

# Ultrathin, transferred layers of thermally grown silicon dioxide as biofluid barriers for biointegrated flexible electronic systems

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Materials that can serve as long-lived barriers to biofluids are essential to the development of any type of chronic electronic implant. Devices such as cardiac pacemakers and cochlear implants use bulk metal or ceramic packages as hermetic enclosures for the electronics. Emerging classes of flexible, biointegrated electronic systems demand similar levels of isolation from biofluids but with thin, compliant films that can simultaneously serve as biointerfaces for sensing and/or actuation while in contact with the soft, curved, and moving surfaces of target organs. This paper introduces a solution to this materials challenge that combines (i) ultrathin, pristine layers of silicon dioxide (SiO<sub>2</sub>) thermally grown on device-grade silicon wafers, and (ii) processing schemes that allow integration of these materials onto flexible electronic platforms. Accelerated lifetime tests suggest robust barrier characteristics on timescales that approach 70 y, in layers that are sufficiently thin (less than 1 μm) to avoid significant compromises in mechanical flexibility or in electrical interface fidelity. Detailed studies of temperature- and thickness-dependent electrical and physical properties reveal the key characteristics. Molecular simulations highlight essential aspects of the chemistry that governs interactions between the SiO<sub>2</sub> and surrounding water. Examples of use with passive and active components in high-performance flexible electronic devices suggest broad utility in advanced chronic implants.

thin-film encapsulation | thermal silicon dioxide | transfer printing | reactive molecular simulation | chronic implant

Advanced concepts in materials science and engineering form the foundations for emerging classes of high-performance, flexible electronic/optoelectronic devices, with levels of functionality that far exceed those of passive components and arrays. These systems are of interest because they can conform to the surfaces of biological systems in ways that enable important capabilities of relevance to both biomedical research and clinical practice. Examples include devices for continuous monitoring of health status through the skin (1–9), optical stimulation of targeted neural circuits in the brain (10–13), and electrophysiological mapping on the epicardial surface (14–17). These platforms are unique because their lightweight construction, thin geometry, and low bending stiffness allow high-quality, minimally invasive interfaces to soft, dynamic biological tissues, in a manner that cannot be replicated with conventional wafer-based forms of electronics. Such physical properties and mechanical attributes follow from the successful codevelopment of organic, inorganic, and hybrid inorganic/organic semiconductor materials together with mechanical designs and manufacturing schemes that enable

their deployment in systems that can bend to small radii of curvature and, in some cases, stretch to high levels of elongation (2, 18–22). Skin-mounted devices, sometimes referred to as “epidermal” electronics (1), represent one of the most successful forms of this technology, where commercial embodiments are just now becoming widely available. Extensions of these types of systems for use as chronic implants have the potential to improve capabilities in human health care across broad categories of disease states and disorders (23, 24). A daunting challenge is in the development of materials that can serve as long-lived, perfect barriers to biofluids at thicknesses that allow high-quality sensing/actuating interfaces to the surrounding biology without adversely affecting the compliant mechanics.

In an ideal scenario, this material would encapsulate the entire front and back surfaces of the electronics, to prevent biofluid penetration across any exposed interfaces, with the following additional characteristics: (i) biocompatible molecular composition;

## Significance

A critical obstacle of flexible electronics for chronic implants is the absence of thin-film barriers to biofluids with multidecade lifetimes. Previously explored materials are unsuitable due to limitations of (i) extrinsic factors, such as the practical inability to avoid localized defects, and/or (ii) intrinsic properties, such as finite water permeability. The work presented here overcomes these challenges by combining pristine thermal SiO<sub>2</sub> layers with processing steps for their integration onto flexible electronics. Experimental and theoretical studies reveal the key aspects of this material system. Accelerated immersion tests and cyclic bending measurements suggest robust, defect-free operation with various electronic components and an integrated system for multiplexed mapping of electrophysiological signals. The findings have broad relevance to diverse biointegrated electronics and optoelectronics.

