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Evaluation of Frequency Domain Analysis of Multiwavelength Photoacoustic Signal for differentiating Malignant from Benign and Normal prostate in an Ex-vivo study with human prostates

Saugata Sinha, PhD*,1, Navalgund A. Rao, PhD1, Bhargava K. Chinni, MS2, and Vikram S. Dogra, MD2

¹Rochester Institute of Technology, 1 Lomb memorial Drive, Rochester, NY, USA 14623

²University of Rochester, 601 Elmwood Avenue, Rochester, NY, USA 14642

Abstract

Objectives—The purpose of this study was to investigate the feasibility of differentiating malignant prostate from benign prostatic hyperplasia (BPH) and normal prostate tissue by performing frequency domain analysis of photoacoustic images acquired at 2 different wavelengths.

Methods—We performed multiwavelength photoacoustic imaging on freshly excised human prostate specimens taken from a total of 30 patients undergoing prostatectomy for biopsyconfirmed prostate cancer. Histologic slides marked by a genitourinary pathologist were used as ground truth to define regions of interest (ROIs) in the photoacoustic images. Primarily, 3 different prostate tissue categories, namely malignant, BPH, and normal, were considered, while a fourth category named nonmalignant was formed by combining the ROIs corresponding to BPH and normal tissue together. We extracted 3 spectral parameters, namely slope, midband fit, and intercept, from power spectra of the radiofrequency photoacoustic signals corresponding to the 3 primary tissue categories.

Results—We analyzed data from 53 ROIs selected from the photoacoustic images of 30 patients. According to the histopathologic analysis, 19 ROIs were malignant, 8 were BPH, and 26 were normal. All the 3 spectral parameters and C-scan grayscale photo - acoustic image pixel values were found to be significantly different (P<.01) between malignant and normalignant prostate as well as malignant and normal prostate.

Conclusions—Preliminary results of our ex vivo human prostate study suggest that spectral parameters obtained by performing frequency domain analysis of photoacoustic signals can be used to differentiate between malignant and nonmalignant prostate.

Keywords

Frequency domain analysis; genitourinary ultrasound; multiwavelength; photoacoustic imaging; power spectrum; prostate cancer

^{*}Corresponding Author information: Saugata Sinha, PhD., Mailing Address: TA 36, VNIT Campus, South Ambazari Road, Nagpur, Maharashtra, India, Pin: 440010, Rochester, NY, USA 14642, Telephone: 91-8806120222, saugata.sinha@ece.vnit.ac.in.

INTRODUCTION

For American men, prostate cancer is the second leading cause of cancer-induced death, preceded by lung cancer. The American Cancer Society estimated that in the United States for the year 2015, about 220,800 new cases of prostate cancer would be diagnosed, with about 27,540 deaths. Typically, screening for the presence of prostate cancer is performed by checking prostate specific antigen levels and conducting a digital rectal examination. Persistent elevated prostate-specific antigen levels and suspicious lesions felt on the digital rectal examination often lead to transrectal ultrasound (US)-guided biopsy. Due to the isoechoic nature of approximately half of prostate cancer lesions and the similar appearances of some commonly occurring nonmalignant and malignant prostate conditions on US images, transrectal US has poor sensitivity for detecting prostate cancer. Prostate biopsies under transrectal US guidance are now largely systematic, with many popular schemes in use, and even with these procedures, there is a more than 30% chance of a misleading diagnosis because of sampling errors.

To increase the sensitivity of transrectal US, ultrasoundbased techniques that can be easily integrated with the available technology to produce coregistered images have been investigated. Notable examples are contrast-enhanced US and real-time elastography, but they also could not improve the prostate cancer—detecting sensitivity to a reasonable level. ^{2,5,6} Other imaging modalities, including magnetic resonance imaging, computed tomography, and positron emission tomography, have demonstrated limited use in the detection of prostate cancer and are primarily reserved for the evaluation and staging of advanced cancer. ^{7,8} Clearly there is a need for a new imaging technique that accurately detects prostate cancer with high sensitivity.

Photoacoustic imaging promises to become a valuable tool in many clinical areas where there are unmet needs, as evidenced by several review articles. ^{9–11} Photoacoustic imaging, which is based on the photoacoustic effect, is a hybrid noninvasive soft tissue imaging modality. The generation of a US wave by a light-absorbing material after the absorption of laser light is known as the photoacoustic effect. Inside the absorbing material, the absorbed light energy produces localized heating and subsequent rapid thermal expansion, which in turn produces an increase in pressure. This increased pressure is released in the form of broadband US waves, also known as photoacoustic waves. 12 The photoacoustic wave depends on the absorbed light energy, which in turn depends on the product of the local optical absorption coefficient and the local exposure of optical energy in the tissue. ¹³ Thus, photoacoustic image depicts the spatially varying optical absorption property of the tissue, provided the tissue is uniformly illuminated. Being a hybrid imaging modality, photoacoustic imaging retains some of the specific advantages of both the pure optical as well as US imaging modalities. As the variation of the optical absorption property is more pronounced than the weak echogenicity of the soft tissues, photoacoustic imaging can be used more efficiently than US imaging for tissue differentiation. At the same time, as with pure US imaging, it provides good spatial resolution at a considerable depth inside the tissue, in contrast with pure optical imaging, in which the resolution degrades substantially with increasing depth. ^{12,14} Photoacoustic imaging can depict the optical absorption property of tissue constituents up to a few centimeters deep with submillimeter resolution. ¹⁵

