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## First In-Vivo Human Imaging at 10.5T: Imaging the Body at 447 MHz

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### Abstract

**Purpose**—To investigate the feasibility of imaging the human torso and to evaluate the performance of several RF management strategies at 10.5T.

**Methods**—Healthy volunteers were imaged on a 10.5T whole-body scanner in multiple target anatomies, including the prostate, hip, kidney, liver, and heart. Phase-only shimming and spoke pulses were used to demonstrate their performance in managing the  $B_1^+$  inhomogeneity present at 447 MHz. The imaging protocols included both qualitative and quantitative acquisitions to show the feasibility of imaging with different contrasts.

**Results**—High-quality images were acquired and demonstrated excellent overall contrast and SNR. The experimental results matched well with predictions and suggested good translational capabilities of the RF management strategies previously developed at 7T. Phase-only shimming provided increased efficiency but showed pronounced limitations in homogeneity demonstrating the need for the increased degrees of freedom made possible through single-spoke and multi-spoke RF pulse design.

**Conclusion**—The first in-vivo human imaging was successfully performed at 10.5T using previously developed RF management strategies. Further improvement in the RF coils, transmit chain, and full integration of parallel transmit functionality are needed to fully realize the benefits of 10.5T.

### Keywords

10.5T; Body Imaging; Parallel Transmit; Ultra-High Field Imaging; Magnetic Resonance Imaging

## INTRODUCTION

Since the introduction of the first 7T whole-body human MRI (1)(2), the last two decades have seen a significant increase in utilization of ultra-high field (UHF) scanners in human research, eventually paving the way to the recent approval of 7T for clinical use. However,

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the enthusiasm for increasing field strengths continues beyond 7T. Before the arrival of the 10.5T whole-body scanner at the University of Minnesota, several systems greater than 7T have effectively demonstrated improved human imaging and spectroscopy (2–6). While the majority of 7T work has focused on applications in the head, the feasibility and advantages of musculoskeletal and torso imaging at UHF have also been demonstrated (7,8). Although UHF imaging is generally challenging, the motivation is driven primarily by the observation that the sensitivity of MRI increases with field strength (1,9). Sensitivity gains can potentially contribute to higher spatial resolution providing richer anatomical and functional detail or contribute to improved acquisition efficiency in cases where signal averaging is required, especially with the low sensitivity of non-proton nuclei. Additional and significant advantages of UHF also include increased parallel imaging performance (10,11), spectral dispersion (12) and quantification (13), and greatly improved contrast to noise ratios in susceptibility weighted anatomical imaging (13–16) and in functional mapping of the brain (17). Many of these advantages promise to provide new insights into biological structure and function as well as to increase the sensitivity and resolution of biomarkers for accessing metabolic information in the brain and body.

Harnessing the power of UHF, however, has not been straightforward, involving a combination of RF hardware, RF management, and methodological developments. Since its introduction, a major challenge of UHF imaging is the transmit  $B_1$  ( $B_1^+$ ) inhomogeneities observed as signal non-uniformities due to the shorter RF wavelengths in tissues resulting in destructive interference patterns (1,18–20). This problem can be ameliorated or corrected using parallel transmit instrumentation (18,21) together with various strategies such as  $B_1^+$  phase and/or amplitude shimming (18,22–24), transmit SENSE (e.g., (25–28)), spoke pulses (e.g., (24,29–32)), k-T pulses (33), etc., to generate uniform flip angles over a targeted region.

The aforementioned concepts for dealing with  $B_1^+$  inhomogeneities are widely adopted in both brain and body imaging at 7T. However, with an even shorter within-tissue wavelength of approximately 7cm at 10.5T, it was unclear how well the RF management methods previously developed at 7T would mitigate the field strength-dependent challenges at 10.5T, especially in the human torso.

Another critical concern at UHF is local RF heating as a result of higher peak local specific absorption rates (SAR) and reduced SAR efficiency,  $B_1^+/(SAR)^{0.5}$ . To safely manage the power delivered to the body, power limits derived from electromagnetic simulations validated by experimental studies are required (34). In combination, the tradeoff between the maximum achievable  $B_1^+$ , transmit homogeneity, and local SAR needs to be carefully considered as all three can compromise final image SNR and contrast. The sweet spot where a reasonable solution can be found for all three narrows with increasing field where optimizing for one characteristic can compromise the others.

Local transmitters close to the surface of the body have been the preferred approach for UHF imaging in the human torso. While in some recent cases these local transmit arrays have been paired with separate receive-only elements (35–38), many often still operate solely as transceiver arrays (39–42). In our previous work, we developed a 10-channel transceiver

dipole array (43) for 10.5T body imaging and reported simulation results and experimental data obtained with a human-torso sized phantom. This relatively simple RF torso array, where each element is heavily loaded by the body and far from its neighbors, was straightforward to validate and thus was approved for human imaging by the FDA prior to any RF coil designed for the head. Using this array, human imaging was possible as an additional component to an ongoing 10.5T safety study, allowing us to explore the feasibility and challenges of imaging the human torso at 447MHz. Therefore, although imaging human brain function and anatomy remains the primary motivation for the development of the 10.5T system, the body images shown in this work were from the first human studies performed at this field strength, with the very first acquisition targeting the prostate (Supporting Information Figure S1 *available online*).

In this preliminary investigation, we acquired data in five anatomies, including the prostate, hip, kidney, liver, and heart, to explore the target and field dependent characteristics of RF management strategies, the ability to implement standard target specific acquisitions, and to determine the extent to which expected contrasts could be obtained. With this work, we demonstrate the potential of 10.5T as a cutting edge, whole-body imaging system using current parallel transmit RF management methods with the overall goal of exploiting such extremely high field strengths to enhance biomedical research and discovery.

## METHODS

### MRI Scanner

MRI experiments were conducted on a whole-body 10.5T magnet (Agilent Technologies, Oxford, UK) and associated imaging system (Siemens Healthineers, Erlangen, Germany) following an IRB approved protocol with an FDA Investigational Device Exemption (IDE). This passively shielded magnet has a clear bore diameter of 88 cm, is 4.40 m in length and weighs 110 tons. The 4700 L of liquid helium is cooled to 2.3 K to maintain the superconductivity of the magnet conductor which is required to be < 3 K based on the manufacturer's specifications. The field homogeneity of the magnet is <0.07 ppm / 25 cm and can be adjusted by second and third order room temperature shims driven by 20 A amplifiers. The scanner is equipped with 32 receivers, a 16-channel "Step 2" parallel transmit (pTx) system with each channel driven by a 2 kW power amplifier (Stolberg HF-Technik AG, Stolberg, Germany), and a whole-body SC 72 gradient system (Siemens Healthineers, Erlangen, Germany) which can achieve a maximum amplitude of 70 mT/m and slew rate of 200 T/m/s. The patient accessible bore size with the covers in place is 60 cm in diameter.