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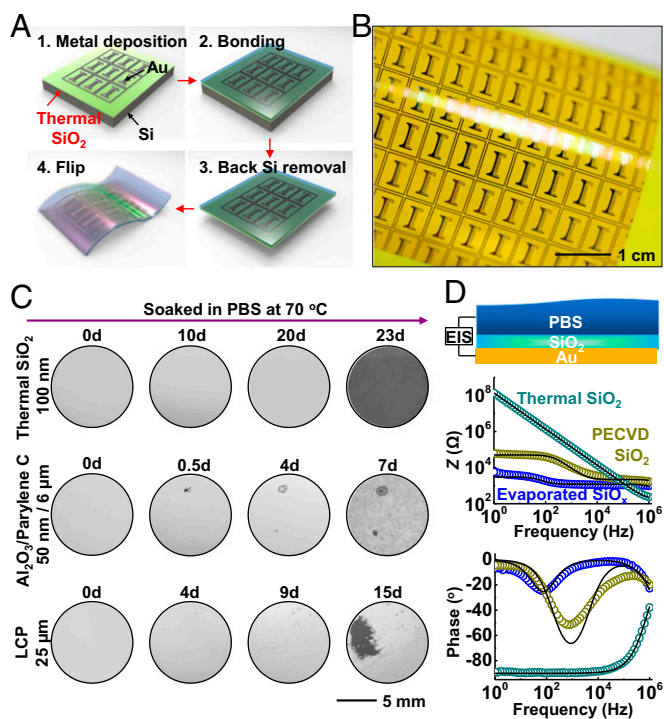
(ii) high electrical capacitance (for electrical interfaces); (iii) low thermal conductivity and thermal mass (for thermal interfaces); (iv) good optical transparency (for optical interfaces); (v) low areal mass density (for minimized inertial load); (vi) low flexural rigidity (for conformal integration onto curved surfaces); (vii) defect-free, material perfection over large areas (several or many square centimeters); (viii) thermal and chemical compatibility with polymer substrates (for device fabrication) and (ix) lifetimes of multiple decades in electrolyte solutions at physiological pH and temperature, under cyclic bending conditions (for robust operation throughout the life of the patient). Despite more than a decade of research on this topic in academic and industrial groups around the world, there is currently no proven material system that offers these properties.

Established encapsulation schemes for conventional electronic implants such as pacemakers, cochlear implants, and deep-brain stimulators, rely on thick (millimeter-scale), rigid enclosures constructed using bulk metal or ceramic parts, incompatible with the types of flexible platforms discussed here (23, 25–27). Strategies based on thin flexible films are suitable for passive arrays of sensing/actuating electrodes or related devices (28–32), but they are not immediately applicable to active, semiconductor-based electronic platforms where continuous, or nearly continuous, applied voltages and induced currents are essential for operation (14, 18, 33–35). Organic/inorganic multilayer encapsulation schemes designed to protect flexible consumer electronic devices from oxygen and moisture have some promise (36–38), but known adaptations of them cannot address the extremely demanding conditions encountered in the body, where full immersion in warm, circulating biofluids on multidecade timescales is required.

Here, we report a different approach, based on an unusual materials solution that offers all of the nine attributes listed above. The scheme combines (i) defect-free, ultrathin layers of  $\text{SiO}_2$  grown at high temperatures on the pristine, single crystalline surfaces of device-grade silicon wafers, with (ii) procedures for integrating these layers as uniform, front-side biofluid barriers and biointerfaces on flexible electronic platforms, and as backside barriers on their thin polymer supports. Detailed studies and comparative measurements against many of the most widely explored thin-film encapsulation strategies illustrate the exceptional characteristics that are possible. Thicknesses can range between tens and thousands of nanometers, in robust flexible geometries that are compatible with all important classes of materials and devices for flexible electronics. A combination of temperature-dependent measurements, microscopy investigations, electrical leakage and permeation tests, electrochemical impedance spectroscopic characteristics, and molecular dynamics simulations reveal the essential materials properties. Experiments with basic components, ranging from passive elements such as resistors, capacitors, and diodes to active, metal-oxide semiconductor transistors and multiplexed arrays, demonstrate compatibility with the highest performance types of flexible electronic devices.

## Results

**Thermal Growth of Ultrathin Layers of  $\text{SiO}_2$  and Their Integration onto Flexible Plastic Substrates.** Fig. 1A shows the four main steps for thermally growing, transferring, and integrating ultrathin layers of  $\text{SiO}_2$  onto flexible electronic platforms. The process begins with thermal oxidation of a silicon wafer at  $\sim 1,100^\circ\text{C}$ . Standard semiconductor processing techniques and/or more recent methods in growth and transfer printing, enable fabrication of high-quality electronics on this layer of oxide, which for the illustrative example here consists simply of a pattern of gold (Au). The transfer consists of bonding the top surface of this substrate onto a thin polymer film (polyimide, 25  $\mu\text{m}$  thick) on a glass substrate as a temporary, rigid support to facilitate manual manipulation. A combination of dry etching steps removes the silicon in a way



