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Data Article

Comprehensive data compilation on the mechanical properties of refractory high-entropy alloys

J.-P. Couzinié^{a,*}, O.N. Senkov^b, D.B. Miracle^b, G. Dirras^c^a Université Paris Est, ICMPE (UMR 7182) CNRS-UPEC, 2-8 rue Henri Dunant, 94320 Thiais, France^b Air Force Research Laboratory, Materials and Manufacturing Directorate, Wright-Patterson AFB, OH 45433, USA^c Université Paris 13, LSPM (UPR 3407) CNRS, 99 avenue J.B. Clément, 93430 Villetaneuse, France

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ABSTRACT

This data article presents the compilation of mechanical properties for 122 refractory high entropy alloys (RHEAs) and refractory complex concentrated alloys (RCCAs) reported in the period from 2010 to the end of January 2018. The data sheet gives alloy composition, type of microstructures and the metallurgical states in which the properties are measured. Data such as the computed alloy mass density, the type of mechanical loadings to which they are subjected and the corresponding macroscopic mechanical properties, such as the yield stress, are made available as a function of the testing temperature. For practical use, the data are tabulated and some are also graphically presented, allowing at a glance to access relevant information for this attractive category of RHEAs and RCCAs.

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Specifications table

Subject area	Materials Science
More specific subject area	Refractory high-entropy alloys (RHEAs) and refractory complex concentrated alloys (RCCAs)

* Corresponding author.

E-mail address: couzini@icmpe.cnrs.fr (J.-P. Couzinié).

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Type of data	Table, figures
How data was acquired	Compilation of data from available literature. Data extracted from studies on 122 alloys reported in the period from 2010 to January 2018
Data format	Analyzed
Experimental factors	Data compilation from available literature. Data sheet contains about 54 references.
Experimental Features	Extensive Data compilation. Alloys' mass densities and Young modulus were computed using the rule of mixtures (ROM) for the different reported alloy compositions.
Data source location	From the literature, as well as the authors' calculations. References are given in the corresponding sections.
Data accessibility	Data are with the article
Related research article	Direct submission. Most relevant research article: Senkov, Oleg; Miracle, Daniel; Chaput, Kevin; Couzinié, Jean-Philippe, Development and Exploration of Refractory High Entropy Alloys – A Review, <i>Journal of Materials Research</i> , 33 (19), (2018), 3092–3128, https://doi.org/10.1557/jmr.2018.153 [1]

Value of the data

- The comprehensive data compilation provides up-to-date mechanical properties of RHEAs and RCCAs tested under uniaxial loading on the basis of published reports from 2010 through the end of January 2018.
- The dataset contains pertinent references, readily accessible to all researchers.
- Processed data may be used to evaluate the potential of RHEAs and RCCAs as possible structural materials.
- The data compilation can be used as a primary tool and as a guidance for further development of RHEAs and RCCAs.
- This data compilation can enable machine learning and data analytics methods to extract insights and trends not available from individual studies, thus accelerating the development of these alloys.

1. Data

Refractory High Entropy Alloys (RHEAs) and Refractory Complex Concentrated Alloys (RCCAs) are attractive materials and promising candidates for structural high temperature applications. Deriving from a new alloying design strategy, RHEAs contain five or more elements with concentration between 5 and 35 at% and RCCAs expand this vast range of new alloys even further by including three or more principal elements and expanding the concentrations of these elements beyond 35% [1]. Further, RHEAs are sometimes considered to be only single-phase, disordered solid solution alloys, while RCCAs can have any number of phases and can also include ordered, intermetallic phases. The presented database is a compilation of the mechanical properties of RHEAs and RCCAs from a large number of studies published during the 2010-January 2018 period. Each row in Table 1 corresponds to one mechanical test for an alloy composition in an experimentally characterized metallurgical condition. The data are gathered in a table compiling all the published results such that it could be graphically represented and analyzed afterward [2]. The table also provides the alloy densities calculated in this work using rule of mixtures (ROM), as well as Young's moduli for single-phase alloys calculated using ROM.

2. Experimental design, materials, and methods

The presented data sheet is a compilation of essential data on RHEAs and RCCAs. All RHEAs and RCCAs reported in the literature through the end of January 2018 crystallize with at least one phase

Table 1

RHEAs and RCCAs for which mechanical tests are reported in literature. Each line represents the result of a test on a specific alloy composition. The experimental Young modulus is given in brackets in the adequate column. Values appearing in brackets in the yield strength column correspond to the fracture stress without plastic deformation See text for explanations [57–60].

