

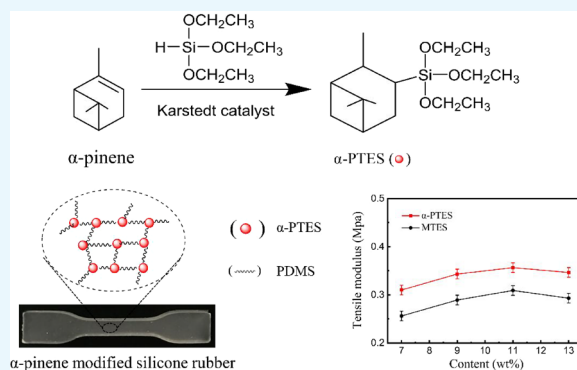
# Using $\alpha$ -Pinene-Modified Triethoxysilane as the New Cross-Linking Agent To Improve the Silicone Rubber Properties

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**ABSTRACT:**  $\alpha$ -Pinene-modified triethoxysilane ( $\alpha$ -PTES) was synthesized by hydrosilylation in the presence of Karstedt's catalyst. The structure of  $\alpha$ -PTES was determined by Fourier transform infrared spectroscopy and nuclear magnetic resonance. Under the catalysis of an organotin catalyst,  $\alpha$ -PTES, which was the cross-linking agent, and the hydroxy-terminated poly(dimethylsiloxane) matrix were utilized to prepare the room-temperature vulcanized silicone rubber. Morphology, thermal performance, and mechanical properties of the modified silicone rubber were investigated by scanning electron microscopy, thermal gravimetric analysis, dynamic mechanical analysis, and a universal testing machine. Because of the strong rigidity of the ring structure of  $\alpha$ -pinene, the thermal and mechanical properties of modified silicone rubber were improved greatly than those of the silicone rubber, and the cross-linking agent of which was methyltriethoxysilane. Results showed that the tensile strength and the break at elongation increased by 69.2 and 125%, respectively, and they are nearly doubled compared to the unmodified silicone rubber.



## INTRODUCTION

The structure of the polysiloxane contains inorganic and organic groups, which make polysiloxane have the function of inorganic and organic materials.<sup>1</sup> Room-temperature vulcanized (RTV) silicone rubber is a polymer elastic material, which is synthesized from polysiloxane, and shows heat resistance, weather resistance, biocompatibility, ozone resistance, electrical insulation, chemical stability, and so on.<sup>2–5</sup> In addition, RTV silicone rubber is widely applied in the electrical, petroleum, chemical, construction, munition, aerospace, and space exploration fields due to its unique properties.<sup>6,7</sup> However, the poor mechanical properties cause a weak intermolecular force of the RTV silicone rubber, limiting the practical application.<sup>8</sup> Thus, it is highly desirable to improve the mechanical properties of the RTV silicone rubber.<sup>9</sup>

Chemical modification, such as modification of the cross-linking agent and poly(dimethylsiloxane) (PDMS) matrix, and filler incorporation could significantly improve the mechanical properties and thermostability of the silicone rubber.<sup>10–14</sup> The utilized fillers that made of carbon nanotubes (CNTs) and iron oxide ( $\text{Fe}_2\text{O}_3$ ) were made by Li et al., and the thermostability of the silicone rubber was improved.<sup>15</sup> By using polymethyl-(ketoxime)siloxane (PMKS) as a new cross-linking agent, Zhan et al. improved not only thermal but also mechanical properties of room-temperature vulcanized (RTV) silicone rubbers.<sup>16</sup> Studies on the thermal degradation properties of poly(dimethyldiphenyl)siloxane copolymers, PDMS, and poly-

(dimethyldiphenyl)siloxane) were conducted by Deshpande and Rezac, and the results showed the reduction of activation energy when phenyl groups were introduced.<sup>17,18</sup>

In recent years, with the global resource crisis and awareness of environmental protection, renewable biomass resources are good alternatives for petroleum-based compounds.<sup>19–21</sup> The rigid structures, such as lignin, cyclodextrin, and rosin, of biomass resources have great potential to prepare polymers with high mechanical and thermal properties.<sup>22,23</sup> Choi et al. studied the RTV silicone rubber and significantly improved its mechanical properties and thermal performance by using the rosin-grafted poly(dimethylsiloxane) (RGSO).<sup>24</sup> The effects of acrylic acid-modified aminopropyltriethoxysilane (APA-APTES), which was the cross-linking agent, on the thermostability and mechanical properties of modified silicone rubber were studied by Yang et al.<sup>25</sup> The maleated rosin-modified fluorosilicone rubbers (MR-FSR) were synthesized by Xu et al., and the imide-containing vinyl fluorosilicone resin (MR-VFS) was the novel cross-linking agent. The results showed that the high-temperature thermostability and tearing strength of fluorosilicone rubber could be greatly increased by MR-VFS.<sup>26</sup> Li et al. found that the rosin-modified aminopropyltriethoxysilane (RA) was the cross-linking agent, and

