

FIFTY YEARS OF RESEARCH IN ARDS

V_T Selection in Acute Respiratory Distress Syndrome

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Abstract

Mechanical ventilation (MV) is critical in the management of many patients with acute respiratory distress syndrome (ARDS). However, MV can also cause ventilator-induced lung injury (VILI). The selection of an appropriate V_T is an essential part of a lung-protective MV strategy. Since the publication of a large randomized clinical trial demonstrating the benefit of lower V_Ts, the use of V_Ts of 6 ml/kg predicted body weight (based on sex and height) has been recommended in clinical practice guidelines. However, the predicted body weight approach is imperfect in patients with ARDS because the amount of aerated lung varies considerably due to differences in inflammation, consolidation, flooding, and atelectasis. Better approaches to setting V_T may include limits on end-inspiratory

transpulmonary pressure, lung strain, and driving pressure. The limits of lowering V_T have not yet been established, and some patients may benefit from V_Ts that are lower than those in current use. However, lowering V_Ts may result in respiratory acidosis. Tactics to reduce respiratory acidosis include reductions in ventilation circuit dead space, increases in respiratory rate, higher positive end-expiratory pressures in patients who recruit lung in response to positive end-expiratory pressure, recruitment maneuvers, and prone positioning. Mechanical adjuncts such as extracorporeal carbon dioxide removal may be useful to normalize pH and carbon dioxide levels, but further studies will be necessary to demonstrate benefit with this technology.

Keywords: acute respiratory distress syndrome; tidal volume; mechanical ventilation

Mechanical ventilation (MV) is critical for survival of many patients with acute respiratory distress syndrome (ARDS). However, MV can also cause ventilation-induced lung injury (VILI), which can exacerbate or perpetuate injury from the original cause of ARDS, such as pneumonia, sepsis, or trauma (1–5). One mechanism of VILI is overdistention of aerated lung tissue (6). Patients with ARDS are especially vulnerable to this, because the volume of aerated lung available for ventilation is reduced greatly in some patients. Therefore, a V_T that might be gentle and harmless in a normal subject may cause serious injury from overdistention in patients with ARDS. To prevent or reduce VILI from

overdistention, we usually use V_Ts that are substantially smaller than those that were used in the past, before the potential for VILI from overdistention was recognized (7, 8).

Setting V_T is an important part of MV management of patients with ARDS. Several approaches for adjusting V_T to prevent VILI have been suggested. In this review, we explain the rationale behind different methods, review data that support them, and comment on certain practical aspects of setting V_T for patients with ARDS. This discussion is written with the assumption that the ventilator mode allows direct control over V_T, as with the volume-assist/control mode, or indirect control, as

with pressure-assist/control mode in patients who are not making respiratory efforts. Moreover, additional considerations are needed when patients are making spontaneous inspiratory efforts even when on controlled modes of ventilation. The risks and management of spontaneous breathing during mechanical ventilation have been expertly reviewed recently (9).

Volume-Control versus Pressure-Control Modes

In volume-assist/control modes, depending on the patient's respiratory system compliance, the resulting inspiratory

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alveolar pressure may be low, intermediate, or high. If it is too high, the clinician may reduce the set V_T . With a mode that allows direct control of the pressure during inspiration, as with the pressure control mode, the V_T that results from the inspiratory pressure increment depends on the magnitude and duration of the increment and a patient's respiratory system compliance (lung and chest wall combined) and airway resistance. The pressure control increment and duration can be adjusted if the initial V_T is not at the desired volume. Some modes, such as pressure-regulated volume control and autoflow, allow control over the V_T if the patient has no respiratory efforts. However, control over V_T is lost in these modes when patients begin to make spontaneous respiratory efforts (9).

Pressure and volume are inextricably entwined according to each patient's respiratory system pressure-volume relationship. Therefore, theoretically we can achieve the same V_T and airway pressure pattern of ventilation with either mode. The choice of modes is usually dictated by clinicians' experiences and preferences. Some prefer the pressure-control mode because they can set the pressure during inspiration to a level that they think is safe. This may have some merit when patients are passive, not making any efforts to breathe. However, if patients make inspiratory efforts in the pressure-control mode, the resulting V_T s can be large even though the airway pressure is not high, causing substantial overdistention (10, 11). Thus, one advantage of the volume-control mode is that we have better control over V_T s. A disadvantage of the volume-control mode is that the inspiratory flow is preset. In patients who have a high inspiratory drive, the flow setting may result in frequent double breaths, which can cause VILI from overdistention. (Figure 1). Nevertheless, although the volume- and pressure-control modes are very different, current data do not show any difference in clinical outcomes between the modes (11).