Composition (mole fraction)	Ref.	ρ ($\text{g}\cdot\text{cm}^{-3}$) ROM	Young modulus (GPa) ROM	Young Modulus (GPa) (experimental) /first principles	Equilibrium conditions	Single/ Multiphase material	Type of present phases	Tension/ Compression	Testing T (°C)	σ_V (MPa)	σ_V/ρ ($\text{MPa}\cdot\text{cm}^3\cdot\text{g}^{-1}$)
Al0.25MoNbTiV	[3]	7.1	163.6	168.0 [57]	AC	S	BCC	C	RT	1250	176.9
Al0.25NbTaTiV	[4]	8.8	130.0	(94.0)	AC	S	BCC	C	RT	1330	151.2
Al0.25NbTaTiZr	[5]	8.6		(118.0)	HIP+A	M	BCC+B2	C	RT	1745	203.1
Al0.25NbTaTiZr	[5]	8.6		(63.0)	HIP+A	M	BCC+B2	C	1000	366	42.6
Al0.2MoTaTiV	[6]	9.3	184.0		AC	S	BCC	C	RT	1021	110.3
Al0.3HfNbTaTiZr	[7]	9.6	108.3	(63.0)	AC	S	BCC	C	RT	1188	124.4
Al0.3NbTa0.8Ti1.4V0.2Zr1.3	[8]	7.7	110.2		HIP+A	S	BCC	C	RT	1965	255.0
Al0.3NbTa0.8Ti1.4V0.2Zr1.3	[8]	7.7			HIP+A	S	BCC	C	1000	166	21.5
Al0.3NbTa0.8Ti1.4V0.2Zr1.3	[8]	7.7			HIP+A	S	BCC	C	800	678	88.0
Al0.3NbTaTi1.4Zr1.3	[8]	8.1			HIP+A	M	BCC+B2	C	RT	1965	242.9
Al0.3NbTaTi1.4Zr1.3	[8]	8.1			HIP+A	M	BCC+B2	C	1000	236	29.2
Al0.3NbTaTi1.4Zr1.3	[8]	8.1			HIP+A	M	BCC+B2	C	800	362	44.7
Al0.4Hf0.6NbTaTiZr	[8]	9.1	110.0		HIP+A	S	BCC	C	RT	1841	202.5
Al0.4Hf0.6NbTaTiZr	[8]	9.1			HIP+A	S	BCC	C	1000	298	32.8
Al0.4Hf0.6NbTaTiZr	[8]	9.1			HIP+A	S	BCC	C	800	796	87.6
Al0.4Hf0.6NbTaTiZr	[9]	9.1	110.0	(78.1)	HIP+A	S	BCC	C	RT	1841	202.5
Al0.4Hf0.6NbTaTiZr	[9]	9.1			HIP+A	S	BCC	C	1200	89	9.8

Ai0.4Hf0.6NbTaTiZr	[9]	9.1	(23.3)	HIP+A	S	BCC	C	1000	298	32.8
Ai0.4Hf0.6NbTaTiZr	[9]	9.1	(48.8)	HIP+A	S	BCC	C	800	796	87.6
Ai0.5CrNbTi2V0.5	[10]	5.8		A	M	BCC+Laves	C	RT	1340	232.4
Ai0.5CrNbTi2V0.5	[10]	5.8	143.0	AC	S	BCC	C	RT	1240	215.0
Ai0.5CrNbTi2V0.5	[10]	5.8		A	M	BCC+Laves	C	1000	90	15.6
Ai0.5CrNbTi2V0.5	[10]	5.8		A	M	BCC+Laves	C	800	445	77.2
Ai0.5CrNbTi2V0.5	[10]	5.8		A	M	BCC+Laves	C	600	930	161.3
Ai0.5HfNbTaTiZr	[7]	9.3	106.9	AC	S	BCC	C	RT	1302	139.4
Ai0.5Mo0.5NbTa0.5TiZr	[5]	7.6	(132.0)	HIP+A	M	BCC+H2	C	RT	2350	309.7
Ai0.5Mo0.5NbTa0.5TiZr	[5]	7.6	(78.0)	HIP+A	M	BCC+H2	C	1000	579	76.3
Ai0.5MoNbTiV	[3]	6.8	158.4	AC	S	BCC	C	RT	1625	238.3
Ai0.5NbTa0.8Ti1.5V0.2Zr	[8]	7.6	111.3	HIP+A	M	BCC+H2	C	RT	2035	269.2
Ai0.5NbTa0.8Ti1.5V0.2Zr	[8]	7.6		HIP+A	M	BCC+H2	C	1000	220	29.1
Ai0.5NbTa0.8Ti1.5V0.2Zr	[8]	7.6		HIP+A	M	BCC+H2	C	800	796	105.3
Ai0.5NbTaTiV	[4]	8.5	126.7	AC	S	BCC	C	RT	1012	119.6
Ai0.6MoTaTiV	[6]	8.7	174.1	AC	S	BCC	C	RT	962	110.9
Ai0.75HfNbTaTiZr	[7]	9.1	105.3	AC	S	BCC	C	RT	1415	155.6
Ai0.75MoNbTiV	[3]	6.6	153.8	AC	S	BCC	C	RT	1260	191.0
Ai1.5MoNbTiV	[3]	6.1	142.4	AC	S	BCC	C	RT	500	82.5
AiCr0.5NbTiV	[11]	5.6	124.1	A	S	BCC	C	RT	1300	230.6
AiCr0.5NbTiV	[11]	5.6		A	S	BCC	C	1000	40	7.1
AiCr0.5NbTiV	[11]	5.6		A	S	BCC	C	800	640	113.5
AiCr1.5NbTiV	[11]	5.6		A	S	BCC	C	600	1005	178.2
AiCr1.5NbTiV	[11]	5.9		A	M	BCC+Laves	C	RT	1700	290.1
AiCr1.5NbTiV	[11]	5.9		A	M	BCC+Laves	C	1000	75	12.8
AiCr1.5NbTiV	[11]	5.9		A	M	BCC+Laves	C	800	970	165.5
AiCr1.5NbTiV	[11]	5.9		A	M	BCC+Laves	C	600	1370	233.8
AiCrMoNbTi	[12]	6.6		A	M	BCC+unknown	C	RT	(1010)	-
AiCrMoNbTi	[12]	6.6		A	M	BCC+unknown	C	1200	105	16.0
AiCrMoNbTi	[12]	6.6		A	M	BCC+unknown	C	1000	594	90.5

