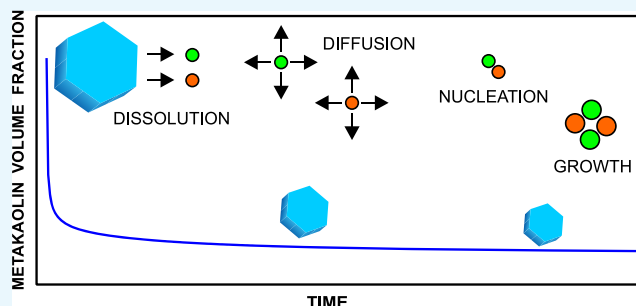


# Modeling Dissolution–Precipitation Kinetics of Alkali-Activated Metakaolin

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**ABSTRACT:** The numerical model HydratiCA was used to simulate the reaction kinetics of alkali-activated metakaolin, a material belonging to a class of sustainable binders alternative to Portland cement. The full chemistry of the system, including solid phases and aqueous species, is taken into account in these simulations. Specifically, metakaolin dissolution, reaction product nucleation and growth, and ion speciation, and diffusion in solution are simulated. The sodium aluminosilicate (N–A–S–H), formed by the reaction of metakaolin in alkaline solution, is implemented in the model as a combination of co-precipitating pseudo-zeolitic phases, with variable stoichiometry. The results show how variations of the reaction pathways, occurring when alkaline activators of different composition and concentration are used, can be associated with different macroscopic behaviors in terms of mechanical performance and durability. Reconciling these macroscopic properties with the basic chemical processes will be a fundamental technological challenge for the deployment of sustainable technologies in the construction industry.



## 1. INTRODUCTION

The sustainable development goals outlined in the United Nations 2030 Agenda include actions oriented at mitigating climate change, building resilient infrastructures, and promoting the development of sustainable cities.<sup>1</sup> This need of imagining a sustainable future has boosted cement chemistry research aimed at defining a new generation of green building materials. Among the possible innovative alternatives to Portland cement, alkali-activated materials (also named geopolymers) represent a viable solution, with a consolidated scientific literature. Lack of internationally recognized standards and regulations<sup>2</sup> has so far hindered the use of alkali-activated cements in practical applications, although actions are being taken in this direction.<sup>3</sup>

The concept beyond this class of cements is the replacement of limestone (impure  $\text{CaCO}_3$ ), as a primary raw material, with aluminosilicates from various sources. The production of Portland cement by  $\text{CaCO}_3$  calcination bears a huge environmental footprint because one mole of  $\text{CO}_2$  is emitted for each mole of processed  $\text{CaCO}_3$ .

In alkali-activated cements, reaction products are formed by alkaline hydrolysis of precursor aluminosilicates. In this context, clay is a widely available and economically viable raw material for the supply of Al–Si reactants to be used for alkali activation. The simplest clay mineral, in terms of chemistry, is kaolinite ( $\text{Al}_2\text{Si}_2\text{O}_5(\text{OH})_4$ ), which upon calcination over a temperature range of 550–800 °C releases water vapor and transforms to the dehydroxylated form  $\text{Al}_2\text{Si}_2\text{O}_7$ , commonly referred to as metakaolin (although metakaolinite would be a more appropriate definition). Partial or total loss of its crystalline structure, subsequent to thermal treatment, enhances its reactivity in alkaline environment. Extensive

literature on the properties of alkali-activated metakaolin can be found in review papers.<sup>4–7</sup>

Despite the extensive research performed on such materials, specific details of the reaction pathways leading to the formation of a hardened material from the dissolution of metakaolin in alkaline solution remain uncertain and are still a matter of debate. The implementation of mathematical models may bridge the gap between the empirical knowledge of the macroscopic properties of alkali-activated metakaolin and the associated physical and chemical processes operating at small scales. A knowledge-based approach will likely drive a faster and more robust innovation in the design of such materials.

Progress in this direction has been made by a number of studies that used atomistic simulations to quantitatively assess, at small space and time scales, structural breakup during metakaolin dissolution,<sup>8</sup> clustering of Al–Si units,<sup>9</sup> and nanostructural details of the product of aluminosilicate alkali activation.<sup>10,11</sup> The reaction kinetics of alkali-activated systems has been simulated by empirical models,<sup>12,13</sup> which, however, did not explicitly describe the full chemistry and mineralogy of the system.

In this study, the dissolution–precipitation kinetics of metakaolin in alkali solution is simulated using the cellular automaton reaction–diffusion model HydratiCA. By defining a database of chemical reactions, each described by a specific stoichiometry, with direct and inverse rates, the time-dependent concentration of metakaolin, reaction product, and aqueous species is tracked over a time interval of hours.

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The implementation of this numerical model is intended to provide possible answers to questions such as:

- What are the underlying mechanisms inducing the observed differences in terms of macroscopic properties (e.g., setting time, mechanical strength) when different alkali activators are used?
- How do the rates of nucleation and growth and stoichiometry of the reaction product change when the alkali concentration is varied?

This numerical study represents a starting point for the definition of a detailed quantitative description of the chemical kinetics inherent to alkali activated systems.

