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Relationships of quantitative ultrasound parameters with cancellous bone microstructure in human calcaneus *in vitro*.

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Abstract

Ultrasound parameters (attenuation, phase velocity, and backscatter), bone mineral density (BMD), and microarchitectural features were measured on 29 human cancellous calcaneus samples *in vitro*. Regression analysis was performed to predict ultrasound parameters from BMD and microarchitectural features. The best univariate predictors of the ultrasound parameters were the indexes of bone quantity: BMD and bone volume fraction (BV/TV). The most predictive univariate models for attenuation, phase velocity, and backscatter coefficient yielded adjusted squared correlation coefficients of 0.69 - 0.73. Multiple regression models yielded adjusted correlation coefficients of 0.74 - 0.83. Therefore, attenuation, phase velocity, and backscatter are primarily determined by bone quantity, but multiple regression models based on bone quantity plus microarchitectural features achieve slightly better predictive performance than models based on bone quantity alone.

Keywords

quantitative ultrasound; cancellous bone; microstructure; bone mineral density

I. INTRODUCTION

Because of low cost, portability, and lack of ionizing radiation, quantitative ultrasound is an attractive alternative to x-ray bone densitometry for the assessment of osteoporotic fracture risk (Langton *et al.*, 1984;Laugier, 2008; Laugier, 2011; Barkmann and Glüer, 2011). A recent position paper by the International Society for Clinical Densitometry indicates growing acceptance of quantitative ultrasound (Krieg *et al.*, 2008).

It is well understood that fracture risk depends not only on BMD (the current gold standard diagnostic measurement) but also on structural properties of the bone. Correlative studies involving quantitative ultrasound measurements and micro computed tomography (microCT) measurements on cancellous bone samples provide insight into relationships

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between macroscopic ultrasound properties and microarchitectural features. Previous regression studies have been conducted in human calcaneus (Nicholson *et al.*, 2001;Chaffai *et al.*, 2002;Wear and Laib, 2003), tibia and femur (Hakulinen *et al.*, 2006;Karjalainen *et al.*, 2009), and femur (Padilla *et al.*, 2008). The literature in this area of investigation was recently reviewed thoroughly by Padilla *et al.* (2008). These studies were based on linear regression analysis, which is the most straightforward approach when the true functional dependencies of the output variables (e.g., ultrasound properties) on the input variables (e.g., BMD and microarchitectural features) are unknown.

This paper reports multiple regression analysis to predict quantitative ultrasound parameters from BMD and microarchitectural measurements in 29 human cancellous calcaneus samples *in vitro*. This analysis provides insight into determinants of clinical ultrasound measurements. The calcaneus is important because it is the most common bone measured by clinical bone sonometers.

The contributions of this paper are as follows. 1) This paper reports multiple regression analysis to predict broadband ultrasonic attenuation and phase velocity as functions of BMD and microarchitecture in human calcaneus and provides independent data to compare with similar human calcaneus studies reported previously by Nicholson *et al.* (2001) and Chaffai *et al.* (2002). 2) This paper reports measurements of relationships between ultrasound backscatter, BMD, and micro-architecture in human calcaneus and investigates the degree of reproducibility of similar studies reported previously only by Chaffai *et al.* (2002) and Wear and Laib (2003). (The latter study utilized a different set of bone samples than the set reported in the present paper and only considered mean trabecular thickness but not other microarchitectural features such as bone volume fraction and mean trabecular number). 3) This paper provides an analysis of the range of values of correlation coefficients among ultrasound parameters, BMD, and microarchitectural features reported in this study and previous studies on human cancellous bone (Nicholson *et al.*, 1998;Trebacz and Natali, 1999;Nicholson *et al.*, 2001;Chaffai *et al.*, 2002;Hakulinen *et al.*, 2006;Padilla *et al.*, 2008;Karjalainen *et al.*, 2009).

II. METHODS

A. Bone samples

Twenty-nine excised human calcaneus samples (extracted from 29 human calcanei) were defatted using a trichloro-ethylene solution. According to previous studies, defatting has a small effect on ultrasound parameters (Langton *et al.*, 1996;Alves *et al.*, 1996;Njeh and Langton, 1997;Nicholson and Bouxsein, 2002;Hoffmeister *et al.*, 2002). The lateral cortical layers were sliced off leaving two parallel surfaces with direct access to trabecular bone. Cortical end-plates have been reported to have a small but measureable (15%) effect on measurements of broadband ultrasound attenuation (Xia *et al.*, 2005). A thin layer of cortical bone remained along the other surfaces of the bone. This cortical layer (see periphery of bone sample in Figure 1) was excluded from regions of interest for bone densitometry, microCT, and ultrasound measurements. The mean sample thickness was 1.8 cm (standard deviation = 0.23 cm).