Methods for Setting V_T

Setting V_T according to Body Weight

A historical approach set V_T s according to actual body weight. Larger patients generally have larger lungs, so patients with larger lungs would usually receive larger

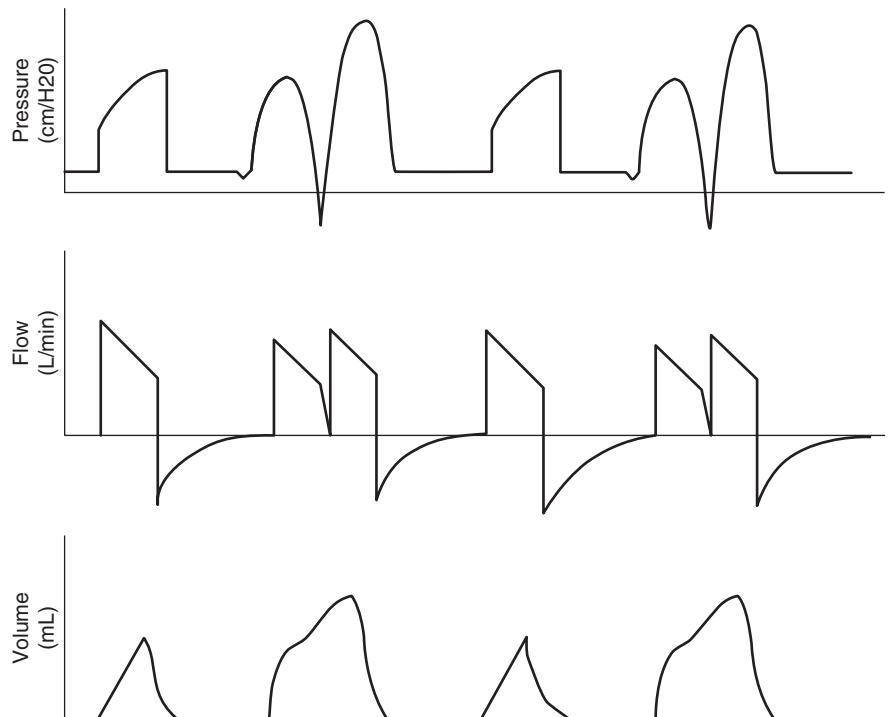


Figure 1. Patient-ventilator dyssynchrony with triggering of double breaths from the ventilator in volume-assist control mode. The *first channel* demonstrates airway pressure with a normal breath followed by a double breath triggered by the patient. The *second channel* shows flow during a normal breath followed by a double breath. Patient inspiratory effort continues beyond the set ventilator inspiratory time, resulting in airway pressure decreasing below the positive end-expiratory pressure and triggering a second breath during the same patient effort. This may result in high lung pressures (during the double breath: *top panel*) and high volumes. The *third channel* demonstrates increased volumes during double-triggered breaths. If patients consistently trigger double breaths, they will not be receiving low V_T s for lung protection during the double breaths and are at increased risk for overdistention.

V_T s. In a comprehensive review of acute respiratory failure in adults from 1972, the authors recommended generous V_T s of 10 to 15 ml/kg (7). There were two problems with this recommendation. First, although lung size correlates with body weight, body weight varies substantially between patients because of differences in adipose tissue, muscle mass, and extravascular fluid, independent of lung size. Second, these large V_T s would tend to cause VILI from overdistention in patients at risk for or with established ARDS.

Four randomized clinical trials of traditional, generous V_T s versus lower V_T s in patients with or at risk for ARDS used estimations of lean body weight to set V_T s (12–15). One trial used an equation for “ideal body weight” that did not account for variations in lung size according to sex (13). Two of the trials used equations for “predicted body weight” (PBW) that accounted for both sex and height (14, 15):

$$\text{female PBW (kg)} = 45.5 + 0.91 \text{ (cm of height} - 152.4)$$

$$\text{male PBW (kg)} = 50 + 0.91 \text{ (cm of height} - 152.4)$$

Several subsequent clinical studies and randomized trials used PBW to set V_T s (16–20), and some clinical guidelines recommended this approach (21, 22).