**Fig. 1.** Materials and integration strategies for use of ultrathin layers of  $\text{SiO}_2$  thermally grown on device-grade silicon wafers, as water barriers in flexible electronics. (A) Schematic illustration of schemes for exploiting layers of thermal  $\text{SiO}_2$  for encapsulation in test structures: (1) electron beam evaporation, photolithography, and etching of Mg to form “I”-shape patterns as test structures on  $\text{SiO}_2$  thermally grown on a silicon wafer; (2) pressure bonding the top surface to a glass substrate that supports a thin film of polyimide (Kapton; 25  $\mu\text{m}$ ); (3) removal of the silicon wafer from back side by dry etching; (4) release of the final flexible test structure from the glass substrate. (B) Optical image of a sample produced in this manner, with a  $\sim 100\text{-nm}$ -thick layer of thermal  $\text{SiO}_2$  on its top surface. (C) Sequential images of Mg encapsulated by layers of thermal  $\text{SiO}_2$  and  $\text{Al}_2\text{O}_3/\text{Parylene C}$  and a bulk film of liquid crystal polymer (LCP) soaked in PBS solution at  $70^\circ\text{C}$ . (D) EIS and modeling results for layers of  $\text{SiO}_2$  grown by thermal oxidation and deposited by PECVD and electron beam evaporation.

that terminates at the bottom surface of the  $\text{SiO}_2$  (*Materials and Methods*). Peeling the device from the temporary support completes the process, to yield a piece of flexible electronics encapsulated across its entire front surface with a layer of thermal  $\text{SiO}_2$  as a defect-free barrier to biofluids, with chronic stability. Unlike traditional processing flows in which deposition of barrier layers occurs last, the scheme reported here starts with a planar, fully formed barrier and then builds device functionality directly on top. Similar growth and transfer processes can deliver a layer of  $\text{SiO}_2$  to the bottom of the flexible substrate to prevent biofluid penetration from the back side. Details appear in *Materials and Methods*. Fig. 1B displays an image of a test vehicle that incorporates a front-side layer of  $\text{SiO}_2$  with thickness of 100 nm (*SI Appendix, Fig. S1*). These steps can be easily scaled to the largest silicon wafers currently available (450-mm diameter), thereby allowing for systems with overall sizes that can provide nearly full area coverage across any internal organ of the human body. As in semiconductor manufacturing, the cost per unit area will decrease with increasing wafer sizes. In matured manufacturing processes, the costs for implementing these barrier coatings on biomedical implants have the potential to approach costs that are only incrementally larger than those of the wafers themselves.

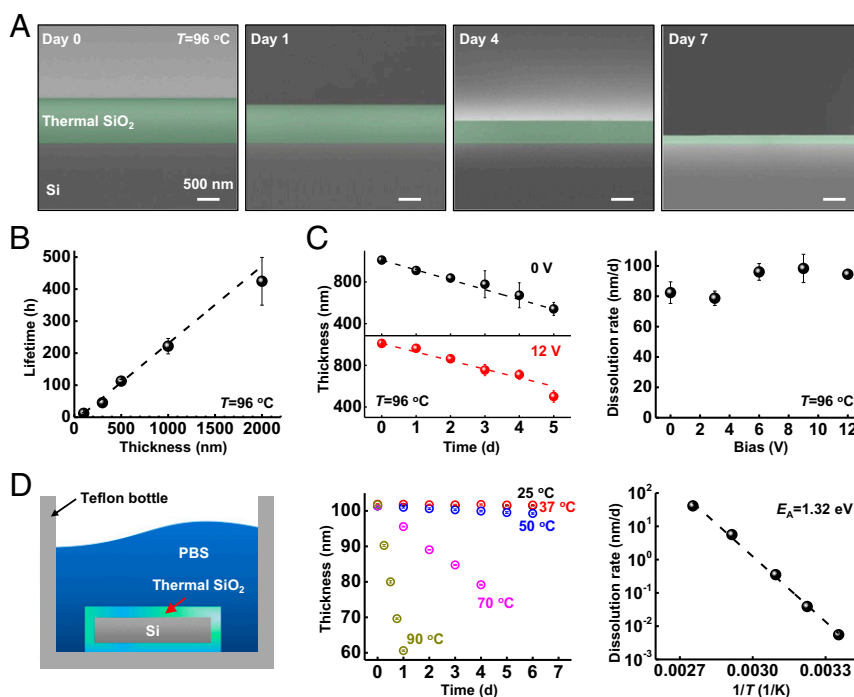
A thin, uniform layer of magnesium (Mg) (200 nm thick,  $\sim 1\text{-cm}^2$  area) formed by electron beam evaporation serves as a convenient