## 2. COMPUTATIONAL METHODS

**2.1. Overview.** The HydratiCA model was developed at the National Institute of Standards and Technology on the basis of a cellular automaton algorithm for the simulation of reaction-transport processes.<sup>14,15</sup> HydratiCA has been successfully used for the simulation of systems related to Portland cement;<sup>16–20</sup> however, the flexibility of this model allows different chemical systems to be simulated.<sup>21,22</sup>

The computational domain is built by mapping the phases present in the system as discrete units of concentration, called cells, onto a mesh of lattice sites with a given lattice spacing  $\lambda$ . At each discrete time step  $\tau$ , the system's evolution is simulated by changing the number of cells of each component at each lattice site according to a set of stochastic rules that model the diffusive transport of the aqueous species and the chemical reactions occurring between components within a given neighborhood of a lattice site. These stochastic reaction-transport equations converge to the continuum standard rate laws and the diffusion equation in the limit  $\lambda, \tau \rightarrow 0$ .

The user defines the physicochemical properties of the phases present in the system as well as the thermodynamic and kinetic parameters governing diffusive transport and chemical reactions.

A generic dissolution–precipitation equilibrium of the type



is simulated by assigning an equilibrium constant (or solubility product)  $K_{\text{eq}}$  and a rate constant  $k^+$  for the direct reaction (dissolution in the case of eq 1). At each time step, the occurrence of dissolution or precipitation depends on the value of the supersaturation  $S$  at each lattice site. The value of the rate constant for the inverse reaction is simply  $k^- = k^+/K_{\text{eq}}$ .

Precipitation of a new solid phase can occur, provided that this has previously nucleated at locations of the spatial domain where the supersaturation is high enough. The nucleation rate is defined, based on classical nucleation theory, by the following equation

$$I(S) = A \times S \exp\left(-\frac{W}{\ln^2 S}\right) \quad (2)$$

The pre-exponential factor  $A$  is defined as

$$A = \left(\frac{4\pi}{3\nu_0}\right)^{1/3} \left(\frac{\sigma}{k_{\text{B}}T}\right)^{1/2} D \quad (3)$$

and the dimensionless parameter  $W$  is

$$W = \frac{16\pi\nu_0^2\sigma^3}{3(k_{\text{B}}T)^3} \quad (4)$$

The parameters present in eqs 3 and 4 are the volume occupied by a molecule of the newly formed phase in the nucleus ( $\nu_0$ ), the surface energy at the interface nucleus/solution ( $\sigma$ ), the diffusion coefficient of the solute species ( $D$ ), and the thermal energy  $k_{\text{B}}T$  (with  $k_{\text{B}}$  being the Boltzmann constant).

A detailed description of the algorithm, along with its validation, can be found in the literature cited at the beginning of this section.

**2.2. System Definition.** The system simulated in this study consists of a single metakaolin platelet having a size of  $9 \times 9 \times 3 \mu\text{m}^3$ , in aqueous solution, with a water/metakaolin mass ratio of 0.56. Periodic boundary conditions are applied to the computational domain of  $11 \times 11 \times 5$  voxels ( $1 \mu\text{m}/\text{voxel}$ ). Such an idealized small system was chosen to minimize computational time, considering that the focus of this investigation is to understand the reaction kinetics rather than the microstructural evolution of the system. The alkaline activators used in the simulations were sodium silicate ( $\text{Na}_2\text{SiO}_3$ ) and sodium hydroxide ( $\text{NaOH}$ ). Three different runs were performed, each with a different combination of activator and molar concentration (Table 1). The selected

**Table 1. Mix Design for the Simulated Systems**

run	H <sub>2</sub> O/MK	activator	reaction time (h)
1	0.56	8 mol/L Na <sub>2</sub> SiO <sub>3</sub>	12
2	0.56	4 mol/L Na <sub>2</sub> SiO <sub>3</sub>	12
3	0.56	8 mol/L NaOH	12

molar concentrations are close to those typically used in experiments and correspond to bulk molar Na/Al ratios  $\leq 1$ , which are commonly recommended to avoid efflorescence.<sup>23</sup>

The reaction product of alkali-activated metakaolin consists in a sodium aluminosilicate hydrate, named N–A–S–H, following the convention used for Portland cement phases (N = Na<sub>2</sub>O; A = Al<sub>2</sub>O<sub>3</sub>; S = SiO<sub>2</sub>; H = H<sub>2</sub>O). This phase is characterized by an X-ray diffraction pattern typical of amorphous or semi-amorphous matter and, in the published literature, is also referred to as N–A–S–H gel, aluminosilicate gel, or geopolymer gel, although the use of the term “gel” is too generic and does not provide a clear picture about the small-scale structural nature of this phase. The bulk chemical composition of N–A–S–H is affine to that of sodium zeolites and, although the exact nature, composition, structure, and even nomenclature of this phase is still debated, recent evidence based on atomistic models and total scattering data<sup>10</sup> confirmed the hypothesis that this phase consists of defective nanocrystalline zeolitic domains.<sup>24</sup> On the basis of the above considerations, N–A–S–H is implemented in the model as a solid with variable stoichiometry, in which the chemical variability is simulated by co-precipitation of four zeolitic end-members, similar to the approach used to simulate calcium-silicate hydrates (C–S–H) precipitation in Portland cement systems.<sup>16</sup> This allows a reaction product of variable chemical composition to precipitate, depending on the aqueous solution composition. In the absence of thermodynamic and kinetic data relative to the N–A–S–H product, the use of a combination of zeolitic phases represents a valid approximation, given the chemical and structural affinity of these phases. A similar approach was used to simulate the formation of N–A–S–H at thermodynamic equilibrium, in a thermodynamic model of alkali-activated cement.<sup>25</sup> The selected end-members