According to the National Institutes of Health ARDS Network protocol, the goal for V_T s is 6 ml/kg PBW, with an inspiratory plateau pressure (P_{plat}) limit of 30 cm H₂O. If the P_{plat} exceeds 30 cm H₂O on a V_T of 6 ml/kg PBW, the protocol recommends a reduction in V_T to 5 or 4 ml/kg PBW if arterial pH is greater than 7.15. The goal of 6 ml/kg PBW was chosen to be lung protective without causing severe respiratory acidosis in most patients. The ARDS Network trial demonstrated

improved clinical outcomes with a V_T goal of 6 ml/kg PBW as opposed to a V_T goal of 12 ml/kg PBW. Some investigators suggested that it is not necessary to reduce V_T s if the Pplat is less than 30 or 32 cm H_2O (23, 24). However, an analysis of the ARDS Network V_T trial suggested that there were beneficial effects of V_T reduction even among patients whose Pplats would have been ≤ 26 cm H_2O if they received V_T s of 12 ml/kg PBW (25). Two other studies suggested that Pplats in the mid-20s were safer than Pplats in the high 20s (20, 26).

A shortcoming of the PBW approach is that the volume of aerated lung varies substantially among patients with ARDS because, at a given sex and height, there is a substantial variability in normal lung volumes (27). Moreover, among patients with ARDS, there are large differences in the extent of the lung inflammation, edema, atelectasis, and consolidation. These are the main reasons that, at a given V_T , Pplats vary greatly among patients with ARDS of the same sex and height. The Pplat limit of 30 cm H_2O leads to additional reductions in V_T in patients with more extensive disease. However, in some patients, high inspiratory pressures are caused by high chest wall elastance and weight rather than extensive lung disease (28, 29). A better approach could be to set V_T according to some objective measure of aerated lung volume, such as the functional residual capacity (30, 31).

Setting V_T to Reduce Driving Pressure

Driving pressure (DP) is easily calculated at the bedside as the difference between the airway inspiratory plateau pressure and the positive end-expiratory pressure (PEEP) ($DP = P_{plat} - PEEP$). It is determined by the ratio of the V_T to the compliance of the respiratory system (C_{RS}) ($DP = V_T / C_{RS}$). Because C_{RS} is directly related to the size of the lung participating in ventilation, driving pressure reflects the size of the V_T in relation to the aerated lung volume. Assuming no auto-PEEP, DP estimates the average increase in alveolar pressure during inspiration and decrease during exhalation. Unlike Pplat and PEEP, which are static estimates of stress in the respiratory system, DP is a dynamic indicator, the change in stress with each breath. An individual patient data meta-analysis of predictors of mortality included more than 3,000 patients with ARDS enrolled in clinical trials of lung-protective ventilation

strategies (32). All patients in the meta-analysis were ventilated with a PEEP of at least 5 cm H_2O . DP was the strongest predictor of mortality among the mechanical ventilation variables that clinicians can manipulate (V_T , Pplat, PEEP, and respiratory rate). At a constant DP, variations in V_T , PEEP, and Pplat did not predict mortality. The median DP was approximately 14 cm H_2O , and the slope of the relationship of mortality to DP appeared to increase above 14 cm H_2O (Figure 2). This might suggest that we should reduce V_T until DP is below 14 cm H_2O . When DP is less than 14 cm H_2O with V_T greater than 6 ml/kg PBW, the value of further V_T reduction is likely less, as other factors may take on more importance. The magnitude of the effect of DP on mortality in this meta-analysis may be partly attributable to the higher range of DPs included from the studies examining higher versus lower V_T (33). In the V_T trials, DP ranged from approximately 10 to 15 cm H_2O in the low V_T groups and approximately 20 to 25 cm H_2O in the control groups. Subsequent mechanical ventilation trials on higher versus lower PEEP levels limited V_T to 6 ml/kg PBW, and DP ranged from 12 to 17 cm H_2O in both control and intervention groups. However, in the patient data meta-analysis, the mortality rate among patients with DP below 14 cm H_2O was still approximately

20%. Furthermore, the slope of the relationship between DP and mortality appears to be positive even at DP below 14 cm H_2O , suggesting that there is no safe upper limit for DP in patients with ARDS on positive pressure ventilation.

