Contents lists available at [ScienceDirect](http://www.sciencedirect.com/science/journal/22135979)

Photoacoustics

journal homepage: www.elsevier.com/locate/pacs

Review of cost reduction methods in photoacoustic computed tomography

Afreen F[a](#page-0-0)tima a,b,1 a,b,1 a,b,1 a,b,1 , Karl K[ra](#page-0-0)tkiewicz a,1 , Rayyan Manwar a,1 , Mohsin Zafar a , Ruiying Zhang c , Bin Huang^{[d](#page-0-4)}, N[e](#page-0-5)da Dadashzadeh^e, Jun Xia^{[f](#page-0-6)}, Kamran (Mohammad) Avanaki^{[a,](#page-0-0)[g](#page-0-7)[,h,](#page-0-8)}*

^a *Department of Biomedical Engineering, Wayne State University, Detroit, MI, USA*

^b *Department of Electrical & Computer Engineering, Wayne State University, Detroit, MI, USA*

^c *Edan Medical, Sunnyvale, USA*

^d *3339 Northwest Ave, Bellingham, WA, USA*

^e *R&D Fiber-Laser Department, Coherent Inc., East Granby, CT, USA*

f *Department of Biomedical Engineering, The State University of New York, Buffalo, NY, USA*

^g *Department of Neurology, Wayne State University School of Medicine, Detroit, MI, USA*

^h *Molecular Imaging Program, Barbara Ann Karmanos Cancer Institute, Wayne State University, Detroit, MI, USA*

ARTICLE INFO

Keywords: Low-cost Photoacoustic computed tomography PACT

ABSTRACT

Photoacoustic Computed Tomography (PACT) is a major configuration of photoacoustic imaging, a hybrid noninvasive modality for both functional and molecular imaging. PACT has rapidly gained importance in the field of biomedical imaging due to superior performance as compared to conventional optical imaging counterparts. However, the overall cost of developing a PACT system is one of the challenges towards clinical translation of this novel technique. The cost of a typical commercial PACT system originates from optical source, ultrasound detector, and data acquisition unit. With growing applications of photoacoustic imaging, there is a tremendous demand towards reducing its cost. In this review article, we have discussed various approaches to reduce the overall cost of a PACT system, and provided a cost estimation to build a low-cost PACT system.

1. Introduction

Photoacoustic computed tomography (PACT) is a major configuration of photoacoustic imaging (PAI), a novel hybrid imaging modality that combines optical excitation of the target sample with acoustic detection that is generated due to thermal expansion of the sample as shown in [Fig. 1](#page-1-0). In PACT, high energy pulsed laser light is diffused to create a full field illumination that covers the sample (tissue), and photoacoustic waves are generated $[1-3]$. The waves around the tissue are collected by wideband ultrasound transducers [[4](#page-9-1)[,5\]](#page-9-2). The detection scheme can be realized either by a single ultrasound transducer which rotates around the sample ([Fig. 2\(](#page-1-1)a)), a linear array [\(Fig. 2\(](#page-1-1)b)), or a stationary ring array of 128, 256, or more number of transducer elements (Fig. $2(c)$) [\[6–12\]](#page-9-3). The ultrasound waves collected from the object are acquired using a data acquisition (DAQ) unit, and an image reconstruction algorithm is used to reconstruct a PACT image. The image shows vascular and functional information of the tissue.

The rising number of investments in research and development coupled with the constant pace of technological advancement leading to the development of hybrid imaging systems is primarily driving the

growth of the global preclinical imaging market [\[13](#page-9-4)]. The global optical imaging market is anticipated to be approximately \$1.9 billion by end of 2018, growing at a compound annual rate (CAGR) of 11.37%. Among the optical imaging modalities, photoacoustic and near-infrared spectroscopy contributes ˜6.85% combined [\[14](#page-9-5)]. PACT has gained even more popularity for deep tissue imaging (within the range of several centimeters [\[15–17\]](#page-9-6)) where coarse resolution is acceptable. Over the past few years, various preclinical and clinical applications of this technique have been demonstrated, including functional brain imaging, small-animal whole-body imaging, breast cancer screening [\[1\]](#page-9-0), and guidance of lymph node biopsy [[18\]](#page-9-7). Several improvements have been applied to PACT to overcome its limitations [[3](#page-9-8)[,19–26](#page-9-9)]. The main reason for the popularity of PAI compared to optical imaging methods is that, the acoustic scattering in tissue is about three orders of magnitude lower than optical scattering [[3](#page-9-8),[27–30\]](#page-9-10).

Considering many advancements of photoacoustic imaging in PACT system development, it is still in its early stage for clinical use compare to established imaging modalities such as magnetic resonance imaging, positron emission tomography and computed tomography. The major hurdle is cost. The cost of PACT systems which are commercially

<https://doi.org/10.1016/j.pacs.2019.100137>

Received 4 December 2018; Received in revised form 11 May 2019; Accepted 13 June 2019 Available online 26 July 2019

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[⁎] Corresponding author at: Department of Biomedical Engineering, Wayne State University, Detroit, MI, USA.