B. Bone Densitometry

Bone mineral density (BMD) was measured using a Hologic QDR 4500 dual energy x-ray absorptiometry (DXA) system operating in single beam mode. Areal density was determined for central regions of interest (ROIs) so that cortical bone was excluded. The ROIs were approximately $1.8 \text{ cm} \times 3.6 \text{ cm} \times 1.8 \text{ cm}$ (where the last dimension corresponds to the bone sample thickness, which is in the direction parallel to the DXA beam and perpendicular to the plane of Figure 1). Duplicate measurements (without repositioning) were performed on each specimen. The average coefficient of variation for the duplicate areal density determinations was 1.6%. The average areal density (g/cm²) was divided by the thickness of each sample to give volumetric density (g/cm³).

C. MicroCT

Three-dimensional (3-D) trabecular bone microstructure was measured using micro computed tomography (µCT 100, Scanco Medical, Basserdorf, Switzerland). The Scanco μ CT 100 is a cabinet cone-beam scanner with a microfocus x-ray source and a charge coupled device detector (3072×400 elements array). After ultrasound and DXA measurements had been performed, cancellous bone specimens were cut down to dimensions approximately 2.0 cm \times 4.0 cm \times 1.8 cm and imaged at an isotropic voxel size of 17.2 µm (nominal resolution). This resolution has been reported to be sufficient to reveal significant differences between normal and osteoporotic human trabecular bone for bone volume fraction (BV/TV), trabecular thickness (Tb.Th), degree of anisotropy (DA), trabecular number (Tb.N), trabecular spacing (Tb.Sp), and structural model index (SMI) (Isaksson *et al.*, 2011). Within the 2.0 cm \times 4.0 cm \times 1.8 cm reconstruction volume, an interior volume, approximately 1.8 cm × 3.6 cm × 1.6 cm (similar to the DXA analysis volume) was delineated for micro-structural analysis. A constant threshold to distinguish trabecular bone from background was chosen through histogram analysis of each specimen. The threshold was designated at a value below the broad peak in the histogram corresponding to trabeculae. From these segmented images, automated distance transformation algorithms were used to calculate BV/TV, Tb.Th, Tb.Sp, Tb.N, SMI, bone surface fraction (BS/BV), and connectivity density (Conn.D.) based on methods of Hildebrand and Ruegsegger (Ruegsegger et al., 1996;Hildebrand and Ruegsegger, 1997; Hildebrand et al., 1999). Principal material orientations (H1, H2, and H3) and degree of anisotropy (DA) were calculated using 3-D mean intercept length techniques.

D. Ultrasound

Prior to ultrasonic interrogation, samples were vacuum degassed underwater in a desiccator. Subsequently, samples were allowed to thermally equilibrate to room temperature. Water temperature was measured with a digital thermometer for each experiment and ranged between 19° C and 21° C. The relative orientation between the ultrasound beam and the calcaneus samples was the same as with *in vivo* measurements performed with commercial bone sonometers, in which sound propagates in the mediolateral (or lateromedial) direction. Samples were interrogated in a water tank using a Panametrics (Waltham, MA) 5800 pulser/receiver and Panametrics V301 1" diameter, focused (focal length = 1.5"), broadband transducers with center frequencies of 500 kHz. Bone samples were placed in the focal

plane. The diameter of the central lobe of the focused beam at the focal plane ranged from 18 mm to 8 mm across the analysis band from 300 kHz to 700 kHz. (The central lobe width is given by $2.44\lambda z/d$, where λ = wavelength, z = focal length, and d = transducer aperture diameter (Goodman, 1968)). The central portions of the samples were scanned in order to approximate as closely as possible the ROI used in the DXA measurements. Received signals were digitized (8 bit, 10 MHz) using a LeCroy (Chestnut Ridge, NY) 9310C Dual 400 MHz oscilloscope and stored on computer (via GPIB) for off-line analysis.

