

Article

Easy-to-Build Textile Pressure Sensor

Francisco Pizarro *, Piero Villavicencio, Daniel Yunge , Mauricio Rodríguez , Gabriel Hermosilla and Ariel Leiva

Pontificia Universidad Católica de Valparaíso, Escuela de Ingeniería Eléctrica, Avenida Brasil 2147, Valparaíso 2362804, Chile; piero.villavicencio.a@mail.pucv.cl (P.V.); daniel.yunge@pucv.cl (D.Y.); mauricio.rodriguez.g@pucv.cl (M.R.) gabriel.hermosilla@pucv.cl (G.H.); ariel.leiva@pucv.cl (A.L.)

* Correspondence: francisco.pizarro.t@pucv.cl; Tel.: +56-32-227-3687

Received: 28 February 2018; Accepted: 10 April 2018; Published: 13 April 2018



Abstract: This article presents the design, construction, and evaluation of an easy-to-build textile pressure resistive sensor created from low-cost conventional anti-static sheets and conductive woven fabrics. The sensor can be built quickly using standard household tools, and its thinness makes it especially suitable for wearable applications. Five sensors constructed under such conditions were evaluated, presenting a stable and linear characteristic in the range 1 to 70 kPa. The linear response was modeled and fitted for each sensor individually for comparison purposes, confirming a low variability due to the simple manufacturing process. Besides, the recovery times of the sensors were measured for pressures in the linear range, observing, for example, an average time of 1 s between the moment in which a pressure of 8 kPa was no longer applied, and the resistance variation at the 90% of its nominal value. Finally, we evaluated the proposed sensor design on a classroom application consisting of a smart glove that measured the pressure applied by each finger. From the evaluated characteristics, we concluded that the proposed design is suitable for didactic, healthcare and lifestyle applications in which the sensing of pressure variations, e.g., for activity assessment, is more valuable than accurate pressure sensing.

Keywords: pressure measurement; textiles; wearable sensors; easy-to-build

1. Introduction

Nowadays, wearable devices have become an important subject in the research community [1–3]. The possibility of connecting ordinary objects and obtaining data from them in real time has the potential to increase and improve the decision-making concerning a number of objects and situations that could not previously be measured. This opens up a substantial new area of applications in smart industries, as well as in the domains of education, biomedicine, and healthcare [4–9].

In order to turn these ordinary objects into candidates for wearable connected devices, it is important to make the sensors and communication systems as lightweight, flexible, and thin as possible, so that they use a low volume when integrated into a system [10]. It is under these conditions that textile sensors, which introduce the smart clothing concept, have been an interesting topic in recent years, based on the fact that clothing and apparel have large portable surfaces into which sensors and electronics can be integrated [11–14].

Several studies on the development of textile sensors and its physical characteristics have been conducted in the last years [15–17]. These studies include flexible temperature sensors [11,18], strain gauge sensors [15,19,20], electromagnetic induced sensors [21] and pressure sensors [22]. Amongst these sensors, pressure sensors have been widely studied because of its multiple applications, such as in the healthcare domain [23–27], sports monitoring [28–30] and eating habits monitoring [31].

Specifically, pressure sensors have different ways of measuring the pressure variation [32]. These sensors can work either measuring capacitive changes [24,29,33], piezoelectric voltages generated

by pressure [34], or resistance variation generated by pressure [31], where piezo-electrical [35] and piezo-resistive [36] polymers are widely used for these purposes.

One common characteristic of these pressure sensors is that they necessitate the use of machinery, for example sewing machines, in order to be built. This characteristic limits the possibility of replicating sensors for educational purposes, where machinery is either expensive, or difficult to obtain. In order to introduce wearable technologies in engineering schools, it is important to students to be able to deal with the implementation aspects of such sensory systems, and to evaluate independently the issues and advantages of textile sensors in a real-world scenario. Therefore, it is necessary to have easy-to-build textile sensors in order to permit students to understand the sensing and data interpretation processes involved.

This article presents the design, construction and evaluation of an easy-to-build textile resistive pressure sensor. The sensor was evaluated in terms of linear range, construction repeatability and recovery time. Finally, the sensor was used in a classroom environment application.

2. Sensor Design and Construction

The designed sensor works on the basis of the resistance variation through pressure application. The sensor itself is based on a structure proposed in [36] and consists of a sandwich made of two conductive Shieldex NoraDell woven fabric sheets [37] with a Low Density Polyethylene (LDPE) sheet between the conductive fabrics, which makes it different from previous designs in literature [36]. The Shieldex NoraDell woven fabric sheets have been largely used for microwave applications due to its good conductivity and radiation efficiency characteristics [38–41], having a surface resistance lower than $0.009 \Omega/\text{sq}$ and a maximum thickness of 0.13 mm. Between the two conductive sheets is placed a sheet of Antistat black conductive bag (ANT006BCB) [42] widely used for anti-static applications. These bags are made of Low Density Polyethylene (LDPE) with a 0.1016 mm carbon layer, having a surface resistivity of 10^4 to $10^6 \Omega$. The combination of the conductive textile sheets with the polymer sheet creates a piezo-resistive effect that translates the applied pressure on the sheet sandwich into a resistance variation [36]. Finally, the conductive sheets are connected through Shieldex 117/17 DTEX conductive threads for the measurement of their resistance. Figure 1 shows an exploded view of the designed sensor. In terms of the geometry of the sensor, and in order to make an easy and replicable design, a square-shaped sensor was constructed. A top view of the sensor is shown in Figure 2.

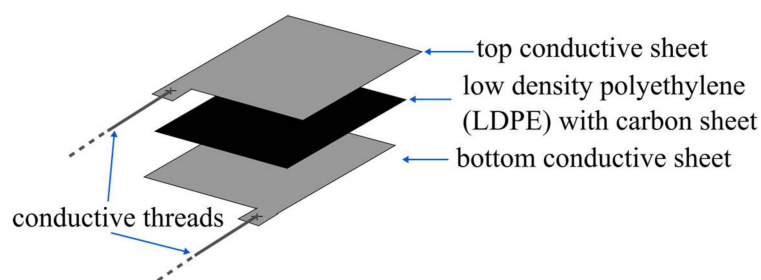


Figure 1. Exploded view of the resistive textile pressure sensor.