The tissue and its major constituents (water, oxyhemoglobin, and deoxyhemoglobin in blood, lipid, fat, melanin, collagen, etc) have widely varying absorption spectra¹⁰ in the near-infrared region that not only provide abundant contrast features but also open the door for photoacoustic imaging-based spectroscopy with multiwavelength photoacoustic imaging. In the case of multiwavelength photoacoustic imaging, different photoacoustic images of the same tissue sample are acquired by using different wavelengths of a tunable laser. Generally, the wavelengths are chosen in such a manner that each wavelength corresponds to the peak of the absorption spectrum of a particular light absorbing tissue constituent. The spectroscopic application of photoacoustic imaging lies in determination of the concentration of specific chromophores present in the tissue, which can be further used for functional imaging as well as noninvasive tissue characterization. ^{15,16} Laufer et al ¹⁷ determined the blood oxygen saturation in a cuvette from photo-acoustic spectra taken at multiple wavelengths in the range of 740 to 1040 nm. Allen et al 18 performed spectroscopic photoacoustic imaging of human arterial tissue ex vivo to demonstrate the feasibility of detecting the presence of lipid in human aorta. Zhang et al¹⁹ measured dynamic blood oxygen saturation variation under different physiologic states from photoacoustic microscopic data acquired in vivo on Sprague Dawley rats.

Quantitative reconstruction of the chromophore concentration or optical absorption property of soft tissue from the multiwavelength photoacoustic image pixels is very difficult, as the pixel values depend on several factors, such as the optical absorption and scattering inside the tissue and frequency-dependent acoustic attenuation. Although there are several methods proposed by different research groups for quantitative recovery of the absorption property and chromophore concentration, some of the methods can be applied to only specific cases: ie, their application is limited by the assumption on which they have been built, whereas the more general methods have been tested only in simulation.²⁰ An alternative approach for tissue characterization using photoacoustic data is analysis of the photoacoustic frequency spectrum, as it carries valuable information about the shape and size of the photoacoustic absorbers. 13 Frequency domain analysis, in which spectral parameters, namely slope, midband fit, and intercept, are extracted from the power spectra of the time dependent signals within the usable bandwidth, is a widely used technique in pulse-echo US imaging for tissue characterization. ^{21,22} Application of this technique on photo -acoustic image data is more recent. Using frequency domain analysis on a high-frequency photoacoustic signal generated by ex vivo ocular tissue, Silverman et al²³ found that spectral slope and midband fit parameters were higher around the iris pigment epithelium. Kumon et al²⁴ implemented a frequency domain analysis technique in an in vivo photoacoustic imaging study with a prostate cancer murine model involving 7 rats, and they showed that midband fit and intercept parameters were significantly different between malignant and normal tissue regions. In a phantom study, slope values corresponding to 2 different-diameter microsphere distributions were shown to be significantly different from each other by Yang et al. 25 In a simulation study, a series of hypotheses relating the size and distribution of the spherical photoacoustic absorbers to extracted photoacoustic spectral parameters was derived by Xu et al, ²⁶ and they validated those hypotheses using a phantom study. Hysi et al²⁷ studied the change in photo acoustic spectral parameters with the change in red blood cell aggregation and oxygenation using an experimentally acquired photoacoustic signal generated by

porcine red blood cells along with a Monte Carlo-based theoretical model. In a phantom study with microspheres, Chitnis et al²⁸ investigated the effect of effective absorber size extracted from the high-frequency photoacoustic spectrum, slope, and midband fit on the mean absorber diameter of the microspheres. Xu et al²⁹ performed ex vivo as well as in situ experiments on mouse models to investigate the feasibility of differentiating fatty liver from normal liver using photo-acoustic spectral parameters. This article presents the results of a large-scale study of frequency analysis of photoacoustic signal data collected from biopsy-proven ex vivo prostate tissue samples. Although the frequency domain analysis is not entirely independent of light absorption and scattering inside the overlying tissue, we postulate that it may provide additional information about the dimensions of photo-acoustic absorbers, and that information may be used to differentiate different pathologic tissue types.

MATERIALS & METHODS

Before proceeding with the study, approval from the Institutional Review Board was obtained, along with consent from each patient. This study was in compliance with the Health Insurance Portability and Accountability Act. This experimental study consisted of frequency domain analysis performed on 3-dimensional (3D) photoacoustic data generated by freshly excised human prostate specimens collected from patients undergoing prostatectomy for biopsy-confirmed prostate cancer. The objective of the study was to verify the feasibility of differentiating among malignant prostate tissue, benign prostatic hyperplasia (BPH), and normal prostate tissue using frequency domain analysis of the 3D photoacoustic data. Although the experimental protocol and the experimental setup for acquiring photoacoustic data generated by the excised human prostate specimens were described in some of our earlier reports, ^{30–32} here those things are described in a concise way for the sake of completeness and continuity.

Figure 1 shows the ex vivo photoacoustic imaging system developed in our laboratory. We used acoustic lensfocusing based transillumination geometry. In this setup, the light source and US transducer are placed on the opposite sides of the tissue specimen, and the acoustic lens focuses the photoacoustic wave on the transducer array. Figure 1A shows the concept behind our acoustic lens—based focusing approach. Once the prostate specimen was illuminated with a pulsed laser beam, the light-absorbing tissue constituents absorbed laser light and emitted photo - acoustic waves, which traveled in all directions. The portions of the photoacoustic waves collected by the acoustic lens were focused by the lens on the transducer array. To achieve unit magnification, the object distance (ie, the distance between the acoustic lens and the object plane) and the image distance (ie, the distance between the acoustic lens and the transducer array) were made equal to twice the focal length of the acoustic lens.