E-mail address: mrn.avanaki@wayne.edu (K.M. Avanaki).

 $^{\rm 1}$ These authors have contributed equally.

Fig. 1. Principle of photoacoustic signal generation, detection, and acquisition.

Fig. 2. Typical configurations of a PACT. (a) Single/multi element transducers in ring fashion, (b) linear-array, and (c) ring/circular transducer array.

Table 1

available is provided in [Table 1](#page-1-2). The majority of the cost originates from three main components: (1) optical source, (2) ultrasound detector, and (3) DAQ unit.

Different optical sources for the implementation of a low-cost PACT system have been discussed in [\[31](#page-9-11)[,32](#page-9-12)]. Typically, a Q-switched Nd: YAG pulsed laser is employed in commercially available PACT systems that costs in the range of \$15˜\$100 K USD depending on the level of energy/pulse and the pulse width. Some of these laser sources provide built-in fixed wavelength options, typically at 532 nm and 1064 nm. There is an additional cost for continuous wavelength tuning feature (650–950 nm) that is provided by optical parametric oscillator (OPO) and typically used for PA imaging of specific endogenous or exogenous chromophores. Commercial PACT systems come with application specific ultrasound transducer probe which are typically charged in the range of \$1K˜\$200 K. Based on the application and system configuration, the geometry (i.e. linear [[33\]](#page-9-13), two-dimensional (2D) [\[34](#page-9-14)], arc,

ring [[35\]](#page-9-15), or hemisphere [[36\]](#page-9-16)), number of elements (64–2048), and center frequency (1–55 MHz) of the transducer varies. Linear arraybased configurations offer fast image acquisition; however, they rely on expensive hardware and data acquisition unit. The cost of PACT systems increases due to expensive software packages for system control, image reconstruction, display and post-processing (˜\$1K–\$50 K). The cost of a commercial PACT system is ˜\$50K–\$500 K. Vevo LAZR and LAZR X (Fujifilm VISUALSONICS, Canada) [\[37\]](#page-9-17), Nexus 128+ (Endra Life Sciences, USA) [[38\]](#page-9-18), LOUISA 3D (TomoWave, Inc, USA) [[39,](#page-9-19)[40](#page-9-20)], and MSOT inVision 128 (iTheraMedical GmbH, Germany) [\[33](#page-9-13)] are commercial PACT systems that provide real-time volumetric vascular/ functional images [[41–43](#page-9-21)].

Due to the increasing number of applications of PACTs, there is an urgent need to make cost-effective, compact and portable PACT systems. In the following sections, we have discussed the cost-reduction methods in PACT systems. Firstly, we reviewed alternate affordable

laser sources, followed by in-depth discussion of low-cost ultrasound transducer configurations, and finally examples of low-cost DAQs. Based on the elaborative review on the low-cost solutions, at the end we have estimated the cost of a low cost PACT system.

2. Conventional cost-reduction methods

Here, we have discussed the conventional approaches for cost reduction of PACT systems in terms of their major hardware components. In Section 2.1, we have reviewed the light sources. Low-cost ultrasound detection apparatus for the PACT systems are discussed in Section 2.2. Finally, DAQs are reviewed in Section 2.3.

2.1. Affordable compact light sources

Although typically in PACT systems, nanosecond pulsed laser sources with average pulse energy of 10–100 mJ are desirable [\[44](#page-9-22)], other, lower-cost light sources such as laser diodes (LD), light-emitting diodes (LED), flash lamps, electrically-pumped lasers, and opticallypumped lasers can be used [\[45–48](#page-9-23)]. Since the beam divergence and beam quality of the light sources used in the configuration of PACT are not required to be stringent, there is more options than expensive lasers with fine linewidth. In the following sub-sections, we review the light sources that are being used for low-cost PACT systems.

