

# Fast propagation regions cause self-sustained reentry in excitable media

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**Self-sustained waves of electrophysiological activity can cause arrhythmia in the heart. These reentrant excitations have been associated with spiral waves circulating around either an anatomically defined weakly conducting region or a functionally determined core. Recently, an ablation procedure has been clinically introduced that stops atrial fibrillation of the heart by destroying the electrical activity at the spiral core. This is puzzling because the tissue at the anatomically defined spiral core would already be weakly conducting, and a further decrease should not improve the situation. In the case of a functionally determined core, an ablation procedure should even further stabilize the rotating wave. The efficacy of the procedure thus needs explanation. Here, we show theoretically that fundamentally in any excitable medium a region with a propagation velocity faster than its surrounding can act as a nucleation center for reentry and can anchor an induced spiral wave. Our findings demonstrate a mechanistic underpinning for the recently developed ablation procedure. Our theoretical results are based on a very general and widely used two-component model of an excitable medium. Moreover, the important control parameters used to realize conditions for the discovered phenomena are applicable to quite different multicomponent models.**

excitable media | spirals | reentry | cardiology | ablation

In their seminal theoretical work, Norbert Wiener and Arturo Rosenbluth (1) showed in 1946 that the self-sustained activity in the cardiac muscle can be associated with an excitation wave rotating around an obstacle. This mechanism has since been very successfully applied to the understanding of the generation and control of malignant electrical activity in the heart (2). It is also well known that self-sustained excitation waves, called spirals, can exist in homogeneous excitable media. It has been demonstrated that spirals rotating within a homogeneous medium or anchored at an obstacle are generically expected for any excitable medium. Examples are known in myocardial tissues and the mammalian brain (3, 4), in the aggregation of amoeba colonies (5), in autocatalytic chemical reactions (6, 7), and in the spreading depression in chicken retina (8), as well as in the catalytic reactions of carbon monoxide gas on a platinum surface (9) and also in intracellular calcium dynamics (10). Spirals have important consequences for medicine, where they are known to cause sudden cardiac death (11, 12). Recently, an atrial defibrillation procedure was clinically introduced that locates the spiral core region by detecting the phase-change point trajectories of the electrophysiological wave field and then, by ablating that region, restores sinus rhythm (13, 14). This is clearly at odds with the Wiener–Rosenbluth mechanism because a further destruction of the tissue near the spiral core should not improve the situation.

Here, we show theoretical results that help to resolve this issue. We found that spirals can be anchored not only at an obstacle, but also at a region where the propagation velocity is higher than in the surrounding medium. Moreover, in the presence of such a fast propagation region (FPR), spirals can be nucleated after application of one stimulus only. Thus, FPRs can be more

disruptive to plane wave propagation than the obstacle, where spiral generation needs at least two stimuli (15–17). In general, our findings have important consequences for excitable media dynamics and, in particular, provide understanding of the medical ablation procedure that can stop atrial fibrillation (13, 14) by destruction of a FPR at the spiral core.

## Mathematical Model

Because the phenomenon of spiral generation is universal, it is best investigated from a general point of view. Let us consider a medium that consists of active elements locally connected to each other by a diffusion-like coupling (characterized by a coupling strength  $D$ ). The medium's resting state can be excited by the application of a suprathreshold external stimulus that initiates a propagating excitation wave. Such a wave consists of a rapid transition (wavefront) from a stable resting state to an excited state, followed by a plateau, and finally by a recovery transition (waveback) toward the resting state.

This type of dynamics is usually modeled by a system of nonlinear reaction–diffusion equations. For instance, such systems are commonly used to simulate electrophysiological waves in cardiac or nervous tissue (18), chemical waves in *Dictyostelium discoideum* (19), and in the chemical Belousov–Zhabotinsky reaction (20).

Our study is based on the general two-component reaction–diffusion system of the form

$$\frac{\partial u}{\partial t} = \nabla \cdot (D \nabla u) + AF(u, v), \quad [1]$$

## Significance

Rotating spiral waves have been observed in a wide variety of nonlinear spatially distributed systems in physics, chemistry, and biology, called excitable media. In medicine, they are associated with cardiac arrhythmias. Nevertheless, how exactly these waves are initiated in excitable tissue remains largely unknown. Several candidate mechanisms have been proposed over the last century, largely based on the assumption of wave breaking due to unexcitable obstacles or the medium's refractoriness. Here, we have identified a generic mechanism for self-sustained spiral wave generation in inhomogeneous excitable media by localized regions with the fast propagation velocity. We believe our theory creates constructive options to fight these deadly phenomena.

