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Fabrication of Transparent UV-Cured Coatings with Allyl-Terminated Hyperbranched Polycarbosilanes and Thiol Silicone Resins

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INTRODUCTION

Ultraviolet (UV)-cured coatings possess numerous merits including low VOC, energy saving, and fast curing speed.^{1–3} However, many UV-cured materials suffer from relatively poor thermal stability⁴ and low hardness.^{5–7} Materials with poor thermal stability are liable to decompose at relatively low temperature.^{8,9} Additionally, the coatings with low pencil hardness are very easy to be scratched.^{5–7} Nowadays, many efforts have been made to overcome these shortcomings.

Many experiments have confirmed that hyperbranched polymers can reduce the VOC emission of UV-cured coatings for reduction in the content of the reactive diluent and solvent.^{2,12–15} In addition, the functional groups on the surface of hyperbranched polymers will increase the cross-linking density, which will benefit preparation of coatings with moderately high hardness.^{12–14} As hyperbranched polymers, hyperbranched polycarbosilanes have Si–C bonds contributing to the relative stability of the carbosilane because of less sensitivity to nucleophilic attack.¹⁵

UV-cured silicone coatings have been proven to possess spectacular performances such as good UV resistance and thermal stability, wide operating temperature, high transparency, and low humidity absorption.^{1,4,10,11} Thiol-ene reactions initiated by UV have been widely applied to develop silicone materials under mild reaction conditions due to their advantages including high effectivity, no photoinitiator required, relative tolerance to lots of functional moieties, no oxygen inhibition, and less by-products.^{16,17} Recently, a kind of transparent flexible silicone material with thermal decomposition temperatures about 340 °C has been produced by UV-initiated thiol-ene reaction from hyperbranched polycarbosilanes and thiol silicone resins.¹⁸ Inspired by this interesting work, a class of UV-cured transparent solvent-free coatings with pencil hardness of 4–9 H, initial thermal decomposition temperature higher than 236 °C, transmittance higher than 94%, and water absorption no more than 0.04 wt % were prepared.

RESULTS AND DISCUSSION

Effect of UV Curing Time. UV curing time has a significant impact as shown in Table 1. Even if the curing time is only 5 s, the curing degree is as high as 98.2%. The pencil hardness increases continuously from B to 8 H when the curing time increases from 5 to 30 s. If the curing time is longer than 30 s, it will have a less effect on the curing degree and pencil hardness, which is quite similar to the epoxymodified silicone coating reported previously.¹ The surface water contact angles are almost constant, $101.3-105.4^{\circ}$, and water absorption is no more than 0.04 wt %.

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Table 1. Effect of UV Curing Time⁴

entry	curing time/s	curing degree/%	pencil hardness	surface water contact angle/deg	water absorption/ wt %
1	5	98.2	В	101.3	0.04
2	10	98.8	2 H	103.4	0.02
3	15	98.5	3 H	104.2	0.01
4	20	98.8	5 H	104.3	0.02
5	30	99.6	8 H	105.3	0.01
6	40	99.6	8 H	104.6	0.03
7	50	99.7	8 H	104.8	0.02
8	60	99.7	8 H	105.4	0.04

^{*a*}Conditions: R/Si and thiol content of thiol silicone resin are 1.4 and 0.004 mol g^{-1} , respectively. The terminated hyperbranched polycarbosilane is G1. n(thiol):n(allyl) = 1.4:1.

The Effect of the Molar Ratio of Thiol to Allyl. The effect of the molar ratio of thiol to allyl (n(thiol):n(allyl)) is shown in Figure 1. It is obvious that the silicone coatings have



Figure 1. Effect of n(thiol):n(allyl) on the pencil hardness of the coatings. Conditions: R/Si of thiol silicone resin is 1.4. The hyperbranched polycarbosilane is G1. The coatings were all cured for 30 s.

a fairly high pencil hardness (6-8 H). When n(thiol):n(allyl)increases from 1.3:1 to 1.4:1, the pencil hardness reaches the highest for the highest cross-linking density of cured materials. The pencil hardness of the UV-cured epoxy-modified silicone resin coating reported by our group can reach 5 H,¹ while those of the UV-cured coatings reported by other groups are generally not higher than 4 $H^{2-4,12}$ As argued by previous works,^{12–14} the abundant functional groups on the surface of hyperbranched polymers will increase the cross-linking density, which will benefit preparation of coatings with moderately high hardness. Similarly, the much higher pencil hardness of the UV-cured coatings obtained might be contributed by plenty of allyls in the hyperbranched polycarbosilanes, which will react with the thiol group of the thiol silicone resin by UV-initiated thiol-ene reaction without an additional photoinitiator and increase the cross-linking density of the cured coatings. On the basis of these results, a conclusion might be drawn that the coatings have very high pencil hardness, which can be good candidates to overcome the problems such as scratches on the surface and marks produced during transportation or work.