2.1.1. Laser diodes (LDs)

LDs are examples of electrically-pumped lasers. In LDs, the gain is obtained by an electrical current flowing through p-i-n structure of the semiconductor medium. LDs can be manufactured based on different technologies and wide variety of them are commercially available in laser industry [\[49–52](#page-9-24)]. LDs usually operate in the wavelength range between 750 nm to 980 nm [\[53](#page-10-0)[,54](#page-10-1)] and are also available in visible wavelengths ranging from 400 nm to 650 nm, where blood absorption is strong (> 10 cm⁻¹) and water absorption is weak (< 10^{-3} cm⁻¹) [[53–55](#page-10-0)]. Attempts have been made to use LDs in handheld devices because of their compact size [[56–60](#page-10-2)]. One of the LDs that has been developed to use in PACT system is developed by Kohl et al. [[61\]](#page-10-3) and Canal et al. [\[62](#page-10-4)]. This LD is a pulsed ultra-compact multi-wavelength LD array source which delivers pulse energies comparable to nanosecond Nd: YAG lasers. The laser system has a footprint of 20 cm^2 and provides pulses with a pulserepetition rate (PRR) of 10 kHz, pulse energy of 1.7 mJ, and pulse width of 40 ns at single wavelengths of 808 nm, 915 nm, 940 nm, or 980 nm. Daoudi, et al. [\[58](#page-10-5)] also developed an LD that is appropriate for PACT system. This LD is made based on diode stacks technology [\[58\]](#page-10-5). In this laser, the diodes are driven by a customized laser driver (Brightloop, France). This LD is measured to produce pulses with pulse width of 130 ns, PRR of 10 kHz, and emission wavelength of 805 nm. The PACT system that uses this laser has experimentally been utilized for phantoms and *in-vivo* imaging of human proximal interphalangeal joint as shown in [Fig. 3](#page-2-0) [\[58\]](#page-10-5). There are several other studies that have used light source array to increase the laser energy [\[56](#page-10-2)[,63\]](#page-10-6). The only limitations of using

array light source is the large beam size and circularity issues of the light source in addition to the requirement of using a larger pump driver [[59,](#page-10-7)[64](#page-10-8)]. This limitation is especially problematic in photoacoustic microscopy where a tight focus is needed, not in PACT where a diffused light is used. If the laser energy and pulse width of the LD array is the same as a high energy Nd:YAG laser, we expect to see the same quality PA images.

2.1.2. Light emitting diodes (LEDs)

LED is a category of light sources that has been used in PACT system due to their extremely compact size, lightweight, long lifetime, and lowcost potentials. Although the fundamental process of light generation in LEDs is similar to LDs, LEDs do not generate stimulated emission [[65](#page-10-9)]. Therefore, their optical spectrum is broad bandwidth, their spatial coherence is low, and they are not technically considered as laser sources. However, they are still proper light sources for applications that do not require a narrow linewidth light source such as PA imaging. LEDs can be manufactured in a wide wavelength range [[66–68\]](#page-10-10). Broad wavelength range of LEDs makes them ideal candidates for spectroscopic applications in PA field [[69](#page-10-11)[,70\]](#page-10-12). The enormous progress in creating high-power LEDs has brought attentions to them as an efficient low-cost light source for large output signals. LEDs provide pulse energies of tens of μJ when operated in pulsed mode at low duty cycles (< 1%) and are driven by ten times of their rated current [\[69\]](#page-10-11). PreXionLED (PreXion Corp.,Tokyo, Japan), is LED arrays that can provide pulses with 1 kHz PRR, 100 ns pulse width, and 200 μJ pulse energy at wavelengths of 750 nm, 850 nm, and 930 nm [\[68,](#page-10-13)[70](#page-10-12)]. Using LED arrays, imaging of PA contrast agent, i.e., Indocyanine green (ICG) under several centimeters of chicken breast tissue was successfully demonstrated [\[67](#page-10-14)]. Additionally in [\[70](#page-10-12)], these LED arrays have been utilized in various clinical applications such as assessment of peripheral microvascular function and dynamic changes, diagnosis of inflammatory arthritis, and detection of head and neck cancer. The LED arrays (PreXion Corporation), and a resulting image from the PACT setup is shown in [Fig. 4.](#page-3-0) Kang et al. also used LED arrays for tube phantoms imaging on mouse skull and human skull samples [[71](#page-10-15)]. LED arrays was also used by Dai et al. for performing *in vivo* mouse ear vasculature imaging.

2.1.3. Xenon flash lamp (XFL)

XFL is a very low cost high energy light source for PACT when single-mode operation and high spatial resolution are not required. XFLs have cathode and anode electrodes facing each other in a Xenonfilled glass bulb and they emit by arc discharge. XFLs emit in a broad spectrum from UV to IR, and they have high intensity, high stability, and long life-time. Pulsed XFLs with high pulse energy and microsecond pulse widths have been used as a low-cost alternative light source in PACT systems. Wong et al. demonstrated *in vivo* rat imaging using an XFL. The vasculature in a rat body was clearly observed in the PACT image as shown in [Fig. 5](#page-3-1) [\[72](#page-10-16)]. Since the optical illumination from XFLs meets requirement of human's laser exposure, XFLs can potentially be applied to human tissue for imaging purposes.

Fig. 3. (a) A schematic of the handheld PACT probe. US: ultrasound array transducer, P: deflecting prism, DOE: diffractive optical elements, DS: diode stack, MCL: micro-cylindrical lenses, CR: Aluminum cooling rim. Photoacoustic/ultrasound images of a human proximal interphalangeal joint in (b) sagittal and (c) transverse planes. Reproduced with permission from Ref. [\[58](#page-10-5)].

Fig. 4. (a) Photo of a pair of dual-wavelength LED bars that emits 690-nm and 850-nm light alternatively. (b) PA (pseudo color) and US (gray scale) combined image showing the microvessels in the cross-section of a human finger. Reproduced with permission from Ref. [[70\]](#page-10-12).