test vehicle for examining the water barrier properties of thin layers of SiO<sub>2</sub> grown and processed in this manner. Here, the strong reactivity of Mg with water [ $\text{Mg} + 2\text{H}_2\text{O} \rightarrow \text{Mg}(\text{OH})_2 + \text{H}_2$ ] quickly produces defects that can be visualized easily by standard microscopy techniques. As shown in Fig. 1C and *SI Appendix, Tables S1 and S2*, a 100-nm-thick layer of thermal SiO<sub>2</sub> survives for 22 d of complete, continuous immersion in phosphate-buffered saline (PBS) solution at pH of 7.4 and a temperature of 70 °C. After this period, the Mg layer dissolves at once, in a spatially uniform fashion across the entire area of the sample. Experiments performed in the same manner but with other candidate barrier materials, including various chemistries, deposition methods, thicknesses, and single/multilayer configurations, provide points of comparison. The results for all cases examined here indicate rapid degradation of the Mg in modes that involve either permeation directly through the barrier materials themselves (e.g., polymers deposited by spin coating), or through isolated, “pinhole” defects in the layers [e.g., silicon nitrides formed by plasma-enhanced chemical vapor deposition (PECVD)]. Specific examples of these intrinsic (former case) and extrinsic (latter case) effects appear in Fig. 1C. The only system, other than thermal SiO<sub>2</sub>, that shows stable operation is a stainless-steel foil with thickness of 50 μm (*SI Appendix, Fig. S2*). This option is, however, not suitable for capacitive, biosensing applications, and it has only limited value in other possible biointerface measurements, such as those based on thermal or optical interfaces. Barrier layers formed by other deposition techniques, such as plasma-assisted atomic layer deposition (ALD), O<sub>3</sub>-assisted ALD, and anodization show pinhole-like defects as well (39–42). For example, although plasma-assisted ALD-deposited SiN<sub>x</sub> has a low intrinsic water vapor transmission rate, pinholes lead to extrinsic effects that limit the encapsulation performance of the entire barrier (40). The extent and nature of these types of extrinsic effects are expected to vary depending on the deposition

methods, the deposition tools, and the detailed conditions for deposition and postprocessing, but they are unlikely to reach, on a consistent basis, the completely defect-free levels needed for the uses envisioned here. We note that additional areas of potential application of thermal SiO<sub>2</sub> barriers are in aseptic packaging, food containers, and others. Here, the performance of thermal SiO<sub>2</sub> thin-film barriers surpasses that of polymer-based antimicrobial food packaging layers by many orders of magnitude. Compared with some of the most advanced multilayer systems, such as the Barix barrier (developed by Vitex Systems, Inc.), thermal SiO<sub>2</sub> offers much lower water vapor transmission rates, even at thicknesses that are orders of magnitude smaller (37).

Electrochemical impedance spectroscopy (EIS) analysis of layers of SiO<sub>2</sub> formed by thermal growth and comparisons to those formed by other methods yield additional insights. One can interpret the EIS measurement by the equivalent circuit shown in *SI Appendix, Fig. S3A*. A pinhole-free ideal oxide in contact with the PBS solution can be represented by the solution resistance ( $R_{sol}$ ) in series with the oxide capacitance ( $C_{ox}$ ). In practice, the presence of pinholes provides a parasitic branch that contains the resistance of the solution within the pore ( $R_{po}$ ), in series with a parallel combination of charge transfer resistance ( $R_{CT}$ ) and double-layer capacitance ( $C_{dl}$ ).

Fig. 1D presents results obtained in PBS solution. In direct contrast to electron beam evaporated SiO<sub>x</sub> and PECVD SiO<sub>2</sub>, thermal SiO<sub>2</sub> exhibits a nearly perfect capacitive response: in the log-log impedance vs. frequency figure (Fig. 1D, *Middle*), a plot of the impedance ( $Z$ ) as a function of the frequency ( $f$ ) exhibits a slope of  $-1$ . The results indicate that the oxide defines the total impedance, and that the signal is not corrupted by resistive leakage through pinholes/pores or by direct permeation. The plot in the bottom part of Fig. 1D, *Bottom*, shows that the phase remains fixed at  $-90^\circ$  for frequencies up to  $10^4$  Hz



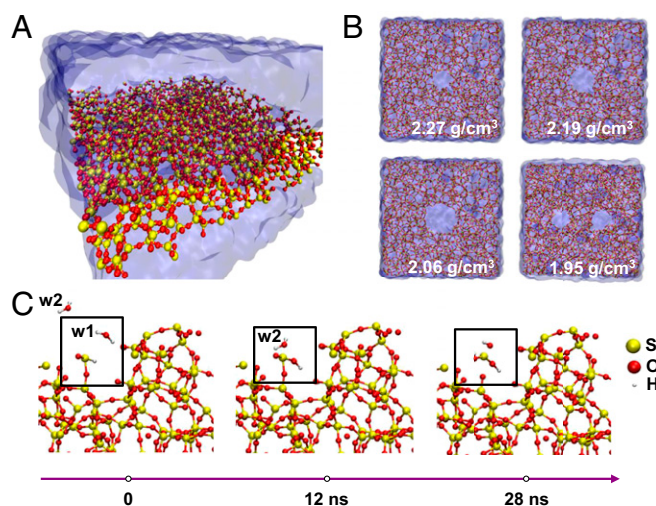
**Fig. 2.** Failure mechanisms associated with thermal SiO<sub>2</sub> encapsulation layers. (A) SEM images showing decreases in the thickness of a 1,000-nm-thick layer of thermal SiO<sub>2</sub> as a result of soaking in PBS at 96 °C. (B) Time before the leakage current reaches more than 100 nA, for thermal SiO<sub>2</sub> measured in an electrical leakage test (described in *SI Appendix, Fig. S4*). (C) Thickness changes associated with a 1,000-nm-thick layer of thermal SiO<sub>2</sub> without DC bias and with 12-V bias (*Left*), and extracted dissolution rate for voltages of 0, 3, 6, 9, and 12 V (*Right*). (D) Thermal SiO<sub>2</sub> on the surfaces and edges of a piece of Si in PBS solution (*Left*) allowed measurements of changes in thickness at different temperatures (*Center*). The results indicate a linear relationship between the dissolution rate and  $1/T$  (*Right*).