Received: April 21, 2019

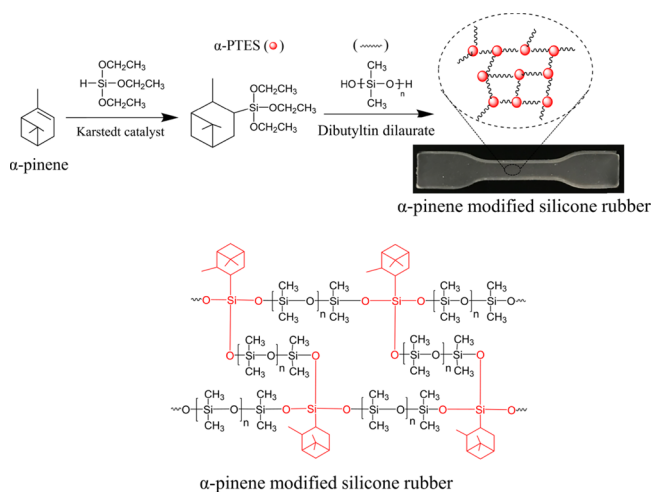
Accepted: June 27, 2019

Published: July 10, 2019

the hydroxy-terminated poly(dimethylsiloxane) (PDMS) was the matrix; RTV silicone rubber could be modified under the catalysis of an organotin, which exhibited a significant enhancement in the mechanical properties and thermostability significantly.<sup>7</sup> Because of the rosin's polar hydrogenated phenanthrene ring structure and good rigidity, improvements in the mechanical properties and thermal performance of silicone rubber could be successfully achieved according to the research mentioned above.

The two main components secreted by pines are rosin and turpentine.<sup>27,28</sup> Turpentine is mainly composed of terpene compounds such as  $\alpha$ -pinene and  $\beta$ -pinene and has strong chemical reactivity for oxidation, isomerization, rearrangement, addition, polymerization, and other chemical reactions.<sup>29</sup> In addition, turpentine has similar rigidity and chemical stability to petroleum-based cycloaliphatic compounds.<sup>30,31</sup> These properties make turpentine have great potential in the preparation of polymers with high thermal stability and mechanical properties. Xu et al. prepared the bio-based alkyd resin by utilizing raw materials including tung oil and turpentine-based acrylate (IBOA). The results showed that when the content of IBOA was increased, the water resistance, thermostability, pencil hardness, and mechanical properties of the alkyd resins became much better.<sup>32</sup> Wu et al. prepared a two-component aqueous terpene epoxy resin (EP)/polyurethane (PU) composite polymer by cross-linking of terpene-based epoxy resin polyol dispersion prepared from turpentine with polyisocyanate, and the composite product has good gloss, impact strength, adhesion, flexibility, stain resistance, heat resistance, and blocking resistance.<sup>33,34</sup> Meanwhile, there was little research on the modification of silicone rubber by turpentine.

In this work,  $\alpha$ -pinanyltriethoxysilane ( $\alpha$ -PTES) was prepared by the hydrosilylation of  $\alpha$ -pinene and methyltriethoxysilane in the presence of Karstedt's catalyst. To prepare the RTV silicone rubber (Figure 1), hydroxy-terminated poly(dimethylsiloxane) (PDMS) and  $\alpha$ -PTES, which was a new cross-linking agent, were further used. The effects of  $\alpha$ -PTES on morphologies and mechanical and thermal properties of modified silicone rubber were investigated in this paper.



**Figure 1.** Synthetic route for  $\alpha$ -pinene-modified RTV silicone rubber (SR $\alpha$ PT) and pinanyl triethoxysilane ( $\alpha$ -PTES).

## RESULTS AND DISCUSSION

**Properties of  $\alpha$ -PTES.** *FT-IR Analysis.* The chemical structures of  $\alpha$ -pinene, triethoxysilane, and  $\alpha$ -PTES were determined through FT-IR spectra. The spectrum in Figure 2a shows that the absorption peak is at 3024  $\text{cm}^{-1}$  (stretching vibrations due to unsaturated C–H), 885  $\text{cm}^{-1}$  (bending vibration due to unsaturated C–H), and 1658  $\text{cm}^{-1}$  (stretching vibration of C=C). As shown in Figure 2, after hydrosilylation with triethoxysilane, at 1658  $\text{cm}^{-1}$ , the C=C stretching vibration of  $\alpha$ -pinene disappeared in spectra of Figure 2a,c. The absorption peaks were at 2198 and 852  $\text{cm}^{-1}$  (Si–H stretching) as shown in Figure 2b, which also shows that characteristic peaks of Si–H at 2198 and 852  $\text{cm}^{-1}$  are almost completely disappeared, indicating the successful synthesis of  $\alpha$ -PTES (spectra in Figure 2b,c).