2.1.4. Solid-state diode-pumped laser (DPL)

Main categories of optically pumped lasers are lamp-pumped lasers (LPL) and diode-pumped lasers. Solid-state DPLs are known as either bulk lasers, that have a crystal as their active media, or fiber lasers, in which light propagates in active optical fibers as the gain media [[73–75\]](#page-10-17). Solid-state DPLs can be designed to produce power levels of a few mWs to multiple KWs due to their high energy conversion efficiency. Solid-state DPLs make compact lasers and a better candidate for PA imaging than bulky water-cooled lamp-pumped lasers. Wang et al. used a compact high-power DPL (Montfort Laser GmbH Inc., Germany) for deep tissue *in vivo* PACT imaging [[76\]](#page-10-18). It has a miniature size of $13.2 \times 14.0 \times 6.5$ cm 3 , a weight of 1.6 kg, average power output of 4 W with a high pulse energy of up to 80 mJ at the wavelength 1064 nm with a PRR up to 50 Hz (see Fig. $6(a)$). Using this laser system as shown in [Fig. 6\(](#page-4-0)b), they successfully imaged murine whole-body vascular structures and cardiac functions *in vivo*, and mapped the arm, palm and breast vasculatures of living human subjects.

2.1.5. Continuous wave (CW) lasers

Continuous-wave (CW) operation mode of a laser stands for the case that the laser is continuously pumped and continuously emits light. The CW emission of a laser can occur in either a single resonator mode or in multiple modes. Some of the CW lasers that are inexpensive, compact, and durable with an average power of several Watts, are generated by LDs [\[44\]](#page-9-22). LeBoulluec et al. designed a frequency domain- PA imaging system and used a CW LD as the light source with central wavelength of 785 nm and 100 mW output power [[77](#page-10-19)]. They tested the imaging system on several tissue-like phantoms, where, CW PA detection used a narrowband ultrasonic transducer and a lock-in amplifier with high sensitivity and strong noise rejection. In Ref. [[78\]](#page-10-20), another inexpensive, compact and durable single frequency intensity modulated CW laser diode based PA system was reported as shown in [Fig. 7](#page-4-1) (a). This system was successfully employed to image ˜3 mm deep vessels in tissue ([Fig. 7](#page-4-1)(b)).

In [Table 2,](#page-5-0) we have summarized different laser sources that have been used in PACT imaging systems with their specifications and particular imaging applications.

2.2. Less expensive photoacoustic signal detection methods

Another major pricy component of a PAI system is the detection unit. A considerable cost reduction is achieved if we can utilize the existing ultrasound detection system and integrate the PAI system into it. Typically, piezoelectric thin films are used to fabricate ultrasound transducers based on piezoelectric effect [[83](#page-10-21)]. The most popular piezoelectric materials are the polycrystalline ferroelectric ceramic materials, such as barium titanate (BaTiO3) and lead zirconate titanate (PZT), which consist of randomly oriented crystallites (grains), separated by grain boundaries [\[84](#page-10-22)]. These materials are much less expensive than single crystals (lead magnesium niobate–lead titanate (PMN–PT) and lead zinc niobate–lead titanate (PZN–PT)) but offer strong piezoelectric properties along polarization axes. Piezoelectric polymers such as polyvinylidene (PVDF) and its copolymer with trifluoroethylene (TrFE) have also been found to be useful for producing high frequency transducers [[85,](#page-10-23)[86\]](#page-10-24). PZT has been the dominant material for the active elements of transducers and arrays [\[87–90](#page-10-25)]. A summary of the low-cost PA ultrasound detection methods is provided in [Table 3.](#page-6-0)

Fig. 5. (a) Xenon flash lamp illumination, (b) PACT image of a mouse body *in vivo*. Reproduced with permission from Ref. [\[72](#page-10-16)].

Fig. 6. (a) Photographs of a diode-pumped Nd:YAG laser; (b) mouse anatomical and functional imaging; (i) PA image of cerebral vasculature of a mouse brain. CoS: confluence of sinuses, ICV: inferior cerebral vein, SSS: superior sagittal sinus, TS: transverse sinus, (ii) PA cross sectional image of the heart region. ST: sternum, HT: heart, LL: left lung, RR: right lung, (iii) PA cross sectional image of liver region. LLV: left lobe of liver, PV: portal vein, RLV: right lobe of liver, IVC: inferior vena cava, (iv) PA cross sectional image of kidney region. Reproduced with permission from Ref. [\[76](#page-10-18)].

2.2.1. Single element transducers

One way to reduce the overall cost of a PACT system is by reducing the number of transducers. Several strategies have been evaluated. The scanning of a single-element finite-size transducer, due to its simplicity and high sensitivity, is widely used in the implementation of PACT

[[91](#page-10-26)[,92](#page-10-27)]. The disadvantage of this configuration is a low temporal resolution. Scanning a number of single element transducers, also called multi element transducer PACT (MET-PACT), can greatly reduce the cost for a PACT system while preserving a high temporal resolution. Several groups including ours have demonstrated the use of this

Fig. 7. (a) Schematic of the CW PACT system, (b) amplitude image of a rabbit tibial artery (TA) and a tibial vein (TV) acquired with the CW PA imaging system. Reproduced with permission from Ref. [[79](#page-10-28)].