The conductive textile sheet has a surface of $W_{cond} \times l_{cond}$ where $W_{cond} = l_{cond} = 2$ cm. The conductive textile sheet has also a small surface of $W_{term} \times l_{term}$ that acts as a terminal for the sensor and where the conductive thread is sewed. The dimensions of the terminal are $W_{term} = 0.7$ cm and $l_{term} = 0.6$ cm. Regarding the LDPE sheet, the surface $W_{LDPE} \times l_{LDPE}$ is larger than the conductive textile sheets in order to avoid direct electrical contact between them. The dimensions of the LDPE sheet are $W_{LDPE} = 2.5$ cm and $l_{LDPE} = 3.3$ cm. Finally, the three sheets are glued together with a thin double-sided adhesive tape, and sealed with a flexible plastic film for protection. The final textile resistive sensor is depicted in Figure 3.

The construction of the sensor is relatively easy, and was done using only standard office tools and done by hand. The construction procedure, which consists of measuring and marking the dimensions on each sheet (conductive and LDPE), cutting and consolidating the sensor, does not take more than 15 min for a person who reads the building instructions for the first time. This characteristic makes the sensor suitable for its use in a classroom environment.

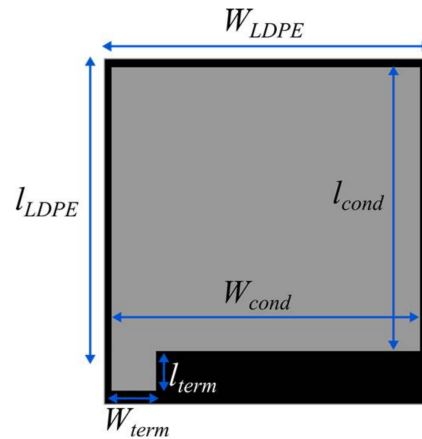


Figure 2. Top view with dimensions of the resistive textile pressure sensor.



Figure 3. Top view with dimensions of the resistive textile pressure sensor.

3. Measurement Results

In order to validate the pressure sensor, several measurements were done. Five different scenarios took place to validate different aspects of the constructed sensor, namely time response, linearity and replicability. For the time response, the recovery time when the sensor was released was assessed. Then, for the linearity evaluation (hysteresis and variance), the sensor was measured when decreasing and increasing pressures were applied. Finally, all these measurements were repeated over five constructed sensors in order to validate their replicability.

3.1. Recovery Time

The first important variable to measure for wearable sensors is the recovery time. This is the time that the sensor requires for getting back to its nominal state or zero-state once the pressure is no longer applied. The measurement of this time must be performed first, because it determines the minimal and maximal waiting times between the subsequent measurements.

For this measurement, the constructed sensor is connected to an Arduino LilyPad, where the resistance variation as a function of time is measured through the LilyPad with an application written

for that purpose. To apply the pressure to the sensor, a special container was constructed in order to put weights and apply a controlled and uniform pressure over the sensor. The container was constructed using a 3D printer, fed with standard polylactic acid (PLA) filaments. The base dimensions of the container were defined the same as those of the conductive sheet of the sensor ($W_{cond} \times l_{cond}$) in order to apply a uniform pressure over the sensor.

Finally, in order to measure the recovery time, an offset was defined as the zero value of the sensor. This offset was set at 2.4 k Ω which corresponds to the average measured resistance when there is no pressure applied over the sensor. To measure the recovery time, a pressure is applied to the sensor. Once the sensor reaches the resistance value that corresponds to the applied pressure, the pressure is taken away from the sensor. The recovery time corresponds then to the time from which the pressure is no longer applied over the sensor, till the time at which the sensor reaches the defined offset. Another time that will be measured will be the time to the sensor for come back to a 90% of the nominal value. This value can be useful, for example, for dynamic pressure sensing applications. Figure 4 shows the measurement procedure of the recovery time.

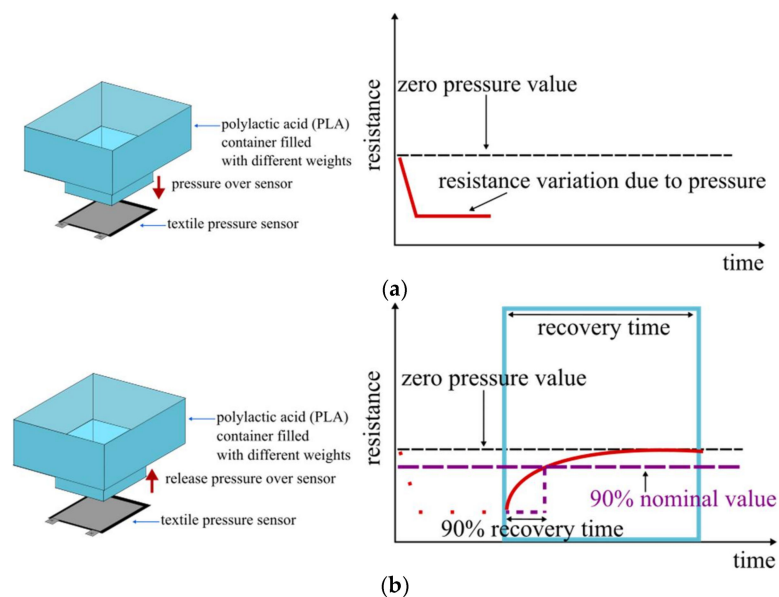


Figure 4. Measurement of recovery time of the textile pressure sensor: (a) Applied pressure to the sensor and resistance-time variation. (b) Released pressure from the sensor and resistance-time variation.

For the test, the applied pressure varies from 2 to 70 kPa. Table 1 shows the average measured values of the recovery time of the constructed sensors for each applied pressure and the average measured values of recovery time to a 90% of the threshold.