The dipole array used in this study was interfaced to the scanner by means of a 16-channel interface box which facilitates transmit-receive switching and signal preamplification. To minimize vestibular effects when moving through the static magnetic field (44–47), the speed of the table was limited to 19 mm/s as compared to 38 mm/s typically used at 7T. After RF and B<sub>0</sub> calibration scans, eye tracking and cognitive tests were performed while RF shims and/or pTx pulses were calculated to make full use of the limited amount of time subjects spent at isocenter.

## Subject Recruitment

All volunteers who participated in this study provided written informed consent to participate in the FDA and IRB approved safety study. The primary objective of the study was to assess the effects of field exposure on vestibular, cognitive, and physiologic function. The safety data collected during the protocol will be reported separately. In vivo imaging was a secondary objective of the study and was not performed until the subject's second time in the scanner. On the day imaging was to be performed, subjects were in the scanner for 90 min of which approximately 60 min were used for imaging and the rest for safety specific measurements.

Exclusion criteria to 10.5T exposure and imaging were strictly enforced. Subjects were required to have no history of embedded metal, either through surgery or accidentally, while also being free from symptoms or specific diagnosis of vestibular or cognitive impairment. Experience as a subject in a 7T scan was also a requirement for participation in the 10.5T studies. For those subjects who had not previously experienced imaging at 7T, a 7T pre-scan was first conducted to acclimate individuals to scanner procedures and being in a research environment. For body (i.e. torso) imaging, a total of 20 subjects (14/6 males/females) were imaged, ranging in age from 21Y to 65Y ( $36.95 \pm 13.87$ ), in weight from 56.7 kg to 102.06 kg ( $75.11 \pm 13.37$ ) and in BMI from 19.53 kg/m<sup>2</sup> to 33.47 kg/m<sup>2</sup> ( $25.33 \pm 3.53$ ). The permitted size of subjects allowed in the 10.5T was restricted to the weights of the virtual human models employed for electromagnetic calculations of the RF coil with margins of  $\pm 25\%$ . This resulted in a continuous range of allowable weights from 43 to 120 kg.

## RF Field Management

**Static Phase-only RF Shimming (Phase Shimming)**—RF shimming with various cost functions was used to manage the tradeoff between efficiency and homogeneity in the imaged target anatomies. The calibration methods needed for static RF shimming included tools to measure the relative complex  $B_1^+$  from each transmit element of the transceiver array (19,48). This method uses a low flip angle approximation to allow the robust estimation of each transmit channel's spatially varying relative magnitude and phase (49,50). Using these calibration data, phase-only (50) as well as phase and magnitude (phase-magnitude) RF shimming (51) are possible. In the context of this study “phase shimming” will refer only to the phase-only optimization of RF while the phase-magnitude approaches will be addressed through the use of spoke pulses detailed below.

In all cases, phase shimming was performed within a region of interest (ROI) defined on anatomic images by the operator. Depending on the subject and anatomy of interest, optimal channel-dependent properties were determined using a cost function that maximized efficiency, maximized homogeneity, or optimized for a trade-off between the two. For the prostate, phase shimming performance was characterized by the  $B_1^+$  transmit efficiency defined as the ratio of the magnitude of the sum (MOS) to the sum of the magnitude (SOM) of the channel-dependent complex  $B_1^+$  fields acquired from the low flip angle calibration data. Inhomogeneity was measured by the coefficient of variation (CV) of the MOS of  $B_1^+$  within the ROI. All calculations were performed in MATLAB (The MathWorks, Inc.,

Natick, MA) using custom software. Calculated shims were written to a file and read into the transmit array interface on the scanner's host computer.

**Spoke Pulses**—As an alternative approach to phase shimming, spoke pulses were implemented in which both phases and magnitudes for each channel were designed to minimize transmit field inhomogeneity. While a single spoke pulse is essentially equivalent to a static phase and magnitude shim, the design process and implementation followed the same path as for multi-spoke pulses. Spoke pulses were designed to address field inhomogeneities in larger targets including the kidneys, heart, and liver. As previously described, magnitude least squares optimization (52) with Tikhonov regularization was used to balance between RF power and excitation fidelity. The regularization parameter was automatically determined based on the L-curve criterion using the `l_curve()` function from the MATLAB `regtools` package (53). Similar to previous predictions and experimental results at 7T, it was expected that pulses with higher numbers of spokes would provide increased degrees of freedom to better mitigate  $B_1^+$  inhomogeneity at 10.5T (54). The pulse design made use of the same rapidly acquired channel-wise complex  $B_1^+$  map estimates used for phase shimming along with  $B_0$  maps acquired with a standard multi-echo gradient echo acquisition (Supporting Information Tables S1 and S2 *available online*).

**Peak Achievable  $B_1^+$  in the Prostate**—The actual flip angle imaging method (AFI) (55) was used to measure  $B_1^+$  in the prostate and for estimating peak achievable  $B_1^+$  given the complete transmit chain. The maximum achievable  $B_1^+$  was calculated by rescaling the measured  $B_1^+$  by the maximum transmitter voltage available on the scanner. A linear regression was conducted to characterize the peak  $B_1^+$  empirically in the anterior-posterior dimension of the subjects. Direct measurements of  $B_1^+$  and estimates of peak achievable  $B_1^+$  were performed in the prostate due to the limited motion present in this anatomical target.

### Coil Validation & Establishing Safe Operating Limits

The RF transmit array (coil) used in this study consisted of a previously detailed 10-channel dipole antenna array (43). Prior to in vivo imaging, the coil went through a validation procedure similar to previously published strategies (34). First, electromagnetic (EM) simulations and experimental studies in phantoms were used to demonstrate consistency between the two with respect to magnetic and electric fields. Briefly, for comparison with simulation, experimental  $B_1^+$  maps were acquired with AFI and local SAR values were calculated from fiber optic probe measurements during separate heating studies. Second, to determine safe operating power limits, electromagnetic simulations were performed in the Ella, Duke, and Fats29 virtual family human body models (Sim4Life, Zurich Medtech, Zurich, Switzerland) with the coil appropriately positioned to separately target the heart, mid-torso (kidney and liver), and pelvis (hips, prostate, or uterus) of each model. Using the channel-wise EM-field simulations, phase shimming solutions were determined in each target anatomy across all human body models. For each model and target location, local SAR values averaged over 10 g of tissue ( $SAR_{10g}$ ) were determined for the static phase-only shim solutions from efficiency to homogeneity. The peak  $SAR_{10g}$  value from all models and targets was 0.59 W/kg arising from a total input power of 1 Watt, resulting in a global phase shimming limit of 34 W total power (i.e. 3.4 W per channel) based on the IEC guidelines for

peak local SAR in the torso (i.e. 20 W/kg) (56). In practice, an effective total power limit of 17 W (i.e. 1.7 W per channel) was used, providing a safety factor of 2. This value was deemed to be conservative for initial in vivo studies at 10.5T realizing that the human body model sizes and shapes (57) as well as target size and location (58) impact local SAR estimates.