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Table 2

Optical window: $A < 600$ nm, 600 nm $\lt B < 900$ nm, and $C > 900$ nm.

Only CW laser energy is provided in Watts.

^b NA: Not applicable.

Fig. 8. A multi element transducer PACT system comprised of a portable EKSPLA laser head, power supply for the laser, chiller, DC supply for the motor driver, NI DAQ, NI trigger, servo motor, motor gear, 3-axis translation stage, and 16 sets of transducers and amplifiers. Reproduced with permission from Ref. [\[98](#page-10-30)].

configuration with a high frame rate $($ $-1-2s)$ and several-centimeter penetration depth [[93–97\]](#page-10-29). The major drawback in using multiple single element transducers in a PACT is that all of them cannot be placed experimentally at the same distance from the scanning center. Each of them rotates around the sample in concentric circles with slight difference in radius $($ -1 -3 mm). Based on trial and error, this issue can be resolved. However it is time consuming and becomes even more complex when the number of transducers increases. In Ref. [\[98](#page-10-30)], a MET-PACT with 16 single-element 5 MHz ultrasound transducers (Technisonic, ISL-0504-GP) have been implemented. More can be read in Refs. [[98,](#page-10-30)[99\]](#page-10-31). The transducers spatially separated with 22.5° from each other were inserted and fitted along the circumference of the circular ring made up of polyactic acid (PLA) plastic (15 cm diameter) (see [Fig. 8\)](#page-5-1). A data correction algorithm was performed to resolve the difficulty in placing the transducers at the same distance from the scanning center. The use of partial view detection with reflectors is another method to decrease the numbers of ultrasound transducers needed [[98,](#page-10-30)[100\]](#page-10-32).

2.2.2. Linear array transducers

In addition to MET-PACT, linear detector arrays have also been studied. A large planar detector can be a piezoelectric plate much larger than the object to be imaged [[101](#page-10-33)]. Linear arrays can be easily manufactured and fabricated in batches, hence the production cost is lower and yield-rate can be very high as compared to custom-made curved or ring arrays [\[102](#page-10-34)[,103\]](#page-10-35). Most importantly, these arrays have been commonly used in clinical applications and can easily be integrated with the light sources. Four linear array US/PA transducers are shown in [Fig. 9](#page-6-1) where they are coupled with different configurations of light sources.

Linear array-based photoacoustic imaging could be the closest configuration of photoacoustic imaging to the clinic. The appearance of the PA probe in this configuration is similar to the US probe that clinicians are used to work with, in addition to the hand-held and compact nature of them.

Several groups have implemneted linear array PACT. In Refs. [[58](#page-10-5)[,104\]](#page-10-36), the ultrasound detection is performed with an ultrasound pulse/receiver array (based on the commercial Esaote SL3323 ultrasound probe) composed of 128 elements, each with a length of 5 mm and a pitch of 0.245 mm. The array has a central frequency of 7.5 MHz

Fig. 9. Linear array transducers used in photoacoustic signal detection, (a) Reproduced with permission from Ref. [\[104\]](#page-10-36), (b) Reproduced with permission from Ref. [[18\]](#page-9-7), (c) Reproduced with permission from Ref. [[67\]](#page-10-14), and (d) Visualsonic PA probe. Reproduced with permission from Fujifilm VisualSonics Inc.

and a measured −6 dB bandwidth of around 100%. Li et al. developed and engineered a handheld probe-based photoacoustic imaging system that was built on an open-platform ultrasound imaging system with a 128-element linear array ultrasound scanner (7 MHz, LA0303, S-sharp, Taiwan). Several real-time systems for small animal experiment have also been reported. Due to the limited aperture of linear array transducers, features with high aspect-ratio or orientations oblique to the transducer surface suffer distortion and azimuthal resolution is reduced. Chinni et al. have designed and implemented a novel acoustic lens based focusing technology that improves the overall aperture of the linear array transducer [[105](#page-10-41)]. In this system, all generated PA waves from the laser get focused simultaneously by the lens onto an image plane to produce a 2D mapping of the absorber distribution. The lens is not digital however, equally effective focusing can be achieved by judicious choice of lens material for signals over a large band of frequencies. A linear array transducer was used to capture the focused PA signals. By scanning the linear array in the image plane, both C-scan and volumetric data sets were generated. The acoustic lens did not consume electrical power, eliminates the dedicated software and hardware for beamforming and image reconstruction. The system is compact and economical with lower system design and fabrication cost.