(capacitive response of a  $R$ - $C$  series circuits), as further support of this conclusion. The phase rises to  $-40^\circ$  at  $10^6$  Hz as the solution resistance begins to contribute to the response. The oxide capacitance extracted from the plot ( $\sim 1$  nF) is consistent with the known thickness and dielectric constant. Because  $C_{dl} \gg C_{ox}$ , this parameter does not affect the measurements of thermal  $\text{SiO}_2$  (*SI Appendix*, Fig. S3).

**Chemical and Physical Effects in Electrical Leakage Through Layers of  $\text{SiO}_2$ .** Results of electrical leakage tests (see *SI Appendix* for experimental details) conducted using thermal  $\text{SiO}_2$  at thicknesses of 100, 300, 500, 1,000, and 2,000 nm at  $96^\circ\text{C}$  to accelerate failure-related chemical/physical processes appear in Fig. 2A and *SI Appendix*, Fig. S4, with comparison with conventional inorganic and organic materials (*SI Appendix*, Figs. S4 and S5). The results show abrupt transitions to high leakage currents at time durations that depend linearly on the thickness. Fig. 2A displays colorized cross-sectional scanning electron microscope (SEM) images of a 1,000-nm-thick layer at various times after immersion. The results indicate a systematic reduction in the thickness, likely due to dissolution by hydrolysis,  $\text{SiO}_2 + 2\text{H}_2\text{O} \rightarrow \text{Si}(\text{OH})_4$  (*SI Appendix*, Fig. S6; dissolution occurs also for stainless steel as summarized in *SI Appendix*, Fig. S7). The timescale for complete dissolution is consistent with that for the appearance of large leakage currents, as shown in Fig. 2B, which illustrates the linear dependence of lifetime (i.e., time to large leakage current) on thickness. This linear form, and its zero intercept, also suggests that hydrolysis proceeds exclusively by surface reactions without a significant role of reactive diffusion into the bulk of the  $\text{SiO}_2$  or of permeation through defect sites. Additional studies show that the dissolution rate for thermal  $\text{SiO}_2$  does not depend on electrical bias for values relevant to biointegrated electronics (Fig. 2C).

Temperature-dependent studies of the rate of hydrolysis of thermal  $\text{SiO}_2$  in PBS reveal additional details. These experiments use thermal  $\text{SiO}_2$  grown on all surfaces of the silicon wafer, including its edges (Fig. 2D), to avoid any exposed Si, which itself will dissolve according to  $\text{Si} + 4\text{H}_2\text{O} \rightarrow \text{Si}(\text{OH})_4 + 2\text{H}_2$  (*SI Appendix*, Fig. S8). The dissolution rates depend exponentially on  $1/T$ , consistent with Arrhenius scaling and an apparent activation energy  $E_A = 1.32$  eV (Fig. 2D). This energy is higher than that inferred from previous studies of natural quartz mineral and fused amorphous silica (0.48–1.11 eV) in deionized water or various aqueous solutions (such as NaCl solution), possibly due to the formation of activated complexes on the surfaces of  $\text{SiO}_2$  in PBS (43, 44). For comparison, measurement of the dissolution rate at a pH of 7.4 and  $70^\circ\text{C}$  yields a value of 5.6 nm/d ( $2.9 \times 10^{-13}$  mol/cm $^2$ -s), which is roughly one order of magnitude higher than that of quartz or amorphous silica in deionized water at the same temperature (44, 45). This increase is likely due to an expected “salt effect” that leads to enhanced reaction rates in PBS (46). From these measurements, a multiphysics computational model for the temperature and pH dependence of the dissolution rate has been developed and validated (*Materials and Methods*). The dissolution rate is found to have a half-order dependence on hydroxide concentration (*SI Appendix*, Fig. S9). Simulations can yield estimates of the lifetime of thermal  $\text{SiO}_2$  layers for pH values ranging from 7 to 12, and temperatures from 25 to  $90^\circ\text{C}$ . At a pH of 7.4 and  $37^\circ\text{C}$ , the dissolution rate for thermal  $\text{SiO}_2$  is  $\sim 4 \times 10^{-2}$  nm/d, corresponding to a lifetime of nearly 70 y. This timescale exceeds the lifetime of most patients who might benefit from chronic flexible electronic implants, for a layer with thickness of 1,000 nm, sufficiently thin to meet the key requirements outlined previously.