Another problem with using DP to set V_T is that Pplat, one of the components of DP, is influenced by the chest wall. Two patients with the same DP might have very different risks for VILI. At a given DP, a patient with a stiff or heavy chest wall likely has less overdilatation of the lung than a patient with a normal chest wall. Therefore, a better indicator of dynamic stress in the lung would be the transpulmonary driving pressure ($DP-Pl$), which is the difference in transpulmonary pressure ($Pl = \text{airway pressure} - \text{pleural pressure}$) between end-expiration and end-inspiration (34). However, there are several assumptions and potential limitations of measuring Pl , and we do not know the safe upper limit for $DP-Pl$ (35). This probably varies depending on the severity of the lung injury from pneumonia, sepsis, or whatever the inciting cause of ARDS.

Setting V_T to Reduce Lung Stress

The stress of an object is the force applied to it divided by its surface area. In the lungs, a static Pl represents the stress in the lungs at a given lung volume (34). At the end of inspiration, Pl represents the highest level

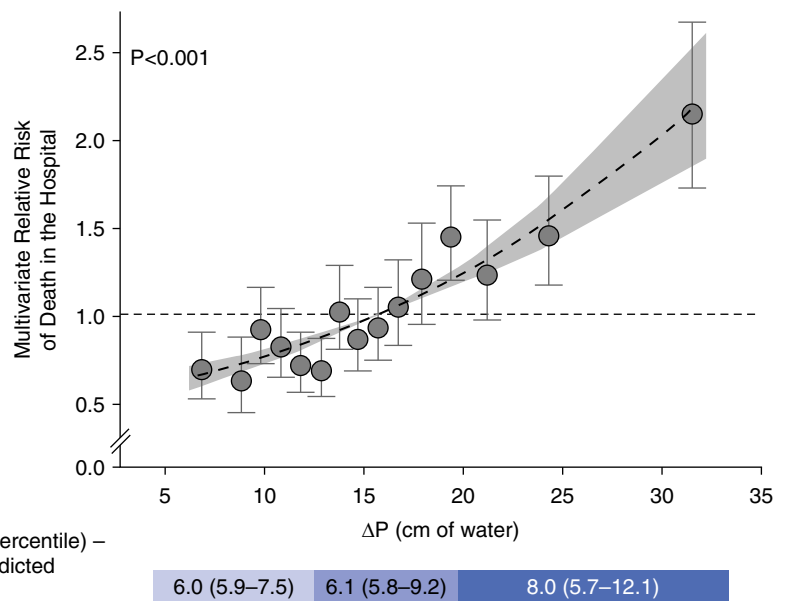


Figure 2. Relative risk of death in the hospital versus driving pressure in the combined cohort after multivariate adjustment. Even below the median driving pressure of 14 cm H_2O , there is still a significant risk of death in the hospital. Reprinted by permission from Reference 32.

of stress during the respiratory cycle, which is determined by the PEEP and the size of the V_T relative to the amount of aerated lung. Thus, P_L may be used as a marker of potential overdistention injury, and V_T could be limited to maintain end-inspiratory P_L below a critical limit. A previous investigation suggested a critical limit of 27 cm H₂O for end-inspiratory P_L in humans (36). Other models, however, have proposed much lower limits for acceptable lung stress during inspiration. Using a theoretical model, Gattinoni and colleagues suggested the limit to avoid overdistention was an end-inspiratory P_L of 15 cm H₂O, which corresponds to approximately 70 to 75% of total lung capacity (TLC) in normal humans (37). In healthy pigs, ventilator-induced pulmonary edema occurred at an average inspiratory P_L of 13 cm H₂O (38).

At this time, the only method for estimating pleural pressure in patients is esophageal manometry, and several questionable assumptions are required when we use this technique (35). Furthermore, there are different methods of calculating P_L , which yield results that sometimes differ substantially depending on which calculation is used (39). At this time, there do not appear to be clear boundaries for P_L in humans. In the future, clinicians will need reliable measurements for P_L and reliable targets for safe limits of stress before this measure can be used to optimize V_T s.