Table 1. Average recovery time of the constructed sensors as function of the applied pressure.

Applied Pressure (kPa)	Recovery Time (s)	90% Recovery (s)
2	22.6	0
4	24.6	0
6	30.4	0
8	28.9	1
10	30.0	1.9
20	32.0	15
30	36.0	15
40	30.6	14.3
50	35.3	13
60	32.3	14
70	35.3	17

The measurement results show that the maximum recovery time was obtained with an applied pressure of 50 kPa and the lower time was obtained at 2 kPa. There is no noticeable tendency towards a time variation with the augmentation of the pressure. The recovery time was found between 30 and 35 s for pressures above 6 kPa. For the comeback time to the 90% of the defined threshold, it was found that for lower pressure (from 2 to 8 kPa) the sensor almost instantly comes to a resistance value that is within the established threshold. For higher pressures, the times varies from 13 to 17 s, depending on the applied pressure.

3.2. Decreasing Pressure Range

To evaluate the hysteresis aspect we separately evaluate the sensors when decreasing and increasing pressure is applied to them. For the decreasing pressure test, the resistance value is measured between the terminals of the sensor as a function of a time-decreasing and equally applied pressure over the surface of the sensor. Two variants of the test were conducted; one having a short pause between measurements (30 s), and the other having a long pause between measurements (180 s). This was done to check for time response effects.

The measurement setup is shown in Figure 5a. For this measurement, the container is filled with the desired weight and placed over the pressure sensor to measure the resistance variation using a multimeter connected to the textile conductor. Figure 5b shows a picture of the implemented measurement setup.

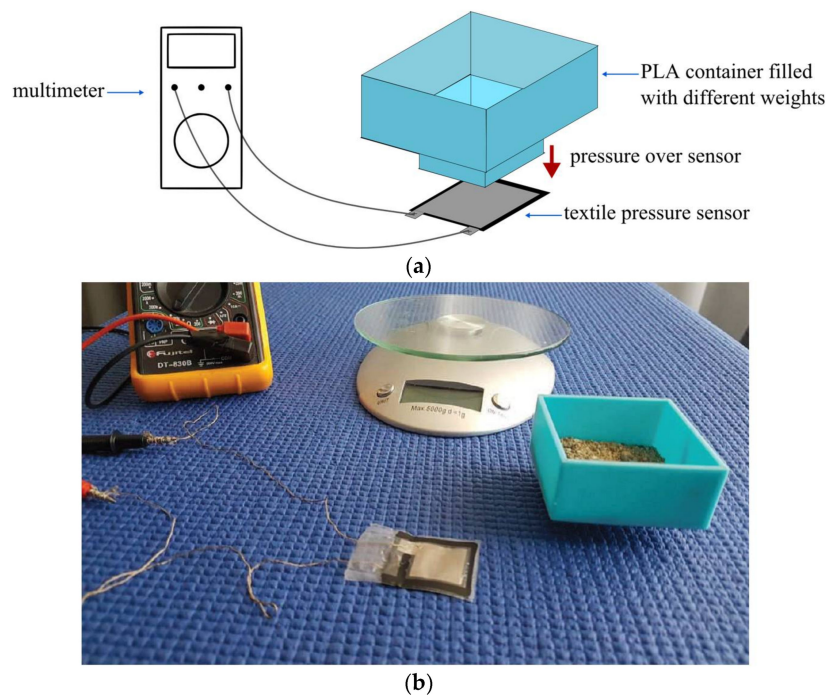


Figure 5. Measurement setup used for pressure variation measurement: (a) Schematic of the measurement setup. (b) Picture of the measurement setup.

The measurement results of both case scenarios are shown in Figures 6 and 7 for the five constructed sensors. The applied pressure varies from 70 kPa to 0 kPa with a pause between tests of 30 s and 180 s, respectively. From the results shown in Figures 6 and 7, two characteristic zones of the sensor can be determined. At the lower applied pressures (from 0 to 1 kPa), there is no significant variation of the resistance of the sensor, as expected. For this reason, sensors in the literature [27,29,43] do not use this pressure range, especially when movement or folding are involved [27]. For pressures above 1 kPa, a wide linear range of resistance variation was obtained for the five constructed sensors.

The average resistance in this zone varied from 2.2–0.41 k Ω for applied pressures between 1 kPa and 70 kPa.

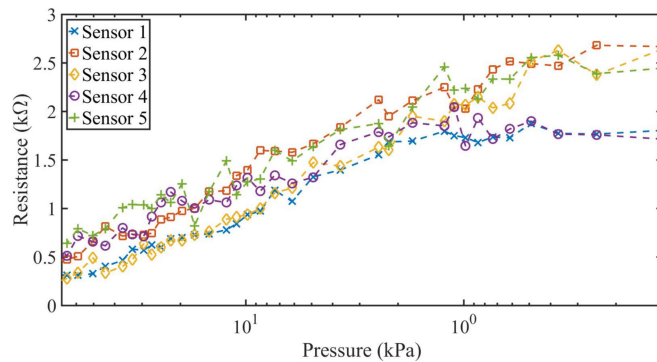


Figure 6. Measured resistance against decreasing pressure variations for the five constructed textile pressure sensor with short pause time (30 s) between measurements.

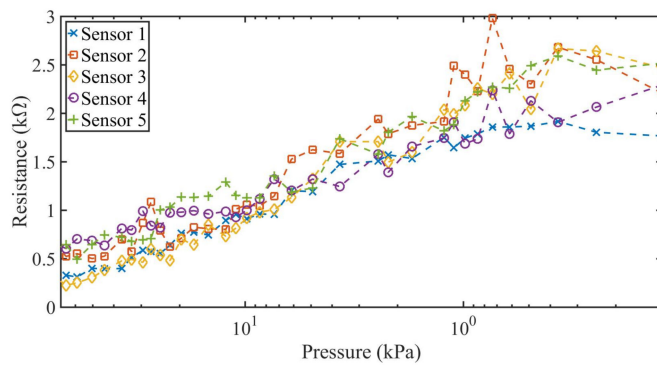


Figure 7. Measured resistance against decreasing pressure variations for the five constructed textile pressure sensor with a long pause time (180 s) between measurements.