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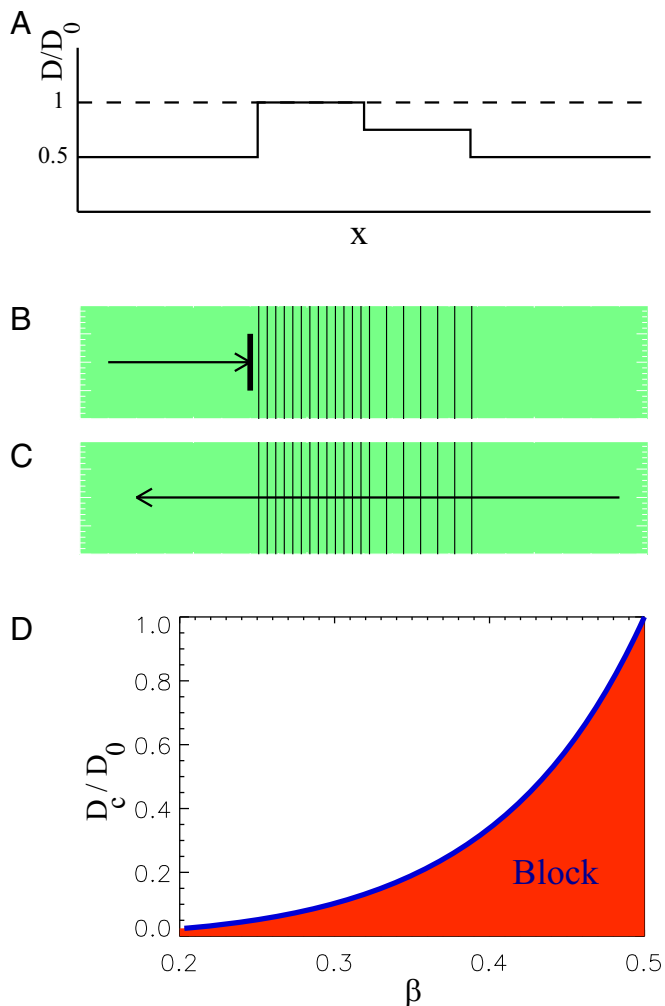
$$\frac{\partial v}{\partial t} = \epsilon G(u, v). \quad [2]$$

Here, the local kinetics of an activator  $u$  and an inhibitor  $v$  is specified by the nonlinear functions  $F(u, v)$  and  $G(u, v)$ . Our numerical simulations are based on a slightly modified Barkley model (21) that is a very common example of a two-component reaction–diffusion system (Eqs. 1 and 2), where the nonlinear functions  $F(u, v)$  and  $G(u, v)$  are:

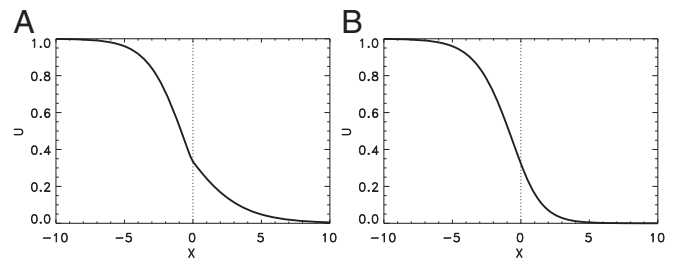
$$F(u, v) = u(1 - u) \left( u - \frac{v + b}{a} \right), \quad [3]$$

$$G(u, v) = \begin{cases} u - v, & u \geq v, \\ k_\epsilon(u - v), & u < v. \end{cases} \quad [4]$$

The parameter  $\epsilon \ll 1$  predetermines a large time-scale difference between the fast activator  $u$  and the slow inhibitor  $v$ . This excitable medium model assumes the existence of a stable resting state at  $u = 0$  and  $v = 0$ .



**Fig. 1.** Conditions for a unidirectional propagation block due to a sharp increase of the coupling strength  $D$ . (A) The stepwise spatial variation of the parameter  $D$ , with  $D_0 = 2$ . (B) A right-traveling wave is blocked because it cannot overcome a large step in  $D$ , where  $D/D_0$  is greater than the critical value. (C) A left-traveling wave propagates over the two steps in  $D$ , both of which are less than the critical value. (D) The critical value of the coupling strength  $D_c/D_0$  at the inhomogeneity boundary as a function of the excitation threshold  $\beta$ .