For spoke-pulses, both single- and two-spoke solutions were determined in each target anatomy across all human body models using the methods detailed above. For the single- and two-spoke solutions, the peak local SAR<sub>10g</sub> values for a total input power of 1 Watt across all models and targets were 0.90 W/kg and 1.1 W/kg, respectively. Using the same total power limit of 17 W, spoke excitation was performed with a safety factor >2 for the kidney and >10 for the heart and liver due to the acquisition methods and parameters used for imaging (Supporting Information Table S2). In the kidney, >98% of the power deposition was the result of a fat suppression pre-pulse using a default phase shim solution. The spoke pulses delivered <2% of the total power in these acquisitions.

### Imaging Protocols

Due to different geometries and motion sensitivities, the resultant protocols for the imaged anatomies differed in terms of slice planning, matrix size and/or triggering strategy (acoustic for heart, respiratory for kidney) as detailed below.

**Prostate Imaging**—Prostate imaging was performed to investigate the performance of phase shimming at 10.5T. Due to its small size, central location in pelvis, and limited motion, high transmit efficiency and acceptable homogeneity were expected with this RF management approach. The prostate also allowed exploration of multiparametric and quantitative imaging including the acquisition of T<sub>2</sub>-weighted and diffusion contrasts typical of standard diagnostic protocols. A multi-slice static phase shimming was performed to optimize B<sub>1</sub><sup>+</sup> efficiency, followed by a combination of the following acquisitions in each subject: AFI B<sub>1</sub><sup>+</sup> mapping, T<sub>2</sub>W TSE for anatomy, T<sub>1</sub> mapping using an adiabatic inversion prepared single-shot Turbo-FLASH, T<sub>2</sub> mapping using a CPMG multi-echo spin-echo sequence, and diffusion weighted imaging. Detailed protocol parameters are provided in Supporting Information Table S1. Parametric maps for T<sub>1</sub>, T<sub>2</sub>, and ADC were calculated by using standard non-linear least squares fitting functions in MATLAB.

**Hip Imaging**—Hip imaging was performed with larger fields of view than the prostate with phase shimming focused on the cartilage and other soft tissue structures around the femoral head. Initial fat suppressed GRE images allowed the overall image uniformity and fat suppression across the pelvis to be assessed, while typical anatomy-specific acquisitions, including a merged multi-echo gradient echo (MEDIC) (59) and proton density weighted TSE (PD-TSE) acquisition, were performed to assess the ability to obtain clinically relevant contrasts. For phase shimming, bilateral hip imaging is more challenging than the prostate because the ROIs needed for optimization are larger and spatially separated. The acquisition details for the hip studies are included in Supporting Information Table S1.



**Kidney Imaging**—Kidney imaging included breath-hold, fat-suppressed sequences to visualize anatomy, as well as non-contrast inflow enhanced acquisitions to delineate vessels. Phase shimming in the kidneys is more challenging than in the hips. Despite the fact that both are bilateral structures, the kidneys are larger and more posteriorly positioned in the torso and experience respiratory related motion requiring a breath-hold calibration scan. When visualizing the renal arteries as well as the renal parenchyma, the RF optimization becomes even more complex as the region between the kidneys and the descending aorta also needs to be included (51). Phase shimming was performed on two different ROIs; one ROI including the renal arteries and one excluding the renal arteries. To address the posterior position of the kidneys, the use of single-spoke RF pulses was explored to improve transmit homogeneity and contrast uniformity in the kidneys and renal arteries. Acquisition methods used for this anatomy are provided in Supporting Information Table S2.

**Liver Imaging**—Liver imaging was performed to explore the limits of transmit homogeneity as it is the largest internal organ in the human body, excluding the interstitium. Phase shimming was compared against single- and two-spoke pulses with respect to  $B_1^+$  uniformity across the liver. This comparison was accomplished by applying the RF management strategies to low flip angle GRE acquisitions and comparing the images with corresponding predicted  $B_1^+$  profiles. Breath-holding was used to reduce respiratory motion artifacts in both the calibration and anatomic imaging experiments. Acquisition parameters are provided in Supporting Information Table S2.

**Cardiac Imaging**—Cardiac imaging included RF shimming and retrospectively gated GRE CINE imaging of four chamber and short axis views. Cardiac gating was made possible by a previously reported acoustic cardiac trigger (60). Calibration scans were acquired as a single cardiac phase during diastole within a single breath-hold. Phase shimming was compared against single-spoke pulses in a four-chamber CINE acquisition. Detailed acquisition parameters are provided in Supporting Information Table S2.

## RESULTS

### Prostate Imaging

The local phase shimming ROI was placed around the prostate on three axial slices that were evenly spaced covering the majority of the gland. The estimated  $B_1^+$  profile and efficiency maps before and after shimming along with the acquired low-flip angle GRE images are shown in Figure 1. By using efficiency or tradeoff shimming solutions, the average  $B_1^+$  efficiency increased from  $36.0 \pm 5.2\%$  prior to shimming to  $79.7 \pm 4.5\%$  in the 9 prostate subjects, while inhomogeneity decreased from an initial value of  $0.486 \pm 0.063$  to  $0.211 \pm 0.068$ , suggesting the effectiveness of using phase shimming to mitigate  $B_1^+$  inhomogeneity for this target. Both axial and coronal  $T_2W$  TSE images are shown in Figure 2 to demonstrate the image quality of clinically relevant acquisitions at 10.5T. As an example, a complete set of axial and coronal  $T_2W$  TSE images is shown in Supporting Information Figure S2. As part of a multi-parametric study, data were acquired in a subset of participants allowing for calculation of quantitative maps including  $T_1$ ,  $T_2$ , ADC, and high b-value DWI images (Figure 3). The mean  $T_1$  from 3 subjects was  $2603 \pm 189$  ms and the mean  $T_2$  and

ADC from the peripheral zone of 2 subjects were  $83.5 \pm 2.1$  ms and  $1792 \pm 105$  ( $10^{-6}$  mm<sup>2</sup>/s), respectively. The average  $B_1^+$  in the prostate across all subjects was  $10.2 \pm 1.9$   $\mu$ T, and the average CV was  $13.0 \pm 2.4\%$ . A linear regression analysis suggested that  $B_1^+$  decreases at a rate of approximately 0.82  $\mu$ T per cm in anterior-posterior (AP) distance across the pelvis with a maximum  $B_1^+$  of 13.0  $\mu$ T at an AP dimension of 16.5 cm.