Table 2. Solid Phases Used in the Numerical Model

phase	formula	molar mass (g/mol)	density (g/cm <sup>3</sup> )
metakaolin	Al <sub>2</sub> Si <sub>2</sub> O <sub>7</sub>	222.13	2.60
N–A–S–Ha	Na <sub>2</sub> Al <sub>2</sub> Si <sub>2</sub> O <sub>8</sub> ·5H <sub>2</sub> O	246.05	1.99
N–A–S–Hb	NaAlSi <sub>2</sub> O <sub>6</sub> · <i>n</i> H <sub>2</sub> O	202.14 + <i>n</i> × 18.02	1.98 ( <i>n</i> = 4) – 2.29 ( <i>n</i> = 1)
N–A–S–Hc	Na <sub>2</sub> Al <sub>2</sub> Si <sub>3</sub> O <sub>10</sub> ·2H <sub>2</sub> O	380.22	2.25
N–A–S–Hd	Na <sub>4</sub> Al <sub>3</sub> Si <sub>3</sub> O <sub>12</sub> (OH)·2H <sub>2</sub> O	501.18	2.31

Table 3. List of Chemical Reactions<sup>a</sup>

reaction	log K <sub>eq</sub>	k <sup>+</sup>
Al <sub>2</sub> Si <sub>2</sub> O <sub>7</sub> + 4OH <sup>−</sup> + 5H <sub>2</sub> O → 2Al(OH) <sub>4</sub> <sup>−</sup> + 2H <sub>3</sub> SiO <sub>4</sub> <sup>−</sup>	19.52	1.43 × 10 <sup>−4</sup>
Na <sub>2</sub> Al <sub>2</sub> Si <sub>2</sub> O <sub>8</sub> ·5H <sub>2</sub> O + 2OH <sup>−</sup> + H <sub>2</sub> O → 2Na <sup>+</sup> + 2Al(OH) <sub>4</sub> <sup>−</sup> + 2H <sub>3</sub> SiO <sub>4</sub> <sup>−</sup>	−9.55	5.50 × 10 <sup>−15</sup>
NaAlSi <sub>2</sub> O <sub>6</sub> ·H <sub>2</sub> O + 2OH <sup>−</sup> + 3H <sub>2</sub> O → Na <sup>+</sup> + Al(OH) <sub>4</sub> <sup>−</sup> + 2H <sub>3</sub> SiO <sub>4</sub> <sup>−</sup>	−7.70	5.50 × 10 <sup>−15</sup>
NaAlSi <sub>2</sub> O <sub>6</sub> ·4H <sub>2</sub> O + 2OH <sup>−</sup> → Na <sup>+</sup> + Al(OH) <sub>4</sub> <sup>−</sup> + 2H <sub>3</sub> SiO <sub>4</sub> <sup>−</sup>	−4.14	5.50 × 10 <sup>−15</sup>
Na <sub>2</sub> Al <sub>2</sub> Si <sub>3</sub> O <sub>10</sub> ·2H <sub>2</sub> O + 3OH <sup>−</sup> + 5H <sub>2</sub> O → 2Na <sup>+</sup> + 2Al(OH) <sub>4</sub> <sup>−</sup> + 3H <sub>3</sub> SiO <sub>4</sub> <sup>−</sup>	−17.66	5.50 × 10 <sup>−15</sup>
Na <sub>4</sub> Al <sub>3</sub> Si <sub>3</sub> O <sub>12</sub> (OH)·2H <sub>2</sub> O + 2OH <sup>−</sup> + 7H <sub>2</sub> O → 4Na <sup>+</sup> + 3Al(OH) <sub>4</sub> <sup>−</sup> + 3H <sub>3</sub> SiO <sub>4</sub> <sup>−</sup>	−3.64	5.50 × 10 <sup>−15</sup>
H <sub>3</sub> SiO <sub>4</sub> <sup>−</sup> + OH <sup>−</sup> → H <sub>2</sub> SiO <sub>4</sub> <sup>2−</sup> + H <sub>2</sub> O	0.90	6.03 × 10 <sup>−2</sup>

<sup>a</sup>K<sub>eq</sub>: equilibrium constant; k<sup>+</sup>: rate constant, expressed as mol m<sup>−2</sup> s<sup>−1</sup>.

include zeolite phases that are commonly observed in Na-activated systems, such as zeolite A, Na-faujasite, and zeolites of the sodalite series.<sup>24,26</sup> Other commonly occurring zeolites in such systems are natrolite<sup>27,28</sup> and analcime.<sup>29</sup> Although other zeolitic phases may form under a variety of chemical compositions and curing conditions, it is stressed here that the phases selected are not intended to cover the whole range of crystalline zeolite phases, but rather to span a wide enough compositional interval for the N–A–S–H model. The properties of the solid phases and the set of reactions implemented in the model are reported in Tables 2 and 3.

The first reaction listed in Table 3 accounts for metakaolin dissolution. Quantitative data on metakaolin solubility are not available, and the equilibrium constant was calculated using the formation enthalpy and entropy data retrieved from literature.<sup>30</sup> Strictly speaking, the equilibrium constant obtained from this reaction does not represent a solubility product. However, written in this form, this chemical equation stresses the dependence of metakaolin solubility upon solution pH.

Al(OH)<sub>4</sub><sup>−</sup> was observed to be the dominant Al species in strongly alkaline solutions.<sup>31</sup> H<sub>3</sub>SiO<sub>4</sub><sup>−</sup> and H<sub>2</sub>SiO<sub>4</sub><sup>2−</sup> are the two dominant Si species in alkali-activated metakaolin systems,<sup>32</sup> with the pH-dependent equilibrium between these two species being controlled by the speciation equation reported in Table 3. The equilibrium constant for this reaction was calculated from geochemical databases.<sup>33</sup> In the absence of published data on the reaction rate k<sup>+</sup>, the reported value was assumed on the basis of the one used in a previous HydratiCA model for the formation of Ca complexes in solution.<sup>17</sup>

The rate constant for metakaolin dissolution was calculated using literature data from dissolution experiments<sup>34</sup> performed at a liquid/metakaolin mass ratio of 100, considering that at high dilution, the dissolution rate approximates the value of the rate constant.