**Fig. 2.** Stationary profile of a front initially propagating from left to right and stopped due to a jump in the medium's parameters at  $x = 0$ . Numerical simulations of a slightly modified Barkley model (Eqs. 1–4) with  $\epsilon = 0$ . (A)  $D = 1$  for  $x < 0$ ,  $D = 2$  for  $x > 0$  and  $A = 1$  everywhere. (B)  $A = 1$  for  $x < 0$ ,  $A = 2$  for  $x > 0$ , and  $D = 1$  everywhere.

### Unidirectional Propagation Block in a One-Dimensional Medium

For a general excitable medium, unidirectional propagation block can be realized based on a phenomenon termed source–sink mismatch in the cardiology literature (22). This we demonstrate exemplarily in Fig. 1, where we assume that an initially homogeneous one-dimensional (1D) medium with the coupling strength  $D = D_0$  is remodeled so that the coupling strength is decreased everywhere except in a central region (Fig. 1A). In the central region, we assume a stepped variation so that the coupling strength steps from left to right from  $D/D_0 = 0.5$ , over  $D/D_0 = 1.0$ , to  $D/D_0 = 0.75$ , and then back to  $D/D_0 = 0.5$ . A wave traveling to the right is blocked (Fig. 1B), whereas a wave traveling to the left passes through. The conduction block for the right-traveling wave can be explained by the source–sink mismatch induced by a sharp increase of the coupling strength  $D$  above a critical value (23–25). In other words, the flux generated by the poorly coupled cells (source) with  $D/D_0 = 0.5$  is insufficient to raise the activity of the well-coupled cells (sink) with  $D/D_0 = 1.0$  above the excitation threshold. Because of the two-step increase, the left-traveling wave propagation continues because the individual changes in  $D$  at each step do not exceed the critical value (Fig. 1C). Finally, the left-traveling wave is leaving the central region because well-coupled elements (source) very easily excite poorly-coupled cells (sink). Although this step sequence might seem artificial at first sight, let us point out that the phenomenon is general. All it requires is a sufficiently steep increase of the coupling strength on one side and a smoother one on the other.

To clarify the conditions for a possible propagation block induced by a fast parameter increase in a 1D medium, we consider a limiting case  $\epsilon \rightarrow 0$  and set  $v(x, 0) = 0$ . In this limit, Eq. 1 describes a bistable distributed system, where, in addition to the resting state, there exists an excited state  $u = 1$  and an unstable steady state  $u = \beta$ , which represents the excitation threshold. Under certain conditions, it is possible to induce a wavefront (e.g., propagating from left to right) and corresponding to a transition from  $u = 0$  to  $u = 1$  (26). The propagation velocity of this front reads

$$c_p = \sqrt{2AD}f(\beta), \quad [5]$$

where the function  $f(\beta)$  is determined by the specific form of  $F(u, 0)$ . Thus, in a homogeneous medium, the propagation velocity is an increasing function of both parameters  $A$  and  $D$ .

To analyze the conditions for a conduction block, we are taking into account that the time derivative in Eq. 1 vanishes in the case of a motionless front. Hence, the profile of the front in the general case of the synchronous jumps of the

parameters  $A$  and  $D$  at  $x = 0$  is a solution of the ordinary differential equation

$$\frac{d}{dx} \left( D(x) \frac{du}{dx} \right) + A(x) F(u, 0) = 0, \quad [6]$$

where  $A(x) = A_L$ ,  $D(x) = D_L$  for  $x \leq 0$  and  $A(x) = A_R$ ,  $D(x) = D_R$  for  $x > 0$ . The boundary conditions and the continuity condition at  $x = 0$  read as

$$\begin{aligned} u|_{x=-\infty} &= 1, & u|_{x=\infty} &= 0, \\ \frac{du}{dx}|_{x=-\infty} &= \frac{du}{dx}|_{x=\infty} &= 0, \end{aligned} \quad [7]$$