Figure 1B shows the actual ex vivo photoacoustic imaging setup developed in our laboratory. The adjustable laser arm holds the fiber bundle, which delivers the pulsed laser light from the tunable laser (wavelength, 700–1000 nm; pulse repetition frequency, 10 Hz; pulse duration, 5 nano - seconds; Ekspla, Vilnius, Lithuania) on the tissue sample holder. Although the physical dimensions of the sample holder allow it to accommodate tissue samples up to 4 cm thick, the maximum depth at which actual photoacoustic imaging can be performed

inside the tissue is much less than 4 cm. The water-sealed cylinder suspended on the sample holder contains the custom-designed acoustic lens (focal length, 39.8 mm; diameter, 32 mm) and the 32 element 1-dimensional (1D) US transducer array (center frequency, 5 MHz; bandwidth, 60%; pitch, 0.7 mm; elevation, 1 mm; Olympus NDT, State College, PA). During photoacoustic imaging, both the cylinder and the sample holder were filled with saline water. The fiber bundle carrying arm and the cylindric container are attached to each other, and together they are referred to as the photoacoustic camera. The depth of the field of the lens is approximately ±0.5 cm around the focal plane. Figure 1A shows that if we receive the signal at each of the 32 elements of the 1D transducer array over a sufficiently long time gate and then map the corresponding arrival times to distances, then we will get 32 adjacent 1D radiofrequency photoacoustic signals or A-line photoacoustic signals, which can be further processed to produce a focused B-scan image representing a particular sagittal plane. To acquire photoacoustic data generated by an excised prostate specimen, the specimen was held stationary by the sample holder, and using dual-axis linear stepper motors, the photoacoustic camera raster scanned the specimen to acquire a set of photoacoustic A-line signals over a long time gate. A C-scan image (ie, image representing a particular crosssectional plane) was formed by using the mean of each envelope-detected photoacoustic Aline signal over a small time gate. The transducer array is connected to a custom-designed data acquisition system (Apcon, Rochester, NY) to digitize and store the photoacoustic radiofrequency signals in the computer. We used our own MATLAB-based software (version 2012a; The MathWorks, Inc, Natick, MA) to form different C- or B-scan images from the stored photoacoustic data set.

Theoretically, the point spread function of the photo- acoustic imaging system can be expressed as convolution of the acoustic lens point spread function and transducer point spread function. We experimentally determined the point spread function of the photoacoustic system in the XZ plane using a lead pencil of 0.2 mm in diameter as target in a water bath. The pencil was placed perpendicular to the axis of the transducer array so that it behaved like a point source in the XZ plane. Figure 2 shows the experimental setup for measuring the point spread function of our ex vivo photoacoustic imaging probe. Here the lead pencil was placed in a water bath. Pulsed laser light from the tunable laser illuminated the pencil from the side. The probe was placed directly on top of the pencil in such a way that the pencil remained at a right angle to the X-axis or azimuth of the transducer array. The pencil was placed approximately below the center of the transducer array. The distance between the face of the probe and the pencil was kept very small (≈5 mm), so that an object distance approximately equal to twice the focal length of the acoustic lens could be maintained. Once the laser illuminated the pencil, it emitted a photoacoustic wave, which was focused by the acoustic lens on the transducer array. For determining the point spread function, an 800-nm wavelength for the tunable laser was used. Figure 3 shows the 2dimensional (2D) point spread function of the ex vivo photoacoustic imaging probe in the XZ plane. The full width half maximum values of the 2D point spread function along lateral and axial directions were 2.45 and 0.34 mm, respectively.

Photoacoustic imaging at multiple wavelengths was performed on freshly excised prostate specimens collected from patients undergoing prostatectomy for biopsy confirmed prostate cancer. Immediately after surgery, the excised prostate gland was sent to the surgical

pathology laboratory, where it was inked and cut into thin sections (2–5 mm thick and 2–4 cm wide) by a genitourinary pathologist. One such section with a grossly visible nodule was selected, immersed in normal saline to prevent dryness, and sent to our laboratory, where we acquired photoacoustic images of it at multiple wavelengths. Once photoacoustic imaging was done, the prostate specimen was returned to the surgical pathology laboratory for histopathologic analysis. The complete process of sectioning the excised prostate gland, acquiring the photoacoustic images, and then returning the specimen to the surgical pathology laboratory was finished within 1 hour after surgery. The specimen was verified and approved by the genitourinary pathologist to ensure that the histopathologic procedure on the prostate specimen was not compromised. The laser intensity on the excised prostate specimen was maintained at around 5 mJ/cm², which is well below the safe human exposure limit according to American National Standards Institute guidelines.³³

Originally, the photoacoustic imaging was performed at 5 different wavelengths. Among them, signals acquired at 2 different wavelengths were analyzed and are presented here. The original 5 wavelengths were chosen in such a way that each wavelength corresponded to the peak of the absorption spectrum of a particular chromophore in the 700- to 1000-nm wavelength range. Chromophores are the light-absorbing tissue constituents. Following are the pairs of selected wavelengths and chromophores with peak absorption at the selected wavelength: 760 nm, deoxyhemoglobin; 850 nm, oxyhemoglobin; 930 nm, fat; and 970 nm, water. 34–36 A wavelength of 800 nm was chosen, as at this wavelength, the absorption coefficients of both deoxyhemoglobin and oxyhemoglobin are equal. 15,35 Figure 4 shows the absorption spectra of 4 different chromophores in the 700- to 1000-nm wavelength range. As it can be seen from Figure 4, absorption spectra of fat and water are 1 order magnitude smaller than those of deoxyhemoglobin and oxyhemoglobin. Due to the small values of fat and water absorption spectra, we hypothesize that the photoacoustic signal acquired within the 700- to 1000-nm wavelength range would be primarily composed of the contributions from deoxyhemoglobin and oxyhemoglobin. Here, photoacoustic signals acquired only at 760 and 800 nm were analyzed as at these 2 wavelengths; absorption coefficients of deoxyhemoglobin and oxyhemoglobin were fairly high among the 5 wavelengths at which ex vivo photoacoustic images were acquired. The genitourinary pathologist performed a histopathologic analysis on each excised prostate specimen, which was imaged in our laboratory. The marked histologic slides were used as ground truth in this study. The scanned images of the marked slides were coregistered manually with the Cscan photoacoustic images of the specimens to identify the regions of interest (ROIs) corresponding to different pathologic tissue types.