2.3. Low-cost DAQ and other associated electronic components

Eliminating the need for a high-speed sampling rate requirement may be the most efficient way to reduce the size and cost of data acquisition (DAQ) [\[109\]](#page-10-42). Gao et al. developed a palm-size sensor to use a rectifier circuit (Fig. $10(a)$) to convert the high-frequency PA signal to low-frequency [[109](#page-10-42)]. The proposed photoacoustic receiver could potentially reduce the cost and device size efficiently. The photoacoustic

Table 3

Summary of less expensive PA signal detection methods.

Fig. 10. (a) Photograph of the proposed photoacoustic sensor that can fit in the palm of one's hand. Reproduced with permission from Ref. [[109\]](#page-10-42), A: PA signal input, B: amplifier, C: rectifier, D: Arduino board, and E: display, (b) photoacoustic cell. Its mass is 1.70 kg. (1) The box which contains the electronics and the batteries, (2) photoacoustic cell with an embedded microphone, a laser diode and a photodiode, (3) standard 3.5 mm stereo connectors. Reproduced with permission from Ref. [[110\]](#page-10-46), (c) photograph of the miniature DAQ and control dedicated for PA measurements. Reproduced with permission from Ref. [[111\]](#page-10-47), (d) a photograph of the delay-line module. Reproduced with permission from Ref. [\[112](#page-10-48)].

signal detected by an oscilloscope and its rectified DC signal detected by the proposed palm-size sensor after normalization were in good agreement. The ultrasound transducer used in this case was 1 MHz with 60% fractional bandwidth (V303-SU, Olympus, USA). The rectified photoacoustic DC signal is then sampled by a low-speed analog to digital converter (ADC) with 10 kHz sampling rate and processed by a low-cost microprocessor board (e.g., Arduino Uno).

Low-cost computer-based DAQ has also been investigated. Mihailo et al. used a sound card as DAQ for a low-cost, portable photoacoustic instrument [[110](#page-10-46)]. The device consists of a detection unit comprising of a photoacoustic cell with an embedded laser diode, a photodiode, an electret microphone (60 \times 40 \times 40 mm³), and a signal processing and power supply unit in a box containing batteries and electronics $(160 \times 140 \times 60 \text{ mm}^3)$ ([Fig. 10](#page-7-0)(b)). A PC with an Asus SiS7012 16-bit sound card is required to operate the device and for data processing. The sound card generates the signal for the laser diode or LED modulation and processes signals from the microphone and photodiode. The

experimental points are obtained at a maximum of 48 kHz sampling rate. The described portable photoacoustic apparatus showed good agreement with the results of conventional photoacoustic devices.

A miniature system for data acquisition and control, dedicated for photoacoustic measurements, was developed by Starecki and Grajda [[111](#page-10-47)]. Based on the concept of virtual instruments (intensive use of electronics and digital signal processing), most of the expensive and/or inconvenient elements (mechanical chopper or lock-in amplifier) were eliminated. This system is comprised of two parts. First, the analog module that is used for two-stage PA signal amplification and conversion to digital samples. Second, the digital module acts as a controller of the analog part and simultaneously as a slave for external master controller. This device (Fig. $10(c)$) is capable of data acquisition and basic digital signal processing (i.e. averaging). The advantages of the designed device are very low cost $($$100$), small size, and high func$ tional flexibility. Most of the measurement factors, e.g. analog path gain, light source modulation frequency, number of samples per period, etc. are programmable and can be changed at run-time.

In Ref. [[112](#page-10-48)], a multiway delay line module was proposed to reduce the numbers of DAQ channels required for PACT system and hence the overall cost. The circuitry consisted of multiple voltage comparator (MVC), precise rectify circuit (PRC), delay line module (DLM), multiway adder (MA), and an FPGA board ([Fig. 10\(](#page-7-0)d)). The DLM (4:1) module was connected immediately to the PA detection array. It accommodated three delay units and a transmission unit, which combined the four inputs into one output series in time. The first PA signal was utilized as a reference signal and used to reconstruct the PA signals later. Additionally, the other three PA signals were transformed by three delay line units with different delay time. Finally, four synchronized input signals were combined into one pulse train output in time series. The feasibility of the module was tested through imaging phantoms and the reconstructed images were comparable to the conventional detection method. To improve the image quality, the authors suggested to use denoising technique as a part of the post-processing method.

Implementation of real-time signal sampling was made possible using 8-bit RISC Atmel microcontroller as shown in [Fig. 10\(](#page-7-0)c). It has an internal memory of 512 bytes and 10-bit ADC which is sufficient for 250 ksps data acquisition and real-time operations like averaging. Due to in-circuit programmable components, upgrades of the device were easy. Small size and low power consumption made the device a very good choice for implementation of low-cost photoacoustic instruments.