The equilibrium constants for the dissolution–precipitation equilibrium of N–A–S–H were calculated from solubility data for end-member N–A–S–Ha (zeolite A<sup>35</sup>), end-member N–A–S–Hb (analcime;<sup>36</sup> zeolite Y<sup>37</sup>), and end-member N–A–S–Hc (natrolite<sup>37</sup>). The equilibrium constant for end-member N–A–S–Hd (hydro-sodalite) was calculated from a value of the Gibbs free energy of the formation reported elsewhere.<sup>38</sup>

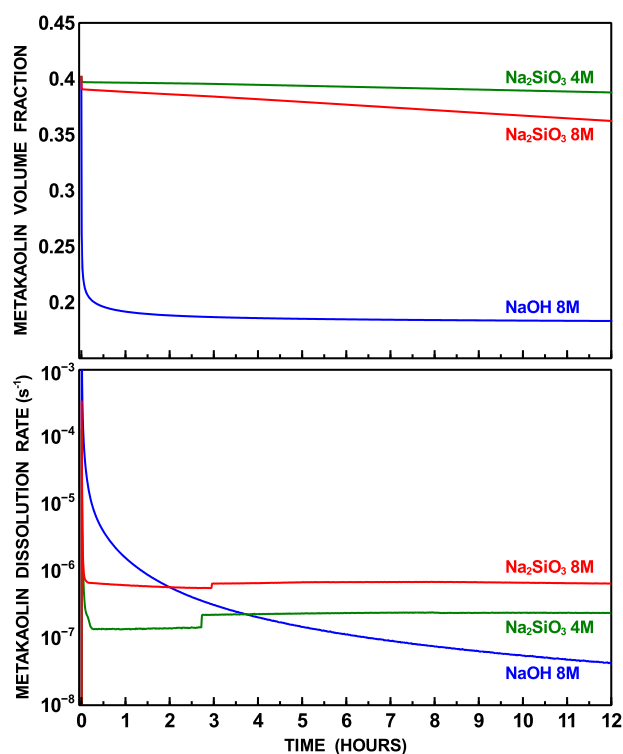
The values of the dissolution rate constants for the N–A–S–H end-members were assigned on the basis of the data from a study on zeolite dissolution.<sup>39</sup> Although this value is relative to zeolites with heulandite composition, in the absence of more specific data, this value is assumed to be valid for all N–A–S–H end-members. This selected dissolution rate constant k<sup>+</sup> = 5.50 × 10<sup>−15</sup> is in the range of values relative to other Na-tectosilicates.<sup>40</sup>

The formation of aqueous Al–Si complexes subsequent to metakaolin dissolution, which is often postulated on the basis of NMR data,<sup>32,41,42</sup> is not explicitly simulated. Such Si–Al entities are broadly defined “oligomers” in the literature, relying on a model dating back to 1959.<sup>43</sup> However, this term is a fairly generic one and is more often used in the field of organic chemistry. Here, it is preferred to adopt the term “nucleus” to describe nano-sized entities formed from the aggregation of aqueous species. Therefore, the formation of Al–Si species, as precursors of the final reaction product (a process that is generally referred to as “oligomer condensation” in the literature) is here regarded as a nucleation event and simulated using the mathematical formalism expressed by eqs 2–4. This “nucleation” formalism is considered more suitable for the description of the precipitation of inorganic solids and is in line with the current views on phase separation from aqueous solutions.<sup>44–46</sup> In the present simulations, the occurrence of N–A–S–H nucleation is restricted to the surface of metakaolin (heterogeneous nucleation), based on previous experimental evidence.<sup>41,42,47</sup>

The pre-exponential factor *A* and the energy barrier *W* present in eq 2 were obtained by using values of the molecular volume *v*<sub>0</sub> obtained from the molar mass and density<sup>48,49</sup> of the N–A–S–H end-members. The diffusion coefficient *D* was set to 1 × 10<sup>−9</sup> m<sup>2</sup>/s on the basis of the data from silica diffusivity.<sup>50</sup> The value of the surface energy *σ* was set to 0.20 J/m<sup>2</sup>, which is in the range of suggested values for amorphous silica.<sup>51</sup>

### 3. RESULTS AND DISCUSSION

**3.1. Metakaolin Dissolution.** The time-dependent volume fraction and dissolution rate of metakaolin after 12 h of simulated reaction are displayed in Figure 1. Dissolution initially occurs at a fast rate, which quickly decays within the



**Figure 1.** Volume fraction and dissolution rate for the three simulated systems.

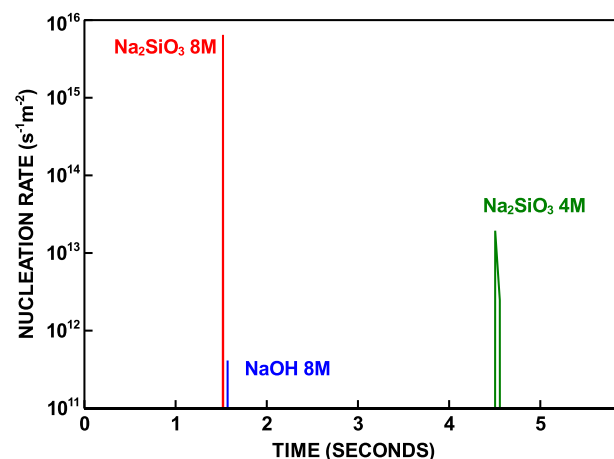
first 30 min. Such a fast reaction, restricted to the very early stage and followed by a much slower rate of reaction, is commonly observed in indirect experimental methods based on calorimetry performed on alkali-activated metakaolin and other calcined clays.<sup>52–54</sup>