### Hip Imaging

Unilateral and bilateral hip imaging were performed in one and two subjects, respectively. The local phase shimming ROIs were drawn by outlining the femoral head and associated cartilage in the coronal and axial planes with a negative ROI removing the bone thus leaving the signal from a thin rim of soft tissue for optimization (61). After phase shimming, the average  $B_1^+$  efficiency increased from  $47.8 \pm 5.8\%$  to  $66.1 \pm 7.2\%$  and the average  $B_1^+$  inhomogeneity decreased from  $0.697 \pm 0.130$  to  $0.503 \pm 0.162$ . The acquired images are shown in Figure 4 and demonstrate excellent lipid suppression throughout the pelvis, effective mitigation of  $B_1^+$  inhomogeneity in the ROIs, and the ability to visualize fine structures on the 0.7mm isotropic MEDIC images. Important tissue contrast was obtained on the PD weighted images allowing visualization of the labrum.

### Renal Imaging

Renal imaging studies were performed in 4 subjects. Shimming ROIs circumscribed each kidney on a set of three axial calibration slices acquired in a single breath hold. The shimming solution was calculated using an efficiency cost function. The average  $B_1^+$  efficiency increased from  $46.1 \pm 6.8\%$  to  $67.9 \pm 3.8\%$ , and the average  $B_1^+$  inhomogeneity decreased from  $0.494 \pm 0.008$  to  $0.360 \pm 0.011$ . For the vessel imaging acquisitions (4 cases), the ROIs for shimming covered the kidneys and the renal arteries, including the descending aorta (51). In total, the average  $B_1^+$  efficiency increased from  $45.4 \pm 5.8\%$  to  $61.5 \pm 3.1\%$ , and the average  $B_1^+$  inhomogeneity decreased from  $0.456 \pm 0.101$  to  $0.299 \pm 0.047$ . Inflow-enhanced GRE images were acquired and processed providing maximum intensity projection (MIP) images that demonstrated high inflow contrast and clear visualization of both the proximal and distal renal arteries (Figure 5). Single-spoke RF pulses were compared against the performance of phase shimming at mitigating  $B_1^+$  inhomogeneity. The single-spoke pulse optimized on the larger ROI provided the best depiction of the left and right renal arteries (Figure 6).

### Liver Imaging

Due to the limitation of coil positioning, only one subject was included in the liver study. The shimming ROIs were drawn on three evenly spaced axial slices acquired through the liver. Static phase-only shimming optimized for homogeneity resulted in increased  $B_1^+$  efficiency from 0.428 to 0.505 and decreased inhomogeneity from 0.436 to 0.287. Single-spoke and two-spoke pTx pulses were also designed using the same ROIs, and images were obtained to compare against those acquired with the phase shim solution. Simulated and experimental results demonstrated high concordance with greatly improved  $B_1^+$  homogeneity and contrast uniformity over the liver when taking advantage of the increased degrees of freedom afforded by the two-spoke pulse (Figure 7).



## Cardiac Imaging

Cardiac imaging was performed in one subject. Phase shimming was performed for short-axis and four-chamber views, yielding an average increase in  $B_1^+$  efficiency from  $0.383 \pm 0.019$  to  $0.712 \pm 0.063$ , while keeping almost the same level of inhomogeneity (before:  $0.376 \pm 0.047$  versus after:  $0.380 \pm 0.059$ ). The CINE images before and after phase shimming showed improved RF efficiency and a shift of the dark RF band to outside of the heart (Figure 8b). Compared with phase shimming, the single-spoke solution mitigated  $B_1^+$  inhomogeneity especially at the atrium and base of ventricle of the heart, as depicted in Figure 8e. The Bloch simulation also showed that the single-spoke solution reduced the inhomogeneity from 0.42 to 0.21 and increased the average flip angle by 27% for the same RF power, all suggesting the importance of incorporating pTx into field and power management.

## DISCUSSION

In this study, we performed the first in vivo human imaging at 10.5T (447MHz) with the goal of exploring the feasibility of obtaining images of multiple anatomical targets in the torso at this high magnetic field using the RF management strategies developed for 7 Tesla. The well-known difficulties arising from  $B_1^+$  inhomogeneities associated with decreasing RF wavelengths (19) make torso imaging at 10.5T particularly challenging. While previous simulations had indicated such imaging would be feasible in the human torso at 10.5T (43), there had not been an experimental confirmation to date. In addition, the simulations did not provide insights as to the obtainable image quality or tissue contrasts that could be expected at this extremely high field strength.

In these initial studies with the current RF coil and transmit chain configuration, phase shimming provided sufficient  $B_1^+$  peak performance and homogeneity to perform anatomic and quantitative imaging in the prostate. The small volume and the central position of the prostate in the pelvis enabled this relatively simple strategy, optimized primarily for transmit efficiency, to be successful in most cases. As the anatomical targets in the body increased in size and asymmetry, however, additional degrees of freedom were required, either through single-spoke or multi-spoke RF pulses, to obtain the desired homogeneity in signal and contrast. With increasing constraints on  $B_1^+$  homogeneity, transmit efficiency dropped to a point where it was difficult to obtain some desired contrasts due to the limited peak  $B_1^+$  or SAR efficiency. This fact highlights the need for improved RF coil and transmit chain efficiency as well as further integration of more SAR efficient pTx pulses into standard acquisition strategies.

Despite the limitations with the current coil and phase shimming, quantitative imaging was successfully performed in the prostate. While the  $T_2$  values appear to be in a reasonable range for 10.5T, the reported  $T_1$  values appear longer than expected compared with the limited studies done at 7T (62). ADC values, which should be independent of field strength, also appear to be larger than expected compared to quantitative studies reported at 3T (63). However, for all parameters, the acquisition, subject, and field dependent variability cannot be adequately assessed until more extensive targeted evaluations are performed.