AICrMoNbTi	[12]	6.6				A	M		C	800	860	131.0
AICrMoNbTi	[12]	6.6				A	M		C	600	1060	161.4
AICrMoNbTi	[12]	6.6				A	M		C	400	1080	164.5
AICrMoNbTi	[13]	6.6				A	S		BCC	1200	150	22.8
AICrMoNbTi	[13]	6.6				A	S		BCC	1000	550	83.8
AICrMoNbTi	[13]	6.6				A	S		BCC	800	875	133.2
AICrMoNbTi	[13]	6.6				A	S		BCC	600	930	141.6
AICrMoTi	[13]	6.0				A	S		BCC	1200	100	16.7
AICrMoTi	[13]	6.0				A	S		BCC	1000	375	62.7
AICrMoTi	[13]	6.0				A	S		BCC	800	875	146.3
AICrMoTi	[13]	6.0				A	S		BCC	600	1020	170.5
AICrMoTi	[13]	6.0				A	S		BCC	400	1070	178.9
AICrNbTiV	[11]	5.8				A	M		BCC+Laves	RT	1550	269.2
AICrNbTiV	[11]	5.8				A	M		BCC+Laves	1000	65	11.3
AICrNbTiV	[11]	5.8				A	M		BCC+Laves	800	860	149.4
AICrNbTiV	[11]	5.8				A	M		BCC+Laves	600	1015	176.3
AlHfNbTiZr	[7]	8.9			(103.0)	AC	M		2 BCC	RT	1489	168.0
AlMo0.5Nb1.00.5TiZr	[5]	7.1			(122.0)	HfP+A	M		BCC+B2	RT	2197	307.4
AlMo0.5Nb1.00.5TiZr	[5]	7.1			(70.0)	HfP+A	M		BCC+B2	1000	745	104.2
AlMo0.5Nb1.00.5TiZr	[8]	7.1				HfP+A	M		BCC+B2	RT	2000	279.8
AlMo0.5Nb1.00.5TiZr	[8]	7.1				HfP+A	M		BCC+B2	1000	745	104.2
AlMo0.5Nb1.00.5TiZr	[9]	7.1			(178.6)	HfP+A	M		BCC+B2	800	1597	223.4
AlMo0.5Nb1.00.5TiZr	[9]	7.1			(27.0)	HfP+A	M		BCC+B2	RT	2000	279.8
AlMo0.5Nb1.00.5TiZr	[9]	7.1			(36.0)	HfP+A	M		BCC+B2	1200	250	35.0
AlMo0.5Nb1.00.5TiZr	[9]	7.1			(80.0)	HfP+A	M		BCC+B2	1000	745	104.2
AlMo0.5Nb1.00.5TiZr	[14]	7.1				HfP+A	M		BCC+B2	800	1597	223.4
AlMo0.5Nb1.00.5TiZr	[14]	7.1				HfP+A	M		BCC+B2	RT	2000	279.8
AlMo0.5Nb1.00.5TiZr	[14]	7.1				HfP+A	M		BCC+B2	1200	250	35.0
AlMo0.5Nb1.00.5TiZr	[14]	7.1				HfP+A	M		BCC+B2	1000	745	104.2
AlMo0.5Nb1.00.5TiZr	[14]	7.1				HfP+A	M		BCC+B2	800	1597	223.4

AINbTiVZr0.1	[16]	5.5				A	M	B2+Al3Zr5	C	RT	1290	233.2
AINbTiVZr0.1	[16]	5.5				A	M	B2+Al3Zr5	C	800	865	156.4
AINbTiVZr0.1	[16]	5.5				A	M	B2+Al3Zr5	C	600	975	176.3
AINbTiVZr0.25	[16]	5.6				A	M	B2+Al3Zr5	C	RT	1360	243.8
AINbTiVZr0.25	[16]	5.6				A	M	B2+Al3Zr5	C	800	855	153.3
AINbTiVZr0.25	[16]	5.6				A	M	B2+Al3Zr5	C	600	1065	190.9
AINbTiVZr0.5	[16]	5.6				A	M	B2+Al3Zr5+Laves	C	RT	1485	262.9
AINbTiVZr0.5	[16]	5.6				A	M	B2+Al3Zr5+Laves	C	800	675	119.5
AINbTiVZr0.5	[16]	5.6				A	M	B2+Al3Zr5+Laves	C	600	1135	200.9
AINbTiVZr1.5	[16]	5.8				A	M	B2+Al3Zr5+Laves	C	RT	1535	262.6
AINbTiVZr1.5	[16]	5.8				A	M	B2+Al3Zr5+Laves	C	800	180	30.8
AINbTiVZr1.5	[16]	5.8				A	M	B2+Al3Zr5+Laves	C	600	(1195)	204.4
Co.1Hf0.5Mo0.5NbTiZr	[17]	7.8				AC	M	BCC+MC	C	RT	1183	151.5
Co.3Hf0.5Mo0.5NbTiZr	[17]	7.7				AC	M	BCC+MC	C	RT	1201	156.2
CoCrMoNb	[18]	8.8				AC	M	BCC+Laves	C	RT	(1419.6)	-
CoCrMoNbTi	[18]	7.8				AC	M	BCC+Laves	C	RT	(1096.8)	-
CoCrMoNbTi0.2	[18]	8.5				AC	M	BCC+Laves	C	RT	(1905.6)	-
CoCrMoNbTi0.4	[18]	8.3	220.1			AC	S	BCC	C	RT	(1771.3)	-
CoCrMoNbTi0.5	[18]	8.2				AC	M	BCC+Laves	C	RT	(1609.2)	-
CrHfNbTiZr	[19]	8.2			(112.0)	A	M	BCC+Laves	C	RT	1457	176.9
CrHfNbTiZr	[19]	8.2			(112.0)	A	M	BCC+Laves	C	RT	1420	172.4
CrHfNbTiZr	[19]	8.2			(112.0)	AC	M	BCC+Laves	C	RT	1375	167.0
CrHfNbTiZr	[19]	8.2			(112.0)	A	M	BCC+Laves	C	RT	1328	161.3
CrHfNbTiZr	[19]	8.2			(112.0)	A	M	BCC+Laves	C	RT	1322	160.5
CrMo0.5NbTi0.5TiZr	[20]	8.0				HfP+A	M	2 BCC+Laves	C	RT	1595	199.5
CrMo0.5NbTi0.5TiZr	[20]	8.0				HfP+A	M	2 BCC+Laves	C	1200	170	21.3
CrMo0.5NbTi0.5TiZr	[20]	8.0				HfP+A	M	2 BCC+Laves	C	1000	546	68.3
CrMo0.5NbTi0.5TiZr	[20]	8.0				HfP+A	M	2 BCC+Laves	C	800	983	122.9
CrNbTiVZr	[21]	6.6				HfP+A	M	BCC+Laves	C	RT	1298	197.8
CrNbTiVZr	[21]	6.6				HfP+A	M	BCC+Laves	C	1000	259	39.5