$$D_L \frac{du}{dx} \Big|_{x=0^-} = D_R \frac{du}{dx} \Big|_{x=0^+}. \quad [8]$$

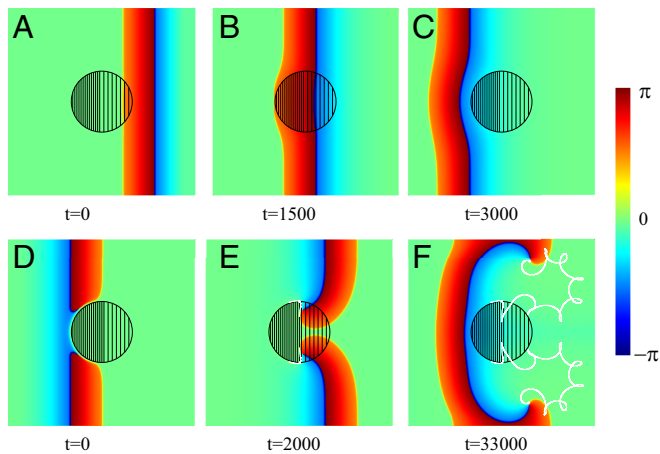
Multiplying Eq. 6 by  $du/dx$ , integrating over  $x$  from  $-\infty$  to  $\infty$ , and using Eqs. 7 and 8, we obtain the following equation:

$$D_L A_L \int_1^{u(0)} F(u, 0) du = D_R A_R \int_0^{u(0)} F(u, 0) du, \quad [9]$$

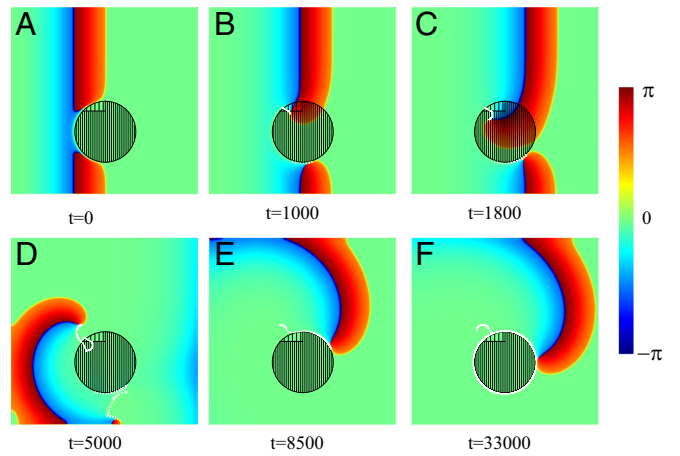
that determines the value  $u(0)$  at the point of the parameter jump as a function of the ratio  $D_R A_R / (D_L A_L)$ . Note that the front can be stopped only if  $u(0) \leq \beta$ . Thus, Eq. 9 for  $u(0) = \beta$  gives the critical ratio  $D_R A_R / (D_L A_L)$ , above which the propagating block can be observed for general form of the kinetic function  $F(u, 0)$ .

Fig. 1D summarizes the analytical results for the critical value of the relative increase of the coupling strength  $D_c/D_0$  that leads to propagation block as a function of excitation threshold  $\beta$ . Note that a region with a stronger coupling strength  $D/D_0$  can be recognized as a FPR because the propagation velocity is proportional to  $\sqrt{D}$ , according to Eq. 5. For the function  $F(u, 0)$ , given by Eq. 3, the critical ratio  $D_R A_R / (D_L A_L)$  can be expressed analytically as

$$\frac{D_R A_R}{D_L A_L} \geq \frac{(1 - \beta^2)(1 - \beta)^2}{\beta^3(2 - \beta)}. \quad [10]$$



**Fig. 3.** Spiral wave initiation due to a FPR in a 2D inhomogeneous medium. Within the left-hand part of the central circular FPR  $D = D_0 = 2$  (dense filling). Within the right-hand part,  $D/D_0 = 2/3$  (rare filling). Within the rest of the medium,  $D/D_0 = 1/2$ . Snapshots of a left-traveling wave (A–C) and a wave propagating in the opposite direction (D–F) are shown. The trajectories of the created phase-change points are shown by white lines (E and F).



**Fig. 4.** Spiral wave initiation due to an asymmetric FPR slightly shifted of center. Within the FPR  $D = D_0 = 2$  (dense filling), except a small region where  $D/D_0 = 5/6$  (rare filling). Within the rest of the medium,  $D/D_0 = 0.5$ . (A) A wave initially propagating from the left is blocked and broken. (B–D) The trajectories of the spiral tips are shown by white solid and dotted lines. (E and F) One spiral tip disappears due to the collision with the medium's boundary (dotted line). The trajectory of the remaining tip is shown (solid line).