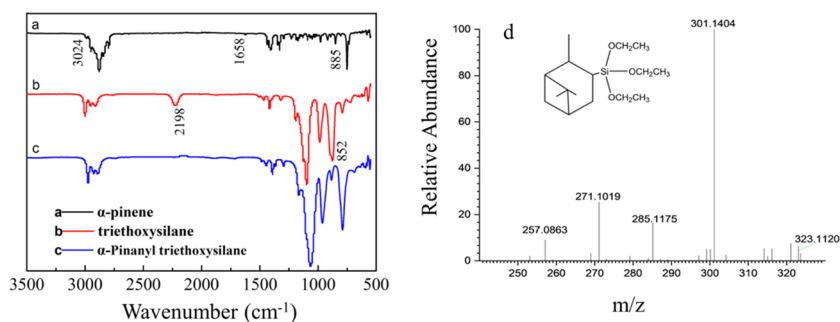
*MS Analysis.* As the chemical formula of  $\alpha$ -pinanyl triethoxysilane ( $\alpha$ -PTES) is  $\text{C}_{16}\text{H}_{32}\text{O}_3\text{Si}$ , the exact mass is 300.2121. As shown in Figure 2d, 285.1175 is the value of mass of  $\alpha$ -PTES losing one methyl group, 271.1019 is the value of mass of  $\alpha$ -PTES losing one ethyl group, and 257.0863 is the value of mass of  $\alpha$ -PTES losing one methyl group and one ethyl group. MS  $m/z$  (CI):  $(\text{M} + \text{Na})^+$  calcd for  $\text{C}_{16}\text{H}_{32}\text{O}_3\text{SiNa}$  323.2013; found, 323.1120, and this confirms that the target product has been formed.

*NMR Analysis.* Figure 3 shows the  $^1\text{H}$  NMR spectra in  $\text{CDCl}_3$ , which further confirmed the structure of  $\alpha$ -PTES. The protons of the C=C in  $\alpha$ -pinene are related to the fascicles of signal peaks at 4.24 ppm. In addition, at 4.24 ppm, the clusters of signal peaks were resulted from the chemical shifts in Si–H protons. According to curves in Figure 3a,c, the protons of the Si–C for the product are associated with the fascicles of signal peaks at 1.46 and 1.1 ppm, confirming that the target product has been formed. Also, the peak at 7.26 ppm is  $\text{CDCl}_3$ .

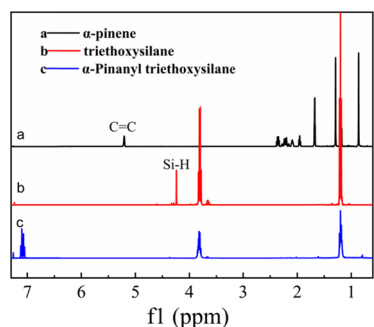
**Characterization of SR $\alpha$ PT and SRTE.** Under the condensation reaction of cross-linking agents and poly(dimethylsiloxane) (PDMS), SR $\alpha$ PT and SRTE were synthesized at room temperature using organotin as a catalyst. The components and conditions, such as the cross-linking agent, curing catalyst, environmental conditions, PDMS, and temperature, could affect the cross-linking process. Dibutyltin dilaurate catalyst (180  $\mu\text{L}$ ) and PDMS (5000 mPa·s, 30 g) in this experiment were utilized to all the samples. We used the  $\alpha$ -PTES instead of MTES as the cross-linking agent to study the effects of  $\alpha$ -PTES on the thermal performance and mechanical properties of modified RTV silicone rubber.

**Morphologies.** As shown in Figure 4a (SRTE-4), the RTV silicone rubber is colorless and transparent when the cross-linker is MTES. However, when the cross-linking agent is  $\alpha$ -PTES instead of MTES, the modified RTV silicone rubber has low transparency (Figure 4a, SR $\alpha$ PT-2). There may be a change in the microstructure. As shown in Figure 4b–f, the morphologies of modified RTV silicone rubbers are characterized by using scanning electron microscopy. Rigid ring structures of  $\alpha$ -PTES would increase the molecular chain rigidity of the polymer matrix. Therefore, as the  $\alpha$ -PTES increases, the modified RTV silicone rubber becomes rougher than the unmodified silicone rubber.<sup>36</sup> In addition, the microphase in RTV silicone rubber would be separated because of the aggregation of the rigid ring groups in  $\alpha$ -pinene.<sup>13,37</sup>