Hf0.75NbTa0.5Ti1.5Zr1.25	[26]	8.4		(80.0)	CR+A	S	BCC	C	72	640	76.1
Hf0.75NbTa0.5Ti1.5Zr1.25	[26]	8.4		(78.0)	CR	S	BCC	C	-43	1200	142.7
Hf0.75NbTa0.5Ti1.5Zr1.25	[26]	8.4		(78.0)	CR	S	BCC	C	-43	1180	140.3
Hf0.75NbTa0.5Ti1.5Zr1.25	[26]	8.4		(80.0)	CR+A	S	BCC	C	-43	1020	121.3
Hf0.75NbTa0.5Ti1.5Zr1.25	[26]	8.4		(78.0)	CR	S	BCC	C	-103	1380	164.1
Hf0.75NbTa0.5Ti1.5Zr1.25	[26]	8.4		(78.0)	CR	S	BCC	C	-103	1370	162.9
Hf0.75NbTa0.5Ti1.5Zr1.25	[26]	8.4		(80.0)	CR+A	S	BCC	C	-103	1250	148.6
Hf0.75NbTa0.5Ti1.5Zr1.25	[26]	8.4		(78.0)	CR	S	BCC	C	-153	1640	195.0
Hf0.75NbTa0.5Ti1.5Zr1.25	[26]	8.4		(78.0)	CR	S	BCC	C	-153	1550	184.3
Hf0.75NbTa0.5Ti1.5Zr1.25	[26]	8.4		(80.0)	CR+A	S	BCC	C	-153	1370	162.9
Hf0.75NbTa0.5Ti1.5Zr1.25	[26]	8.4		(80.0)	CR+A	S	BCC	C	-196	1920	228.3
Hf0.75NbTa0.5Ti1.5Zr1.25	[26]	8.4		(78.0)	CR	S	BCC	C	-196	1880	223.5
Hf0.75NbTa0.5Ti1.5Zr1.25	[26]	8.4		(78.0)	CR	S	BCC	C	-196	1750	208.1
Hf0.75NbTa0.5Ti1.5Zr1.25	[26]	8.4		(80.0)	CR+A	S	BCC	C	-268.8	2390	284.2
Hf0.75NbTa0.5Ti1.5Zr1.25	[26]	8.4		(78.0)	CR	S	BCC	C	-268.8	2250	267.5
Hf0.75NbTa0.5Ti1.5Zr1.25	[26]	8.4		(78.0)	CR	S	BCC	C	-268.8	2210	262.8
HfMe0.25NbTa1Zr	[27]	9.9	121.0	(96.0)	AC	S	BCC	C	RT	1112	112.2
HfMe0.5NbSi0.3TiV0.5	[28]	8.5			AC	M	BCC+M5Si3	C	RT	1617	191.0
HfMe0.5NbSi0.3TiV0.5	[28]	8.5			AC	M	BCC+M5Si3	C	1200	166	19.6
HfMe0.5NbSi0.3TiV0.5	[28]	8.5			AC	M	BCC+M5Si3	C	1000	398	47.0
HfMe0.5NbSi0.5TiV0.5	[28]	8.2			AC	M	BCC+M5Si3	C	RT	1787	218.7
HfMe0.5NbSi0.5TiV0.5	[28]	8.2			AC	M	BCC+M5Si3	C	1200	188	23.0
HfMe0.5NbSi0.5TiV0.5	[28]	8.2			AC	M	BCC+M5Si3	C	1000	614	75.2
HfMe0.5NbSi0.7TiV0.5	[28]	7.9			AC	M	BCC+M5Si3	C	RT	2134	270.1
HfMe0.5NbSi0.7TiV0.5	[28]	7.9			AC	M	BCC+M5Si3	C	1200	235	29.7
HfMe0.5NbSi0.7TiV0.5	[28]	7.9			AC	M	BCC+M5Si3	C	1000	673	85.2
HfMe0.5NbTa1Zr	[27]	9.9	130.5	(102.0)	AC	S	BCC	C	RT	1317	132.8
HfMe0.5NbTiV0.5	[28]	9.0	131.9		AC	S	BCC	C	RT	1260	140.4
HfMe0.5NbTiV0.5	[28]	9.0			AC	S	BCC	C	1200	60	6.7
HfMe0.5NbTiV0.5	[28]	9.0			AC	S	BCC	C	1000	368	41.0