A through-transmission method was used to measure normalized broadband ultrasonic attenuation (nBUA) and velocities. Using two opposing coaxially-aligned transducers (one transmitter and one receiver), transmitted signals were recorded both with and without the bone sample in the acoustic path. The bone samples were larger in cross-sectional area than the receiving transducer aperture. Attenuation coefficient was estimated using a log spectral difference technique (Kuc and Schwartz, 1979). Attenuation was characterized by the slope of a least-squares linear fit of attenuation coefficient (dB/cm) vs. frequency, resulting in the nBUA (dB/cmMHz) (Langton 1996). Phase velocity and signal velocity were measured using methods published previously (Wear, 2000a; Wear, 2000b; Wear, 2007. For signal velocity, the third zero crossing in advance of pulse envelope maximum (which corresponded approximately to the leading edge of the pulse used in this investigation) was used as a time-of-arrival marker. Since the speed of sound in calcaneus, approximately 1475–1650 m/s (Droin et al., 1998), is comparable to that in distilled water at room temperature, approximately 1480-1490 m/s, potential diffraction-related errors (Xu and Kaufman 1993) in this substitution technique may be ignored (Droin et al. 1998). All frequency domain analysis was performed over the range from 300 kHz to 700 kHz.

Backscatter coefficients were measured using a reference phantom method (Yao et al., 1990). Good agreement between experimental measurements using this method and theoretical predictions based on Faran's theory of scattering (Faran, 1951) for ultrasonic backscatter coefficients from phantoms consisting of glass spheres embedded in gelatin has previously been reported by this laboratory (Wear, 1999). The backscatter coefficient vs. frequency data were least-squares fit to a power law relationship over the range from 300 kHz to 700 kHz. The midband (500 kHz) value of the power law fit was used in the regression analysis. Backscatter data were gated to exclude the specular reflection at the front surface of the bone sample. Although backscatter measurements are less commonly used to characterize bone than attenuation and sound speed, many studies suggest that backscatter is a useful index of cancellous bone properties (Roberjot et al., 1996; Wear and Garra, 1998; Wear, 1999; Hoffmeister et al., 2000; Roux et al, 2001; Hoffmeister et al., 2002; Jenson et al., 2003; Wear and Laib, 2003; Hakulinen et al., 2005; Hakulinen et al., 2006; Jenson et al., 2006; Hoffmeister et al., 2006; Padilla et al., 2006; Riekkinen et al., 2007; Riekkinen et al., 2008; Ta et al., 2008; Padilla et al., 2008; Wear, 2008; Karjalainen et al., 2009; Litniewski et al., 2009; Litniewski et al., 2011; Hoffmeister, 2011; Padilla and Wear, 2011).

For both through-transmission and pulse-echo measurements, each bone sample was scanned (in 5 mm steps) along the major axis of the bone sample (see Figure 1) so that measurements were acquired from the purely cancellous portion of the bone (that is,

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avoiding the cortical layer along the periphery). Thus, a frequency-dependent volume of interest was swept out with dimensions approximately $[1.8 \text{ cm} (at 300 \text{ kHz}) - 0.8 \text{ cm} (at 700 \text{ kHz})] \times 3.6 \text{ cm} \times 1.8 \text{ cm}$ (where the last dimension corresponds to the bone sample thickness, which is in the direction perpendicular to the plane of Figure 1). Since backscatter data were gated to exclude specular reflections at the front surfaces of calcaneus samples, backscatter volumes of interest were a few millimeters smaller in the thickness dimension than attenuation and velocity volumes of interest. Since an ultrasound beam has maximum intensity near its axis of symmetry, the ultrasound measurements were influenced more by the properties of the central regions of the bone samples than the noncentral regions. This is in contrast to the DXA and microCT measurements, which measured the bone samples essentially uniformly throughout the volumes of interest. This disparity in measurement spatial uniformity could reduce correlations between ultrasound and x-ray-based measurements, especially for highly inhomogeneous bone samples.

E. Data Analysis

Stepwise multiple regression analysis was performed to build linear models of ultrasound parameters as functions of BMD and microarchitectural features. The MATLAB (Natick, MA) function "stepwise" was used. In the case of backscatter coefficient, the data were log transformed prior to multiple regression analysis.

III. RESULTS

Figure 1 shows a slice of a microCT image of a calcaneus sample.

Table 1 shows the means, standard deviations, minima and maxima of ultrasound parameters, density, and microarchitectural parameters. The SMI, which in general can vary from 0 for plate-like architectures to 3 for rod-like architectures (Hildebrand and Ruegsegger, 1997) had a mean value of 2.34, suggesting that the bone samples tended to be more rod-like than plate-like.