The Effect of the R/Si Molar Ratio of Silicone Resin. The effect of R/Si molar ratios of thiol silicone resins is shown in Table 2. After being cured by UV for 30 s, curing degrees are higher than 99.0%, which implies that the coatings are

Table 2. Effect of R/Si Molar Ratios of Thiol Silicone ${\rm Resins}^a$

entry	R/Si molar ratio	curing degree/%	pencil hardness	surface water contact angle/deg	water absorption/ wt %
1	1.3	99.8	9 H	104.4	0.01
2	1.4	99.6	8 H	105.3	0.01
3	1.5	99.3	5 H	105.4	0.03
4	1.6	99.8	4 H	106.4	0.03

^{*a*}Conditions: the thiol content of thiol silicone resin is 0.004 mol g⁻¹. The terminated hyperbranched polycarbosilane is G1. n(thiol):n(all-yl) = 1.4:1. The coatings were cured for 30 s.

almost cured entirely. The pencil hardness of the coatings is fairly high (4-9 H). The pencil hardness decreases with the increment of the R/Si molar ratio, which may be because a relatively high R/Si molar ratio will result in a low cross-linking density. Though there is a small growth of the water absorption when the R/Si molar ratio is increased, the water absorption is still no more than 0.03 wt %.

The Effect of the Thiol Content of Silicone Resin. It is exhibited in Table 3 that thiol content of thiol silicone resins

Table 3. Influence of the Thiol Content of Thiol Silicone ${\rm Resin}^a$

thiol content/ mol g ⁻¹	curing degree/%	pencil hardness	surface water contact angle/ deg	water absorption/ wt %
0.002	97.5	5 H	105.5	0.01
0.003	99.3	6 H	105.4	0.01
0.004	99.6	8 H	105.3	0.01
0.005	98.1	8 H	104.6	0.02
0.006	98.7	8 H	104.9	0.02
	thiol content/ mol g ⁻¹ 0.002 0.003 0.004 0.005 0.006	thiol content/ mol g ⁻¹ curing degree/% 0.002 97.5 0.003 99.3 0.004 99.6 0.005 98.1 0.006 98.7	thiol content/ mol g ⁻¹ curing degree/% pencil hardness 0.002 97.5 5 H 0.003 99.3 6 H 0.004 99.6 8 H 0.005 98.1 8 H 0.006 98.7 8 H	thiol content/ mol g ⁻¹ curing degree/% pencil hardness surface water contact angle/ deg 0.002 97.5 5 H 105.5 0.003 99.3 6 H 105.4 0.004 99.6 8 H 105.3 0.005 98.1 8 H 104.6 0.006 98.7 8 H 104.9

^{*a*}Conditions: R/Si of thiol silicone resin is 1.4. The terminated hyperbranched polycarbosilane is G1. n(thiol):n(allyl) = 1.4:1. The coatings were cured for 30 s.

takes an important role. If the thiol content increases from 0.002 to 0.004 mol g⁻¹, the pencil hardness increases from 5 H to 8 H. A further increment of the thiol content has a less effect on the pencil hardness. The water absorption is still quite low, which is 0.01–0.02 wt %. The curing degree is 97.5–99.6%, and the surface water contact angle is about 105° (Table 3 and Figure S1), which denotes that the curing degree and surface water contact angle are less influenced by the thiol content.

The Effect of Generations of Hyperbranched Polycarbosilanes. The generations of allyl-terminated hyperbranched polycarbosilanes have a crucial impact on the pencil hardness of the coatings as shown in Table 4. As it can be seen, the pencil hardness of the coatings is in the order of G1 > G2 >G0 > G3. A relatively lower pencil hardness of coatings prepared from higher-generation hyperbranched polycarbosilanes with a bigger cross-linking network and the more defects of the molecular structure might be explained by the decrease of the cross-linking density and curing degree.^{19'} To verify the cross-linking density of these coatings, DSC of the coatings was carried out as shown in Figure S2. Obviously, the glass transition temperature (Tg) of the coatings is in the order of G1 > G2 > G0 > G3, which can actually prove that the coatings' cross-linking density is in the order of G1 > G2 > G0> G3.^{1,20,21} Generally speaking, the coating prepared with G1 exhibits optimum comprehensive performance. Highly trans-