The results show that during this stage, dissolution occurs at a faster rate for the system activated by sodium hydroxide, compared to those activated by sodium silicate. The initial faster rate of dissolution for hydroxide-activated metakaolin is due to the absence of silicate ions in the solution at time zero, when metakaolin is mixed with the alkaline solution, which makes the aqueous solution more undersaturated with respect to metakaolin. For the silicate-activated system, the rate of dissolution is proportional to the activator concentration and hence the solution pH.

At 12 h of reaction, the amount of metakaolin, in volume, decreased from 40 to 18% for the hydroxide-activated system. A much smaller decrease is predicted for the silicate-activated systems, with the amount of metakaolin at 12 h being 36 and 39% for the 8 and 4 M solutions, respectively. However, after 12 h of reaction, metakaolin dissolution for the silicate-activated systems proceeds at a nearly constant rate, which is significantly higher compared to the dissolution rate of the hydroxide-activated system, which conversely keeps decreasing due to limited availability of Si in the solution, which hinders N–A–S–H precipitation. Even assuming a constant rate of dissolution for the hydroxide-activated system, after 12 h, it can be predicted that a crossover in the amount of consumed metakaolin occurs approximately after 4 days for the 8 M Na<sub>2</sub>SiO<sub>3</sub> system and after 13 days for the 4 M Na<sub>2</sub>SiO<sub>3</sub>.

**3.2. N–A–S–H Precipitation.** Fast metakaolin dissolution during the very early stage of reaction releases Si and Al ions, which, in combination with Na ions present in the alkaline activator, leads to a supersaturation of the aqueous

solution with respect to N–A–S–H. Figure 2 shows that, for all three simulated systems, nucleation occurs within a few



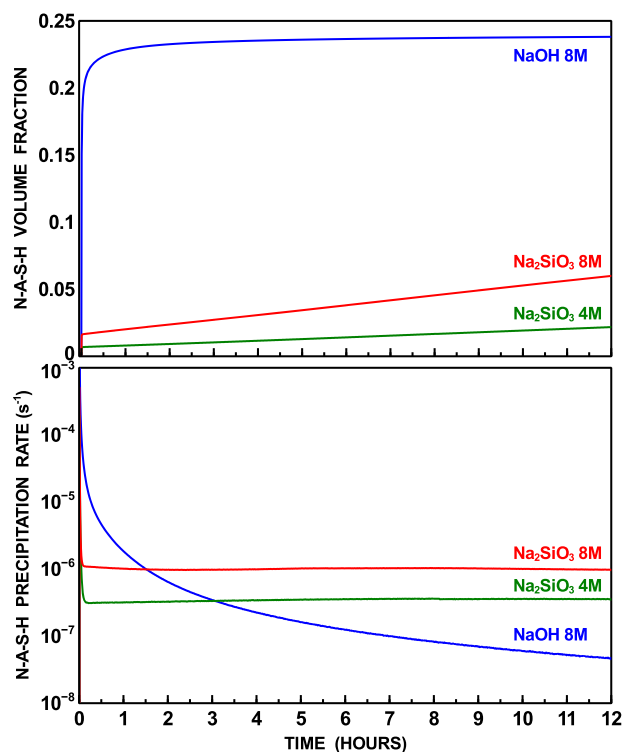
**Figure 2.** Rate of N–A–S–H nucleation for the three simulated systems.

seconds from contact between metakaolin and alkaline solution over a narrow time interval resembling the site-saturation regime, i.e., nucleation can be approximately described as a single event occurring at the very beginning of the reaction. This nucleation behavior is analogous to the one suggested for Portland cement, based on experimental evidence<sup>55</sup> and numerical simulations.<sup>16</sup> The total amount of N–A–S–H nuclei formed, normalized to the metakaolin surface, is  $3.22 \times 10^{14} \text{ m}^{-2}$  for the 8 mol/L Na<sub>2</sub>SiO<sub>3</sub> system,  $1.09 \times 10^{12} \text{ m}^{-2}$  for 4 mol/L Na<sub>2</sub>SiO<sub>3</sub> and  $2.06 \times 10^{10} \text{ m}^{-2}$  for 8 mol/L NaOH. The number of nuclei formed is proportional to the solution supersaturation. During the first few seconds, saturation with respect to N–A–S–H is the lowest for the hydroxide-activated system because Si ions are not initially present in the solution. For comparison, the number of nuclei formed in Portland cement systems was estimated by kinetic modeling to amount to  $4.55 \times 10^{11} \text{ m}^{-2}$ .<sup>56</sup>

After the rapid formation of nuclei at the interface between metakaolin and aqueous solution, N–A–S–H precipitation proceeds by growth. Given the lack of long-range order in the N–A–S–H product, the term growth here does not refer to the incorporation of structural units along specific crystallographic direction, but rather to the attachment of multi-ion clusters to the bulk N–A–S–H phase to form aggregates of poorly crystalline, highly defective nano-sized entities. This process has been postulated to be an intermediate precipitation step leading to the formation of disordered precursors of crystalline phases.<sup>44</sup>