In almost all the studies, RF optimization was conducted immediately following scout acquisitions, serving as an initial  $B_1^+$  field calibration and reference before proceeding with additional acquisitions or the use of different RF management strategies. While phase shimming has limited degrees of freedom compared to other approaches, it remained a fast and effective solution for small ROIs such as the prostate and hips while generally proving capable for both qualitative and, in the prostate, quantitative imaging. Previously, we were able to obtain reasonable results for bilateral hip imaging at 7T (61) using phase shimming. The same approach also provided reasonable bilateral hip images at 10.5T; however, transmit efficiency in the prostate at 10.5T was down to 62% from approximately 80% at 7T. Decreasing transmit efficiency also resulted in decreased SAR efficiency, which, along with a limited peak  $B_1^+$ , made it difficult to obtain some standard contrasts in the hip such as bright fluid signals that are typically provided by dual-echo steady-state type sequences (i.e. DESS) (61). An important point, however, is that clinical imaging of the hip at 3T is usually performed unilaterally, a strategy that would make RF optimization at 10.5T more straightforward.

The limitations of phase shimming were not surprising in larger anatomies such as the liver, heart, and kidney. For these targets, phase-only solutions failed to provide sufficient  $B_1^+$  for the entire ROI. One could in fact observe the limitation from the post-shimming  $B_1^+$  efficiency maps (Figure 1), where phase-only solutions yielded only a narrow band with high efficiency sufficient for the prostate. These limitations can be addressed by using single-spoke or multi-spoke pTx pulses. However, at the present time very few imaging sequences are currently enabled to take advantage of multi-spoke pulses. It is worth noting that the in vivo imaging results were consistent with predictions where the excitation fidelity of a two-spoke pTx pulse greatly improved upon the solution of a single-spoke pulse. These observations suggest that the increased  $B_1^+$  inhomogeneity at 10.5T is predictable and manageable, and that the previously developed methods for imaging at 7T show reasonable translational potential for enabling torso imaging at 10.5T.

With increasing field strength, the compromise between transmit efficiency, SAR efficiency, and transmit homogeneity becomes an increasing limitation for certain acquisitions. These constraints can be tackled through improved transmit chain and RF coil performance and/or through better pTx RF management strategies. For example, the low peak  $B_1^+$  is generally not a major limiting factor for small flip angle imaging. However, it may significantly affect the performance of refocusing and inversion pulses, and, consequently, the image contrast and SNR as observed in the two example TSE imaging series acquired in the prostate (Supporting Information Figure S3). Previous work has shown the feasibility of designing a tailored refocusing or inversion pulse using pTx (64,65) and achieving finer adjustment of  $B_1^+$  inhomogeneity and RF peak and average power in the presence of local or global SAR constraints (66–69). At 10.5T, the use of such tailored pTx pulses is imperative and should be an available alternative to conventional pulses when the latter may not be feasible due to the known limitations of static phase shimming. To design and effectively implement pulses with SAR constraints requires confidence in the simulations used to estimate those values. Typically, virtual observation points (VOPs) are employed to help reduce the computational burden for such calculations (70). Similarly, on the scanner, VOPs and real-time power monitoring hardware can also be implemented to further extend acquisition flexibility.

Developing the confidence in human body models that allows for taking advantage of local SAR control will be critical to fully exploit the pTx system capabilities at UHF and becomes even more imperative at 10.5T.

Besides the static phase shimming and pTx tailored pulses, there are other techniques that may be useful to mitigate  $B_1^+$  inhomogeneity at 10.5T, such as TIAMO (71) and PnP-MR fingerprinting (72). By treating complementary  $B_1^+$  profiles as virtual receive channels, TIAMO uses a GRAPPA reconstruction to yield more homogeneous images at little cost to SNR and SAR (71). The phase configurations used by TIAMO can be predefined empirically. Although less suitable for quantitative imaging, TIAMO may still serve as a calibration-free alternative when static RF shimming is insufficient for imaging large organs such as the liver, and for fast  $B_1^+$  estimation (73). For quantitative imaging, especially T2 mapping at 10.5T, alternative parametric mapping methods such as PnP-MR fingerprinting may be less power demanding as the T2 contrast comes from both the spin echo and stimulated echo pathways and does not require a perfect 180 degree refocusing pulse, although prospective studies are needed to validate quantification accuracy.

While this preliminary study demonstrates the feasibility of obtaining high quality images of the human torso using current RF management methods at 10.5T, quantitative comparisons against 7T are warranted. Such comparisons will require additional attention to the equivalency of the receive chain architecture, including the RF coil. By developing transceiver arrays with higher numbers of transmit channels for 10.5T using dipoles or other relevant resonant structures, increases in peak  $B_1^+$  and SNR are expected (74). For particular torso targets, such coil developments may also be sufficient to minimize the current limitations observed at 10.5T by providing competitive SNR performance compared to RF coils used at 7T. In the case of the prostate, it may be possible to achieve SNRs with the use of a body coil alone at 10.5T that approaches that of 7T studies acquired with an endorectal coil (75–77). Note that high resolution imaging enabled by SNR increases is often accompanied by longer acquisition times and possibly higher power deposition due to the image orientations needed to reduce motion artifacts and the requirement to encode all spins in the slice/volume of excitation. However, the more complex  $B_1^+$  pattern at higher fields improves the spatial encoding capability, which, together with the SNR gain, can improve the parallel imaging performance, leading to a reduction in acquisition time. On the transmit side, the acquisition time may also be reduced by employing reduced field of view excitations, where only spins within regions of interest are excited and spatially encoded by using parallel transmission and multi-dimensional selective pulses (78–80). This may be especially useful for body applications where target anatomies are small compared to the full extent of the body in the plane of the imaging slice.

In the absence of a direct experimental comparison with 7T, the results presented here can be put into context by comparing against previously published work. The manuscript introducing the presently used coil involved simulations with a similar 10 channel dipole array optimized for 7T (43). In that work, phase shimming and spoke pulse designs were used to assess the relative performance between the two field strengths. With respect to the phase only simulations in the prostate, 10.5T simulations predicted slightly higher power efficiency ( $\mu\text{T}/\text{W}^{0.5}$ ) and SAR efficiency but with higher inhomogeneity with CVs more than

doubled at 10.5T. Experimentally these simulation results are partially corroborated by comparing the current 10.5T with previous results obtained with a 10 channel dipole array at 7T where the CV at 7T was half that of 10.5T in the prostate (i.e. 7% at 7T and 13% at 10.5T) (39). With respect to spoke pulses, simulation showed that for the same anatomical target and number of spokes, peak local SAR increased by 25–35% for prostate, 60–80% for kidneys, and 50–90% for heart with comparable excitation fidelity at 10.5T. However, for the kidneys and heart, designing two-spoke pulses at 10.5T appeared to yield similar performance to single-spoke designs at 7T. For prostate, designing two-spoke pulses at 10.5T started to outperform the single-spoke design at 7T. Verification of these previous simulations and other quantitative field strength comparisons will need to be performed in future target specific studies.