Figure 5B shows the scanned histologic slide of the prostate specimen in Figure 5A. Two C-scan photoacoustic images, formed by using the photoacoustic data acquired at 760- and 800-nm wavelengths, are shown in Figure 5, C and D. In Figure 5, B–D, the ROIs corresponding to malignant prostate regions are shown by blue circles, whereas the adjacent normal prostate regions are shown by white circles.

Once ROI selection was completed, power spectra of the preprocessed and windowed photoacoustic A-line signals within the ROI were computed. In this step, the photoacoustic A-line signals were corrected for the wavelength dependent laser input intensity variation

using the input laser intensity measurements taken before each experiment. Then the wavelength-dependent attenuation of laser light during its propagation inside the tissue was corrected. The laser light gets attenuated while propagating through the tissue because of the optical absorption and scattering properties of the tissue. Using the Beer- Lambert law, 1D light attenuation was computed along the depth (Z-axis) inside the tissue for the 2 different wavelengths, and these computations were used to correct the photoacoustic A-line signals for the light attenuation at different depths inside the tissue:

$$\Phi_z = \Phi_0 \exp(\mu_{eff} z) \text{ where } \mu_{eff} = \sqrt{3\mu_a \left(\mu_a + \mu_s'\right)}$$
 (1)

Equation 1 represents the Beer-Lambert law used to compute the light attenuation inside the tissue along the depth. Here μ_{eff} , μ_{a} , and μ_{s}^{\prime} are the effective attenuation coefficient, absorption coefficient, and reduced scattering coefficient of the tissue, respectively. Φ_z and Φ_0 are the light fluence at depth z inside the tissue and at the surface of the tissue. The values of the effective optical attenuation at the wavelengths were calculated by using the corresponding values of $\mu_a,$ and $\mu_s{}^{\prime}$ as reported for human prostate. 37 The different values of μ_{eff} used here were 1.91 cm⁻¹ at 760 nm and 1.79^{cm-1} at 800 nm. Once these corrections were done, the photoacoustic A-line signals were time gated to small sections using a series of sliding Hamming windows. Each of the Hamming windows was 1 microsecond long. The power spectrum of each time-gated A-line photoacoustic signal was computed by calculating the square of the fast Fourier transform of the windowed signal. During windowing, 30% overlap between Hamming windows on successive segments of every Aline was used as a compromise between reducing truncation artifacts in the fast Fourier transform and minimizing overlap. Each computed power spectrum was divided by the 1way power spectrum of the transducer array to remove the artifacts due to the finite bandwidth of the transducer in the usable bandwidth. The usable bandwidth (2.4–7.4 MHz) is the frequency region within -10 dB of the peak of the 1-way power spectrum of the transducer array. The 1-way power spectrum of the transducer array was retrieved from the 2-way (pulse-echo) transfer function of the transducer array provided by the manufacturer. The calibrated power spectrum was converted to a decibel scale. Linear regression was performed to find the straight line best fit to the calibrated power spectrum in the usable bandwidth. The 3 spectral parameters, slope (decibels per megahertz), midband fit (decibels), and intercept (decibels), were extracted from each best-fit straight line. Figure 6 shows an example of the power spectrum analysis applied on a particular photoacoustic Aline signal. Figure 6A shows the C-scan photoacoustic image of the prostate specimen shown in Figure 5A. Each pixel in the C-scan image corresponds to a photoacoustic A-line signal. In Figure 6B, the photoacoustic A-line signal corresponding to the pixel marked by blue in Figure 6A is shown. Figure 6C shows the windowed photoacoustic signal obtained by applying a Hamming window on photoacoustic signal in Figure 6B. The Hamming window has the same length as that of the photoacoustic A-line signal. Figure 6D shows the normalized amplitude spectrum of the photoacoustic A-line signal along with the 1-way normalized amplitude spectrum of the transducer array. Figure 6E shows the best-fit straight line to the calibrated power spectrum of the A-line signal in the usable bandwidth along with

the calibrated power spectrum. The spectral parameters slope and intercept are the slope and intercept of the best-fit straight line, whereas the midband fit is the height of the straight line at 5 MHz (ie, the middle point in the usable bandwidth).

RESULTS

Thirty patients were involved in this study. Data from 53 ROIs were analyzed. According to the histopathologic analysis performed by the genitourinary pathologist, among the 53 ROIs, 19 were malignant, 8 were BPH, and 26 were normal. Another tissue category, named nonmalignant, was introduced here, and under this category all ROIs corresponding to normal and BPH tissue were combined.

Figure 7 shows 4 different bar plots where mean values of 4 different parameters corresponding to 3 different types of ROIs are plotted for the wavelengths of 760 and 800 nm. The 4 parameters consist of 3 spectral parameters and pixel values. The pixel values represent the values of the pixels in the C-scan photoacoustic images. The mean values were computed over the respective number of ROIs that were included in the study corresponding to malignant, BPH, and normal prostate tissue. On each bar representing the mean value of a particular parameter, the error bar represents the standard deviation of the corresponding parameter over the total number of photoacoustic A-lines belonging to the ROIs of a particular tissue type. The ROIs corresponding to BPH and normal prostate tissue are grouped into the nonmalignant category. Similar to Figure 7, the mean values of the 4 parameters corresponding to nonmalignant and malignant ROIs are plotted for both wavelengths in Figure 8.