Figure 3 displays the time-dependent N–A–S–H volume fraction and the rate of precipitation for the simulated systems. In analogy to what was observed for metakaolin dissolution, fast early stage precipitation of N–A–S–H occurs for the hydroxide-activated system. Even in the presence of a smaller amount of nuclei, for the hydroxide-activated system, N–A–S–H precipitation occurs at a faster rate during the 1 h of the reaction as a consequence of the fast release of chemical species by metakaolin dissolution. However, at later stages, while N–A–S–H precipitation in the silicate-activated system proceeds nearly at steady state, a significant decrease in the rate of precipitation is observed for the hydroxide-activated system, consistent with the predicted decaying rate of metakaolin





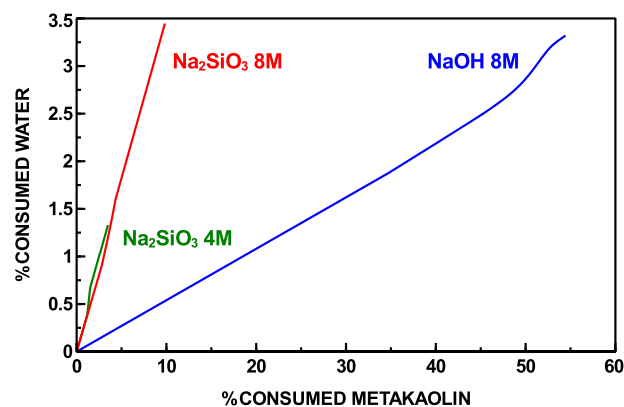
**Figure 3.** N–A–S–H volume fraction and precipitation rate for the three simulated systems.

dissolution (Figure 1). Assuming that the precipitation rates remain constant after 12 h, the amount of N–A–S–H formed is predicted to become larger than that precipitated in the hydroxide-activated system after 3 days for the systems activated by 8 mol/L  $\text{Na}_2\text{SiO}_3$  and 9 days for the one activated by 4 mol/L  $\text{Na}_2\text{SiO}_3$ .

The predicted faster early-stage rate of reaction in the presence of sodium hydroxide may induce a quicker set, in agreement with previous experimental observations performed on alkali-activated metakaolin, suggesting that setting time is proportional to the activator Si/Na ratio.<sup>57,58</sup> On the other hand, the predicted faster rate of N–A–S–H precipitation at later stage, using  $\text{Na}_2\text{SiO}_3$  as alkaline activator, is consistent with the better mechanical performance commonly observed in the presence of sodium-silicate as compared to sodium hydroxide for metakaolin and other alkali-activated materials.<sup>5,52,59</sup>

The N–A–S–H composition predicted by the simulations is dominated, for all systems, by the N–A–S–Hc end-member (Table 2). Growth of the other end-members is kinetically hindered during the first 12 h, when their volume fraction is of the order of  $10^{-8}$  or smaller. No significant change was observed when the stoichiometry and equilibrium constant of the N–A–S–Hb end-member were changed to reflect analcime or zeolite Y chimico-physical properties (see Table 2). Therefore, the predicted chemical composition of the reaction product tends to that of a phase with Na/Al = 1 and Si/Al = 1.5.

**3.3. Aqueous Phase.** Interestingly, the simulation results show that although early-stage reaction kinetics are faster for the hydroxide-activated system, the amount of water consumed after 12 h does not vary significantly compared to the silicate-activated system. This behavior is illustrated in Figure 4, which shows that for a given amount of dissolved metakaolin, the



**Figure 4.** Percentage of water consumed as a function of the percentage of dissolved metakaolin.

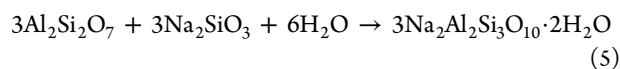
amount of water consumed is significantly smaller for the hydroxide-activated system. The different amount of water consumed during the reaction, depending on the activator used, is a consequence of the reaction stoichiometry, and this point will be illustrated in more detail later in this section. This result, moreover, agrees with previous investigation showing that denser, less porous microstructures develop as the Si/Na ratio of the alkaline activator is increased.<sup>60</sup> Therefore, the better mechanical performance in the presence of sodium silicate, compared to sodium hydroxide, can be attributed to both a faster late-stage rate of N–A–S–H precipitation, as shown in the previous Section 3.2, and enhanced water consumption, leading to the formation of a denser microstructure.

The time-dependent concentrations of Na, Al, and Si ionic species in aqueous solution are displayed in Figure 5. The pH of the pore solution after 12 h is 13.67 for 8 mol/L  $\text{Na}_2\text{SiO}_3$ , 13.47 for 4 mol/L  $\text{Na}_2\text{SiO}_3$ , and 13.12 for 8 mol/L NaOH (14.90, 14.60, and 14.90 at time zero), in agreement with the pH range measured experimentally for alkali-activated metakaolin.<sup>61</sup>

Fast early-stage N–A–S–H precipitation in the hydroxide-activated system is associated with a larger amount of Na and Si aqueous species removed from the pore solution. However, although the concentration of  $\text{Al}(\text{OH})_4^-$  in the silicate-activated systems reaches values as low as a few tens  $\mu\text{mol}$ , a much higher concentration is predicted for the hydroxide-activated system. Interestingly, this behavior was experimentally observed by NMR spectroscopy of alkali-activated metakaolin.<sup>62</sup> The results of those measurements suggested the presence of  $\text{Al}(\text{OH})_4^-$  in the pore solution only for hydroxide-activated metakaolin, whereas no aqueous Al species could be detected in silicate-activated systems. Additionally, the results indicated the presence of  $\text{Na}^+$  in the solution as a charge-balancing ion for  $\text{Al}(\text{OH})_4^-$ .