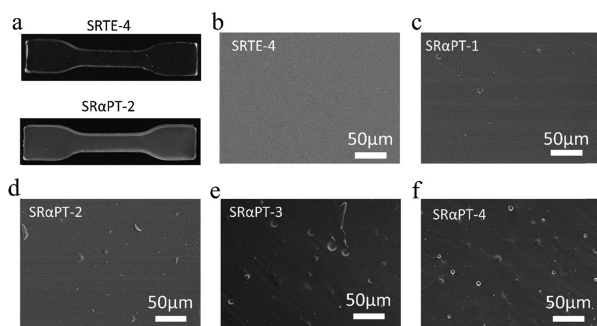
**Thermal Properties.** By conducting the TGA, we investigated the influence of different cross-linker contents



**Figure 2.** (a–c) FT-IR spectra of (a)  $\alpha$ -pinene, (b) triethoxysilane, and (c)  $\alpha$ -pinanyl triethoxysilane ( $\alpha$ -PTES). (d) Mass spectra of  $\alpha$ -pinanyl triethoxysilane ( $\alpha$ -PTES).



**Figure 3.** <sup>1</sup>H NMR spectra of (a)  $\alpha$ -pinene, (b) triethoxysilane, and (c)  $\alpha$ -pinanyl triethoxysilane ( $\alpha$ -PTES).



**Figure 4.** Microstructure and morphology of modified silicone rubber. (a) Photographs of SRTE-4 and SR $\alpha$ PT-2. (b) SEM image of SRTE-4. (c) SEM image of SR $\alpha$ PT-1. (d) SEM image of SR $\alpha$ PT-2. (e) SEM image of SR $\alpha$ PT-3. (f) SEM image of SR $\alpha$ PT-4.

on the thermal properties of modified silicone rubber. There is obvious three-stage weightlessness in the RTV silicone rubber samples. The first stage is mainly the decomposition of RTV silicone rubber side chain groups from 300 to 500 °C, for example, methyl collapses to methylene radicals. The second stage is the RTV silicone rubber's main chain fracture process that generates low molecular rings primarily from 500 to 600 °C. The third stage is a carbonization process from 600 to 800 °C (Figure 5).

We have tested the energy dispersive spectrometry (EDS) of the RSTE-4 residue after the TGA in Figure 6a. From the diagram in Figure 6a, we can see that the elements of the RSTE-4 residue are mainly Si and O, and this is because of the restrained silicone rubber macromolecules with the increase of MTES cross-linking.

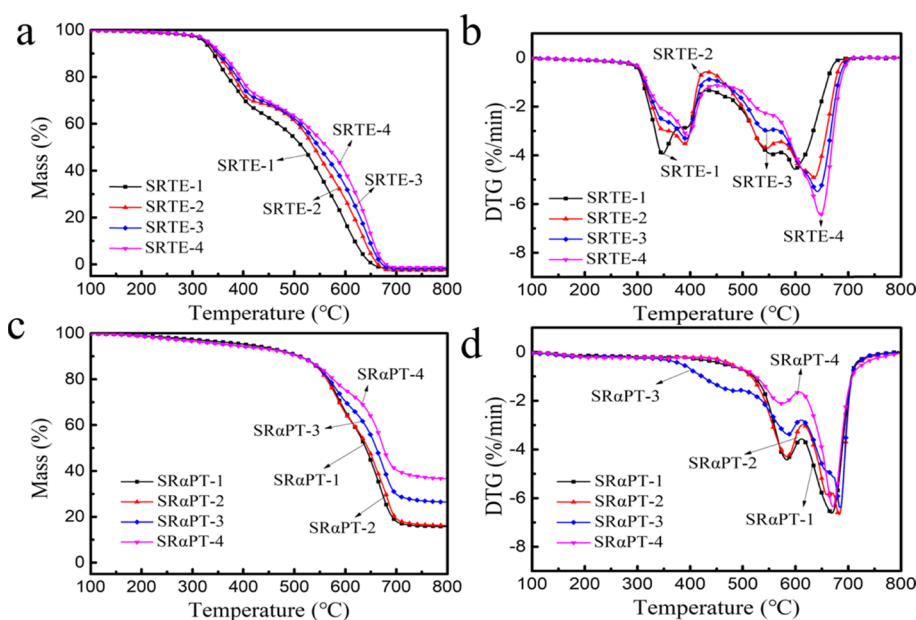
**Cross-Linking Density.** The cross-linking density of RTV silicone rubber has an influence on its mechanical properties. The cross-linking density was measured by an equilibrium

swelling method. As shown in Figure 6b, the  $\alpha$ -PTES-modified silicone rubber (SR $\alpha$ PT) shows an increasing cross-linking density when the content of the cross-linking agent  $\alpha$ -PTES was increased from 7 to 11 wt % and has a slightly decrease as  $\alpha$ -PTES increased to 13%. However, the change in the cross-linking density of silicone rubber (SRTE) is not obvious. Such an increase can be caused by chain entanglement and intermolecular forces, which increase with an increasing content of  $\alpha$ -PTES.