Table 2 shows Pearson's correlation coefficients between BMD and microarchitectural parameters. Table 3 shows Pearson's correlation coefficients between ultrasound parameters and BMD / microarchitectural parameters. The best univariate predictors of the ultrasound parameters were the indexes of bone quantity, BV/TV and BMD.

Figure 2 shows measurements of nBUA plotted vs. BV/TV for the 29 bone samples. A linear regression fit to the data, BUA (dB/cmMHz) = $-0.31 + 125.5 \times BV/TV$, is also shown.

Figure 3 shows measurements of phase velocity at 500 kHz (PV) plotted vs. BV/TV for the 29 bone samples. The dotted line shows the linear fit to data from parallel-nylon-wire phantoms previously reported (Wear, 2005), suggesting that empirical dependence of phase velocity on BV/TV is similar in cancellous bone samples and parallel-nylon-wire phantoms. (Aluminum-foam phantoms also exhibit ultrasonic properties similar to cancellous bone (Le *et al.*, 2010; Zhang *et al.*, 2011)). Figure 3 also shows theoretical predictions of the dependence of phase velocity on BV/TV predicted using Biot and Biot-related theory for poroelastic solids.

Figure 4 shows measurements of backscatter coefficient plotted vs. BV/TV for the 29 bone samples. A power law fit to the data is also shown.

Table 4 shows univariate and multivariate regression models that predict ultrasound parameters from BMD and microarchitectural parameters. Multiple regressions resulted in substantial increases (over univariate regressions based on BMD) in the adjusted squared correlation coefficients for nBUA and backscatter coefficient, and a moderate increase for phase velocity.

IV. DISCUSSION

Regarding the statistical aspects of the dependencies of nBUA, phase velocity, and backscatter coefficient on BMD and microarchitecture in human calcaneus, the regression analysis presented in this paper is for the most part in agreement with two previous reports (Nicholson *et al.*, 2001; Chaffai *et al.*, 2002). As with previous investigations with nBUA and phase velocity (Nicholson *et al.*, 2001) or nBUA, phase velocity and backscatter coefficient (Chaffai *et al.*, 2002), the best univariate predictors of the ultrasound parameters were the indexes of bone quantity, BMD and BV/TV. The best univariate models for nBUA, phase velocity, and backscatter coefficient yielded squared correlation coefficients of 0.69 - 0.73, a little lower on average than values reported by Nicholson *et al.* (2001), 0.74, and Chaffai *et al.* (2002), 0.71 - 0.81. Multiple regression models for attenuation, phase velocity and backscatter raised squared adjusted correlation coefficients to 0.74 - 0.83, consistent with values reported by Nicholson *et al.* (2001), 0.79 - 0.81.

Table 5 shows univariate correlation coefficients between ultrasound parameters and indexes of bone quantity in human calcaneus *in vitro* for the present study and previous studies by Nicholson et al. (2001) and Chaffai et al. (2002). The studies show moderate agreement. The correlation coefficients from Chaffai et al. (2002) tended to be higher than those for the present study, especially for phase velocity vs. BV/TV, backscatter coefficient vs. BV/TV, and backscatter coefficient vs. BMD. However, as shown in Table 5, the correlation coefficients from Chaffai et al. (2002) in all cases were within or near (± 0.01) the high end of the 95% confidence intervals for the correlation coefficients from the present study. Moreover, it is possible that the widths of the 95% confidence intervals for correlation coefficients for Chaffai et al. were comparable to those for the present study since the numbers of samples for the two studies were similar (25 vs. 29). If so, this would imply overlap in 95% confidence intervals for the two studies. However, if differences in correlation coefficients between the two studies are meaningful, then there are some potential contributing factors that might help explain this. First, there may have been biological differences in the populations studied, as evidenced by the differences in Tb.Th: $72 \pm 18 \,\mu\text{m}$ (Chaffai *et al.*) vs. $127 \pm 17 \,\mu\text{m}$ (present study). Second, Chaffai *et al.* used sample volumes that were thinner in the ultrasound propagation direction (approximately 1 cm vs. approximately 1.8 cm for attenuation and velocity—slightly smaller in both studies for backscatter since gating was performed to exclude specular echoes) perhaps resulting in greater intra-sample homogeneity. Third, Chaffai et al. performed microCT analysis on 7mm-diameter-cylindrical cores rather than $1.6 \text{ cm} \times 3.6 \text{ cm} \times 1.6 \text{ cm}$ rectangular-shaped volumes the present study. Such small diameter samples may have been required for the

European Synchrotron Radiation Facility (ESRF) utilized by Chaffai *et al.*, which had a higher spatial resolution of 10 μ m than the spatial resolution of 17.2 μ m in the present study). Fourth, Chaffai *et al.* used a different frequency band of analysis (200 kHz – 600 kHz) than the one used in the present study (300 kHz – 700 kHz).