Despite showing the effectiveness of RF management strategies at 10.5T, this study had several limitations. First, to adhere to the time limit allowed by the FDA approved protocol, the actual scanning lasted no more than one hour, restricting the time usable for high-quality acquisitions. Second, due to the limited extent of the RF coil in the foot-head direction and the fact the study protocol did not permit repositioning the coil, targets including the liver and the heart may have been imaged with sub-optimal coil coverage resulting in degraded imaging performance in the superior or inferior aspects of the anatomy. Third, at the time of this study, the pTx functionality required off-line RF shimming and pulse calculations and associated troubleshooting thus lowering the acquisition efficiency during the limited time allotted for imaging. Streamlining pTx functionality in the software system will be critical to promoting pTx in future prospective studies.

## CONCLUSION

In this study, we present the first ever in vivo human imaging studies at 10.5T (447MHz). Previously developed RF management strategies for imaging at 7T, including phase-only RF shimming and pTx spoke pulses, have been shown to be effective at tackling the  $B_1^+$  inhomogeneity at 10.5T, allowing high quality images to be acquired in multiple target anatomies throughout the human torso. It is evident, however, that further development and integration of pTx functionality, such as target specific RF pulses, are needed to achieve more uniform transmit  $B_1$  fields while optimizing for SAR efficiency since both peak  $B_1^+$  and local SAR were factors limiting the demonstrated applications. When combined with further improvements in the transmit chain efficiency, antenna technology, and local SAR monitoring, proton applications in the human torso at 10.5T are expected to confirm the unique advantages that the increase in field strength can provide.

## Supplementary Material

Refer to Web version on PubMed Central for supplementary material.

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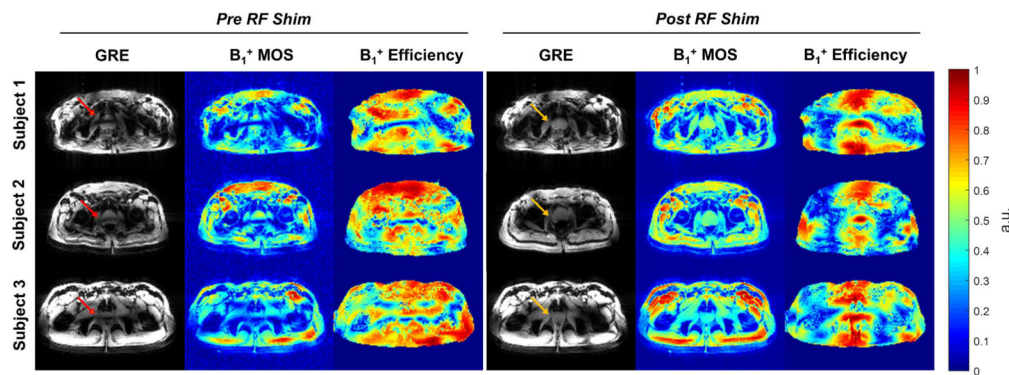
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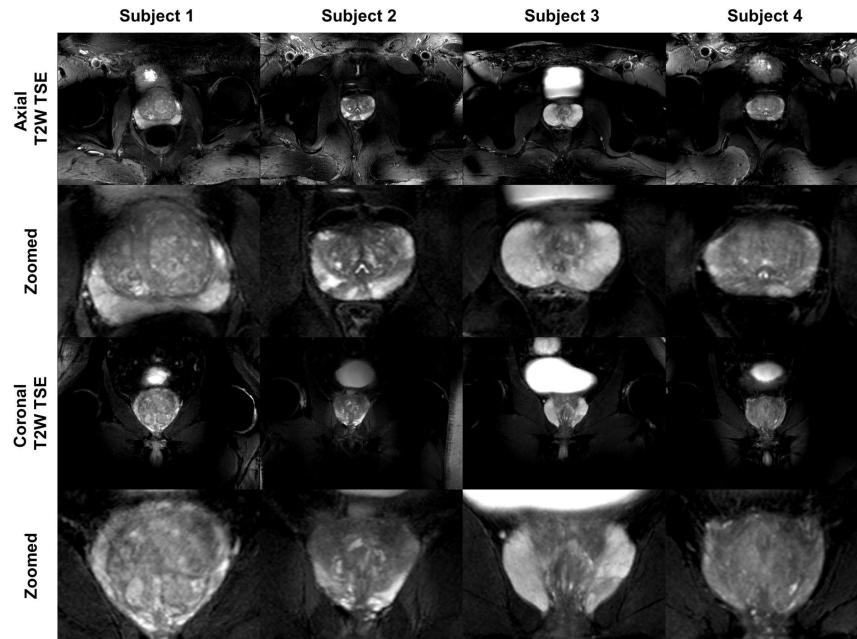
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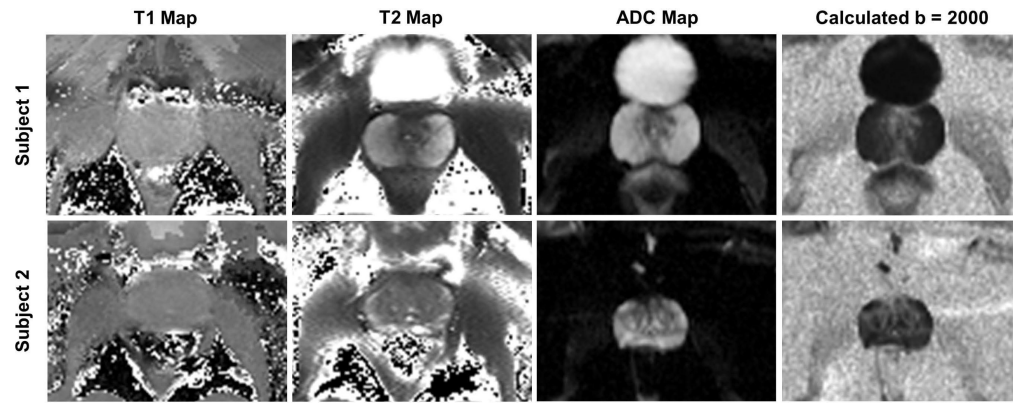


**Figure 1.**

The acquired low-flip angle GRE images and the simulated  $B_1^+$  spatial profiles and efficiency maps in the prostates of three subjects before and after phase-only RF shimming. The simulated  $B_1^+$  MOS images matched closely with acquired images in terms of the spatially varying  $B_1^+$  (note that the acquired images include receive profile information). The  $B_1^+$  efficiency and homogeneity were improved in the prostate after RF shimming (yellow arrows) compared to the pre-shimming results (red arrows). Note that the simulated  $B_1^+$  MOS image is proton density weighted and that the  $B_1^+$  efficiency maps are masked to exclude the background noise.