Although the simulations predict a lower amount of  $\text{Na}^+$  at 12 h, the rate of  $\text{Na}^+$  consumption is 5–13 times bigger for the silicate-activated systems at the end of the simulations.

To better understand these observations, it is convenient to write chemical equations for silicate and hydroxide-activated systems with Na/Al = 1, dominated by the precipitation of a N–A–S–H product with Na/Al = 1 and Si/Al = 1.5, as predicted by the simulations



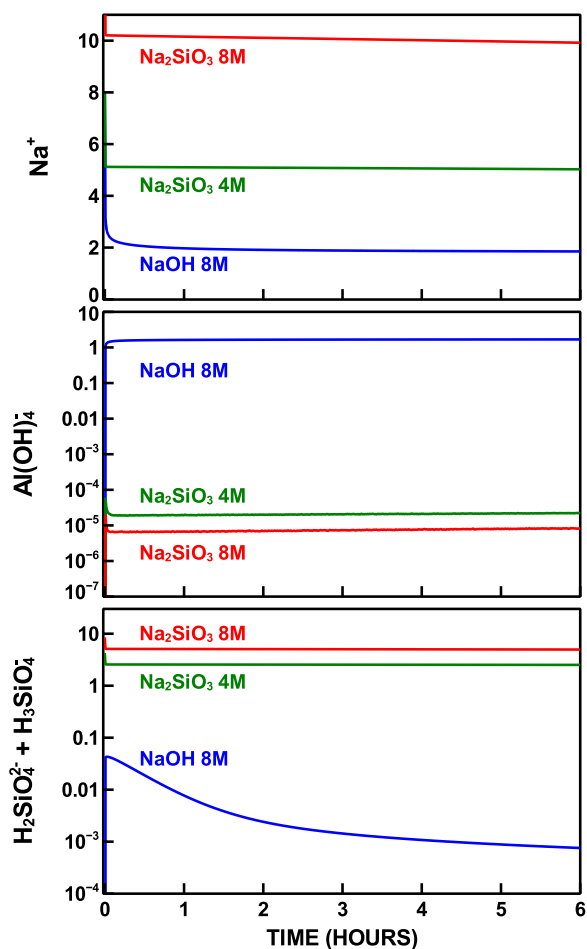
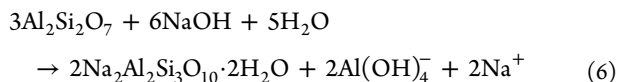


Figure 5. Concentration of aqueous species expressed as mol/L.



These equations imply that

- for each mole of metakaolin consumed, more product is formed in the silicate-activated system;
- for each mole of metakaolin consumed, more water is consumed in the silicate-activated system;
- excess  $\text{Al}(\text{OH})_4^-$  and  $\text{Na}^+$  are present in the pore solution of the hydroxide-activated system.

The presence of excess Na in the pore solution may induce enhanced carbonation for hydroxide-activated metakaolin. Indeed, this behavior was observed in an alkali-activated calcined smectite system, in which the formation of alkali carbonates was detected by XRD only when NaOH was used as an activator.<sup>54</sup>

**3.4. Role of  $K_{\text{eq}}$  and  $k^+$ .** The effect of modifying the values of the N–A–S–H end-members dissolution–precipitation equilibrium constants and dissolution rate constants was investigated by running an additional set of simulations for the three modeled systems. The criteria adopted for varying these values were based on the selection of amorphous, rather than crystalline end-members, as being representative of N–A–S–H. Solubility studies on zeolite A showed that the solubility of the ionic species increased up to 1 order of magnitude for the amorphous precursor, compared to the crystalline phase.<sup>35</sup> Based on this observation, the values of  $K_{\text{eq}}$

were recalculated accordingly for all N–A–S–H end-members. Moreover, based on the measured differences between quartz and amorphous silica, the value of  $k^+$  was increased by an order of magnitude.<sup>40</sup> The densities of the N–A–S–H end-members did not vary compared to the previous simulations, based on the evidence from atomistic models of N–A–S–H structures, which displayed small variations in the density of crystalline, defective, and amorphous structures, for stoichiometries with  $\text{Si}/\text{Al} \leq 2$ .<sup>10</sup> The values of  $K_{\text{eq}}$  and  $k^+$  adopted for this set of simulations are summarized in Table 4.

Table 4. Equilibrium Constant and Dissolution Rate Constant for Amorphous N–A–S–H End-Members<sup>a</sup>

phase	$\log K_{\text{eq}}$	$k^+$
N–A–S–Ha	−5.55	$5.50 \times 10^{-14}$
N–A–S–Hb	−5.70	$5.50 \times 10^{-14}$
N–A–S–Hc	−13.66	$5.50 \times 10^{-14}$
N–A–S–Hd	+4.36	$5.50 \times 10^{-14}$

<sup>a</sup> $K_{\text{eq}}$ : equilibrium constant;  $k^+$ : rate constant, expressed as  $\text{mol m}^{-2} \text{s}^{-1}$ .