A 2-sample, 2-tailed t test was performed with the parameter values to find out whether there was a statistically significant difference between the parameters corresponding to ROIs of different tissue types. Figure 9 shows the results of the t test performed at a 5% significance level with the values of the 4 parameters corresponding to malignant versus normal, malignant versus BPH, BPH versus normal, and malignant versus nonmalignant.

From Figure 9, it can be seen that between malignant and normal prostate tissue, all 4 parameters were significantly different (P < .05) at the 760 and 800 nm wavelengths. Between malignant prostate and BPH tissue, other than slope and pixel values at 800 nm and intercept at 760 nm, the remaining parameters were significantly different (P < .05) at both wavelengths. For BPH versus normal prostate, only the slope at 760 nm was not significantly different (P > .05) among the 4 different parameters at the different wavelengths. Between malignant and nonmalignant prostate, all 4 parameters at both wavelengths were significantly different (P < .05).

DISCUSSION

In this study, 2-sample, 2-tailed t tests were performed to test whether the parameters were significantly different for different tissue categories. For ease of discussion, each of the 4 parameters (slope, midband fit, intercept, and pixel value) at a particular wavelength is referred as a separate parameter. Therefore, for each pair of different tissue types, 2-sample, 2-tailed t tests were performed for 8 different parameters (4 parameters at 2 different

wavelengths). Primarily, 3 pairs of tissue types, namely malignant versus normal prostate, malignant versus BPH, and BPH versus normal prostate, are considered here. For malignant versus normal prostate tissue, 8 of 8 parameters were significantly different (P < .05). For malignant versus BPH, 5 of 8 parameters were significantly different (P < .05), whereas for BPH versus normal prostate, 7 of 8 parameters were significantly different (P < .05). Since the primary focus of this study was to differentiate malignant prostate tissue from other types of prostate tissue, a separate tissue category called nonmalignant was created by combining all of the normal as well as BPH ROIs, and a statistical analysis was performed to determine whether the 8 parameters were significantly different between the 2 different tissue categories. In this case, all 8 parameters were found to be significantly different between malignant and nonmalignant prostate tissue. As far as the number of significantly different parameters are concerned, it is evident that the frequency domain analysis in this study was most effective in differentiating malignant from normal prostate, whereas it was least effective in differentiating malignant prostate from BPH. The tissue-type pair malignant versus nonmalignant could be differentiated with equal effectiveness as tissuetype pair malignant versus normal, as for these pairs of tissue types, the number of significantly different parameters was 8.

As mentioned earlier, 3 different spectral parameters, namely slope, midband fit and intercept, were used in this study to differentiate between different tissue types. For tissue characterization using photoacoustic imaging, the typical practice is to form grayscale photoacoustic images from the amplitudes of the envelope-detected radiofrequency photoacoustic data.³⁸ Regions of interest corresponding to different tissue categories are compared by using the pixel values of the grayscale photoacoustic images. In this study, along with the spectral parameters, we tested whether the grayscale photoacoustic pixel values were significantly different between different tissue categories. When the performances of the parameters (slope, midband fit, intercept, and pixel value) were compared for differentiating between separate tissue categories, it was found that performance of midband fit was the best, as it was significantly different for all of the 4 tissue category pairs at both wavelengths. The corresponding Pvalues were very small also (maximum P = .0021; minimum P = 5.53×10^{-56}). Performances of both photoacoustic pixel value and intercept were in second place after midband fit, as both of these parameters failed to differentiate between a pair of different tissue categories once. The performance of slope came in at third place, as it failed to differentiate between a pair of different tissue categories thrice.

As mentioned earlier, in this study, frequency domain analysis was performed on photoacoustic signals acquired at 2 wavelengths: 760 and 800 nm. If the performance of frequency domain analysis is compared between the wavelengths, from Figure 9, it is evident that the performance at 800 nm was better than that at 760 nm. Between malignant and BPH prostate, both at 760 and 800 nm, 1 spectral parameter was not significantly different. Between normal and BPH prostate, all 3 spectral parameters were significantly different at 800 nm, whereas slope was not significantly different at 760 nm. As for the tissue pairs malignant versus normal and malignant versus nonmalignant, all 3 spectral parameters were significantly different at both 760 and 800 nm. Therefore, considering all 4

different tissue pairs, performance of frequency domain analysis for tissue characterization was better at 800 than at 760 nm.

Figures 7 and 8 show that the average photoacoustic pixel value corresponding to malignant tissue was greater than that of nonmalignant tissue. Generally, malignant tissue growth is associated with extra growth of blood vessels, ¹⁵ and this extra blood content, due to its high optical absorption property, produces photoacoustic signals with higher amplitudes than photoacoustic signals generated by normal tissue. It is also evident from Figures 7 and 8, that average values of midband fit and intercept corresponding to malignant tissue were also greater than that corresponding to normal tissue. As explained in the following section, both midband fit and intercept depend on the optical absorption property of the tissue constituents, which may be the reason why average values of theses parameters were greater for malignant tissue than normal tissue. On the other hand, slope is independent of the optical absorption property. Here, the average slope values corresponding to normal tissue were greater than that corresponding to malignant tissue.