HfMo _{0.75} NbTaTiZr	[27]	9.9	139.1	(109.0) (115)/136.6 [58]	AC	S	BCC	C	RT	1373	138.3
HfMoNbTaTiZr	[27]	9.9	147.0		AC	S	BCC	C	RT	1512	152.1
HfMoNbTaTiZr	[29]	9.9	147.0	136.6 [58]	AC	S	BCC	C	RT	1512	152.1
HfMoNbTaTiZr	[29]	9.9			AC	S	BCC	C	1200	556	55.9
HfMoNbTaTiZr	[29]	9.9			AC	S	BCC	C	1000	814	81.9
HfMoNbTaTiZr	[29]	9.9			AC	S	BCC	C	800	1007	101.3
HfMoNbTaTiZr	[30]	8.7	139.2		AC	S	BCC	C	RT	1719	197.9
HfMoNbTaTiZr	[30]	8.7	139.2		A	S	BCC	C	RT	1575	181.3
HfMoNbTaTiZr	[30]	8.7			AC	S	BCC	C	1200	187	21.5
HfMoNbTaTiZr	[30]	8.7			AC	S	BCC	C	1100	397	45.7
HfMoNbTaTiZr	[30]	8.7			AC	S	BCC	C	1000	635	73.1
HfMoNbTaTiZr	[30]	8.7			AC	S	BCC	C	900	728	83.8
HfMoNbTaTiZr	[30]	8.7			AC	S	BCC	C	800	825	95.0
HfMoTaTiZr	[29]	10.2	155.4		AC	S	BCC	C	RT	1600	157.0
HfMoTaTiZr	[29]	10.2			AC	S	BCC	C	1200	404	39.6
HfMoTaTiZr	[29]	10.2			AC	S	BCC	C	1000	855	83.9
HfMoTaTiZr	[29]	10.2			AC	S	BCC	C	800	1045	102.5
HfNb _{0.18} Ta _{0.18} Ti _{1.27} Zr	[31]	8.5	95.2	(79.0)	CR+A	S	BCC	T	RT	540	63.8
HfNb _{50.5} TiV	[32]	7.8			AC	M	BCC+M5S3	C	RT	1399	179.3
HfNb _{50.5} TiV	[32]	7.8			AC	M	BCC+M5S3	C	1000	240	30.8
HfNb _{50.5} TiV	[33]	7.8			AC	M	BCC+M5S3	C	800	875	112.2
HfNb _{50.5} TiVZr	[33]	7.5			AC	M	BCC+Laves+M5S3	C	RT	1540	204.9
HfNb _{50.5} TiVZr	[33]	7.5			A	M	BCC+Laves+M5S3	C	RT	1483	197.4
HfNb _{50.5} TiVZr	[33]	7.5			AC	M	BCC+Laves+M5S3	C	800	371	49.4
HfNb _{50.5} TiVZr	[33]	7.5			A	M	BCC+Laves+M5S3	C	800	102	13.6
HfNb _{50.5} TiVZr	[33]	7.5			AC	M	BCC+Laves+M5S3	C	600	920	122.4
HfNb _{50.5} TiVZr	[33]	7.5			A	M	BCC+Laves+M5S3	C	600	597	79.4
HfNb _{50.5} TiVZr	[33]	7.5			A	M	BCC+Laves+M5S3	C	400	1273	169.4
HfNbTaTiZr	[7]	9.9	110.6	(55)/88.9 [58]/104.1 [19]	AC	S	BCC	C	RT	1073	108.4

HFNBtTa1Zr	[27]	9.9	110.6	$\frac{85}{58}/\frac{88.9}{104.1}$ [19]	AC	S	BCC	C	RT	1015	102.6
HFNBtTa1Zr	[34]	9.9			SPD+A	M	BCC+HCP	T	RT	1520	153.6
HFNBtTa1Zr	[34]	9.9			SPD+A	M	2 BCC+HCP	T	RT	795	80.4
HFNBtTa1Zr	[34]	9.9	110.6	$\frac{88.9}{58}/\frac{104.1}{119}$	SPD	S	BCC	T	RT	1900	192.0
HFNBtTa1Zr	[34]	9.9	110.6	$\frac{88.9}{58}/\frac{104.1}{119}$	CR+A	S	BCC	T	RT	830	83.9
HFNBtTa1Zr	[35]	9.9	110.6	$\frac{69.3}{58}/\frac{88.9}{104.1}$ [19]	CR+A	M	2 BCC	T	RT	1303	131.7
HFNBtTa1Zr	[35]	9.9	110.6	$\frac{69.3}{58}/\frac{88.9}{104.1}$ [19]	CR	S	BCC	T	RT	1202	121.5
HFNBtTa1Zr	[35]	9.9	110.6	$\frac{69.2}{58}/\frac{88.9}{104.1}$ [19]	CR+A	S	BCC	T	RT	1145	115.7
HFNBtTa1Zr	[36]	9.9	110.6	$\frac{81.0}{58}/\frac{88.9}{104.1}$ [19]	CR+A	S	BCC	T	RT	958	96.8
HFNBtTa1Zr	[36]	9.9	110.6	$\frac{81.0}{58}/\frac{88.9}{104.1}$ [19]	CR+A	S	BCC	T	RT	944	95.4
HFNBtTa1Zr	[36]	9.9	110.6	$\frac{81.0}{58}/\frac{88.9}{104.1}$ [19]	CR+A	S	BCC	T	RT	940	95.0
HFNBtTa1Zr	[37]	9.9	110.6	$\frac{92.0}{58}/\frac{88.9}{104.1}$ [19]	CR+A	S	BCC	T	RT	940	95.0
HFNBtTa1Zr	[38]	9.9	110.6	$\frac{88.9}{58}/\frac{104.1}{119}$	HIP+A	S	BCC	C	RT	929	93.9
HFNBtTa1Zr	[39]	9.9	110.6	$\frac{88.9}{58}/\frac{104.1}{119}$	AC	S	BCC	C	RT	905	91.5
HFNBtTa1Zr	[40]	9.9	110.6	$\frac{88.9}{58}/\frac{104.1}{119}$	AC	S	BCC	C	RT	890	90.0
HFNBtTa1Zr	[41]	9.9	110.6	$\frac{88.9}{58}/\frac{104.1}{119}$	AC	S	BCC	T	RT	828	83.7
HFNBtTa1Zr	[41]	9.9	110.6	$\frac{88.9}{58}/\frac{104.1}{119}$	AC	S	BCC	T	RT	827	83.6
HFNBtTa1Zr	[41]	9.9	110.6	$\frac{88.9}{58}/\frac{104.1}{119}$	AC	S	BCC	T	RT	820	82.9
HFNBtTa1Zr	[41]	9.9	110.6	$\frac{88.9}{58}/\frac{104.1}{119}$	AC	S	BCC	T	RT	803	81.2
HFNBtTa1Zr	[42]	9.9			HIP+A	S	BCC	C	1200	92	9.3
HFNBtTa1Zr	[42]	9.9			HIP+A	S	BCC	C	1000	295	29.8
HFNBtTa1Zr	[42]	9.9			HIP+A	S	BCC	C	800	535	54.1
HFNBtTa1Zr	[42]	9.9			HIP+A	S	BCC	C	800	475	48.0
HFNBtTa1Zr	[42]	9.9			HIP+A	S	BCC	C	800	285	28.8
HFNBtTa1Zr	[42]	9.9			HIP+A	S	BCC	C	600	675	68.2