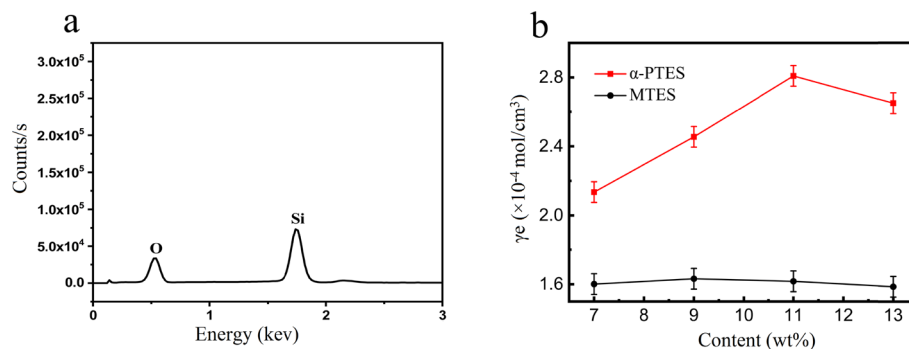
**Mechanical Properties.** As shown in Figure 7a,b, the  $\alpha$ -PTES-modified RTV silicone rubber showed significantly higher mechanical properties than the unmodified silicone rubber. Figure 7c,d shows that the break at elongation and tensile strength of the  $\alpha$ -PTES-modified silicone rubber were significantly improved. The tensile strength of SR $\alpha$ PT-3 was 0.66 MPa, and the break at elongation was 285.8%. They are nearly doubled compared to the SRTE-2 sample. When the elongation is 100%, the tensile moduli of all SR $\alpha$ PT are higher than those of all SRTE in Figure 7e. This is because the rigid ring structure of the  $\alpha$ -PTES increased the rigid segment of the polysiloxane and improved the interaction between the molecules. Thus, it is highly desirable to improve the mechanical properties of the RTV silicone rubber.<sup>38–40</sup>

Moreover, as the  $\alpha$ -PTES content increases from 0 to 13 wt %, the mechanical properties, tensile modulus, and the break at elongation of the RTV silicone rubber increase then decrease and reach the maximum when the  $\alpha$ -PTES content is 11%. Although the microphase separation would occur, a lower  $\alpha$ -PTES cross-linking agent, which could be homogeneously dispersed in the matrix, could be utilized to cure the silicone. As the  $\alpha$ -PTES increased, the mechanical properties of the RTV silicone rubber were improved. Figure 7c–e shows that the break at elongation, mechanical properties, and tensile modulus of RTV silicone rubber begin decreasing when the  $\alpha$ -PTES content exceeding 11 wt %. The decrease may result from the excess  $\alpha$ -PTES, which could cause agglomeration, self-cross-linking, and microphase separation.<sup>15,41</sup> This indicated that the mechanical properties of the silicone rubber could be positively affected by the uniform distribution of the cross-linking agent ( $\alpha$ -PTES). The hardness of modified silicone rubber (SR $\alpha$ PT-4, 30 A) is better than that of silicone rubber (SRTE-4, 21 A) (Figure 7f). In addition, with increasing cross-linking agent ( $\alpha$ -PTES), the hardness of SR $\alpha$ PT increased from 24 to 30 A.

**Dynamic Mechanical Properties.** The curves of storage moduli ( $E'$ ) of SR $\alpha$ PT and SRTE are shown in Figure 8a,b. The  $E'$  is closely related to the chemical structure and cross-linking density of RTV silicone rubber. Compared to SRER-1



**Figure 5.** (a) TG curves of SRTE. (b) DTG curves of SRTE. (c) TG curves of SR $\alpha$ PT. (d) DTG curves of SR $\alpha$ PT.



**Figure 6.** (a) EDS of SRTE-4 residue. (b) Cross-linking densities of SRTE and SR $\alpha$ PT.

(4219 MPa), the  $E'$  values of SR $\alpha$ PT-4 (4446 MPa) increased to 227 MPa. The silicone chain fluidity of the RTV silicone rubber would have significant restrictions because the increased modulus would enhance the chain entanglement and molecular chain rigidity. As the excess  $\alpha$ -PTES would cause the self-cross-linking and agglomeration, the  $E'$  values of SR $\alpha$ PT-4 decreased slightly compared to those of SR $\alpha$ PT-3, resulting in decreasing cross-linking density.<sup>13,38,42</sup>

As shown from Figure 8a,b, there is one  $T_g$  for each sample, which is between  $-135$  and  $-75$  °C. The  $T_g$  of  $\alpha$ -PTES-modified silicone rubber increased from  $-116.3$  (SR $\alpha$ PT-1) to  $-115.0$  °C (SR $\alpha$ PT-4), and the increase was greater than that of the unmodified silicone rubber (SRTE-4). This is because the polysiloxane chain mobility is limited due to the rigid ring structure of  $\alpha$ -PTES and the corresponding less flexible polysiloxane chain.<sup>23,43,44</sup> Figure 8c shows that the glass-transition temperature ( $T_g$ ) of each modified silicone rubber is confirmed by the peak of the  $\tan \delta$  curve.