3.3. Increasing Pressure Range

The same previous scenarios (short pause and long pause between measurements) were used, this time with increasing values of pressure applied over the textile pressure sensor. Figures 8 and 9 show the results of the resistance variation as function of an increasing applied pressure with 30 s pause (short time) and 180 s pause (long time) between measurements. The measurement results are comparable to the results obtained with the decreasing pressure against resistance in terms of linear range and resistance variation, having the same linear variation of the resistance for the five constructed sensors between 1 kPa and 70 kPa. For the linear zone of each individual sensor, it can be observed that there is no significant hysteresis effect.

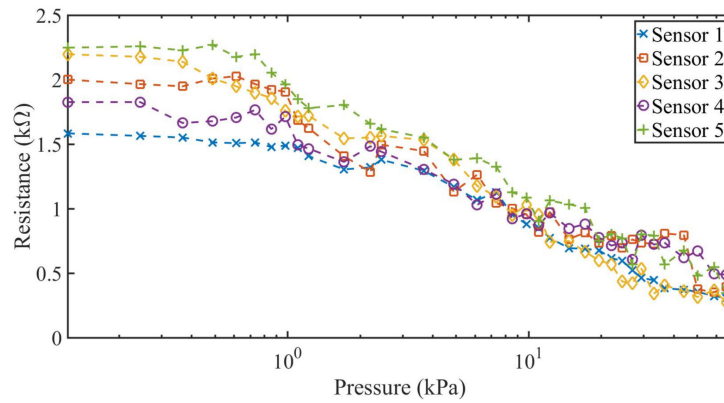


Figure 8. Measured resistance against increasing pressure variations for the five constructed textile pressure sensor with short pause time between measurements.

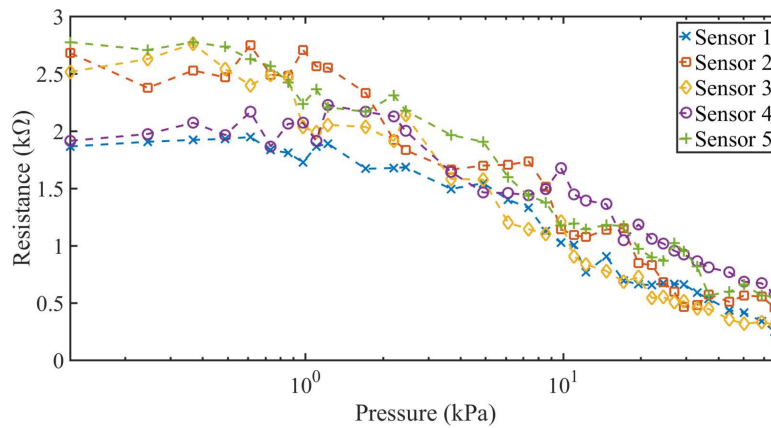


Figure 9. Measured resistance against increasing pressure variations for the five constructed textile pressure sensor with long pause time between measurements.

3.4. Sensor Comparison and Model

It is important to compare and model the constructed sensors in order to determine their substantial differences at the time of constructing this kind of sensor. In order to compare the sensors, a model of the average resistance obtained in function of the applied pressure to each sensor was developed. For this model, only the linear part of the sensor was taken into account, comprising pressures from 1–70 kPa. A logarithmic fitting was obtained from the measured data for each sensor, described in the following equation:

$$R = b + m \cdot \log(P) \quad (1)$$

where R is the resulting resistance in $k\Omega$, P is the applied pressure in kPa, m the slope and b the intercept of the linear function.

As the individual behavior of each sensor is very similar in both cases of increasing and decreasing pressures, the linear function of each sensor was generated from the data of both tests. Furthermore, a single fitting was done for all sensors using all the available measurement data. Table 2 shows the intercept, slope and Mean Square Error (MSE) using the fitting equation in (1), one for each sensor individually, and one for all the measurements done for all sensors using a single fitting generated from all the available data.

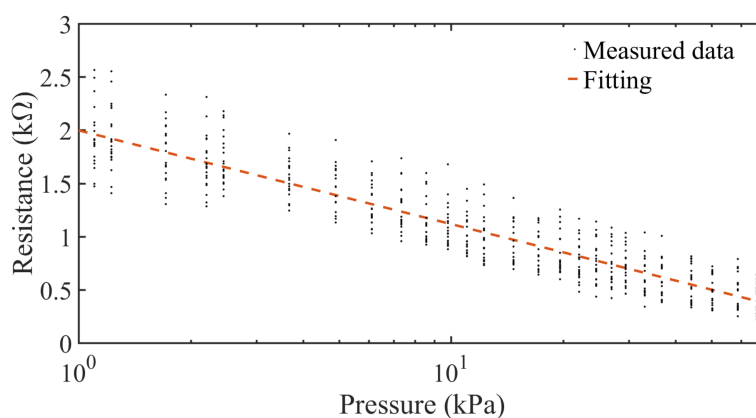
Table 2. Fitting parameters and Mean Square Error obtained from each individual sensor and from all the sensors collectively.

	Intercept	Slope	MSE
Sensor 1	1.964	−0.826	0.01
Sensor 2	2.175	−0.978	0.04
Sensor 3	2.002	−1.002	0.01
Sensor 4	1.877	−0.700	0.03
Sensor 5	2.148	−0.889	0.02
All sensors	1.997	−0.881	0.04

As shown in Table 2, all the sensors have the same decreasing linear behavior in terms of resistance over the augmentation of the pressure, with negligible differences in the slope and intercepts values of the function. Furthermore, the maximum MSE for the constructed sensors is 0.04, which matches the MSE obtained taking into account all the measurements obtained from the five constructed sensors collectively, as shown in Figure 10. The difference found in the intercept and the slope among sensors can be associated with the lax construction tolerances of each sensor, which are acceptable for a sensor completely constructed by hand. On Table 3 are shown the dimensions of each constructed sensor measured with a precision ruler.