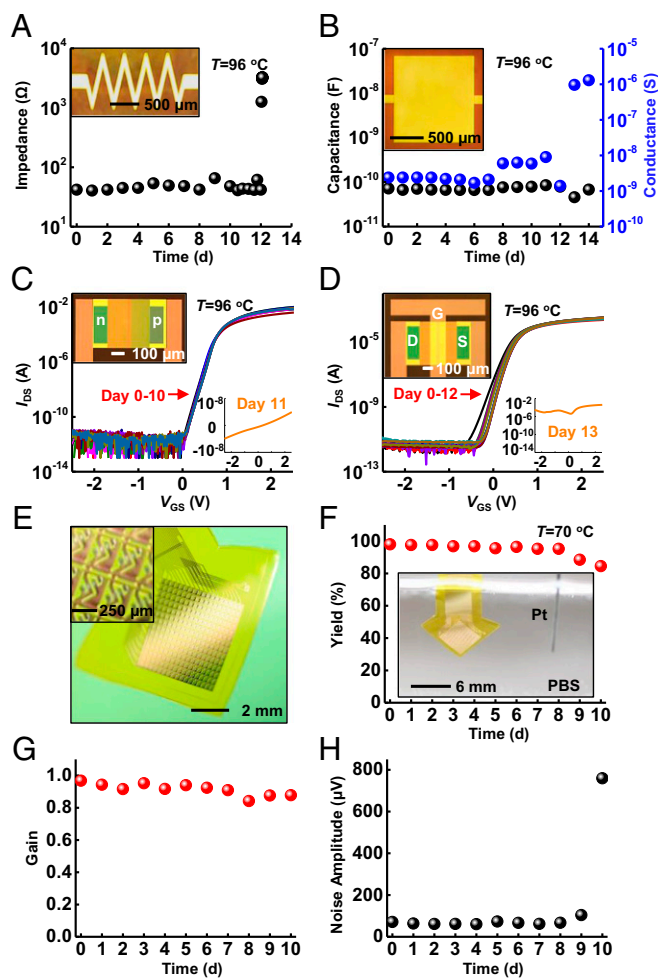
**Theoretical Modeling.** Reactive molecular dynamics (RMD) simulations (Fig. 3A and B) provide some additional insights into the dissolution chemistry. Fig. 3A presents schematic illustrations of the simulation box explained in detail in *Materials and Methods*.



**Fig. 3.** Reactive molecular dynamics (RMD) simulations of hydrolysis of defective layers of  $\text{SiO}_2$ . (A) Perspective snapshot of the  $\text{SiO}_2$  slab in water. (B) Top-view representation of four different oxide densities of the  $\text{SiO}_2$  slab in water. (C) Simulation snapshots of hydrolysis reactions that lead to the dissociation of one molecule of  $\text{SiO}_2$  from the structure.

Adding/removing protons from the system provides a means to adjust the pH of the surrounding bath that is free of ions. As shown in Fig. 3B, adding void-like defects in a perfect material serves as a route to reduce the effective density, motivated partly by previous work that shows that voids and defects larger than 1 nm can exist in  $\text{SiO}_2$  structures (47, 48). Fig. 3C depicts snapshots of sequential reactions that lead to the dissociation of Si from a surface defective site, with a dangling Si–OH, or Si–H bond. On average,  $\sim 80\%$  of the Si in the oxide layer are OH terminated and  $\sim 20\%$  are H terminated. Analysis therefore focuses on the dissolution chemistry of the former. The frame on the left ( $t = 0$  ns) shows two water molecules (labeled w1 and w2) that approach a Si atom at the location of a Si–OH bond. At  $t = 12$  ns, the hydrogen of molecule w1 dissociates and forms a bond with the H from the –OH-terminated Si and yields  $\text{H}_2$ . This reaction increases the length of the bond between the Si and the O on the bottom side from 2.3 to 2.95 Å, with a corresponding reduction in its strength. At  $t = 28$  ns, molecule w2 approaches the Si and one of its hydrogen atoms dissociates in the vicinity of the dissolution site (Fig. 3C). This hydrogen chemically bonds with the dangling O of the Si. Cleavage of the previously weakened Si–O bond releases the ionic species  $\text{Si}(\text{OH})_2^{2+}$ . The w2 remains as  $\text{OH}^-$  for an additional 3 ns and forms a water molecule by bonding with another  $\text{H}^+$  at  $t = 31$  ns. The conversion of  $\text{Si}(\text{OH})_2^{2+} \rightarrow \text{Si}(\text{OH})_4$  finishes at 80–90 ns at  $T = 37^\circ\text{C}$ , such that the final product of dissolution is silicic acid, similar to findings from previous studies of dissolution of bulk Si using comparable models (49). These reaction products appear within the 35-ns timescale of the simulations presented here under accelerated conditions, that is, at  $100^\circ\text{C}$ ,  $\text{Si}(\text{OH})_2^{2+} \rightarrow \text{Si}(\text{OH})_3^+ \rightarrow \text{Si}(\text{OH})_4$  occurs in  $\sim 32$  ns (*SI Appendix*, Fig. S10). Simulation results of different mass density, influence of defects, and temperature dependence on intermediate products during Si hydrolysis are detailed in *SI Appendix* (*SI Appendix*, Figs. S11 and S12).