Using the analytical expression for the time-dependent photoacoustic signal generated by spherical photoacoustic absorber, we can try to discuss the importance of the spectral parameters for tissue characterization:

$$p(t) = \left(\frac{\mu_a \beta c^2 E_0}{2C_p}\right) \left[1 - \frac{ct}{r_d}\right] \text{ for } \frac{r_d - r}{c} < t < \frac{r_d + r}{c}$$
 (2)

Equation 2 gives the analytical expression of the time dependent PA signal generated by a spherical PA absorber where μ_a , β and C_p represent optical absorption coefficient, isobaric volume expansion coefficient and heat capacity per unit mass of the absorber, while c and E_0 represent the velocity of PA wave inside the absorber and input laser fluence received by the absorber. Radius of the absorber and the distance between the observation point and the center of the absorber are represented by r and r_d . The time dependent PA amplitude is represented by p(t). The amplitude spectrum of the PA signal can be found out by taking Fourier transform of Equation 2.

$$P(f) = \left(\frac{\mu_a \beta c^2 E_0}{2C_p}\right) \left(\frac{r^2}{cr_d}\right) \left\{\frac{\left(\frac{2\pi fr}{c}\right) \cos\left(\frac{2\pi fr}{c}\right) - \sin\left(\frac{2\pi fr}{c}\right)}{\left(\frac{2\pi fr}{c}\right)^2}\right\} \tag{3}$$

Equation 3 represents the amplitude spectrum of the photoacoustic signal generated by a spherical absorber, where P(f) represents the amplitude spectrum of the timedependent photoacoustic signal.

The power spectrum of the photoacoustic signal in dB scale is given by Equation 4:

$$p_{dB} = 20 \log_{10} P(f)$$
 (4)

Combining Equations 3 and 4, a more elaborate expression for the power spectrum of the photoacoustic signal, represented by Equation 5, can be obtained:

$$20 \log [P(f)]$$

$$=20 \log \left[\left(\frac{\mu_a \beta c^2 E_0}{2C_p} \right) \left(\frac{r^2}{cr_d} \right) \left\{ \frac{\left(\frac{2\pi fr}{c} \right) \cos \left(\frac{2\pi fr}{c} \right) - \sin \left(\frac{2\pi fr}{c} \right)}{\left(\frac{2\pi fr}{c} \right)^2} \right\} \right]$$

$$=20 \log [\mu_a]$$

$$+20 \log [r^2]$$

$$+20 \log [A]$$

$$+20 \log [B]$$

$$+20 \log [g(f)]$$
(5)

Where

$$A = \frac{\beta c^2 E_0}{C_p}, \ B = \frac{1}{c r_d}, \ g\left(f\right) = \left\{\frac{\left(\frac{2\pi f r}{c}\right) \cos\left(\frac{2\pi f r}{c}\right) - \sin\left(\frac{2\pi f r}{c}\right)}{\left(\frac{2\pi f r}{c}\right)^2}\right\}$$

Now, for computing the spectral parameters, the right side of Equation 5 is fitted to a straight line, and the slope, intercept, and midband fit are extracted from the straight line. It is evident that slope only depends on log[g(f)], as the remaining terms of Equation 5 are independent of frequency; thus, slope is independent of the absorption coefficient μ_a of the absorber. Intercept is determined by the frequency-independent terms: ie, $\log[\mu_a]$ and $\log[r^2]$. Along with $\log[g(f)]$, midband fit depends on $\log[\mu_a]$ and $\log[r^2]$. As slope is independent of the absorption property and only depends on the dimension of the absorber, it is generally regarded as the most useful among the 3 spectral parameters for providing information about the size of the absorber and consequently differentiating between different pathologic tissue types, assuming absorber size changes with the tissue type. According to Equation 2, the photoacoustic pixel values of a grayscale photoacoustic image are generally considered to be dependent on the absorption coefficient of the tissue but independent of the absorber diameter. Therefore, for tissue characterization, midband fit and intercept parameters may be regarded as superior to the photoacoustic pixel value because of their combined dependence on both the absorption coefficient and absorber diameter through the terms $\log[\mu_a]$ and $log[r^2].$

In this study, we performed experiments with freshly excised human prostate samples. Although the potential for tissue differentiation has been demonstrated ex vivo, we believe it can be extended to in vivo situations also but with certain caveats. For an in vivo study, the corresponding photoacoustic spectral parameters may change from those of the ex vivo study because of the changes in tissue physiologic characteristics and the presence of overlying tissue on the ROI. Due to the optical scattering and absorption properties, the overlying tissue substantially affects the input laser fluence, which in turn affects the photoacoustic signal generated by the ROI. For our experimental study, we incorporated a

1D model to correct for the wavelength dependent laser light attenuation inside the tissue. Since we performed experiments with thin excised tissue specimens, the 1D correction model is sufficient. For an in vivo study, however, a detailed 2D or 3D model-based optical inversion scheme^{20,39} may be required to correct for the effect of the overlying tissue on the input laser fluence. For in vivo human prostate imaging, instead of transillumination mode photoacoustic imaging, reflection mode photoacoustic imaging has to be implemented. In that case, noninvasive laser light delivery to the human prostate is always a challenge.^{40,41} As mentioned earlier, an elaborate data correction scheme has to be implemented for in vivo prostate imaging to correct for the nonuniform laser illumination caused by the overlying tissue. This study was limited to an analysis of photoacoustic signal frequencies in the range of 2.4 to 7.4 MHz. This range is compatible with what is used in clinical US imaging, and we believe this limitation will also apply to clinical photoacoustic imaging.

In conclusion, we can say that the results of this experimental study indicate that the spectral parameters as well as the photoacoustic pixel values extracted from 3D photoacoustic data generated by freshly excised human prostates can differentiate malignant prostate tissue from BPH as well as normal prostate tissue.