Table 3. Conductive sheet dimensions (in centimeters) of each conductive sensor.

	Sensor 1	Sensor 2	Sensor 3	Sensor 4	Sensor 5
W_{cond}	1.991	1.85	1.92	1.91	1.91
l_{cond}	1.8	1.89	1.81	1.86	1.82

**Figure 10.** Measured data of the five constructed sensors and logarithmic fitting of the data.

4. Use-Case of the Proposed Sensor

A use-case using the proposed sensor was done in a classroom environment, where the students construct and measure the sensor inserted in an application. The characterization of the sensor shows that the sensor has a linear behavior when pressures above 1 kPa are applied, with a mean recovery time of 30 s. These characteristics, adding the fact that the sensor has a fabrication tolerance reflected on the MSE, make the sensor difficult for its use in static pressure measurement for critical safety applications, where a threshold of pressure is determined in order to make an action. Nevertheless, the sensor characteristics can be suitable for applications where it is important to measure variations or tendencies of applied pressures as for example, lifestyle applications (e.g., posture correction, walking behavior).

The proposed application for the proof of concept consists in a glove where the pressure sensors are installed on its fingertips and measure the behavior of the sensor when a pressure is applied (e.g.,

when grabbing and holding a glass). The objective of this application is to recognize when the glove is holding an object, and which finger makes the higher pressure to hold it.

First of all, the students construct and install the sensors in a wool glove using an instructive given to them. Figure 11 shows the sensors installed on the glove. The students connect the sensors to an Arduino Lilypad (state of the art wearable microcontroller). The Lilypad measures the pressure variation through a voltage difference caused by the resistance variation of the constructed pressure sensors. This was done using a dedicated application installed by the students. Finally, the microcontroller was connected to a computer for visualization of the results. Figure 12 shows the experimental setup done by the students.

Figure 13 shows the measurement results obtained with the sensors installed on the glove on each fingertip. The measured experience consisted of three steps: the glove in steady state, the glove grabbing and holding an object and finally releasing the object. First of all, we can notice that there is a slight difference in the steady states amongst the sensors. This can be explained due to the constructed tolerance of each sensor. Another factor that might influence the steady state resistance of each sensor is that the different curvatures of the fingertips deform the sensors differently.

The second noticeable characteristic of the measurement is when a glass is grabbed using the glove. It can be clearly noticed the change of the pressure applied by each individual finger translated on the voltage lecture on the microcontroller. For example, we can notice that the thumb is the finger that applies more pressure when grabbing and object. Finally, when the glove releases the glass, we can notice the release behavior on the sensors and clearly the tendency to come back to the steady state. Another remarkable aspect of this measurement is that the recovery time can be redefined as thresholds within a percentage of the initial value, as now dynamics are measured. Under these terms, the recovery time can be drastically reduced. In this use-case, as shown in Figure 13, if a threshold of the 90% of the initial value is set, the recovery time is reduced to 5 s.

With this experiment the students have accomplished the whole system comprehension in terms of sensor construction, connection, programming and interpretation of measured results to characterize the behavior of each finger when holding a glass.

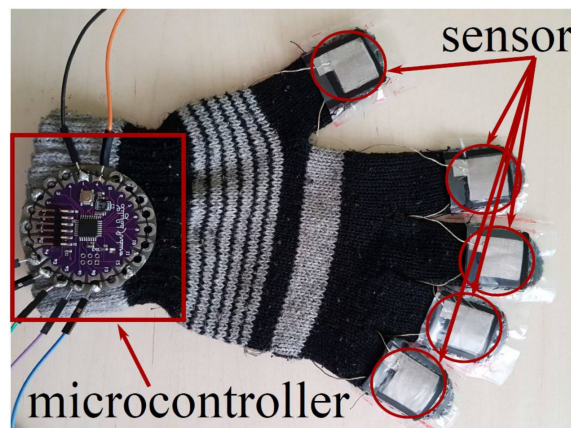


Figure 11. Wool glove with pressure sensors installed and connected to microcontroller.

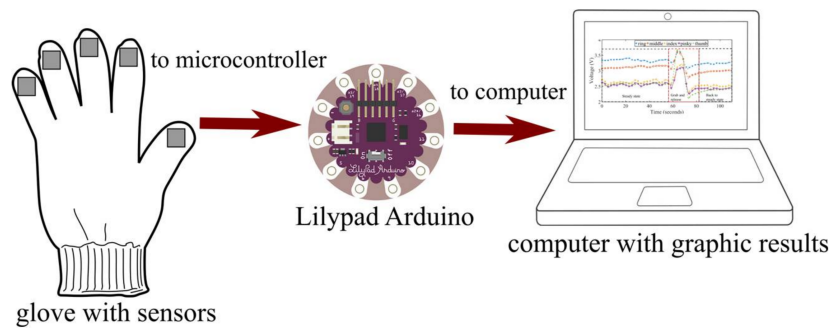


Figure 12. Experimental setup for pressure variation measurement using proposed easy-to-build sensor.

