighted images and ADC map are shown in Figure 6.

At 1.5 T, the bore temperature ranged from 17 to 18 °C, and at 3.0 T the bore temperature ranged from 21 to 24 °C.

As designed, image distortions can be assessed using the rigid geometry components, especially the regularly spaced grid in the center of the diffusion phantom side. For example, in Figure 7, which shows computer aided design (CAD) drawings (A, B) and diffusionweighted images (C, D) of the phantom, the  $T_1/T_2$  unit located on the left side of the coil (C), appears wider than the CAD drawing (A), and the diffusion unit located on the right side of the coil (D), appears narrower than the CAD drawing (B) for that particular configuration of the phantom units. The geometric distortion array has center-to-center spacing 20 mm in the horizontal and vertical directions; we measured the horizontal (R/L) center-to-center distances to be 19 mm in Figure 7 D. The vertical (A/P) center-to-center distances in Figure 7 D were 20 mm, as in the CAD drawing.

# **DISCUSSION**

In this study a phantom was designed, evaluated and characterized for quantitative multiparametric MRI studies of the breast. The breast phantom can be used to test fat suppression techniques; mimics  $T_1$  and ADC values measured *in vivo*; allows comparison testing of the left and right sides of the coil; and can be used to measure image distortion. Ideally, this breast phantom will be a tool to assess system-to-system variability, coil variability, longitudinal variation (4, 6), and variability across sequences, e.g., when evaluating imaging protocols for a clinical trial. This breast phantom allows users to optimize clinical imaging protocols without additional accrual of volunteers or patients.

The phantom design presented here sought to balance the competing goals of minimizing cost and complexity and maximizing functionality. A phantom with additional features could be useful in multiple clinical settings, but such a phantom would be prohibitively expensive, limiting widespread adoption. Hence, several compromises were made to arrive at a costeffective phantom with clinically relevant imaging features. These compromises included: reducing the number of intended compartments (spheres in the  $T_1/T_2$  phantom unit and tubes in the diffusion phantom unit), using readily available containers and materials when possible, and ability to position the phantom units on each side of the coil. The breast phantom outer shell is flexible and the phantom unit position can be adjusted in the medial/ lateral plane. These design choices allowed the breast phantom to physically fit into MRI breast coils from two major vendors, which are representative of the commercially available breast coils. This is an improvement over a previous breast phantom, which fits in the coil of only one vendor (6).

Unlike previous breast phantoms  $(6, 7)$ , this phantom incorporates diffusion mimics. One challenge in developing the diffusion phantom unit was selecting appropriate materials that at bore temperature exhibit the range of ADC values reported in the literature for normal and diseased breast tissue in vivo (9, 11). Here, water doped with PVP was used to achieve ADC values ranging from  $600 \times 10^{-6}$  mm<sup>2</sup>/s to  $2121 \times 10^{-6}$  mm<sup>2</sup>/s in the phantom at bore temperatures, simulating the range of ADC values reported in the literature for malignant lesions and normal tissues.

Another challenge was selection of an appropriate fat mimic to allow for testing the efficacy of different fat saturation techniques frequently used for  $T_1$ -weighted dynamic contrast enhanced (DCE) MRI and required for diffusion weighted MRI of the breast. Several options were tested, including separate materials to mimic the  $T_1$  relaxation time of fat tissue (doped water) and the chemical shift from water (various oils). To reduce complexity, grapeseed oil was used because it simultaneously mimicked both the  $T_1$  relaxation time and chemical shift properties of fat. The signal from the silicone outer shell provided an additional opportunity to assess spectral fat suppression.

The modular design of the breast phantom is advantageous, in particular to the research community, as it will allow customization and reconfiguration to address concerns in breast MRI beyond the  $T_1$  and diffusion characterization reported here. The spheres on the  $T_1$ phantom unit are attached via plastic screws and could be swapped for spheres containing

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other materials. Similarly, the tubes on the diffusion side can be easily removed and replaced with other tubes. Future investigations could include the introduction of mimics for microcalcifications, cysts, presence of biopsy clips, and silicone breast implants. Such modularity is one of several factors that make this breast phantom a robust platform for clinical imaging development, testing, optimization, and quality assurance.