Setting V_T to Reduce Strain

Strain is the ratio of the stretch of an object to its resting length. In the lung, strain at end-inspiration can be represented by the V_T normalized to the FRC measured at an airway opening pressure of 0 cm H₂O. Lung strain is directly related to stress through the specific lung elastance and, like stress, may be used as a marker of overdistention (36). Similar to lung stress, the strain resulting from a given V_T varies substantially among patients with ARDS because of variations in aerated lung volume at FRC (36). In a study by Chiumello and colleagues (36), the same measured strain and stress could be measured with both low V_T s of 6 ml/kg PBW and high V_T s of 12 ml/kg within subgroups of patients that included some without lung disease and some with ARDS, further demonstrating the inadequacy of P_{plat} and V_T per PBW for predicting overdistention injury.

$VILI$ related to excessive strain may be related to both its dynamic and static components. Static strain results from the application of PEEP, which causes an isotonic deformation of the aerated lung above FRC at end-expiration. Dynamic strain results from the cyclic inflation of aerated lung with each tidal breath. Protti and colleagues demonstrated in healthy pigs that ventilator-induced pulmonary edema developed only when V_T s resulted in dynamic lung strains greater than 1.5 to 2.0 (38). In further investigations, lung injury was primarily related to dynamic strain rather than static strain. At the same peak inspiratory strain, ventilation with smaller dynamic and larger static strains was associated with less lung injury than ventilation with smaller static and larger dynamic strains (40).

An individualized setting of V_T based on reducing dynamic strain would be a more direct method to reduce stretch-induced lung injury than setting V_T according to PBW. This method, however, requires a valid measurement of FRC, which can be difficult in critically ill patients. Values of FRC can be measured by gas dilution, nitrogen wash-in/wash-out, and quantitative CT analysis. Unfortunately, these methods are relatively complex, cumbersome, or risky, which has limited the clinical implementation of these techniques.

Another limitation to using strain to set V_T is that in many patients with ARDS, recruitment of lung tissue occurs during inspiration. When this occurs, the ratio of V_T /FRC overestimates the strain in the aerated lung parenchyma because some of the V_T is distributed to some alveoli that open during inspiration rather than stretching of previously aerated alveoli. To reduce this error, strain could be assessed from the ratio of V_T to TLC (41). A challenge to this approach is to define TLC in a patient with ARDS. Another challenge is that we do not know a safe upper limit of strain measured with this approach.

There is increasing interest in electrical impedance tomography (EIT) for monitoring regional changes in lung volume at the bedside. EIT may be useful for monitoring regional compliance and to assess changes in end-expiratory lung volume during PEEP titration. It is unclear if the regional assessment of volume change is an adequate surrogate for global volume change. However, it is noninvasive, is relatively easy to implement, and may be

helpful in adjusting V_T . As research using EIT continues to grow, its use in the clinical setting may also expand (42).

Preventing or Reducing Hypercapnia and Acidosis When Using Small V_T

Smaller V_T may lead to respiratory acidosis, especially in patients with high physiologic dead space, as in ARDS. Some ventilator circuits contain unnecessary dead space. Endotracheal tube extenders and heat and moisture exchangers are attached to the tip of the endotracheal tube and fill with alveolar gas at end-expiration. This CO₂-laden gas is then delivered back into the lungs with the next inspiration. Some heat and moisture exchangers contain as much as 80 ml of volume, which converts otherwise effective alveolar ventilation into dead space. Heated humidifiers are more effective for conditioning inspired air and, because of their location in the ventilator circuit, do not impose additional dead space. In addition, endotracheal tube extenders can be removed from the circuit to reduce instrumental dead space.