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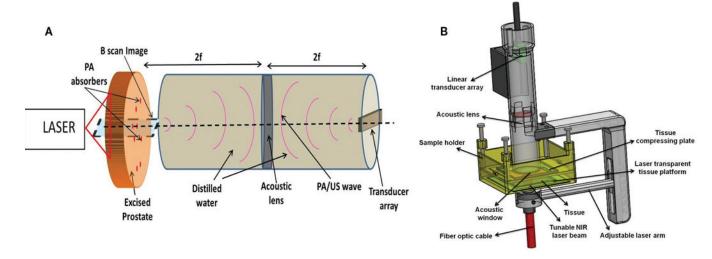


Figure 1. Ex vivo photoacoustic (PA) imaging system. A, Acoustic lens focusing-based photoacoustic image acquisition approach. B, The actual photoacoustic imaging probe with the tissue sample holder.

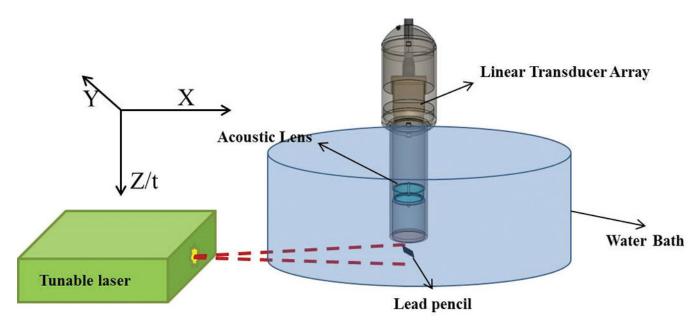


Figure 2. Experimental setup for measuring the point spread function in the XZ plane.

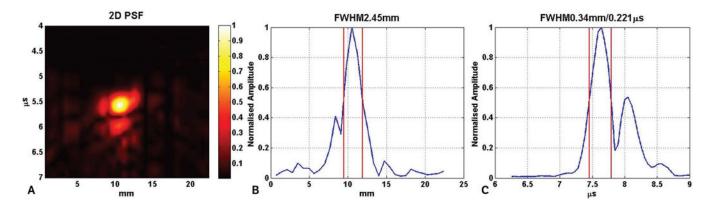


Figure 3.

A, Two-dimensional point spread function (PSF) of the ex vivo photoacoustic imaging probe in the XZ plane. B, Lateral cut (along azimuthal/X-axis) of the 2D point spread function in A. C, Axial cut (along time/Z-axis) of the 2D point spread function in A. The pair of red lines in B and C show the full width half maximum (FWHM) along the lateral and axial directions. The lateral full width half maximum is 2.45 mm, whereas the axial full width half maximum is 0.34 mm.

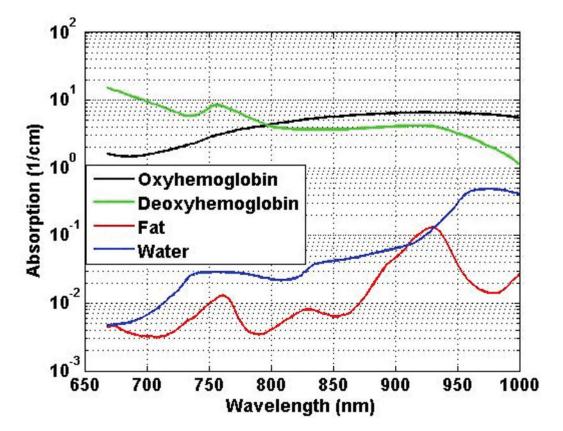


Figure 4. Absorption spectra of different chromophores in the 700- to 1000-nm wavelength range. 36

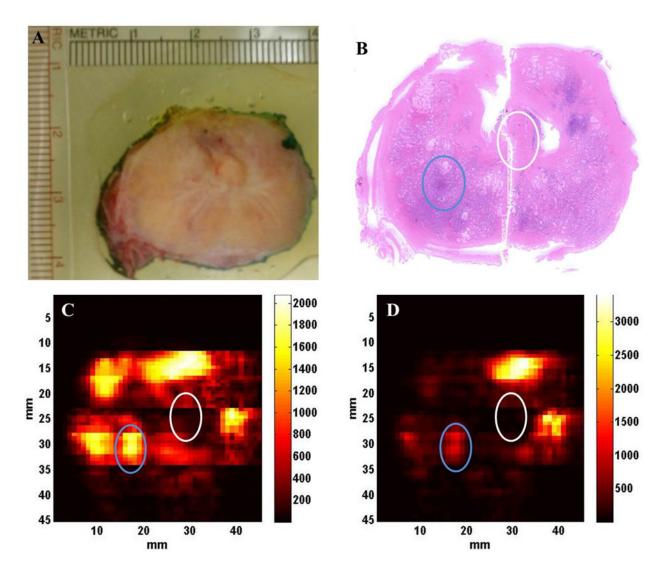


Figure 5.C-scan photoacoustic images of a freshly excised human prostate tissue sample taken at 2 different wavelengths. A, Prostate tissue sample. B, Histologic slide of the prostate tissue sample. C, Photoacoustic image at 760 nm. D, Photoacoustic image at 800 nm. Regions of interest corresponding to the malignant prostate are marked by the blue circles, whereas the adjacent normal ROIs are marked by the white circles in B, C, and D.