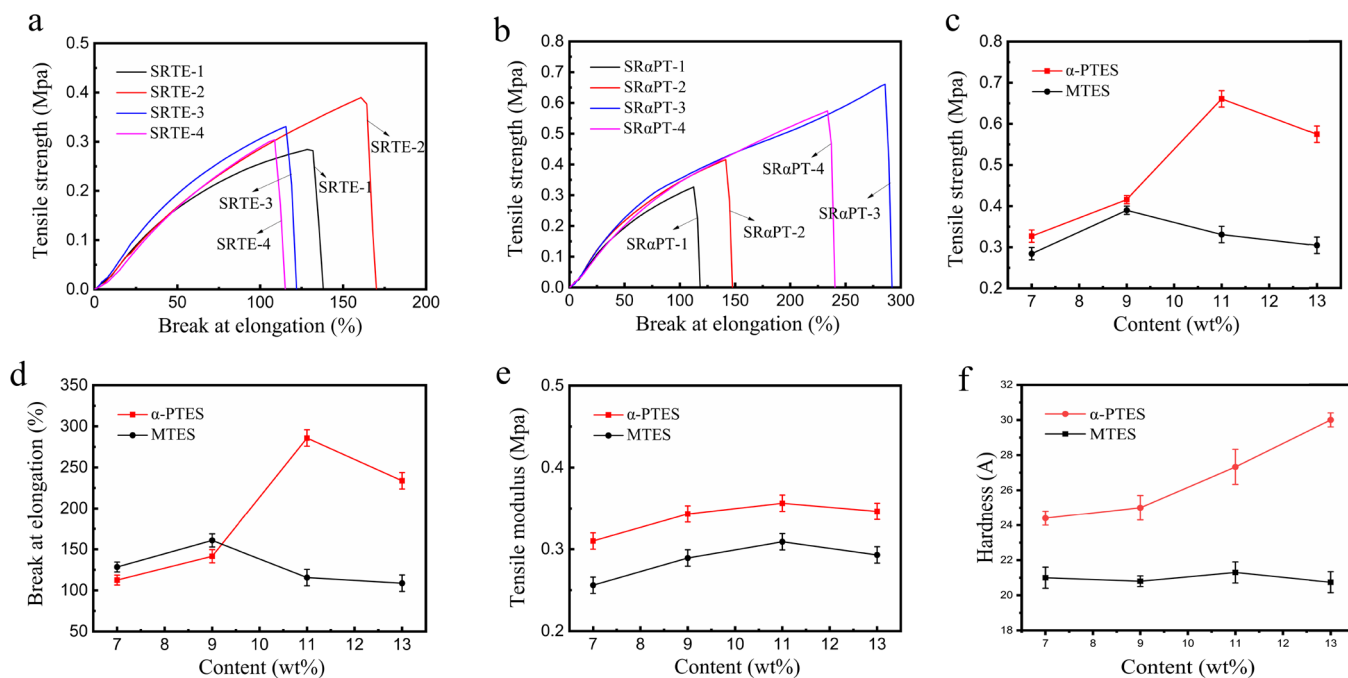
## CONCLUSIONS

Under the catalysis of the Karstedt's catalyst, we synthesized a new cross-linking agent for the preparation of RTV silicone rubber,  $\alpha$ -PTES, through the hydrosilylation of  $\alpha$ -pinene with triethoxysilane.  $^1\text{H}$  NMR and FT-IR confirmed the chemical structure of the cross-linking agent. The rigid ring structure

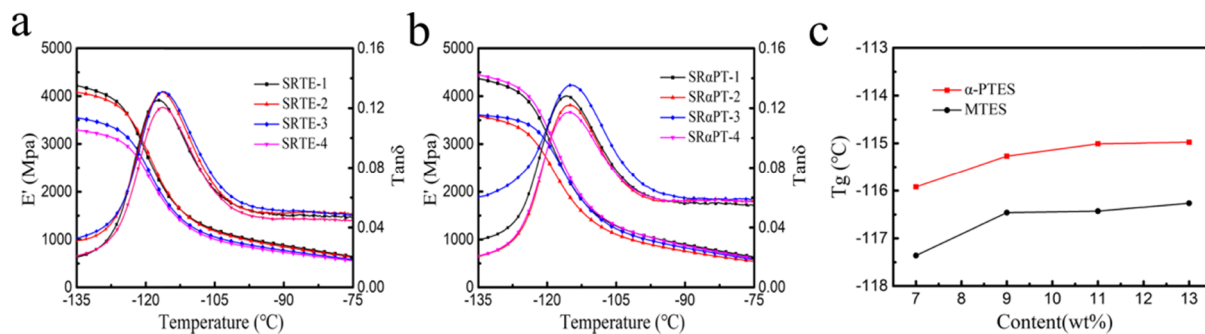
and polyfunctionality of  $\alpha$ -pinene would result in increasing cross-linking density of the modified RTV silicone rubber. Thus, the mechanical and thermal properties of the  $\alpha$ -PTES-modified RTV silicone rubber showed significantly better than those of the unmodified silicone rubber, and the modified silicone rubber (SR $\alpha$ PT-3) has a tensile strength of 0.66 MPa and a break at elongation of 285.8%, which increase by 69.2 and 125%, respectively, and they are nearly doubled compared to the unmodified silicone rubber (SRTE-2). In addition, the  $E'$  values of SR $\alpha$ PT-4 (4446 MPa) increased by 227 MPa compared with those of SRER-1 (4219 MPa). The increased chain entanglement and molecular chain rigidity would enhance the modulus, and the silicone chain fluidity of the silicone rubber would also have significant restrictions. This study shows that by using  $\alpha$ -pinene as a new cross-linking agent, the improvement of the mechanical and thermal properties of the silicone rubber could be achieved.