The current phantom design is not without limitations. While the design enables heterogeneous distribution of the fibroglandular and adipose mimic materials suitable for testing of fat suppression, one limitation is that the physical separation between fibroglandular tissue and adipose tissue is not present in the human breast. To ensure consistent distribution of the fibroglandular and adipose mimic materials while maintaining the stability of these materials, it is best to confine the mimics to sealed containers. The containers in this phantom, made of polycarbonate material, add a separation between fibroglandular and adipose tissue mimics that does not exist in the body. In addition, these containers can contribute susceptibility artifacts and echo-planar imaging artifacts. In its current design, the breast phantom does not possess a mechanism for temperature control or tracking, which is necessary to determine the accuracy of ADC measurements. Another limitation of the current phantom design is that the fibroglandular mimic (35 % w/w corn syrup)  $T_2$  relaxation time varies greatly with magnetic field strength. This is not consistent with properties of breast tissue observed in vivo, where the  $T_2$  relaxation time is independent of field strength (10). Until a more suitable fibroglandular mimic is found, we do not recommend using the breast phantom for  $T_2$  measurements. Finally, over the course of several months, the fibroglandular mimic (35 % w/w corn syrup) was susceptible to bacterial growth when in contact with the silicone shell; this may affect the stability of relaxation properties.

Future designs of the breast phantom will include several revisions to address the identified limitations and to improve the phantom's utility. One such improvement is the capability to assess contrast-enhanced measurements. Typical  $T_1$  measurements in the breast are contrastenhanced with gadolinium; hence, it is worth considering the inclusion of a dynamic contrast component similar to that used by Freed et al. (7) in the next iteration of the phantom. In addition, an alternative adipose tissue mimic will be explored. Natural oils typically demonstrate subtle batch-to-batch variation in properties, making them less than ideal for environments in which both precision and accuracy are essential. Hence, it will be necessary to explore alternative adipose tissue mimics, preferably a synthetic oil, which is shelf-stable and consistent across production batches. However, oil selection is complicated by the requirement that the oil used should ideally mimic both the  $T_1$  relaxation time and the chemical shift observed in adipose breast tissue (synthetic mineral oils tested thus far do not possess a long enough  $T_1$ ). To date, aqueous paramagnetic salt solutions and PVP solutions show excellent stability (results not shown).

In conclusion, we designed a breast phantom that can be used to validate MRI clinical trial sites and for quality control, specifically  $T_1$  relaxation time and ADC measurements. Despite the highlighted limitations, the phantom met the goals of clinically relevant values for breast tissue  $T_1$  and ADC and can be used to test clinical protocols. Additionally, the phantom can be used to examine other imaging challenges common to breast MRI. For

example, the phantom could be used to assess quality of fat suppression technique, EPI distortion artifacts, which are dependent on the phase-encoding direction, gradient nonlinearity effects (21), especially along the long axis of the tubes in the diffusion phantom unit, and measurement variability due to the selected b-values (22). The breast phantom has long-term support from a national metrology institute, which is a benefit for clinical trials using quantitative MRI.

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#### **Figure 1.**

Breast phantom model (A) with the diffusion phantom unit and geometric distortion array on the left and  $T_1/T_2$  phantom unit on the right. (B) Detail of the resolution plate. Photo of prototype (C) prepared for imaging in a dedicated breast MR coil. The breast phantom is compatible with multiple breast coil designs and is able to assess diffusion MRI, which are improvements over previous phantoms.

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# **Figure 2.**

Diffusion phantom axial (A) and coronal (B)  $T_1$ -weighted images of the breast phantom prototype and resolution plate (C).  $T_1/T_2$  relaxation phantom axial (D) and coronal images of layer 1 (E) and layer 2 (F). Layer 1 (E) contains grapeseed oil bulk solution, and layer 2 (F) contains fibroglandular tissue mimic solution. The nipple mimic is denoted with \*. The flexible outer shell allowed some deformation to accommodate coil geometries, but did not affect positioning of the internal elements.