Table 4. Influence of Generations of Hyperbranched Polycarbosilanes^a

entry	generation of hyperbranched polycarbosilanes	curing degree/%	pencil hardness	surface water contact angle/deg	water absorption/%
1	G0	99.6	4 H	104.8	0.02
2	G1	99.6	8 H	105.3	0.01
3	G2	89.7	5 H	105.5	0.01
4	G3	75.6	<6 B	95.1	0.01

^{*a*}Conditions: R/Si and thiol content of thiol silicone resin are 1.4 and 0.004 mol g^{-1} , respectively. n(thiol):n(allyl) = 1.4:1. The coatings were cured for 30 s.

parent materials can be applied to prepare or protect optical devices, $^{22-25}$ and new silicone materials with high transmittance have drawn much attention. It can be obviously seen from Figures 2 and 3 that the coatings have transmittance



Figure 2. Transmittance of the coatings prepared with G0, G1, G2, and G3. Conditions: R/Si and thiol content of thiol silicone resin are 1.4 and 0.004 mol g^{-1} , respectively. n(thiol):n(allyl) = 1.4:1. The coatings were cured for 30 s.

higher than 80% (400–800 nm). Especially, the transmittances of the coatings prepared with G1, G2, and G3 are higher than 94.0% at 800 nm.

The FT-IR spectra of the coatings prepared with G0, G1, G2, and G3, G1, and thiol silicone resin are given in Figure 4. As can be seen from the FT-IR spectra of the coatings cured for 30 s, the characteristic stretching vibration absorption peak of =C-H at 3074 cm⁻¹ and that of C=C in the allyl group at 1627 cm⁻¹ of allyl-terminated hyperbranched polycarbosilanes



Figure 3. Photos of coatings prepared with G0, G1, G2, and G3. G0, G1, G2, and G3 stand for the coatings prepared with G0, G1, G2, and G3, respectively.



Figure 4. FT-IR spectra of the silicone coatings prepared, G1, and the thiol silicone resin with R/Si and thiol content of 1.4 and 0.004 mol g^{-1} , respectively.

disappeared. The tiny characteristic absorption peak of thiol groups at about 2550 cm⁻¹ in the thiol silicone resin also vanished. The characteristic absorption peak of Si–O–Si at 1040 cm⁻¹ and stretching vibration absorption peak of Si– CH_3 at 2966 cm⁻¹ were obviously in existence. These results imply that the coatings can be cured perfectly for only 30 s.

As can be seen from the TGA curves of the coatings prepared with G0, G1, G2, and G3 shown in Figure 5a, the mass residues of these coatings at 800 °C under an atmosphere of N₂ are higher than 50 wt %. The starting thermal decomposition temperature (Td_5) of these coatings is higher than 236 °C; especially, Td_5 of the coating prepared with G1 is as high as 371.1 °C. The relatively lower Td_5 of the coatings



Figure 5. TGA (a) and DTG (b) curves of the coatings prepared with G0, G1, G2, and G3.

prepared with G3 may be attributed to the lowest curing degree. The coatings prepared in this work exhibit superior thermal stability to those UV-cured materials with Td_5 in the range of 189–273.5 °C reported previously.^{25,26}

According to the DTG curves of these coatings shown in Figure 5b, the temperatures at which the maximum degradation speed took place (T_{max}) for these coatings are about 391 °C. The excellent thermal stability for coatings prepared with G0, G1, and G2 can be proven that the thermal degradation process can be divided into two stages: fast degradation stage (320–425 °C) and carbonization stage (438–585 °C). By contrast, thermal degradation of the coating prepared with G3 can be divided into three stages: in addition to fast degradation stage and carbonization stage mentioned, there is an initiated degradation stage (122–308 °C), which might be due to the remaining allyl groups after the thiol-ene-initiated curing reaction for steric hindrance.

CONCLUSIONS

A class of UV-cured transparent solvent-free silicone coatings with high hardness, low water absorption, and fairly high transmittance were prepared from allyl-terminated hyperbranched polycarbosilanes and thiol silicone resins. The features for fabrication of the UV-cured silicone coatings were discussed. When n(thiol):n(allyl) = 1.4:1 and G1 is cured with the thiol silicone resin with R/Si and thiol content of 1.4 and 0.004 mol g⁻¹ for 30 s, the coatings obtained have a pencil hardness of 9 H, water absorption no more than 0.04 wt %, transmittance higher than 94%, and Td_5 as high as 371.1 °C. By comparison with those UV-cured materials reported previously, the coatings prepared in this work exhibit higher pencil hardness and superior thermal stability.