In the present study, the square of the correlation coefficient between signal velocity and BMD ($r^2 = 0.81$) was higher than the correlation between phase velocity and BMD ($r^2 = 0.74$) (see Table 5). Haïat *et al.*, (2005) reported similar results for human femur ($r^2 = 0.82$ for signal velocity and $r^2 = 0.67$ for phase velocity).

The statistical aspects of the dependencies of nBUA, phase velocity, and backscatter coefficient on BMD and microarchitecture in human calcaneus measured in this paper may be compared with results by others not only in human calcaneus but also in tibia and femur as shown in Table 6 and Figure 5 (Nicholson *et al.*, 1998;Trebacz and Natali, 1999;Nicholson *et al.*, 2001;Chaffai *et al.*, 2002;Hakulinen *et al.*, 2006;Padilla *et al.*, 2008;Karjalainen *et al.*, 2009). The average correlation coefficients for all three ultrasound parameters are relatively high, near 0.8, for the indexes of bone quantity (BMD and BV/TV) and lower for the remaining parameters. However, the relatively large ranges of values reported in different studies suggest that considerable uncertainty remains regarding the correlation coefficients between ultrasound parameters and microarchitectural features. Variances among different studies are probably due to a combination of differences in skeletal sites, sample preparation, ultrasound measurement methodology, microCT hardware and microarchitectural feature estimation algorithm. A recent report addresses the effect of microCT image resolution (Isaksson *et al.*, 2011).

CONCLUSION

Ultrasound parameters (attenuation, phase velocity, and backscatter), bone mineral density (BMD), and microarchitectural features were measured on 29 human cancellous calcaneus samples *in vitro*. Regression analysis was performed to predict ultrasound parameters from BMD and microarchitectural features. The best univariate predictors of the ultrasound parameters were the indexes of bone quantity: BMD and bone volume fraction (BV/TV). Therefore, attenuation, phase velocity, and backscatter coefficient are primarily determined by bone quantity, but multiple regression models based on bone quantity plus microarchitectural features achieve slightly better predictive performance than models based on bone quantity alone.

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A slice from a micro-computed tomogram of calcaneus. Some trabeculae appear to terminate as they move into and out of the imaging plane. Image acquired by Andres Laib, Scanco Medical AG, Bruttisellen, Switzerland. A -3 dB beam cross section at 500 kHz is shown.



2.

Measurements of nBUA plotted vs. BV/TV for the 29 bone samples. A linear regression fit to the data is also shown. The dotted lines show the linear regression fit plus or minus one standard error.



Measurements of phase velocity (PV) (at 500 kHz) plotted vs. BV/TV for the 29 bone samples. The dotted line shows the linear fit to data from parallel-nylon-wire phantoms previously reported (Wear, 2005). The other lines show theoretical forms based on Biot theory (Biot 1956a, 1956b, 1956c, 1962, 1963), which has been applied to bone by many investigators (McKelvie and Palmer 1991; Williams 1992; Hosokawa and Otani 1997, 1998; Haire and Langton 1999; Pakula and Kubik, 2002; Hughes et al. 2003; Lee et al. 2003; Mohamed et al. 2003; Cardoso et al. 2003; Fellah et al. 2004; Hosokawa, 2005; Wear et al. 2005; Lee and Yoon 2006; Hughes et al. 2007; Pakula et al. 2008; Fellah et al. 2008; Sebaa et al. 2008; Cardoso et al., 2008; Aygun et al., 2009; Cowin and Cardoso, 2010; Buchanan et al., 2011; Cardoso and Cowin, 2011). The parameters for theoretical predictions were fluid (water) density = 1 g/cm^3 , fluid viscosity = $0.01 \text{ g/cm} \cdot \text{s}$, bulk modulus of fluid = 2.2 GPa, density of solid phase = 1.8 g/cm^3 , Young's modulus of the solid phase (E_s) = 13 GPa or8.3GPa, Poisson's ratio of solid phase = 0.32, Poisson's ratio of trabecular frame = 0.23. The values for the exponent m, where the Young's modulus of the skeletal frame $E_b = E_s$ $(BV/TV)^{m}$, were m = 2.14 (for E_s = 13 GPa) or m = 1.75 (for E_s = 8.3 GPa) (Wear *et al.*, 2005; Pakula et al, 2008).