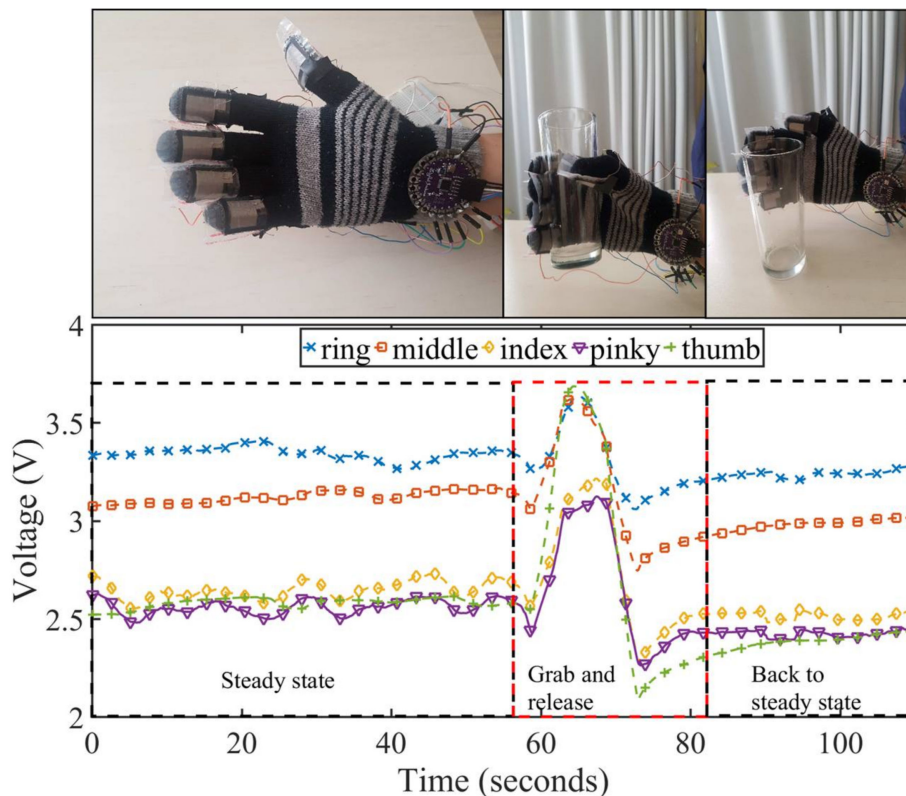


Figure 13. Measured voltage data of five constructed sensors placed in the fingertips of a glove holding a glass.

5. Conclusions

An easy-to-build textile pressure sensor was designed, constructed and evaluated. The sensor consists of two sheets of conductive woven tissue that surrounds a conventional antistatic black conductive sheet. Five measurement scenarios were considered: increasing applied pressure with short time release between measurements, increasing applied pressure with longer time release between measurements, decreasing applied pressure with a short time release between measurements, decreasing applied pressure with a long time release between measurements, and the release time or recovery time of the sensor. The recovery time was measured, obtaining average times that varied from 22 to 35 s depending on the applied pressure, and between zero and 17 s if we consider the 90% of the threshold, also depending on the applied pressure. To notice that in this case, for pressures below 10 kPa, the comeback time to the 90% of the threshold is negligible. In addition, as a possibility for

improving the recovery time, we propose the assessment of different anti-static shields and adhesion methods between sheets that may have different elastic properties.

The constructed sensors showed two distinctive zones in terms of resistance variation as function of the applied pressure. The first zone between 0 and 1 kPa showed no significant variation of the resistance as the pressure increased. This can be expected as the pressures applied were low, and textile pressure sensors hardly work on that range of pressure in the literature. The other resistive zone of the sensor presented a linear behavior within pressure values from 1 to 70 kPa. These applied pressures corresponded to an average variation of the resistance of 2.2 k Ω to 0.41 k Ω . Finally, a fitting equation for each sensor individually and for all sensors collectively was obtained. All the curves obtained presented the same linear behavior, with a comparable MSE, and slight differences in the intercept and the slope. These differences can be associated with the construction discrepancies of each sensor, as expected on a handmade constructed sensor. These results make the sensor more suitable for dynamic pressure sensing applications, where the tendency of the signal is the valuable data to acquire. Moreover, the sensor can be evaluated with uneven pressures applied to it in order to extend the number of applications.

Finally, and taking into account the sensor characteristics, a proof of concept was done in a classroom environment, using the proposed sensor installed in the fingertips of a glove, to measure the pressure variation of each finger when holding a glass with the glove. The measurement results shows that the sensor is useful for this kind of applications, where it can be easily differentiate the steady-state and the impulse response of the system, translated into pressure variations.

The obtained results are promising in terms of possible applications. The advantage of this sensor is that it can be built using classical and basic tools without using any machine and in a period which does not exceed the 15 min for a first-time constructor of the sensor. The easy-to-build characteristic makes the sensor suitable for pedagogic applications, considering that nowadays, wearable devices and Internet of Thing (IoT) are trending topics in research. This sensor will be helpful to teach new engineers important aspects of wearable and connected devices. On this work, for example, an Arduino LilyPad application was written to measure the recovery time, which can be easily extended to communicating the sensing data. Future works include the evaluation of the proposed sensor on a robotic arm, for medical telemonitoring, and structural health monitoring applications.

Acknowledgments: The authors would like to thank the Proyecto VRIEA-PUCV 039.358/2016 funding and the Proyecto VRIEA-PUCV 039.462/2017 funding for the financial support of this article.

Author Contributions: Francisco Pizarro designed the sensor with Piero Villavicencio. Francisco Pizarro and Daniel Yunge wrote the paper and designed the characterization experiments. Piero Villavicencio makes all the measurements for the characterization. Mauricio Rodríguez makes the statistical and fitting analysis of each sensor. Gabriel Hermosilla and Ariel Leiva designed and helped on the measurement on the use-case experiment.

Conflicts of Interest: The authors declare no conflict of interest.

References

1. Lee, M.; Lee, M.R. Beyond the Wearable Hype. *IT Prof.* **2015**, *17*, 59–61. [[CrossRef](#)]
2. Pustiek, M.; Beristain, A.; Kos, A. Challenges in Wearable Devices Based Pervasive Wellbeing Monitoring. In Proceedings of the 2015 International Conference on Identification, Information, and Knowledge in the Internet of Things (IIKI), Beijing, China, 22–23 October 2015; pp. 236–243.
3. Rehman, A.; Mustafa, M.; Javaid, N.; Qasim, U.; Khan, Z.A. Analytical Survey of Wearable Sensors. In Proceedings of the 2012 Seventh International Conference on Broadband, Wireless Computing, Communication and Applications, Victoria, BC, Canada, 12–14 November 2012; pp. 408–413.
4. Chow, V.T.F.; Sung, K.W.; Meng, H.M.; Wong, K.H.; Leung, G.K.S.; Kuo, Y.-H.; Tsoi, K.K.F. Utilizing Real-Time Travel Information, Mobile Applications and Wearable Devices for Smart Public Transportation. In Proceedings of the 2016 7th International Conference on Cloud Computing and Big Data (CCBD), Macau, China, 16–18 November 2016; pp. 138–144.