## MATERIALS AND METHODS

**Materials.**  $\alpha$ -Pinene ( $\omega = 98\%$ ), dibutyltin dilaurate ( $\omega = 95\%$ ), and methyltriethoxysilane (MTES,  $\omega = 98\%$ ) were purchased from Shanghai Aladdin Technology Co., Ltd. Triethoxysilane ( $\omega \geq 99\%$ ) was purchased from Shandong Silicon Branch New Material Co., Ltd. Karstedt's catalyst (Pt of  $\sim 2\%$ , in xylene) was purchased from Shanghai Neutron Star



**Figure 7.** (a) Stress–strain curves of SRTE. (b) Stress–strain curves of SR $\alpha$ PT. (c) Tensile strength of SR $\alpha$ PT and SRTE. (d) Break at elongation of SR $\alpha$ PT and SRTE. (e) Tensile moduli of SR $\alpha$ PT and SRTE at 100% elongation. (f) Hardness of RTV silicone rubber.



**Figure 8.** (a) Curves of storage modulus ( $E'$ ) and  $\tan \delta$  of SRTE. (b) Curves of storage modulus ( $E'$ ) and  $\tan \delta$  of SR $\alpha$ PT. (c)  $T_g$  curves of SR $\alpha$ PT and SRTE.

Chemical Technology Co., Ltd. Hydroxy-terminated poly-(dimethylsiloxane) (PDMS, 5000 mPa·s) was purchased from Hubei New Universal Chemical Co., Ltd. The chemicals were not further purified in this study.

**Synthesis of  $\alpha$ -Pinanyl-Modified Triethoxysilane ( $\alpha$ -PTES).** The reflux condenser, constant pressure dropping funnel, and thermometer were assembled on a 50 mL three-necked flask that was correspondingly filled with  $\alpha$ -pinene (5 g), Karstedt's catalyst (in xylene, Pt of  $\sim 2$  wt %, 82  $\mu$ L), and triethoxysilane (9 g). The mixture was heated to 100  $^{\circ}$ C under continuous stirring for 60 h at a speed of 250 r/min. Finally, the liquid product and the unreacted raw material were distilled off under reduced pressure and normal pressure, respectively.

**Preparation of Modified RTV Silicone Rubber.** While using a nitrogen atmosphere as a protection, we added both the cross-linking agents ( $\alpha$ -PTES or MTES, 2.1 g) and the PDMS (30 g) to the three-necked flask. The blend was then continuously stirred at a speed of 1500 r/min for 15 min at room temperature. Next, we added 180  $\mu$ L of dibutyltin dilaurate catalyst to the same flask and stirred the mixture continuously for 15 min at a speed of 1500 r/min. Finally, we

removed the bubbles and rapidly poured the mixture into a Teflon mold. To make the surface of the obtained modified silicone rubber sheet smooth, we cured the mixture for 7 days at room temperature. The ingredients of each sample are shown in Table 1 in detail.

In all ingredient compositions, dibutyltin dilaurate (180  $\mu$ L) and PDMS (30 g) were respectively functioned as the catalyst

**Table 1. Ingredient Compositions That Were Used To Prepare Modified Silicone Rubber**

sample	PDMS (g)	$\alpha$ -PTES (g)	MTES (g)	catalyst ( $\mu$ L)	$\alpha$ -PTES (wt %)	MTES (wt %)
SRTE-1	30	0	2.1	180	0	7
SRTE-2	30	0	2.7	180	0	9
SRTE-3	30	0	3.3	180	0	11
SRTE-4	30	0	3.9	180	0	13
SR $\alpha$ PT-1	30	2.1	0	180	7	0
SR $\alpha$ PT-2	30	2.7	0	180	9	0
SR $\alpha$ PT-3	30	3.3	0	180	11	0
SR $\alpha$ PT-4	30	3.9	0	180	13	0

and the matrix. As shown in Table 1, the mass fractions of  $\alpha$ -PTES and MTES both increase from 7 to 13 wt %.