Another method to implement the data acquisition part of the PACT is by using very high sampling frequency DAQs and multiplexing hardware/software. For instance, utilizing a 500 MHZ DAQ for an application where 50 MHZ sampling frequency is required, along with a hardware or software multiplexing technique, can produce 10 channel of 50 MHz data. We have summarized different low-cost DAQs and associated electronic components in [Table 4.](#page-8-0)

3. Estimated cost for developing a low-cost PAI system

Various alternative options have been discussed to develop a lowcost PACT system. In the following, we suggest a low-cost PACT system. Based on the review on different alternative low-cost options, LD arrays would be an optimal choice considering the delivered optical energy. An LD array with the central wavelength of 905 nm (905D1S03X, Laser Component Co., Bedford, New Hampshire), a peak power of 6 W, and pulse width of 55 ns operating at maximum repetition rate of 20 kHz was used in Ref. [[59\]](#page-10-7). Stacked configuration will provide maximum output of 650 W with a pulse length of 150 ns. For PA signal detection, multiple single element transducers with a stepper motor scanning system could provide 360° full view of the target with relatively fast acquisition. Utilizing a multi-channel DAQ with a very high sampling frequency and multiplexing techniques could be one low cost acquisition method [\[112\]](#page-10-48). Instead of image reconstruction software that is

Table 4

Summary of low cost DAQs and associated electronic components.

MVC: multiple voltage comparator, PRC: precise rectify circuit, DLM: delay line module, MA: multiway adder, FPGA: field programmable gate array.

Table 5

typically developed and customized for a specific PACT system, one can use an open source freeware such as k-wave toolbox or MATLAB (˜300 USD). Estimated cost of individual component is provided in [Table 5.](#page-8-1)

Low-cost PACT systems will have limited applications where, (1) a high temporal resolution is required, (2) a tunable laser is needed for spectroscopy purposes, (3) or a very high energy is needed for deep tissue imaging.

4. Summary and conclusions

PAI is a high contrast, non-invasive and non-ionizing imaging modality with extensive applications in anatomical and functional imaging that has been used for diagnostics purposes and cancer studies [[59](#page-10-7)[,99](#page-10-31)[,113–118](#page-10-49)]. Cost is one major factor hindering PACT's implementation in clinical field. This paper described a comprehensive review on studies and progresses on ways to lower the cost of a PACT system. At first, light sources, as one major component that is significantly contributing to the cost of PACT, were explained. Various light sources such as LDs, LEDs, XFL, and DPL were explained. The type of the light source in the configuration of a PACT is chosen based on the compactness, temporal resolution, energy and beam profile requirements of the imaging application. These low-cost light sources reduce the overall cost of a PACT system, which eventually leads to easy clinical translatability, however, they come with limitations such as low SNR PA signals which consequently degrade the quality of the reconstructed images. We also mentioned that to attain sufficient SNR, LD or LED arrays are the optimum solution. We further explained that in applications where low power consumption is preferred, semiconductor LDs are the best choice. We then discussed different PA signal detection techniques. We mentioned that instead of using complex and expensive ultrasound transducer arrays, commercially available multiple singleelement transducers or linear arrays can be utilized to reduce the cost. The limitation of these transducer arrays is where mechanically moving the transducers is not feasible or a high temporal resolution is required (> 20 Hz). Additionally, we described methods working based on acoustic reflection to improve the limited view of the PA detection system. We discussed different hardware and software based alternatives to implement low cost DAQs. We described how using very high sampling frequency DAQs and multiplexing hardware/software we can implement low-cost data acquisition systems. The role of wavefront shaping and signal postprocessing in low-cost PACT systems is essential

to improve the image quality [[5](#page-9-2)[,22](#page-9-26),[119–124](#page-10-50)]. For example, selection of an optimum laser pulse duration /pulse shape profile has greatly improved the resolution of the reconstructed image [[32,](#page-9-12)[125](#page-11-0)]. According to [\[60](#page-10-51)], it was shown that in deep tissue imaging, utilizing a laser with an optimum pulse duration, the frequency-dependent acoustic attenuation was greatly reduced. Advanced beamforming techniques has also been studied; for example, Bell et al., showed that the PA image contrast of imaging targets at depths 5–15 mm was improved by 11–17 dB with short-lag spatial coherence (SLSC) beamforming when compared to conventional delay-and-sum (DAS) beamforming [[120](#page-10-52),[121](#page-11-1)[,126\]](#page-11-2). Additionally, adaptive denoising technique in Refs [[122](#page-11-3),[127](#page-11-4)]. indicated that the proposed method increased the SNR of PA signals with fewer acquisitions as compared to common averaging techniques. Another effective technique that has been prescribed to improve the quality of PACT images is compressed sensing and sparse acquisition [\[128–131](#page-11-5)]. Other improvement methods are studied in Refs. [\[5,](#page-9-2)[118](#page-10-53),[122](#page-11-3)]. By implementing these algorithms on multi-core processors such as digital signal processors (DSPs) [[132](#page-11-6)], utilizing parallel processing methods [[133](#page-11-7)], the temporal resolution of data acquisition will not be affected. Based on the review of different approaches, we have estimated that to develop a low-cost PACT system for shallow depth imaging applications with comparable performance to the commercial ones, one should spend ~\$20K-\$80 K (see [Table 5](#page-8-1)); the exact cost depends on the specification of the PACT system. By the advancement of the light sources, reducing their size and increasing their energy [\[134\]](#page-11-8), new and low-cost ultrasound detectors with extremely small element size and low power consumption, e.g., micromachined piezo-electric/capacitive ultrasound transducers (P/CMUTs) [[135–137\]](#page-11-9), and development of ultrahigh speed microcontroller-based DSPs with a large memory and number of bits, the cost of PACT systems will gradually be reduced while the quality of their images will be improved. Finally, utilizing all optical ultrasound detection methods [[138–140\]](#page-11-10), will solve the limitation of PA imaging probes where they require ultrasound conducing material between the imaging sample and the probe, and thus widen the applicability of the PACT devices.