Measurements of backscatter coefficient plotted vs. BV/TV for the 29 bone samples. A power law fit to the data is also shown. The dotted lines show the power law fit plus or minus one standard error.

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Means for absolute values of correlation coefficients for ultrasound parameters versus BMD and microarchitectural features from the present study and seven others (Nicholson *et al.*, 1998;Trebacz and Natali, 1999;Nicholson *et al.*, 2001;Chaffai *et al.*, 2002;Hakulinen *et al.*, 2006;Padilla *et al.*, 2008;Karjalainen *et al.*, 2009). Error bars denote standard deviations.

Table 1.

Means, standard deviations, minima and maxima of ultrasound parameters density parameters and architectural parameters.

	Mean	Std.Dev.	Min	Max
Ultrasound parameters:				
nBUA (dB/cmMHz)	10.45	4.60	2.47	19.39
Signal velocity (m/s)	1543	40	1476	1615
Phase velocity (m/s)	1518	30	1472	1575
Backscat. Coef. (1/cmSr)	0.0219	0.0166	0.0012	0.0793
Density:				
BMD (g/cc)	0.122	0.056	0.002	0.201
Architectural parameters:				
BV/TV	0.086	0.031	0.019	0.151
BS/BV (1/mm)	22.0	3.1	16.2	30.2
Tb.Th (micron)	126	17	99	168
Tb.N (1/mm)	0.99	0.16	0.69	1.29
Tb.Sp (mm)	1.00	0.17	0.74	1.41
SMI	2.34	0.45	1.57	3.64
Connectivity (1/mm3)	3.74	1.26	1.50	6.99
DA	1.65	0.11	1.42	1.91
H1 (mm)	0.90	0.19	0.62	1.34
H2 (mm)	1.47	0.33	1.04	2.44
H3 (mm)	1.02	0.23	0.71	1.75

Table 2.

Pearson's correlation coefficients between BMD and architectural parameters. n: nonsignificant, a: p < 0.05, b: p < 0.01, c: p < 0.001, d: p < 0.0001.

	BMD	BV/TV	BS/BV	Tb.Th	Tb.N	Tb.Sp	SMI	Conn	DA	H1	H2	Н3	
BMD	1.00d	0.78d	-0.56b	0.32n	0.12n	-0.19n	-0.74d	0.44a	0.29n	-0.71d	-0.57b	-0.64c	BMD
BV/TV		1.00d	-0.68d	0.49b	0.13n	-0.18n	-0.75d	0.41a	0.38a	-0.67d	-0.52b	-0.63c	BV/TV
BS/BV			1.00d	-0.91d	0.41a	-0.35n	0.73d	0.18n	-0.61c	0.17n	-0.04n	0.14n	BS/BV
Tb.Th				1.00d	-0.35n	0.30n	-0.46a	-0.32n	0.58c	0.00n	0.19n	-0.02n	Tb.Th
Tb.N					1.00d	-0.98d	0.24n	0.78d	-0.25n	-0.65c	-0.71d	-0.64c	Tb.N
Tb.Sp						1.00d	-0.22n	-0.75d	0.20n	0.69d	0.74d	0.65c	Tb.Sp
SMI							1.00d	-0.18n	-0.45a	0.48b	0.30n	0.43a	SMI
Conn								1.00d	-0.17n	-0.84d	-0.85d	-0.81d	Conn
DA									1.00d	-0.03n	0.29n	0.04n	DA
H1										1.00d	0.94d	0.89d	H1
H2											1.00d	0.87d	H2
H3												1.00d	H3

Table 3.

Pearson's correlation coefficients between ultrasound parameters and BMD and architectural parameters. n: nonsignificant, a: p < 0.05, b: p < 0.01, c: p < 0.001, d: p < 0.0001.