A simple approach to reducing hypercapnia and respiratory acidosis is to increase the respiratory rate. This technique was used in the ARDS Network lower V_T protocol, in which levels of respiratory acidosis on average were quite mild. Recruiting lung can also improve CO₂ clearance (43). The use of higher levels of PEEP and recruitment maneuvers may help to reduce hypercapnia and acidosis in patients who respond with recruitment, by reducing physiologic dead space and shunt (43). In those who do not recruit, higher PEEP can worsen dead space (44). Prone positioning may lead to substantial recruitment in many patients with ARDS, which may also reduce dead space and respiratory acidosis. In addition, increasing the duration of inspiration, as with an end-inspiratory pause, can decrease P_{aCO_2} in small amounts to decrease acidosis from smaller V_T s (45, 46).

Mechanical adjuncts, such as extracorporeal carbon dioxide removal (ECCO₂R), may facilitate the use of very low V_T s by mitigating hypercapnia. Recent trials have demonstrated the feasibility of an ultraprotective ventilation strategy with concomitant use of low-flow venovenous ECCO₂R to reduce respiratory acidosis (47, 48).

In 15 patients, V_T was reduced to approximately 4 ml/kg PBW, and ECCO₂R was effective for preventing severe respiratory acidosis. Six of the patients, however, experienced persistent hypoxemia and required either prone positioning or extracorporeal membrane oxygenation. This unanticipated hypoxemia may be a consequence of lower airway pressures causing increased atelectasis (49). These effects may be counteracted by periodic recruitment maneuvers or higher levels of PEEP. In the second trial, 79 patients were randomized to V_T of 3 ml/kg PBW combined with ECCO₂R or to a control group with V_T of 6 ml/kg PBW. Patients with a $Pa_{O_2}/Fi_{O_2} \leq 150$ demonstrated significantly improved ventilator-free days after 60 days in the ECCO₂R study group, although overall mortality rate did not differ between the two groups (48). More investigation is warranted before fully embracing this technologic adjunct. A multicenter randomized clinical trial is currently enrolling to test the feasibility, safety, and efficacy of using ECCO₂R to enable ultraprotective ventilation (SUPERNOVA [Strategy of Ultraprotective Lung Ventilation with Extracorporeal CO₂ Removal for New-Onset Moderate to Severe ARDS]; Clinicaltrials.gov NCT02282657).

High-frequency oscillatory ventilation (HFOV) delivers small V_T s of approximately 1 to 3 ml/kg PBW at very high respiratory rates (50). These very small V_T s limit overdistention, while relatively high mean airway pressures prevent cyclic alveolar collapse and reopening (51). An early randomized clinical trial of HFOV versus conventional MV in ARDS demonstrated a trend toward lower mortality with HFOV. However, the conventional MV group used generous V_T s of greater than 10 ml/kg PBW, which are now known to be injurious (52). More recent, larger randomized trials demonstrated either no difference in mortality or possible harm with HFOV compared with conventional MV with lower V_T s (18, 19). Each of the HFOV trials were challenged by limitations in their design, which may have led to the HFOV groups receiving more sedation, fluids, vasopressors, and neuromuscular blocking agents. In the absence of convincing evidence of efficacy, the use of HFOV is now largely limited to patients who have failed other therapies or who are not

candidates for mechanical support such as extracorporeal gas exchange.

Lower V_T Reduces VILI Even at Lower Expiratory Pressures and Volumes

VILI may also occur from ventilation with low end-expiratory volume and pressure, perhaps from repeated opening and reclosing of small bronchioles and alveoli and from excessive stress at the margins between aerated and atelectatic or consolidated lung tissue (5, 53). This form of VILI may be reduced with higher levels of PEEP than were used in the past, before VILI was recognized (5, 53). However, recruitment and derecruitment occur at almost all lung volumes in patients with ARDS, even when relatively high levels of PEEP are used (54, 55). Regardless of the volume at end-expiration, the recruiting and derecruiting pressure swings are smaller when low V_T s are used. Therefore, in addition to reducing VILI from overdistention, lower V_T s can also reduce VILI from opening and reclosing or from excessive stress at the margins between aerated and atelectatic air spaces (56, 57). Ultimately, the mechanical power that is applied to the lung decreases exponentially with reductions in V_T , which is a powerful mechanism for reducing VILI (58).