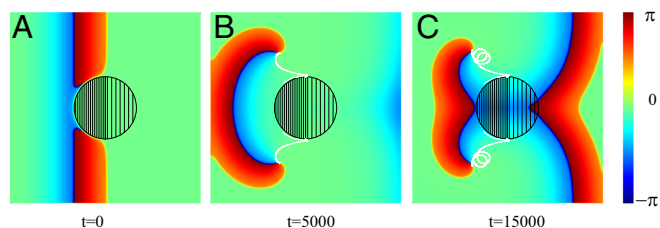
For  $\beta = b/a = 0.44$  used in our simulations, it gives  $D_R A_R / (D_L A_L) \geq 1.903$ .

This analytic prediction agrees with direct numerical computations as illustrated by Fig. 2. In Fig. 2A, the propagation block is due to a jump of the coupling strength  $D$ . Here  $D_L = 1$  and  $D_R = 2$ , while  $A = 1$  everywhere. A wave initiated in the left part of this 1D medium is blocked and approaches a stationary profile shown in Fig. 2A. Note that the spatial derivatives of the variable  $u$  has a jump at the point  $x = 0$  that, however, corresponds to the continuity condition (Eq. 8). Moreover, the front can be stopped, if the parameter  $A$  is nonuniformly distributed (27) (e.g.,  $A_L = 1$  and  $A_R = 2$ ), whereas  $D = 1$  everywhere, as shown in Fig. 2B. Here, the profile of the variable  $u$  is perfectly smooth. In both cases, the ratio  $D_R A_R / (D_L A_L) = 2$  slightly exceeds the critical value determined by Eq. 10. Because of this, the approached value  $u(0)$  is slightly smaller than the excitation threshold  $\beta$ .

### The Effect of FPRs in Two Dimensions

To extend our results on a 2D case, numerical simulations of Eqs. 1–4 with no-flux boundary conditions have been performed for  $a = 1$ ,  $b = 0.44$ ,  $k_\epsilon = 10$ , and  $\epsilon = 0.00011$  in a rectangular region of size  $l_x = l_y = 540$ . Spatial step  $\Delta x = \Delta y = 0.3$ , time step  $\Delta t = 0.01$ . The variable  $u$  and  $v$  are varied within the well-determined range  $0 < u < 1$  and  $0 < v < a - 2b$ . This spatiotemporal dynamics of the variables  $u$  and  $v$  is represented in Figs. 3–7 by color-coded distribution of the excitation phase  $\phi$ , where  $-\pi < \phi < \pi$ . The phase is defined as  $\phi = \alpha + 3\pi/4$ , where an angle  $\alpha$  determines the direction of the vector with components  $(u - 1/2)$  and  $(v - a/2 + b)/(a - 2b)$  on the  $(u, v)$  phase plane. According to this definition,  $\phi = 0$  corresponds to the resting state of the medium (green areas in Figs. 3–7), yellow (dark blue) narrow regions represent the wavefront (waveback), and red areas correspond to a wave plateau, whereas blue ones represent the refractory regions.

Let us now consider a 2D excitable medium with a FPR. Although this example may seem again rather simple, it captures the generic and essential mechanism. Fig. 3 shows numerical results of the wave propagation simulated for the excitable media model described by Eqs. 1–4. Everywhere, except the circular FPR of radius  $R = 90$ ,  $D/D_0 = 1/2$  (with  $D_0 = 2$ ) and within the left half of the FPR  $D/D_0 = 1$  and in the right half



**Fig. 5.** Spiral wave initiation due to a FPR breaking up of a plane wave induced near the left edge of the medium and propagating to the right. (A–C) The parameter  $A$  is fixed to  $A = A_0 = 2$  within the left part of the central circular region (dense filling) and  $A = 0.75A_0$  in the right part (rare filling). Within the rest of the medium,  $A/A_0 = 0.5$ . The trajectories of two created spiral tips are shown by white solid lines in  $B$  and  $C$ .

$D/D_0 = 2/3$ . A planar left-traveling excitation wave initiated at the right propagates unbroken (i.e., the wave travels through the region with a continuous wavefront that speeds up slightly within the FPR) (Fig. 3*B*). Finally, the wave approaches the left medium's boundary and disappears due to the no-flux boundary conditions.