Low-cost PACT systems facilitate the emergence of novel, compact, rapid *in vivo* imaging systems to enhance the accessibility and popularity of PAI in clinical applications. We hope this comprehensive review article will help the researchers recognize the different aspects of developing an affordable yet high-performance PACT system for both research purpose and clinical applications.

Declaration of competing interest

The authors declare no conflict of interest.

Funding

This research was partially funded by the American Cancer Society, Research Grant number 14-238-04-IRG and the Albert and Goldye *J*. Nelson grant.

CRediT authorship contribution statement

Afreen Fatima: Writing - original draft, Writing - review & editing. **Karl Kratkiewicz:** Formal analysis, Investigation, Visualization, Writing - original draft, Writing - review & editing. **Rayyan Manwar:** Data curation, Formal analysis, Investigation, Project administration, Software, Validation, Visualization, Writing - original draft, Writing review & editing. **Mohsin Zafar:** Formal analysis, Investigation, Writing - review & editing. **Ruiying Zhang:** Investigation, Methodology, Validation, Writing - original draft. **Bin Huang:** Methodology. **Neda Dadashzadeh:** Data curation, Validation, Writing review & editing. **Jun Xia:** Data curation, Methodology, Supervision, Validation, Writing - original draft, Writing - review & editing. **Kamran (Mohammad) Avanaki:** Conceptualization, Data curation, Funding acquisition, Methodology, Project administration, Resources, Software, Supervision, Validation, Writing - original draft, Writing - review & editing.

Acknowledgement

We would like to thank Dr. Jalilian from University of Michigan, for her insightful discussion.

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Mohammad R.N. Avanaki. In 2012, Mohammad received a Ph.D. with Outstanding Achievement in Medical Optical Imaging and Computing from the University of Kent in the United Kingdom. His bachelor's and master's degrees with honors are in electronics engineering. In 2014, he completed a three-year postdoctoral fellowship at Washington University in St. Louis, in the OILab. He is currently an assistant professor in the Biomedical Engineering, Dermatology and Neurology departments of Wayne State University and Scientific member of Karmanos Cancer Institute. He is also serving as the chair of bio-instrumentation track.

Neda Dadashzadeh. She is currently working in R&D Fiber-Laser Department, Coherent Inc., East Granby, CT, USA.

Bin Huang is specialized in ultrasound/photo-acoustic imaging, ultrasound/photoacoustic system design andimplementation.

Dr. Jun Xia is currently an Assistant Professor in the Biomedical Engineering Department at the University at Buffalo, The State University of New York. He is an expert in photoacoustic and photothermal imaging and has published over fifty journal articles in the field.

Karl Kratkiewicz graduated with an M.S. in biomedical engineering from Wayne State University, Detroit, Michigan, in 2018. He also graduated summa cum laude with a B.S. in biomedical physics from the Wayne State University Honors College in 2017. He is now a biomedical engineering PhD student at Wayne State University. His area of research includes multimodal (ultrasound/photoacoustic/elastography) imaging and photoacoustic neonatal brain imaging.

Rayyan Manwar received his PhD from University of Windsor, Windsor, Ontario in 2017. His bachelor's degree is in Electrical and Electronic Engineering from Islamic University of Technology (IUT), Gazipur, Bangladesh in 2011. Currently, he is a post doctoral fellow at OPIRA Lab, Wayne State University, Detroit, MI. His research interests include MEMS based design, fabrication and characterization, photoacoustic and ultrasound imaging.

Mohsin Zafar received a Master's Degree in Electrical Engineering from Wayne State University, Detroit in 2018. His bachelor's was in electrical engineering. He is currently doing his Ph.D.in Biomedical Engineering from Wayne State University. He has received various funding awards which includes Rumble Fellowship and Graduate Teaching Assistant.

Ruiying Zhang received her PhD degree from Washington University in St. Louis in 2016 and her bachelor's degree from Wuhan University, China in 2011. Currently, she is working as an imaging scientist in Edan Medical USA. Her research interests focus on PA imaging and ultrasound imaging, especially on developing low-cost PA or ultrasound imaging systems for global healthcare.