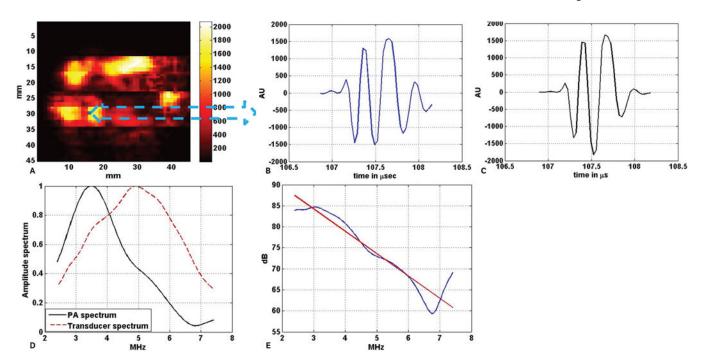


Figure 6.

Example of power spectrum analysis on a single photoacoustic A-line signal. A, C-scan photoacoustic image of the excised prostate specimen shown in Figure 5A. B, Photoacoustic A-line signal generated by the tissue corresponding to the blue pixel in A. C, Windowed photoacoustic signal: ie, the photoacoustic signal in B was multiplied with a Hamming window of the same length. D, Amplitude spectrum of the windowed photoacoustic (PA) A-line signal along with the 1-way amplitude spectrum of the transducer (both normalized) in the useable bandwidth region (2.4–7.4 MHz). E, Calibrated power spectrum fitted to the linear model. The red line in E is the best fit straight line to the power spectrum of the windowed photoacoustic A-line, which is shown by the blue line. AU indicates arbitrary unit.

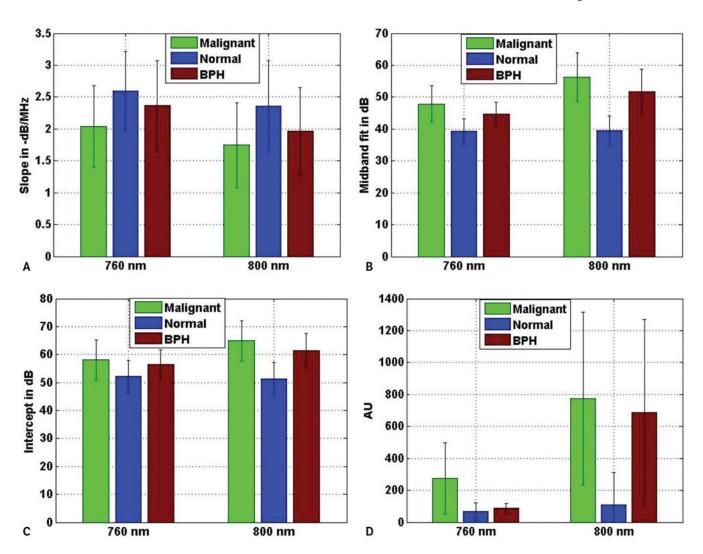


Figure 7.

Average values of slope (A), midband fit (B), intercept (C), and photoacoustic pixel (D) corresponding to different tissue types at 2 different wavelengths. The error bars are the standard deviations of the corresponding parameters over the ROIs belonging to particular tissue types. AU indicates arbitrary unit.

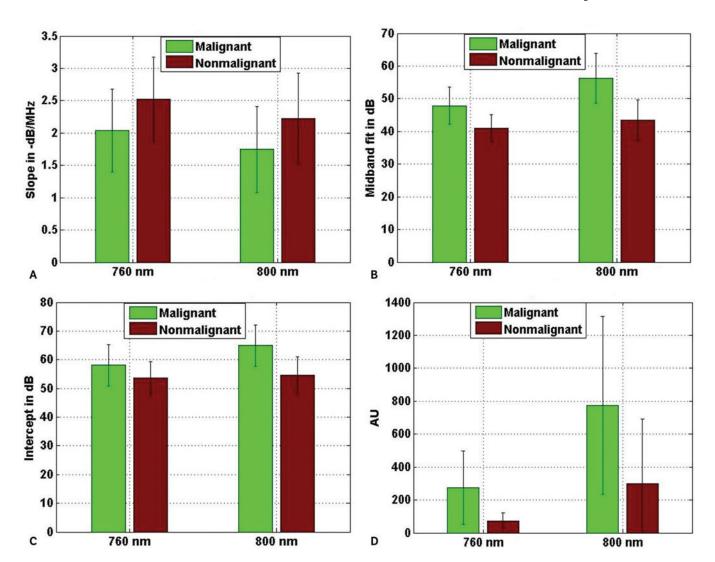


Figure 8.Average values of slope (A), midband fit (B), intercept (C), and photoacoustic pixel (D) corresponding to different tissue types at 2 different wavelengths. The error bars are the standard deviations of the corresponding parameters over the ROIs belonging to particular tissue types.

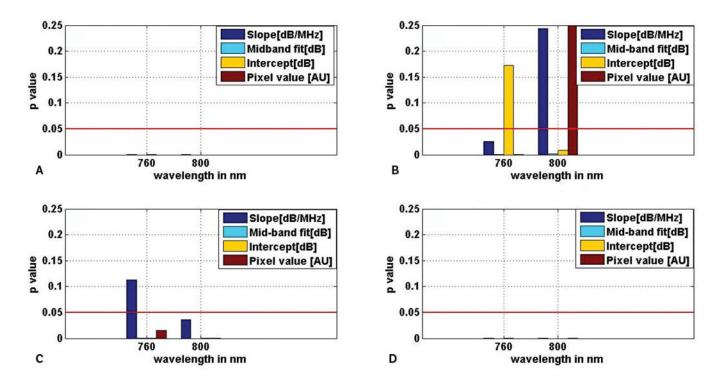


Figure 9. Comparison of spectral parameters between different prostate tissue types: malignant versus normal (A), malignant versus BPH (B), BPH versus normal (C), and malignant versus nonmalignant (D), using a 2-sample, 2-tailed t test. The red lines show the levels corresponding to the decision criterion (P = .05).