This is in stark contrast to a right-traveling wave. There, a plane wave created near the left side of the medium is blocked at the FPR due to the sharp increase of the parameter  $D$  exceeding the critical value. This results in a wave break and the creation of two phase-change points (spiral tips), where the wavefront coincides with the waveback, as shown in Fig. 3*D*. Because of the propagation block, the spiral tips move along the boundary of the FPR until they reach its vertical symmetry axis. There, the increase of the parameter  $D$  is not sufficient to block the wave anymore, and the spiral tips penetrate into the FPR (solid white lines in Fig. 3*E*). Moreover, the waves are able to penetrate into the left-hand part of the FPR like a 1D wave does in Fig. 1*C*. They start to rotate around the phase-change points, and two counterrotating spirals separate from the FPR, as shown in Fig. 3*F*. The further dynamics of these counterrotating spirals is determined by the parameters of the medium and the boundary conditions. They represent a source of a self-sustained activity. It is remarkable that they were created immediately with the first incoming wave.

In the above example, we demonstrated a generic mechanism for the generation of two spirals. Of course, the perfect symmetry observed is a direct consequence of the chosen geometry, and this will not be the case in general. Let us therefore demonstrate an example where the symmetry is broken. As we shall show below, the asymmetry of the inhomogeneity within the FPR allows one of the spirals to travel away, while the other pins to the region. This we show exemplarily in Fig. 4, where an asymmetric inhomogeneity of the region was simulated. As in the previous case, a right-traveling wave is blocked at the FPR (Fig. 4*A*), and two spiral tips are created. A clockwise-rotating spiral penetrates into the central region, while the other, counterclockwise-rotating spiral moves around the FPR (Fig. 4*B*). As a result, the clockwise spiral rotates faster and pushes the counterclockwise spiral toward the medium's boundary (Fig. 4*C*), where it eventually disappears (Fig. 4*D*). The clockwise-rotating spiral continues to move around the FPR (Fig. 4*E*). In other words, the single remaining spiral is pinned and circulates around the FPR.

### Spatial Inhomogeneity of the Parameter $A$

Note that in the two examples illustrated by Figs. 3 and 4, the medium inhomogeneity is solely due to the variations of the coupling strength  $D$ , while the parameter  $A$  is spatially uniform. This parameter characterizes, for example, cardiac ion channel density, which can be effected by heart disease (28). According to

Eq. 10, the inhomogeneity of the parameter  $A$  is equally important for the wave block. To check these predictions, the corresponding numerical computations have been performed for the 2D inhomogeneous medium, where the coupling strength  $D$  is fixed as  $D = 1$ , while  $A = A_0 = 2$  in the left part of the central circular-shaped FPR of radius  $R = 90$  and  $A/A_0 = 0.75$  in the right part, as shown in Fig. 5. Within the rest of the medium,  $A/A_0 = 0.5$ .

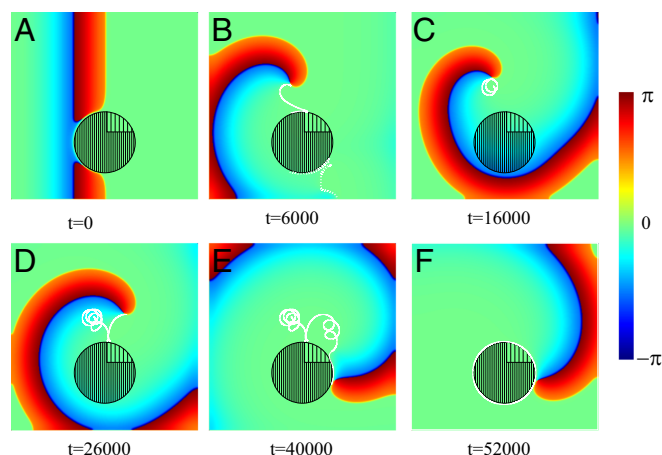
Initially, a plane wave is originated near the left edge of the medium, and the motion of this wave to the right is blocked by the FPR. Again, because of a nonzero value of  $\epsilon$ , the propagating wave is broken, and two spiral tips are created, as shown in Fig. 5*A*. These spiral tips are moving along the FPR boundary. They can penetrate into this region only near the right part of the FPR boundary, where  $A/A_0 = 0.75$ . After this penetration, they also can cross the boundary between the right and left parts of the inhomogeneity, because here the ratio  $A/A_0$  is below the critical one determined by Eq. 10 (Fig. 5*B*). The wavefronts start to rotate around the spiral tips, and then two spiral waves leave the central region, as shown in Fig. 5*C*.