5. Zeng, Y.; Pande, A.; Zhu, J.; Mohapatra, P. WearIA: Wearable device implicit authentication based on activity information. In Proceedings of the 2017 IEEE 18th International Symposium on a World of Wireless, Mobile and Multimedia Networks (WoWMoM), Macau, China, 12–15 June 2017; pp. 1–9.
6. Gonçalves, J.; Leito, L.; Carvalho, V. Analysis of the reliability and accuracy of a wearable device: Comparative study with a certified clinical device. In Proceedings of the 2017 12th Iberian Conference on Information Systems and Technologies (CISTI), Lisbon, Portugal, 21–24 June 2017; pp. 1–6.
7. Zhang, X.; Wu, C.W.; Fournier-Viger, P.; Van, L.D.; Tseng, Y.C. Analyzing students' attention in class using wearable devices. In Proceedings of the 2017 IEEE 18th International Symposium on A World of Wireless, Mobile and Multimedia Networks (WoWMoM), Macau, China, 12–15 June 2017; pp. 1–9.
8. Mosenia, A.; Sur-Kolay, S.; Raghunathan, A.; Jha, N.K. Wearable Medical Sensor-Based System Design: A Survey. *IEEE Trans. Multi-Scale Comput. Syst.* **2017**, *3*, 124–138. [[CrossRef](#)]
9. Frediani, G.; Mazzei, D.; De Rossi, D.E.; Carpi, F. Wearable Wireless Tactile Display for Virtual Interactions with Soft Bodies. *Front. Bioeng. Biotechnol.* **2014**, *2*, 31. [[CrossRef](#)] [[PubMed](#)]
10. Yunge, D.; Park, S.; Kindt, P.; Chakraborty, S. Dynamic Alternation of Huffman Codebooks for Sensor Data Compression. *IEEE Embed. Syst. Lett.* **2017**, *9*, 81–84. [[CrossRef](#)]
11. Mattana, G.; Kinkeldei, T.; Leuenberger, D.; Ataman, C.; Ruan, J.J.; Molina-Lopez, F.; Quintero, A.V.; Nisato, G.; Tröster, G.; Briand, D.; et al. Woven Temperature and Humidity Sensors on Flexible Plastic Substrates for E-Textile Applications. *IEEE Sens. J.* **2013**, *13*, 3901–3909. [[CrossRef](#)]
12. Andreoni, G.; Fanelli, A.; Witkowska, I.; Perego, P.; Fusca, M.; Mazzola, M.; Signorini, M.G. Sensor validation for wearable monitoring system in ambulatory monitoring: Application to textile electrodes. In Proceedings of the 2013 7th International Conference on Pervasive Computing Technologies for Healthcare and Workshops, Venice, Italy, 5–8 May 2013; pp. 169–175.
13. Wu, T.-K.; Lin, C.-C.; Ku, W.-Y.; Liou, Y.-S.; Yang, C.-Y.; Lee, M.-Y.; Lin, W.-Y.; Tsai, T.-H. The Study of the Enhanced External Counterpulsation System Based on Smart Clothes. In Proceedings of the 2016 IEEE First International Conference on Connected Health: Applications, Systems and Engineering Technologies (CHASE), Washington, DC, USA, 27–29 June 2016; pp. 125–129.
14. Kirthika, S.K.; Ponraj, G.; Ren, H. Fabrication and Comparative Study on Sensing Characteristics of Soft Textile-Layered Tactile Sensors. *IEEE Sens. Lett.* **2017**, *1*, 1–4. [[CrossRef](#)]
15. Atalay, O.; Kennon, W. Knitted Strain Sensors: Impact of Design Parameters on Sensing Properties. *Sensors* **2014**, *14*, 4712–4730. [[CrossRef](#)] [[PubMed](#)]
16. Eom, J.; Lee, W.; Kim, Y.H.; Kim, Y.H. Textile-based wearable sensors using metal-nanowire embedded conductive fibers. In Proceedings of the 2016 IEEE SENSORS, Orlando, FL, USA, 30 October–3 November 2016; pp. 1–3.
17. Dai, H.; Thostenson, E.; Schumacher, T. Processing and Characterization of a Novel Distributed Strain Sensor Using Carbon Nanotube-Based Nonwoven Composites. *Sensors* **2015**, *15*, 17728–17747. [[CrossRef](#)] [[PubMed](#)]
18. Sibinski, M.; Jakubowska, M.; Sloma, M. Flexible Temperature Sensors on Fibers. *Sensors* **2010**, *10*, 7934–7946. [[CrossRef](#)] [[PubMed](#)]
19. Mattmann, C.; Clemens, F.; Trster, G. Sensor for Measuring Strain in Textile. *Sensors* **2008**, *8*, 3719–3732. [[CrossRef](#)] [[PubMed](#)]
20. Cochrane, C.; Koncar, V.; Lewandowski, M.; Dufour, C. Design and Development of a Flexible Strain Sensor for Textile Structures Based on a Conductive Polymer Composite. *Sensors* **2007**, *7*, 473–492. [[CrossRef](#)]
21. Teichmann, D.; Kuhn, A.; Leonhardt, S.; Walter, M. The MAIN Shirt: A Textile-Integrated Magnetic Induction Sensor Array. *Sensors* **2014**, *14*, 1039–1056. [[CrossRef](#)] [[PubMed](#)]
22. Lin, X.; Seet, B.C. Battery-Free Smart Sock for Abnormal Relative Plantar Pressure Monitoring. *IEEE Trans. Biomed. Circuits Syst.* **2017**, *11*, 464–473. [[CrossRef](#)] [[PubMed](#)]
23. Trindade, I.; da Silva, J.M.; Rui, M.; Pereira, M.; Lucas, J.; Oliveira, L.; Valentim, B.; Barreto, J.; Santos, S.; Silva, M. Design and Evaluation of Novel Textile Wearable Systems for the Surveillance of Vital Signals. *Sensors* **2016**, *16*, 1573. [[CrossRef](#)] [[PubMed](#)]
24. McKnight, M.; Agcayazi, T.; Kausche, H.; Ghosh, T.; Bozkurt, A. Sensing textile seam-line for wearable multimodal physiological monitoring. In Proceedings of the 2016 38th Annual International Conference of the IEEE Engineering in Medicine and Biology Society (EMBC), Orlando, FL, USA, 16–20 August 2016; pp. 311–314.