**Water Barriers Demonstrated in Key Electronic Devices.** The overall process outlined in Fig. 1A provides versatility for application with nearly any class of silicon or silicon-compatible electronic systems, and with other forms of flexible electronics. Resistors, capacitors, p-n diodes, and metal–oxide–semiconductor field effect transistors (MOSFETs) based on silicon nanomembranes serve as examples, each constructed with a 1- $\mu\text{m}$ -thick layer of



**Fig. 4.** Demonstration of electronic devices and flexible electronic systems encapsulated with thermal SiO<sub>2</sub>. (A–D) Results of soak tests of resistors, capacitors, diodes, and *n*-type metal–oxide–semiconductor transistors with optical images (*Insets*). Tests in PBS solutions at 96 °C indicate that failure occurs at day 12 for all devices. (E) A photograph of a platform of active multiplexed flexible electronics with double-sided thermal SiO<sub>2</sub> encapsulation in a slightly bent configuration. The *Inset* presents a magnified view of the sensing sites, each of which consists of one sensing transistor and one multiplex transistor connected in series. (F–H) Accelerating soak test with *in vitro* measurement of electrical performance including yield (*YY*<sub>0</sub>, defined as the number of working sensing sites divided by the total number of sites), gain (the ideal gain is 1), and mean noise rms. The results indicate device stability throughout 9 d in 70 °C PBS. The *Inset* in *F* presents a photograph of an active multiplex device fully immersed in PBS.

thermal SiO<sub>2</sub> (Fig. 4 A–D, *SI Appendix*, Fig. S13, and tested in the manner illustrated in *SI Appendix*, Fig. S4, *Left*). All devices retain functionality, without measurable change from their initial state, during complete immersion in PBS at 96 °C (*SI Appendix*, Figs. S14 and S15). The SiO<sub>2</sub> fully dissolves in 12 ± 1 d, consistent with data presented previously. At this time, all devices fail suddenly and catastrophically. For example, the resistor behaves as an open circuit (Fig. 4A). For the capacitor, ions penetrate into the polyimide dielectric, which significantly increases the capacitance and contributes to leakage current across this layer (Fig. 4B). The characteristics of the diode and the *n*-channel MOSFET change to resemble those of a resistor, as illustrated in Fig. 4 C and D. As described previously, an additional transfer step can integrate a layer of thermal SiO<sub>2</sub> on the back side of the polyimide substrate, to prevent water penetration through this surface. *SI Appendix*, Fig. S16A, shows a sample with this type of

design, in which a patterned layer of Mg persists unchanged for up to 15 d during complete immersion (without well structure) in PBS at 70 °C. Under similar conditions, samples without the thermal SiO<sub>2</sub> layer on the back side of the polyimide fail within a few hours due to water permeation directly through the polyimide (*SI Appendix*, Figs. S16 and S17). *SI Appendix*, Fig. S18, demonstrates applicable flexibility of this design with 5 mm of bending radius.