The time-dependent rates of metakaolin dissolution and N–A–S–H precipitation are displayed in Figure 6. The most

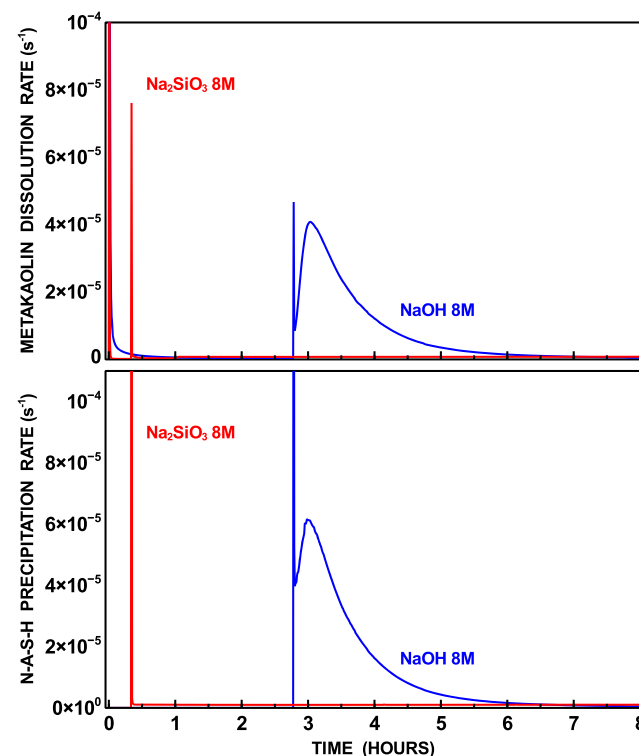


Figure 6. Rates of metakaolin dissolution and N–A–S–H precipitation for the system with amorphous end-members.

notable difference is the delayed N–A–S–H nucleation, which occurs after about 20 min for the 8 mol/L  $\text{Na}_2\text{SiO}_3$  system and after nearly 3 h for the 8 mol/L NaOH system. Nucleation does not occur during the first 12 h for the 4 mol/L  $\text{Na}_2\text{SiO}_3$  system.

Such a delayed N–A–S–H nucleation affects the rate of metakaolin dissolution, which in this case presents two distinct peaks: one at the beginning of the reaction and the other immediately after the nucleation event.

The occurrence of two distinct exothermic peaks, measured by isothermal calorimetry, was observed in a previous investigation on the activation of metakaolin by sodium hydroxide and sodium silicate. These peaks were located at the beginning and after a few hours from the beginning of the reaction. The separation between the two peaks was more pronounced at lower temperatures, whereas the peaks became nearly overlapping at a temperature of 40 °C, when the overall rate of reaction is faster.<sup>63,64</sup>

#### 4. CONCLUSIONS

The HydratiCA model proved to be a promising tool for simulating the reaction kinetics of alkali-activated systems. The possibility of tracking the time-dependent evolution of the amount of solid phases and aqueous species present in the system represents a powerful resource for a better understanding of the basic chemical processes associated with alkali-activated materials.

The results of the numerical simulations presented in this study provided a picture of the influence of different alkaline activators on the reaction pathways of metakaolin-based cement.

The main findings of this numerical study suggest the following:

- The use of NaOH as alkaline activator is associated with a fast early-stage rate of dissolution–precipitation, which may explain the experimental observations suggesting that the setting time depends on the Si/Na ratio of the alkaline activator.
- Alkaline activation by Na<sub>2</sub>SiO<sub>3</sub>, in turn, induces a faster late-stage rate of metakaolin dissolution and N–A–S–H precipitation, as well as a significantly larger amount of water consumption. These predictions can be reconciled with the macroscopic experimental observation that products characterized by better mechanical strength and reduced porosity are formed when sodium silicate is used as activator.
- The N–A–S–H phase, which nucleates immediately after the contact of metakaolin with the alkaline solution, is chemically affine to natrolite, with Na/Al = 1 and Si/Al = 1.5. This stoichiometric constraint, and equilibrium of this phase with the aqueous solution, may explain the experimental observation that Al aqueous species are more easily detected when no Si is present in the alkaline activator. Moreover, the presence of excess Na as a charge-balancing ion may induce enhanced formation of alkaline carbonates in hydroxide-activated metakaolin.

HydratiCA relies on classical nucleation theory for simulating the formation of new phases in solution. One possible improvement in the modeling of alkali-activated materials may consist in the implementation of nonclassical nucleation pathways. Recent research suggested that the formation of new solid phases in the aqueous solution may occur by the aggregation of prenucleation clusters to form stable nuclei. This process has been especially observed during the precipitation of amorphous or defective materials.<sup>65,66</sup> Recently, results of small angle X-ray scattering (SAXS) experiments have shown that the nucleation of calcium-silicate hydrates (C–S–H) in Portland cement occurs by aggregation of prenucleation amorphous entities.<sup>67</sup> Similar results were obtained for metal–organic frameworks topologically affine to

zeolites.<sup>68</sup> SAXS experiments performed on alkali-activated metakaolin showed analogous results with the formation of 2 nm clusters, defined as oligomers by the authors, by the aggregation of smaller particles,<sup>69</sup> suggesting an analogy between condensation of oligomers and nucleation.

One potentially viable numerical approach for the implementation of nonclassical nucleation pathways in alkali-activated system is “population balance modeling”. This numerical scheme can track the time variation in the size distribution of particles present in a given system, similarly to what can be experimentally achieved by SAXS methods. Population balance modeling was recently implemented to the simulation of C–S–H formation by the aggregation of defective crystallites.<sup>70</sup>

It is also important to stress that experimental efforts, oriented at measuring the rate of metakaolin dissolution and N–A–S–H precipitation, as well as the definition of specific N–A–S–H thermodynamic models, will be necessary for developing more accurate numerical models.

The final message of this work is that the use of kinetic, thermodynamic, and multiscale microstructural models of alkali-activated systems should be encouraged, as it will certainly be beneficial to a deeper understanding of the basic chemical aspects of this class of sustainable binders.

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##### Notes

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