MoNbTaTi0.25W	[47]	13.1	249.4			AC	S	BCC	C	RT	1109	84.7
MoNbTaTi0.5W	[47]	12.6	242.0			AC	S	BCC	C	RT	1211	96.1
MoNbTaTi0.75W	[47]	12.2	235.4			AC	S	BCC	C	RT	1304	107.3
MoNbTaTiV	[48]	9.4	172.8	130.5 [58]/139.2 [48]		AC	S	BCC	C	RT	1400	149.4
MoNbTaTiW	[49]	11.0	212.5	(164.0)		AC	S	BCC	C	RT	1515	138.1
MoNbTaTiW	[49]	11.0				AC	S	BCC	C	1200	659	60.1
MoNbTaTiW	[49]	11.0				AC	S	BCC	C	1000	752.8	68.6
MoNbTaTiW	[49]	11.0				AC	S	BCC	C	800	791.3	72.1
MoNbTaTiW	[49]	11.0				AC	S	BCC	C	600	973	88.7
MoNbTaTiW	[47]	11.8	229.4			AC	S	BCC	C	RT	1455	123.8
MoNbTaTiW	[49]	11.8	229.4	(156.0)		AC	S	BCC	C	RT	1343	114.2
MoNbTaTiW	[49]	11.8				AC	S	BCC	C	1200	586	49.8
MoNbTaTiW	[49]	11.8				AC	S	BCC	C	1000	620	52.7
MoNbTaTiW	[49]	11.8				AC	S	BCC	C	800	674	57.3
MoNbTaTiW	[49]	11.8				AC	S	BCC	C	600	689	58.6
MoNbTaTiZr	[50]	9.1			(153.0)	AC	M	2 BCC	C	RT	1390	152.2
MoNbTaTiZr	[51]	9.1				AC	M	2 BCC	C	RT	1375	150.5
MoNbTaTiZr	[52]	10.7	187.0			A	M	2 BCC	C	RT	1100	120.4
MoNbTaTiV	[52]	10.7	187.0			AC	S	BCC	C	RT	1525	142.7
MoNbTaTiW	[53]	12.4	231.8	204.5 [19]/218.0 [58]		SPS	S	BCC	C	RT	2612	211.0
MoNbTaTiW	[54]	12.4	231.8	(180.0)/204.5 [19]/218.0 [58]		HIP+A	S	BCC	C	RT	1246	100.7
MoNbTaTiW	[54]	12.4				HIP+A	S	BCC	C	1600	477	38.5
MoNbTaTiW	[54]	12.4				HIP+A	S	BCC	C	1400	656	53.0
MoNbTaTiW	[54]	12.4				HIP+A	S	BCC	C	1200	735	59.4
MoNbTaTiW	[54]	12.4				HIP+A	S	BCC	C	1000	842	68.0
MoNbTaTiW	[54]	12.4				HIP+A	S	BCC	C	800	846	68.4
MoNbTaTiW	[54]	12.4				HIP+A	S	BCC	C	600	862	69.6
MoNbTaTiW	[47]	13.7	257.8	228.7 [19]		AC	S	BCC	C	RT	996	72.9
MoNbTaTiW	[54]	13.7	257.8	(220.0)/228.7		HIP+A	S	BCC	C	RT	1058	77.5