## MEASUREMENTS AND CHARACTERIZATION

**FT-IR.** Through attenuated total reflectance (ATR), Fourier transform infrared (FT-IR) spectra were performed on a Thermo Scientific Nicolet IS10 spectrometer (Nicolet). Each sample was analyzed through 16 scans between 500 and 3500  $\text{cm}^{-1}$  at a 4  $\text{cm}^{-1}$  resolution.

**NMR.** At two frequencies, 400.13 and 100.61 MHz, an AV400 spectrometer (Bruker, Germany) recorded the  $^1\text{H}$  NMR spectra for  $\alpha$ -PTES. We used tetramethylsilane (TMS) and deuteriochloroform ( $\text{CDCl}_3$ ) as the internal standard and solvent for  $\alpha$ -PTES, respectively. The signals of TMS and  $\text{CDCl}_3$  were the chemical shift values.

**Mass Spectrometry.** Mass spectra were determined by a Reflex III (Bruker, Billerica, MA) time-of-flight mass spectrometer equipped with a reflectron and a 1.25 m flight tube. The sample was analyzed with the accelerating voltage (19 kV) and reflectron voltage (20 kV), and the delay times were 200 ns. All the experiments were carried out in a reflectron mode.

**Density.** Through a pycnometer, the samples' densities were measured.

**TG.** A TG209F1 (Netzsch, Germany) was used to analyze the thermal stability of the sample. The samples were heated from 25 to 800  $^\circ\text{C}$  with a heating rate of 10  $^\circ\text{C}/\text{min}$  in an  $\text{Al}_2\text{O}_3$  crucible under a nitrogen atmosphere.

**Hardness.** The hardness of silicone rubber was determined by an LX-A durometer (Eide fort, China) at room temperature and  $\sim 65\%$  relative humidity.

**Mechanical Properties.** To analyze the mechanical properties of samples, a UTM6502 universal testing machine (Suns) with a capacity of 500 N was used. The analysis was conducted after preparing five dumbbell-shaped specimens by using a crosshead with an RH around 50% at 23  $^\circ\text{C}$  and a speed of 500 mm/min. The data was expressed as the average of five measurements.

**SEM.** At a voltage of 10 kV, the morphologies of all samples were observed through a scanning electron microscope (QUANTA 200, FEI, Holland). After coating the fractured surface of the samples with gold, an analysis was conducted.

**EDS.** The element composition of silicone rubber was determined by X-ACT energy dispersive X-ray spectroscopy (Oxford, England).

**DMA.** A DMA Q800 (TA) was used to analysis the dynamic mechanical property of the sample. Under the stretching mode, at a heating rate of 3  $^\circ\text{C}/\text{min}$  and with a 1 Hz frequency, the samples were analyzed with a scanning temperature range from  $-135$  to  $-75$   $^\circ\text{C}$ .

**Cross-Linking Density.** An equilibrium swelling method was used to recalculate the cross-linking densities of SR $\alpha$ PT and SRTE. Before analysis, at a temperature of 25  $^\circ\text{C}$ , SR $\alpha$ PT or SRTE (around 0.2 g) was immersed into toluene (25 mL) that was in a sealed container for 48 h. After taking the samples out of toluene and weighing them after removing the excess toluene by a filter paper, the samples were immersed into toluene for another time. We repeated the above steps every 3 h until reaching the swelling balance. According to eqs 1 and 2, the cross-linking density was obtained.<sup>8,35</sup>

$$\varphi = (m_0/\rho)/[(m_s - m_0)/\rho_1 + m_0/\rho] \quad (1)$$

$$\gamma_e = \rho/M_C = -[\ln(1 - \varphi) + \varphi + \chi_1\varphi^2]/(\nu_0\varphi^{1/3}) \quad (2)$$

In the above formula,  $\varphi$  is the volume fraction,  $m_0$  is the original sample weight,  $\rho$  is the modified silicone rubber density,  $m_s$  is the swelling weight of the modified silicone rubber,  $\rho_1$  (0.87  $\text{g}/\text{cm}^3$ ) is the toluene density, and  $\nu_0$  (106.54  $\text{cm}^3/\text{mol}$ ) is the toluene molar volume.  $\chi_1$  (0.465) is the interaction parameter of the solvent and polymer,  $M_C$  is the mean molecular weight of the cross-linking points, and  $\gamma_e$  represents the cross-linking density.

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### Notes

The authors declare no competing financial interest.

## ACKNOWLEDGMENTS

This work was supported by National Natural Science Foundation of China (31600462) and Mudanjiang Normal University National Project Cultivation Project (GP2018002).

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