25. Min, S.D.; Yun, Y.; Shin, H. Simplified Structural Textile Respiration Sensor Based on Capacitive Pressure Sensing Method. *IEEE Sens. J.* **2014**, *14*, 3245–3251.
26. Liu, J.J.; Huang, M.C.; Xu, W.; Zhang, X.; Stevens, L.; Alshurafa, N.; Sarrafzadeh, M. BreathSens: A Continuous On-Bed Respiratory Monitoring System with Torso Localization Using an Unobtrusive Pressure Sensing Array. *IEEE J. Biomed. Health Inform.* **2015**, *19*, 1682–1688. [[CrossRef](#)] [[PubMed](#)]
27. Lin, F.; Wang, A.; Zhuang, Y.; Tomita, M.R.; Xu, W. Smart Insole: A Wearable Sensor Device for Unobtrusive Gait Monitoring in Daily Life. *IEEE Trans. Ind. Inform.* **2016**, *12*, 2281–2291. [[CrossRef](#)]
28. Zhou, B.; Sundholm, M.; Cheng, J.; Cruz, H.; Lukowicz, P. Never skip leg day: A novel wearable approach to monitoring gym leg exercises. In Proceedings of the 2016 IEEE International Conference on Pervasive Computing and Communications (PerCom), Sydney, NSW, Australia, 14–19 March 2016; pp. 1–9.
29. Holleczeck, T.; Regg, A.; Harms, H.; Troster, G. Textile pressure sensors for sports applications. In Proceedings of the 2010 IEEE SENSORS, Kona, HI, USA, 1–4 November 2010; pp. 732–737.
30. Meyer, J.; Lukowicz, P.; Troster, G. Textile Pressure Sensor for Muscle Activity and Motion Detection. In Proceedings of the 2006 10th IEEE International Symposium on Wearable Computers, Montreux, Switzerland, 11–14 October 2006; pp. 69–72.
31. Zhou, B.; Cheng, J.; Lukowicz, P.; Reiss, A.; Amft, O. Monitoring Dietary Behavior with a Smart Dining Tray. *IEEE Pervasive Comput.* **2015**, *14*, 46–56. [[CrossRef](#)]
32. Lin, X.; Seet, B.C. A Linear Wide-Range Textile Pressure Sensor Integrally Embedded in Regular Fabric. *IEEE Sens. J.* **2015**, *15*, 5384–5385. [[CrossRef](#)]
33. Meyer, J.; Arnrich, B.; Schumm, J.; Troster, G. Design and Modeling of a Textile Pressure Sensor for Sitting Posture Classification. *IEEE Sens. J.* **2010**, *10*, 1391–1398. [[CrossRef](#)]
34. Choi, S.; Jiang, Z. A novel wearable sensor device with conductive fabric and PVDF film for monitoring cardiorespiratory signals. *Sens. Actuators A Phys.* **2006**, *128*, 317–326. [[CrossRef](#)]
35. Xu, W.; Huang, M.-C.; Amini, N.; He, L.; Sarrafzadeh, M. eCushion: A textile pressure sensor array design and calibration for sitting posture analysis. *IEEE Sens. J.* **2013**, *13*, 3926–3934. [[CrossRef](#)]
36. Goy, C.B.; Menichetti, V.; Yanicelli, L.M.; Lucero, J.B.; López, M.A.; Parodi, N.F.; Herrera, M.C. Design, fabrication and metrological evaluation of wearable pressure sensors. *J. Med. Eng. Technol.* **2015**, *39*, 208–215. [[CrossRef](#)] [[PubMed](#)]
37. Statex Website. Available online: <http://www.statex.biz/> (accessed on 10 December 2017).
38. Klemm, M.; Locher, I.; Trster, G. A Novel Circularly Polarized Textile Antenna for Wearable Applications. In Proceedings of the 34th European Microwave Conference, Amsterdam, The Netherlands, 12–14 October 2004; Volume 1, pp. 137–140.
39. Locher, I.; Klemm, M.; Kirstein, T.; Trster, G. Design and Characterization of Purely Textile Patch Antennas. *IEEE Trans. Adv. Packag.* **2006**, *29*, 777–788. [[CrossRef](#)]
40. Ouyang, Y.; Chappell, W.J. High Frequency Properties of Electro-Textiles for Wearable Antenna Applications. *IEEE Trans. Antennas Propag.* **2008**, *56*, 381–389. [[CrossRef](#)]
41. Salonen, P.; Hurme, H. A Novel Fabric WLAN Antenna for Wearable Applications. In Proceedings of the IEEE Antennas and Propagation Society International Symposium, Columbus, OH, USA, 22–27 June 2003; Volume 2, pp. 700–703.
42. Antistat Website. Available online: <http://www.antistat.co.uk/> (accessed on 10 December 2017).
43. Cheng, J.; Sundholm, M.; Zhou, B.; Hirsch, M.; Lukowicz, P. Smart-surface: Large scale textile pressure sensors arrays for activity recognition. *Pervasive Mob. Comput.* **2016**, *30*, 97–112. [[CrossRef](#)]