MoNbTaW	[54]	13.7		[19]	HIP+A	S	BCC	C	1600	405	29.6
MoNbTaW	[54]	13.7			HIP+A	S	BCC	C	1400	421	30.8
MoNbTaW	[54]	13.7			HIP+A	S	BCC	C	1200	506	37.0
MoNbTaW	[54]	13.7			HIP+A	S	BCC	C	1000	548	40.1
MoNbTaW	[54]	13.7			HIP+A	S	BCC	C	800	552	40.4
MoNbTaW	[54]	13.7			HIP+A	S	BCC	C	600	561	41.1
MoNbTiV	[3]	7.3	169.5	161.1 [57]	AC	S	BCC	C	RT	1200	163.4
MoNbTiV0.25Zr	[55]	7.3	152.9	141.6 [59]	AC	S	BCC	C	RT	1750	241.2
MoNbTiV0.3Zr	[46]	7.2	152.7		AC	S	BCC	C	RT	1455	200.8
MoNbTiV0.5Zr	[55]	7.2	151.6	141.7 [59]	AC	S	BCC	C	RT	1640	227.5
MoNbTiV0.75Zr	[55]	7.2	150.3	141.5 [59]	AC	S	BCC	C	RT	1680	234.5
MoNbTiV1.5Zr	[55]	7.1			AC	M	2 BCC	C	RT	1720	243.9
MoNbTiV2Zr	[55]	7.0			AC	M	2 BCC	C	RT	1520	217.5
MoNbTiV3Zr	[55]	6.9			AC	M	2 BCC	C	RT	1415	205.5
MoNbTiVZr	[46]	7.1	149.2	139.5 [60]/141.1 [59]	AC	S	BCC	C	RT	1779	249.7
MoNbTiVZr	[55]	7.1	149.2	139.5 [60]/141.1 [59]	AC	S	BCC	C	RT	1770	248.5
MoNbTiZr	[55]	7.3	154.5	140.1 [60]/141.7 [59]	AC	S	BCC	C	RT	1560	213.4
MoTaTiV	[6]	9.6	189.8		AC	S	BCC	C	RT	1221	127.4
NbTaTiV	[4]	9.2	133.8	(108.0)	AC	S	BCC	C	RT	1092	119.1
NbTaTiV	[56]	9.2	133.8		AC	S	BCC	C	RT	965	105.2
NbTaTiW	[56]	11.1	189.2	257.3 [58]	AC	S	BCC	C	RT	1420	127.9
NbTaVW	[56]	12.9	207.5		AC	S	BCC	C	RT	1530	118.7
NbTiV0.3Zr	[46]	6.5	99.2		AC	S	BCC	C	RT	866	133.0
NbTiV2Zr	[21]	6.4			HIP+A	M	3 BCC	C	RT	918	143.3
NbTiV2Zr	[21]	6.4			HIP+A	M	3 BCC	C	1000	72	11.2
NbTiV2Zr	[21]	6.4			HIP+A	M	3 BCC	C	800	240	37.5
NbTiV2Zr	[21]	6.4			HIP+A	M	3 BCC	C	600	571	89.1
NbTiVZr	[21]	6.5			HIP+A	M	2 BCC	C	RT	1105	171.1
NbTiVZr	[21]	6.5			HIP+A	M	2 BCC	C	1000	58	9.0
NbTiVZr	[21]	6.5			HIP+A	M	2 BCC	C	800	187	29.0
NbTiVZr	[21]	6.5			HIP+A	M	2 BCC	C	600	834	129.1
NbTiVZr	[46]	6.5	104.3	119.7 [60]/121.1 [59]	AC	S	BCC	C	RT	1104	170.9

with body centered cubic (BCC) structure. The results of 340 mechanical tests on 122 compositions are listed and then partially synthesized in graphical form for better visualization.

Table 1 of the data sheet illustrates the collected data from published studies so far [3–56], for all the RHEAs / RCCAs:

- the *alloy composition*. Alloying elements are classified by alphabetic order and the subscripts indicate atom mole fraction. A subscript of 1 is implied if none is shown.
- the *metallurgical state* of each tested alloy: non-equilibrium state such as-cast state, or optimized state via homogenization and annealing, thermally-processed conditions.
- the *phase content* present in the initial testing condition. From the mechanical properties point of view, it appears crucial, whether an alloy consists of a single phase, or of several phases.
- the *type of mechanical test*: tension or compression. Only mechanical tests with strain rates less than or equal to 10^{-3} s^{-1} are considered here.
- the *testing temperature*.
- The *experimental Young modulus*, when reported.
- the *yield strength* σ_Y .

The *density* of each of the 122 compositions have been calculated on the basis of Rule of Mixtures (ROM) (Eq. 1):

$$\rho_{\text{alloy}} = \frac{\sum_{i=1}^N c_i A_i}{\sum_{i=1}^N c_i M_i} \quad (1)$$

Where c_i is the atomic fraction of element i in the alloy; A_i and M_i are the molar mass and molar volume of element i at room temperature. The *specific strength* is important for some structural applications. Therefore, such an important feature for structural part design, when available, is also listed in Table 1.

The *Young modulus* have also been estimated using ROM for single phase solid solutions (Eq. 2):

$$E_{\text{alloy}} = \sum_{i=1}^N x_i E_i \quad (2)$$

With x_i and E_i are the atomic fraction and the room temperature Young modulus of the alloy element i . Young modulus calculated from *ab initio* methods or determined experimentally are also provided in the table.

Acronyms used in Table 1 represent:

- RT: Room Temperature
- ROM: Rule of Mixtures
- AC: As-Cast
- A: Annealed
- HIP: Hot Isostatic Pressured
- CR: Cold Rolled
- SPS: Spark Plasma Sintering
- SPD: Severe Plastic Deformation
- T: Tension (tensile test)
- C: Compression (compressive test)

It can be seen from Table 1 of the data sheet that RHEAs and RCCAs have been studied over a wide temperature range between $-268.8 \text{ }^\circ\text{C}$ (4.2 K) and $1600 \text{ }^\circ\text{C}$ (1873 K). For quick access and reading, a quantitative representation of the compiled data is illustrated in Figs. 1 and 2. This shows the evolution of yield strength and specific yield strength with temperature for a single phase or multiphase, multi-component alloys whatever the equilibrium condition/alloy processing.