EXPERIMENTS

Materials. 3-Trimethoxysilylpropanethiol, ether, and tetrahydrofuran (THF) were from Beijing HWRK Chem. Co., Ltd. Ether and THF were distilled over potassium for 24 h before use. Dimethyl diethoxysilane, methyl trimethoxysilane, methyltrichlorosilane, and trichlorosilane (TCS) were the products of Shanghai Jiancheng Industry and Trade Co., Ltd. Ammonium chloride, magnesium sulfate anhydrous, and toluene were purchased from Sinopharm Chemical Reagent Co., Ltd., China. 3-Bromopropene, magnesium powder, and iodine were purchased from Adamas Reagent Co., Ltd. (Shanghai), Shanghai Lingfeng Chemical Reagent Co., Ltd., and TCI (Shanghai) Chemical Industrial Development Co., Ltd., respectively. Spiere's platinum catalyst with a platinum concentration of 8000 ppm was prepared by our group. Thiol silicone resins with various thiol contents and R/Si were synthesized according to ref 18, and the thiol contents were calculated according to the ¹H-NMR spectrum shown in Figure S3.

Preparation of Allyl-Terminated Hyperbranched Polycarbosilanes. Allyl-terminated hyperbranched polycarbosilanes were synthesized according to ref 27 (Figure S4), the ¹H-NMR and ¹³C-NMR spectra of which are shown in Figures S5 and S6, respectively. The MALDI-TOF-MS analysis of products is summarized in Table S1.

Preparation of the UV-Cured Transparent Solvent-Free Silicone Coatings. As shown in Scheme S1, the solventfree silicone coatings with thickness about 0.5 mm were prepared by dropping the mixtures in the middle of glass slides followed by spin-coating under a rotate speed of 3000 r/s for 30 s and then curing by UV with a laser wavelength of 365 nm and radiation intensity of 10.6 mW cm⁻² (ZB1000, Changzhou Zibo Electron Technology Co., Ltd., the distance of the glass slides to the light is 20 cm). The thickness of the coatings was controlled by taking a mixture of equal mass onto the glass slides.

Characterization. NMR analysis was carried out using a 400 MHz Bruker AVANCE AV400 spectrometer in CDCl₃ without tetramethylsilane. Fourier transform infrared (FT-IR) analysis was performed using a Nicolet 700 spectrometer (Nicolet Co., Ltd., America). MALDI-TOF-MS analysis was carried out using a Voyager DE RESIN MALDI-TOF-MS (Applied Biosystems, USA) using a mixture of 2,5-dihydroxybenzoic acid in tetrahydrofuran $(0.078 \text{ mg mL}^{-1})$ and sodium trifluoroacetate in tetrahydrofuran (0.068 mg mL⁻¹) with a 1:1 mass ratio as the matrix. The samples were dissolved in THF (10 mg mL $^{-1}$), and the solution of samples and matrix were mixed according to a 1:7 mass ratio. The transmittance spectra of samples were measured using a Unico UV 4802 UV/vis spectrophotometer (Unico Instrument Co., Ltd., Shanghai). The pencil hardness was measured with a BGD 562 pencil hardness meter (Zhenwei Testing Machinery Co. Ltd., Jiangdu, China) according to GBT6739-2006. Thermogravimetric analysis (TGA) was carried out using a TG 209C apparatus (Germany) at a heating rate of 10 °C min⁻¹ under a N_2 atmosphere. Differential scanning calorimetry (DSC) analysis was conducted using a DSC Q100 apparatus with a carrier gas flow rate of 20 mL min⁻¹ under a nitrogen atmosphere. The curing degrees, water absorptions, and surface water contact angles were measured according to refs 18, 27, and 28.

ASSOCIATED CONTENT

Supporting Information

The Supporting Information is available free of charge at https://pubs.acs.org/doi/10.1021/acsomega.0c01338.

¹H-NMR characterization of thiol silicone resin. The synthesis procedure, ¹H-NMR, and ¹³C-NMR spectra, and MALDI-TOF-MS of allyl-terminated hyperbranched polycarbosilanes G0, G1, G2, and G3. Scheme for preparation of the UV-cured transparent solvent-free silicone coatings, contact angles for the coatings with various contents of thiol, and DSC analysis of the coatings prepared with G0, G1, G2, and G3 (PDF)

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Notes

The authors declare no competing financial interest.

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