	BMD	BV/TV	BS/BV	Tb.Th	Tb.N	Tb.Sp	SMI	Conn	DA	H1	H2	Н3
nBUA	0.80d	0.85d	-0.60c	0.50b	0.16n	-0.22n	-0.68d	0.37a	0.41a	-0.64c	-0.48b	-0.60c
Sig Velocity	0.90d	0.77d	-0.47a	0.30n	0.19n	-0.25n	-0.61c	0.43a	0.20n	-0.65c	-0.55b	-0.60c
PhaseVelocity	0.86d	0.81d	-0.45a	0.27n	0.21n	-0.26n	-0.63c	0.46a	0.23n	-0.65c	-0.54b	-0.61c
Backscat Coef	0.75d	0.84d	-0.75d	0.62c	-0.16n	0.14n	-0.83d	0.11n	0.60c	-0.47b	-0.27n	-0.38a

Table 4.

Linear regression models for ultrasound parameters. The third column is the square of the adjusted correlation coefficient of the regression. The fourth column is the increase in the square of the adjusted correlation coefficient compared to a univariate regression based on BMD as the independent variable.

Dependent Variable	Independent Variables	r _{adj} ²	r_{adj}^{2}
nBUA	BMD	0.63	
	BV/TV	0.70	
	BMD, BV/TV	0.75	0.12
	BMD, BV/TV, Tb.Th	0.76	0.13
	BMD, BV/TV, Tb.Th, BS/BV	0.82	0.19
	BMD, BV/TV, Tb.Th, BS/BV, Tb.N	0.83	0.20
Phase Velocity	BMD	0.73	
	BV/TV	0.64	
	BMD, BV/TV	0.77	0.04
	BMD, BV/TV, BS/BV	0.79	0.06
Signal Velocity	BMD	0.81	
	BV/TV	0.59	
	BMD, BV/TV, BS/BV, Tb.Th	0.84	0.03
Backscatter Coef.	BMD	0.54	
	BV/TV	0.69	
	BMD, BV/TV, Tb.Th	0.73	0.19
	BV/TV, Tb.Th	0.74	

Table 5.

Univariate correlation coefficients between ultrasound parameters and indexes of bone quantity in human calcaneus *in vitro* for three studies: 1. Nicholson *et al.* (2001), 2. Chaffai *et al.* (2002), and 3. the present study. 95% confidence intervals for the present study are shown in parentheses.

nBUA vs. BV/TV	0.86 ¹ ,	0.88 ² ,	$0.85 (0.69 - 0.93)^3$
nBUA vs. BMD	-	0.84 ² ,	$0.80\ (0.61 - 0.91)^3$
phase velocity vs. BV/TV	0.86 ¹ ,	0.90 ² ,	$0.81\;(0.62-0.91)^3$
phase velocity vs. BMD	-	0.90 ² ,	$0.86\ (0.71 - 0.93)^3$
signal velocity vs. BV/TV	0.88 ¹ ,	-	$0.77 \ (0.55 - 0.89)^3$
signal velocity vs. BMD	-	-	$0.90 \ (0.80 - 0.95)^3$
backscatter coefficient vs. BV/TV	-	0.91 ² ,	$0.84 \ (0.68 - 0.92)^3$
backscatter coefficient vs. BMD	-	0.89 ² ,	$0.75 \ (0.52 - 0.88)^3$

Table 6.

Means, standard deviations and numbers of reported values for correlation coefficients between ultrasound parameters, BMD, and microarchitectural features from the present paper and seven other papers (Nicholson *et al.*, 1998;Trebacz and Natali, 1999;Nicholson *et al.*, 2001;Chaffai *et al.*, 2002;Hakulinen *et al.*, 2006;Padilla *et al.*, 2008;Karjalainen *et al.*, 2009).

Means	BMD	BV/TV	BS/BV	Tb.Th	Tb.N	Tb.Sp	DA	SMI
Attenuation	0.83	0.83	-0.68	0.63	0.59	-0.55	0.30	-0.74
Velocity	0.85	0.80	-0.61	0.53	0.61	-0.57	0.12	-0.69
Backscatter	0.75	0.78	-0.69	0.58	0.41	-0.47	0.38	-0.69
Std. Dev.s								
Attenuation	0.04	0.12	0.11	0.16	0.25	0.24	0.13	0.08
Velocity	0.09	0.15	0.18	0.28	0.25	0.23	0.30	0.11
Backscatter	0.14	0.11	0.16	0.18	0.50	0.37	0.26	0.20
n								
Attenuation	5	6	4	6	5	5	3	2
Velocity	5	6	4	6	5	5	3	2
Backscatter	3	5	4	5	3	5	3	2