As before, pure mirror symmetric dynamics of two simultaneously created spiral waves can be destroyed by the use of an asymmetric shape of the FPR, as shown in Fig. 6. A planar wave propagating from the left medium's boundary is stopped and broken. As a result, two spiral tips are created (Fig. 6*A*). These two spiral tips first move along the FPR boundary. Then, the clockwise-rotating wave reaches the right part of the FPR, where the ratio  $A/A_0 = 0.75$  is less than a critical value for a wave block. Here, the front can penetrate into the FPR and starts to rotate. This rotation pushes the counterrotating wave toward the bottom boundary of the medium and forces it to disappear (Fig. 6*B*). The remaining spiral wave first makes several rotations near the FPR and then starts to rotate around it, as shown in Fig. 6*C*.

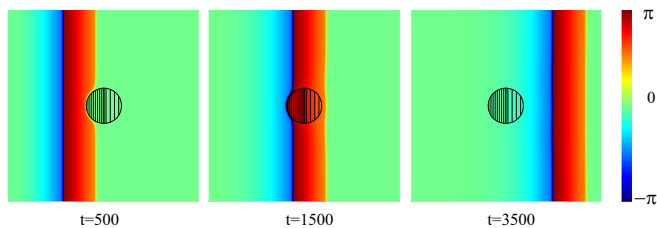
This scenario is very similar to the one illustrated in Fig. 4. Thus, the numerical results obtained for the FPR created by spatial variation of the parameter  $A$  are very similar to ones for spatial variations of the coupling strength  $D$ .

### Discussion

**General Properties.** Our results demonstrate a generic mechanism for spiral wave creation in an excitable media with FPRs.



**Fig. 6.** Spiral wave initiation due to an asymmetric FPR. The parameter  $A$  is fixed to  $A = 0.5 A_0$  everywhere except the circular region, where  $A = A_0 = 2$  (dense filling) and  $A = 0.75 A_0$  (rare filling). Snapshots of a wave propagating from left to right are shown. (A–F) The trajectories of two created spiral tips are shown by white solid and dotted lines in  $B$ – $F$ . One spiral tip disappears due to the collision with the medium's boundary (dotted line). The trajectory of the remaining spiral tip is shown in  $C$ – $F$  (white solid line).



**Fig. 7.** Dynamics of an initially planar wave propagating from left to right in a medium with a small-size FPR. The coupling strength  $D$  is fixed to  $D = 1$  everywhere except the central circular region of the radius  $R = 51$ , where  $D = D_0 = 2$  within the left part (dense filling) and  $D/D_0 = 2/3$  in the right part (rare filling).  $A = 1$  everywhere.

The mechanism requires a sufficiently steep increase of the propagation velocity, due to spatial variations of the parameter  $D$  and/or  $A$ . Please note that spatial variations of the excitation threshold  $\beta$  will not result in a wave break and thus the creation of spiral waves. Moreover, our numerical results clearly demonstrate that the existence of a propagation block strongly depends on the local curvature of the inhomogeneity boundary. In the special case of a straight boundary, the critical ratio  $D_c A_c / D_0 A_0$  is given by Eq. 10. With decreasing radius of the FPR, the critical ratio increases. This can be seen from the following numerical result: Let us assume that the parameter  $A$  is spatially homogeneous ( $A = 1$ ), but within the left part of the central circular shaped FPR  $D = D_0 = 2$ , while in the right one  $D/D_0 = 2/3$ . Everywhere else,  $D/D_0 = 0.5$ . If the radius of the inhomogeneity region is given as  $R = 90$ , an initially planar wave is stopped at its boundary, as shown in Fig. 3D. Nevertheless, for smaller  $R = 51$ , a planar wave penetrates into the FPR, and no spiral tips are created, as shown in Fig. 7.

In addition, as is well known for the case of obstacles, our findings carry over to three dimensions, where the FPRs can nucleate scroll waves (or rotors), which are a 3D version of spirals. In this situation, of course, geometry and inhomogeneity structure will also be very important, just as they are in two dimensions.