In addition to water, ions present in biofluids such as Na<sup>+</sup> and K<sup>+</sup> can also degrade/alter performance, particularly in active semiconductor devices. For example, proximity of Na<sup>+</sup> to the conducting channel of a MOSFET causes its threshold voltage to shift. The challenge is that these and other ions have a non-negligible mobility inside the bulk of the thermal SiO<sub>2</sub> material. The transport is, in general, dependent on electric field, such that operation of the device can enhance this drift. When the ion transport is drift dominated, the failure time is proportional to the ion transition time  $\tau_{trans} = h/\mu\xi = h^2/\mu V = kTh^2/DqV$ , where *h* is the thickness of thermal SiO<sub>2</sub>,  $\mu$  is the mobility of the ion,  $\xi$  is the internal electric field, *V* is the voltage across the SiO<sub>2</sub>, *k* is the Boltzmann constant, *T* is temperature, *D* is the diffusivity of the ion, and *q* is the charge. In practice, the lifetime increases significantly with reductions in voltages (for a fixed thickness) and/or increases in thickness (at fixed voltage). Self-consistent simulations described in *Materials and Methods* show that ions accumulate inside the thermal SiO<sub>2</sub> where they can change the potential distribution in a manner that alters the transport (*SI Appendix*, Figs. S19 and S20). Solutions to the coupled drift-diffusion and Poisson's equation for Na<sup>+</sup> indicate that devices last several times longer than expected based on purely drift-dominated transport (which provides the lower bound for device lifetime; *SI Appendix*, Fig. S21). Penetration of ions can be further retarded by the incorporation of high-quality silicon nitride or phosphosilicate glass, as adopted by the semiconductor industry since the 1980s (50, 51). An ideal barrier for both water and ions may come from thin layers of thermal nitride, oxide/nitride bilayers, or even oxynitrides. Exploration of these possibilities is a topic of current work.

Integration of 900-nm thermal SiO<sub>2</sub> as encapsulation for actively multiplexed electronics designed to allow high-speed spatiotemporal mapping of biopotentials highlights the compatibility of the materials and concepts introduced here with the most sophisticated classes of flexible electronics. Fig. 4E and *SI Appendix*, Fig. S22, present exploded view schematic illustrations of the system and an image of a completed device with top- and bottom-side thermal SiO<sub>2</sub> encapsulation, respectively. This platform provides 252 sensing sites (18 rows by 14 columns) with silicon transistors at each site for actively multiplexed addressing, over an area of 4.5 mm × 4.6 mm. The multiplexing is realized by connecting a pair of transistors in series, one of which functions for capacitive sensing of biopotentials through thermal SiO<sub>2</sub> by connecting its gate terminal to an electrode pad. The other transistor serves as a switch to allow multiplexed readout from the sensing site (*SI Appendix*, Figs. S23 and S24). In addition to its barrier role, the front-side SiO<sub>2</sub> layer acts as the dielectric layer for capacitive coupling. Fig. 4 F–H shows excellent yield, stable high average gain values with low noise operation during complete immersion in PBS solution at 70 °C for 10 d. *SI Appendix*, Fig. S25, illustrates robust performances in bending test. Although the approaches presented here do not encapsulate the exposed edges at the periphery of the overall device platforms, this constraint seems to have little practical effect on the lifetimes for the cases examined. One potential limitation is that SiO<sub>2</sub>/polymer interface might suffer from delamination, especially under external stimuli such as thermal cycles (52). Ongoing efforts seek to eliminate edges entirely by use of slightly oversized layers of thermal SiO<sub>2</sub> together with SiO<sub>2</sub>/SiO<sub>2</sub> bonding chemistries adapted from the semiconductor industry.

## Conclusions

In summary, the results presented here establish materials strategies and integration schemes for use of ultrathin layers of SiO<sub>2</sub>

thermally grown on device-grade Si wafers as long-lived water barriers for active, flexible electronic systems. Comparisons against conventional encapsulation strategies highlight the advantages. Detailed experimental and theoretical investigations reveal that a slow hydrolysis process defines the ultimate lifetimes, consistent with the exceptionally high quality of SiO<sub>2</sub> films formed and manipulated in the schemes introduced here. In regimes of thicknesses compatible with mechanically flexible form factors, and in layouts that can support high-quality electrical interfaces, accelerated testing and modeling at both atomistic and continuum length scales suggest robust operation over many decades at physiological temperatures. Results presented here used PBS as the test solution. Lifetimes in biofluids may be somewhat different, due to differences in composition. Demonstrations at wafer-level sizes and in dual-sided encapsulation geometries illustrate the scalability of these approaches to devices of relevance for nearly all envisioned applications in biointegrated electronics. It is important to acknowledge practical difficulties in application of the ideas presented here to systems with challenging topography such as those that involve arrays of penetrating pin-type electrodes. Future efforts include developing schemes to address

such applications, exploring advanced embodiments that can inhibit both water and ion permeation, and implementing these concepts in electronic and optoelectronic devices for neural and cardiac applications.

## Materials and Methods

Details of fabrication steps, device structures of Mg tests, impedance measurement, and electrical leakage tests are shown in *SI Appendix*. Theoretical analysis including EIS modeling, multiphysics simulations of thermal SiO<sub>2</sub> dissolution, molecular simulations, and sodium ion transport simulations also appear in *SI Appendix*.

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