# **Figure 3.**

Axial  $T_2$ -weighted images acquired without (A) and with (B) spectral fat suppression demonstrate that fat signal is suppressed in the adipose tissue mimic (locations of adipose tissue mimic noted with \*). Additionally, signal from the silicone shell, at the boundary of the breast phantom, is suppressed using spectral suppression techniques (B).



# **Figure 4.**

The  $T_1$  relaxation times (A) and  $T_2$  relaxation times (C) of the fibroglandular and adipose tissue mimics measured on clinical systems at 1.5 T and 3.0 T. The target value ranges based on in vivo measurements from the literature (a. Rakow-Penner et al. and b. Merchant et al.) are shown for  $T_1$  relaxation (B) and  $T_2$  relaxation (D).

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# **Figure 5.**

The Apparent Diffusion Coefficient (ADC) of (A) the diffusion mimics measured on clinical 1.5 T and 3.0 T systems at bore temperature span the range of in vivo values for malignant tumor to healthy tissue (B), as measured in the literature (9, 11): 1. Healthy tissue; 2. Benign mass; 3. Benign lesion; 4. Malignant lesion; and 5. Malignant mass. (A) The measured 25– 75 percentile ranges are: 0 % PVP: 2140 to 2612  $\times$  10<sup>-6</sup> mm<sup>2</sup>/s; 10 % PVP: 1689 to 1802  $\times$  $10^{-6}$  mm<sup>2</sup>/s; 14 % PVP: 1516 to 1593 × 10<sup>-6</sup> mm<sup>2</sup>/s; 18 % PVP: 1358 to 1400 × 10<sup>-6</sup> mm<sup>2</sup>/s; 25 % PVP: 937 to  $1028 \times 10^{-6}$  mm<sup>2</sup>/s; 40 % PVP: 606 to 695  $\times 10^{-6}$  mm<sup>2</sup>/s.



#### **Figure 6.**

 $(A-C)$  Representative diffusion weighted images (b=100, 600, 800 s/mm<sup>2</sup>) and (D) corresponding ADC map measured on the 1.5 T system. The range of ADC values in the phantom (D) covers the range of in vivo ADC values reported in the literature.



#### **Figure 7.**

Comparison of MR representation of the CAD drawing (A, B) and diffusion-weighted image  $(C, D)$  of the breast phantom. In the diffusion-weighted image, the  $T_1/T_2$  phantom unit located on the left side of the coil (C) appears wider than the diffusion phantom unit located on the right side of the coil (D), while they are physically the same size, as demonstrated by the CAD drawing (A and B, respectively). In the geometric distortion plate (D), the centers of the regularly spaced array appear narrower in the horizontal direction of the diffusionweighted image compared to the CAD (B). We measured the horizontal (R/L) center-tocenter distances to be 19 mm in (D); the physical spacing is actually 20 mm.

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# **Table 1**





Rakow-Penner et al. in vivo measurements (10). Rakow-Penner et al. in vivo measurements (10).

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 $b$ <br>Merchant et al. *in vivo* measurements (8). Merchant et al. *in vivo* measurements (8).

 $c_{\mbox{Partridge et al.}}$  in vivo measurements (9). Partridge et al. in vivo measurements (9).

 $d_{\mbox{Partridge et al. }in\ vi\nu\mbox{ one}auxements}$  (11). Partridge et al. in vivo measurements (11).



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**Table 2**







All measurements were made on a 1.5 T small bore MRI system using spin-echo sequences, specifically: inversion recovery method to measure T1, variable echo for T2, and three gradient directions with All measurements were made on a 1.5 T small bore MRI system using spin-echo sequences, specifically: inversion recovery method to measure T1, variable echo for T2, and three gradient directions with

b-values of 0, 100, 600 and 900 s/mm<sup>2</sup> for ADC measurements. Determination of standard deviation is described in the Methods. b-values of 0, 100, 600 and 900 s/mm2 for ADC measurements. Determination of standard deviation is described in the Methods.

# **Table 3**

# 3.0 T NMR measured properties of the phantom components at 20 °C



 ${}^{a}T2$  measurements made using spin-echo technique; details in the Methods section.

 $b_{\text{T2}}$  measurements made using CPMG technique; details in the Methods section.