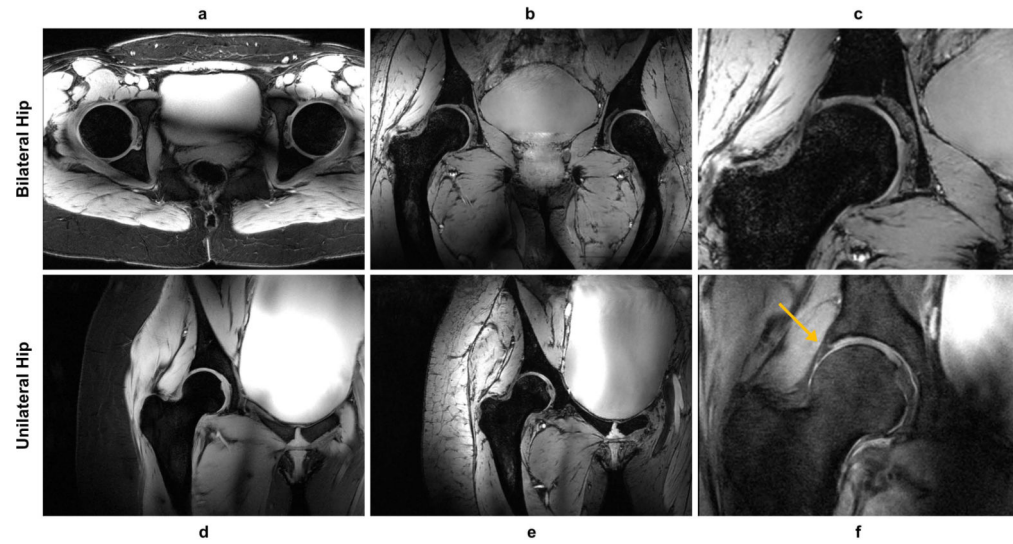
**Figure 2.** Full field of view and zoomed in versions of axial and coronal T<sub>2</sub>W TSE images of prostates from four subjects. The images demonstrate excellent contrast and SNR achieved by phase-only RF shimming. While providing high peak B<sub>1</sub><sup>+</sup> and reasonable homogeneity over the prostate, the local RF shim resulted in unmanaged RF fields outside the immediate region of the targeted anatomy that caused spatially varying destructive interference patterns as observed in the un-zoomed images.



**Figure 3.**

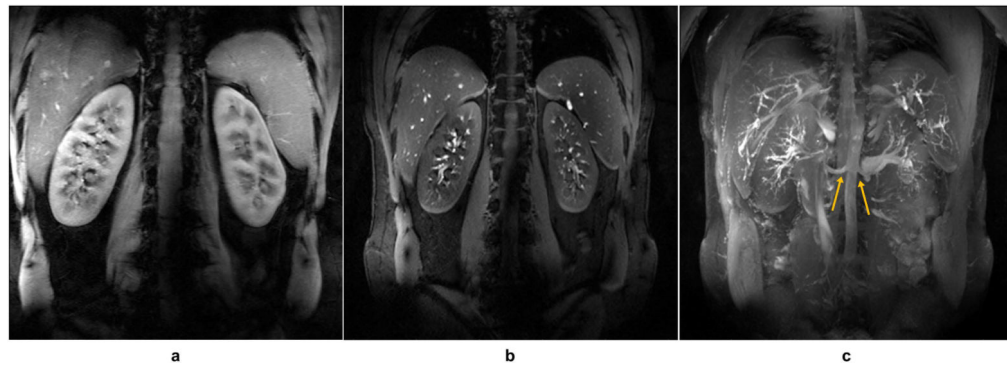
Zoomed-in parametric maps of the prostate including  $T_1$ ,  $T_2$ , ADC, and calculated high b-value DWI ( $b = 2000$ ) generated from IR-FLASH, multi-echo spin echo (SEMC) and SE-EPI DWI acquisitions. This study demonstrates the feasibility of performing quantitative imaging at 10.5T and imaging with diagnostically relevant sequences for this anatomy.





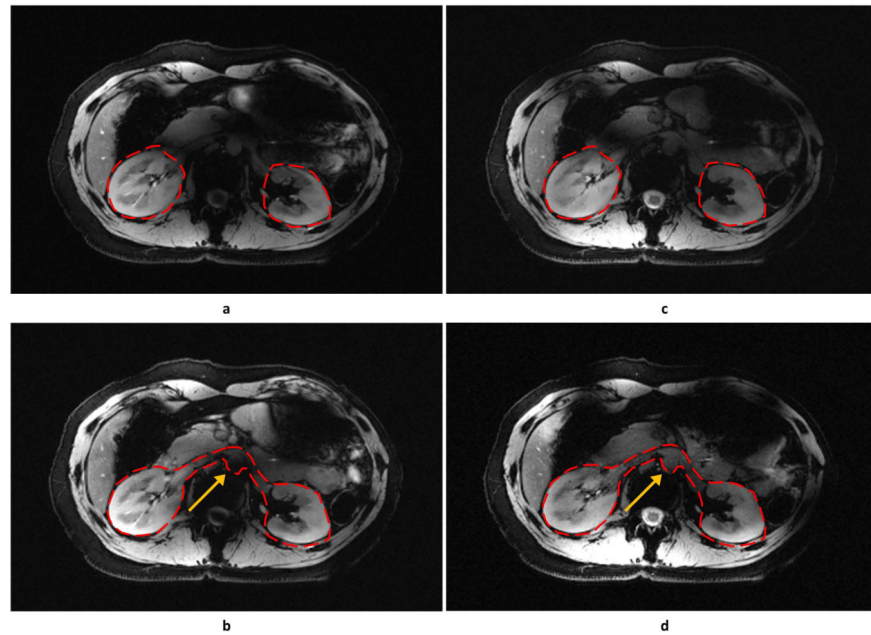
**Figure 4.**

Examples of hip images acquired with different contrasts. For the bilateral hip, 2D axial GRE (a), 3D coronal MEDIC (b), and a zoomed version of the MEDIC acquisition (c) are shown. For the unilateral hip, 2D coronal GRE (d), 3D coronal MEDIC (e), and PD weighted TSE (f) images are shown with the latter showing the expected contrast between the labrum and cartilage (yellow arrow). (a), (d), (f) were acquired with lipid suppression and demonstrated excellent performance and contrast.