Let us stress again that the exemplary shown phenomena are truly generic. In the simulations, the shape and size of the chosen FPR can easily be extended to other geometry and other structured inhomogeneity. The fundamental and generic properties reported remain the same.

The FPR mechanism also represents an important generic correction to the commonly accepted notion that at least two stimuli are needed to create spiral waves in an excitable medium (15–17). Our analysis emphasizes the important role of the FPR as the nucleation center for reentry in contrast to the common expectation that a wave break occurs at the boundary between an excitable and unexcitable region. Please note that a possibility to initiate a permanent reentry activity after a single stimulation was also demonstrated in a much less generic reaction–diffusion system (29, 30) and in a strongly anisotropic 2D tissue (31, 32). In a medium with a nonlocalized inhomogeneity, a creation of a drifting spiral wave, which disappears after several rotations, has been reported (25).

The proposed mechanism for an initiation of a well-developed and permanently rotating spiral wave represents an alternative to the scenarios mentioned above. Because of its simplicity and generality, it can be realized in quite different excitable media.

**Relevance to Ablation Procedures in Medicine.** The spiral wave dynamics illustrated by Fig. 4 resembles many features of the electrophysiological excitation dynamics observed during atrial fibrillation (13, 14). Indeed, it is well known that atrial fibrosis in the aging heart can lead to spatial variations in the electrical conductivity of the functional syncytium, comprising interconnected

cardiomyocytes embedded in a variably sized nonconducting extracellular matrix (33). This can decrease the conductivity of a part of the cardiac muscle, and it is reasonable to assume that some regions within this part remain unchanged. These high-conductivity regions resemble the FPRs in our model. These FPRs can cause malignant electric activity. As shown in our theoretical examples, the single spiral pinned at the FPR can determine the dynamics, because it would have a faster period than the wave trains produced by the pacemaker. This then would lead to the destruction of the cardiac rhythm and would be identified by a cardiologist as cardiac tachycardia or fibrillation.

Of course, the structure of a real atrial tissue is much more complicated than the very general model description considered above. In the modern literature, the Fenton–Karma (FK) model (34, 35) is widely used to simulate electrical activity in atrial tissue in more detail (35, 36). To validate the applicability of our findings, the simulations with the FK model have been performed and are shown in *SI Text*. These data not only reproduce all scenarios obtained above with the Barkley model, but also open new possibilities for self-sustained reentry creation (see Figs. S1–S3). It is shown that for the chosen parameter set of the FK model, the propagation block is achievable at the relatively strong inhomogeneity, which is, however, not unusual for cardiac tissue (36–38).

Note that a variety of cardiac disease processes can cause ion-channel remodeling, in particular, resulting in a variation of the ion current density (28). This remodeling can be simulated in the framework of our model as a variation of the parameter  $A$ . It is natural to assume that, in a living organism, this remodeling can occur not uniformly in space, and one can expect the existence of some spots with relatively small remodeling or even remodeling-free regions. Thus, the ion-channel remodeling is also able to create FPRs and can cause spiral wave creation.

In the context of the proposed mechanism, one can assume that the self-sustained electric activation pattern is due to a spiral wave pinned to a FPR. Hence, a FPR would be identified as the spiral wave core region in this measurement (13, 14). This could be clinically validated by the measurement of the coupling strength within the spiral core and in the surrounding tissue. By destroying the spiral core region (i.e., by completely suppressing propagation in this area), the FPR would be transferred to a real obstacle, where the Wiener–Rosenbluth mechanism would act. This mechanism, however, is less likely to produce reentry, and thus the probability for spiral wave initiation should be significantly reduced. What we described above provides a mechanistic underpinning of the recently clinically introduced local ablation procedure terminating atrial fibrillation (13, 14).

We believe that the FPR mechanism also has important consequences for the understanding of the effects of surgical treatment on epilepsy in the human brain (39). There are already direct experimental measurements indicating the existence of true spiral waves of cortical neuronal activities, which may provide a spatial framework to organize cortical oscillations (4). The discovered mechanism can be one possible reason for a spontaneous spiral wave creation. Like in the case of the cardiac tissue, the necessary conditions for spiral wave initiation can be created by variations of the coupling strength or ion-channel density due to different disease processes.

In conclusion, this study may have important consequences for the treatment of malignant electrical activities in the heart and brain. The generic mechanism presented here remains, of course, to be investigated in more detail.

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