Rethinking Goals for Setting V_T

Several studies strongly suggest that in patients with ARDS, VILI from

overdistention can occur at V_T s and Pplats that are lower than those that are in current use in most intensive care units (20, 25, 26). Unfortunately, there is no reliable test for ongoing VILI from overdistention, like troponin for ongoing cardiac injury. Moreover, despite current guidelines and recommendations for V_T , Pplat, stress, strain, and DP, we do not know safe levels of any of these parameters. Therefore, we propose that any of the methods for setting V_T reviewed here can be used to set the initial V_T . We advocate that the initial V_T should be within the range of 4 to 8 ml/kg PBW, with Pplat less than 30 cm H₂O. The upper part of this range, 7 to 8 ml/kg, should be reserved for patients who have frequent double breaths or severe dyspnea with airway pressure less than PEEP for much of the inspiratory cycle. In patients with moderate and severe ARDS, and especially in patients whose DPs and plateau pressures are not comfortably low (DP > 14 cm H₂O and Pplat > 25 cm H₂O, respectively), we suggest that clinicians push the limits of reducing V_T beyond their current practice, setting V_T s in the lower part of our range of 4 to 6 ml/kg. V_T can then be reduced in small decrements (e.g., 0.5 ml/kg PBW) over several hours while monitoring individual patients' responses for signs of intolerance to the adverse effects of lower V_T s, including hemodynamic changes, gas exchange, and respiratory mechanics (Table 1). In some patients, the ultimate V_T may be considerably lower than those that are in common use today (59). Furthermore, regardless of the method to set the initial V_T , if the same signs of intolerance are used, the same ultimate V_T

Table 1. Signs of Intolerance to Low V_T and Hypercapnia

Signs of Low V_T Intolerance
Tachycardia
Hypertension
Hypotension
Tachypnea
Patient-ventilator dyssynchrony (e.g., double triggering)
Inspiratory airway pressure below PEEP, indicating high work of breathing
Respiratory acidosis
Hypoxemia despite high Fi_{O_2}
Agitation

Definition of abbreviation: PEEP = positive end-expiratory pressure. Physiologic signs that can be assessed for evidence of intolerance to mechanical ventilation with low V_T s and hypercapnia. Patient-ventilator dyssynchrony often manifests as a double breath (Figure 1), which means the end-inspiratory pressure and end-inspiratory lung volume are higher than at the end of synchronous breath, which is a major risk for alveolar overdistention.

will be attained. A shortcoming of this approach is that the signs of intolerance are not very specific to intolerance to hypercapnia and acidosis. However, if we monitor these signs closely over a period of a few hours while lowering V_T in steps, changes in these signs should more specifically represent effects of the lower V_T implementation. If signs of intolerance develop, adjunctive therapies, such as neuromuscular blockade or ECCO₂R, should be considered to facilitate tolerance of low V_T , especially for patients who would likely benefit the most from reduced V_T

Conclusions

The optimal method for setting V_T for patients with ARDS remains unknown. The use of smaller V_T s has been accepted by many since the publication of the National

Institutes of Health ARDS Network study (15, 60). However, some patients remain at risk for overdistention injury even when small V_T s are used, because their aerated lung volumes are greatly reduced (20, 25). As PBW does not correlate well with aerated lung volume, better approaches to setting V_T may involve limiting lung stress, strain, or driving pressure as potential surrogates for VILI from parenchymal overdistention injury. Whatever method is initially used, for patients with moderate to severe ARDS or more severely impaired respiratory mechanics, we suggest the careful, continued further reduction of V_T in a stepwise manner until a patient begins to exhibit physiologic signs of intolerance or the DP or Pplat is in a safer range (Table 1). As is frequently the case, this intervention will have competing effects that must be balanced on a patient-by-patient

basis. Higher levels of PEEP may be necessary to prevent atelectasis that may result from the smaller V_T s. However, higher PEEP may cause overdistention or hemodynamic instability (61). The need for strict control of P_{aCO_2} , as in intracranial hypertension, may outweigh the need to lower V_T to protect the lung. Nevertheless, we recommend keeping V_T at the lowest possible value as dictated by patient tolerance and appropriateness of respiratory mechanics, gas exchange, and hemodynamic parameters. As the technology of ECCO₂R continues to evolve, the limits of MV with low V_T s as a lung-protective strategy should continue to be tested. Further investigations are warranted to determine if pushing the limits of lowering V_T will improve clinical outcomes. ■

Author disclosures are available with the text of this article at www.atsjournals.org.

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