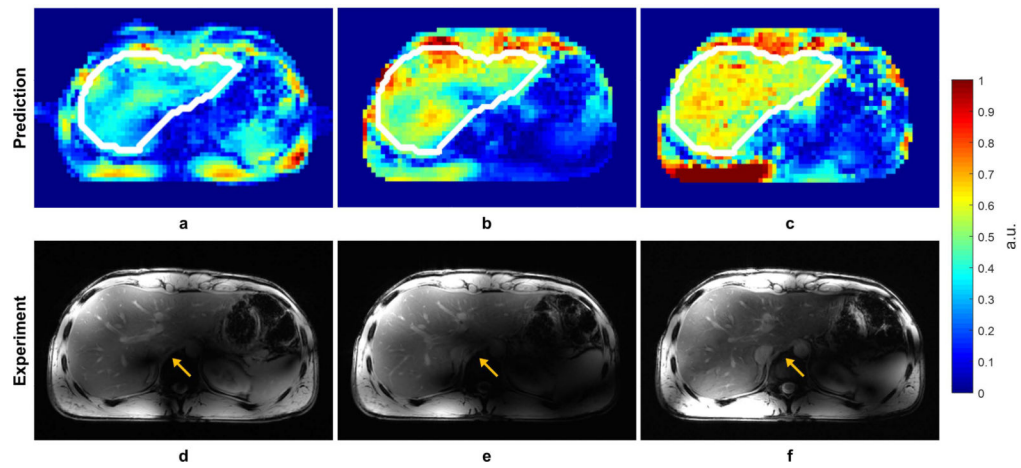


**Figure 5.**

Example of breath-hold renal images acquired with lipid suppression including a 2D coronal anatomic GRE (a) and an inflow-enhanced acquisition (b). (c) Maximum intensity projection (MIP) across the stack of images represented in (b) demonstrates the high inflow-enhancement and background suppression afforded by the increased T1 of tissues and blood at 10.5T. After phase-only shimming, a relatively uniform signal intensity was achieved in the oblique coronal plane over which these images were acquired. The origins of renal arteries are well visualized on the MIP image (yellow arrows), while distal arterial branches can also be appreciated.

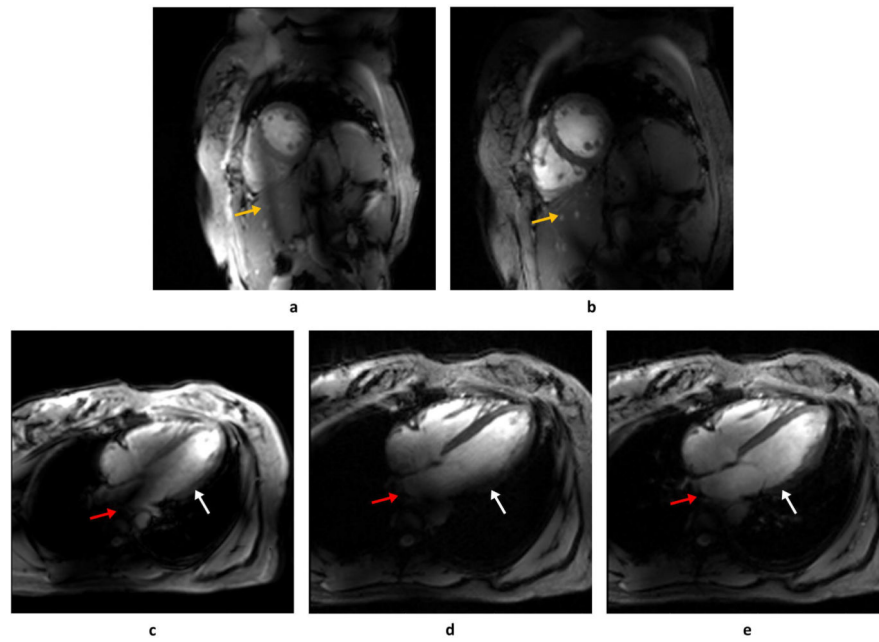


**Figure 6.** Example of fat-saturated, breath-hold 2D axial GRE images of the kidney using different RF management strategies. Shimming ROIs are illustrated by red dashed lines. Static phase-only RF shimming was used in (a) and (b) while single-spoke pTx pulses were used in (c) and (d). Compared with phase-only shimming in the smaller ROI (a), the single-spoke pTx pulse (c) showed similar performance in mitigating  $B_1^+$  inhomogeneity. For the larger ROI, the single-spoke pTx pulse (d) was more effective than the phase-only solution (b) against  $B_1^+$  inhomogeneity as indicated by the yellow arrows.



**Figure 7.**

Predicted  $B_1^+$  profiles (a, b, c) and acquired low-flip angle GRE images (d, e, f) in the liver with different RF management strategies: static phase-only RF shimming with a homogeneity cost function (a, d); single-spoke pTx pulse (b, e); two-spoke pTx pulse (e, f). The acquired images matched well with prediction in terms of predicted  $B_1^+$  profiles. The two-spoke pTx pulse effectively mitigated the  $B_1^+$  inhomogeneity in the liver as demonstrated by improved consistency in contrast throughout the organ (yellow arrows). Note: the experimental data is weighted by the receive profile of the 10-channel dipole array.



**Figure 8.**

A single frame during diastole of the cardiac CINE acquisitions in the short-axis (a, b) and four-chamber (c, d, e) views. Images acquired before phase-only RF shimming (a, c) are contrasted with those with phase-only static RF shims (b, d). In the 4-chamber view a single-spoke pTx pulse was also implemented (e). In the short-axis view, phase-only shimming improved the myocardium-blood pool contrast and shifted a band of low  $B_1^+$  outside of the heart (yellow arrows in a, b). However, in the four-chamber view, the phase-only shimming yielded persistent  $B_1^+$  inhomogeneities in the base of the left ventricle (white arrow) and atrium (red arrow) which were addressed with a single-spoke pTx pulse (e).