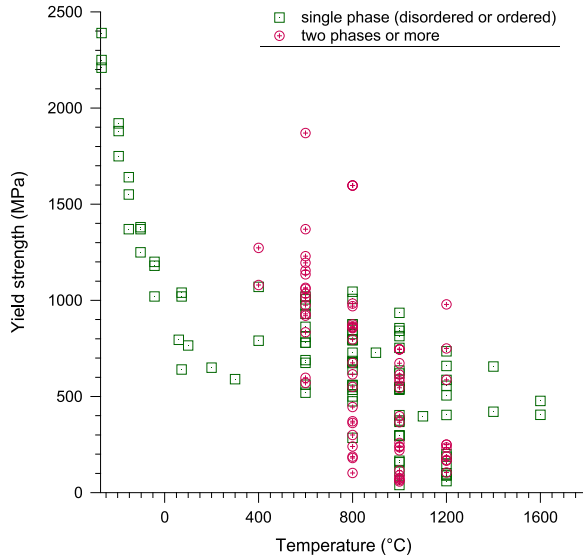


Fig. 1. Evolution of yield strength with temperature in the -268.8°C – 1600°C range. For the sake of clarity all the collected data at room temperature have been excluded of this figure.

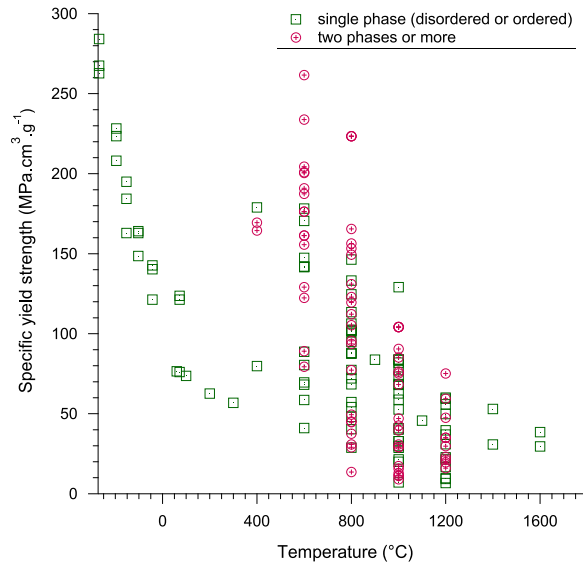


Fig. 2. Evolution of specific yield strength with temperature in the -268.8°C – 1600°C range. For the sake of clarity all the collected data at room temperature have been excluded of this figure.

The data have been processed in order to directly visualize the evolution of mechanical properties with density, which could be very useful in the research for material solutions for applications at a given temperature. Figs. 3 and 4 display the evolution of yield stress with alloy density for the different multi-component at room temperature and 800°C , respectively.

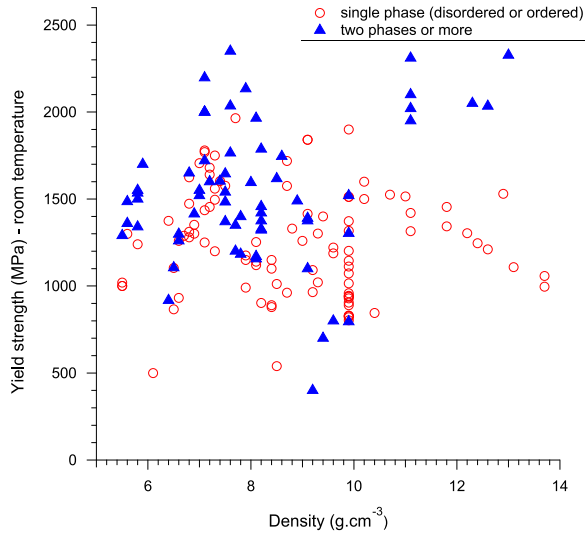


Fig. 3. Evolution of yield strength of RHEAs and RCCAs with alloy density at room temperature. Single and multi-phase alloys are distinguished.

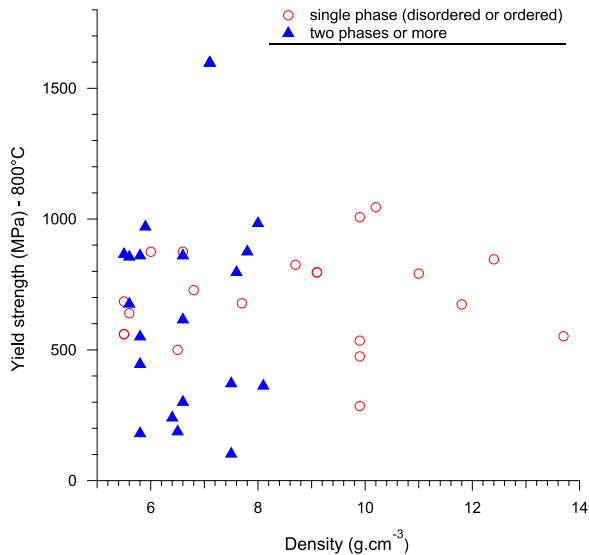


Fig. 4. Evolution of yield strength of RHEAs and RCCAs with alloy density at 800 °C. Single and multi-phase alloys are distinguished.

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Transparency document. Supporting information

Transparency data associated with this article can be found in the online version at <https://doi.org/10.1016/j.dib.2018.10.071>.

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