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A Depth-of-Interaction Encoding PET Detector Module with Dual-Ended Readout Using Large-Area Silicon Photomultiplier Arrays

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Abstract

The performance of a depth-of-interaction (DOI) encoding PET detector module with dual-ended readout of LYSO scintillator arrays using large-area SiPM arrays was evaluated. Each SiPM array, with a surface area $50.2 \times 50.2 \text{ mm}^2$, consists of 12×12 C-series SiPMs from SensL (SensL, Inc). The LYSO array, with a total size of $46 \times 46 \text{ mm}^2$ and a pitch size of 1.0 mm, consists of a 46×46 array of $0.945 \times 0.945 \times 20 \text{ mm}^3$ polished LYSO crystals, separated by Toray reflector. Custom front-end electronics were designed to reduce the 288 SiPM signals of one detector module to 9 signals, 8 for position information and 1 for timing information. Schottky diodes were used to block noise from SiPMs that did not detect a significant number of scintillation photons following a gamma interaction. Measurements of noise, signal, signal-to-noise ratio, energy resolution and flood histogram quality were obtained at different bias voltages (26.0 to 31.0 V in 0.5 V intervals) and at two temperatures (5 °C and 20 °C). Clear acrylic plates, 2.0 mm thick, were used as light guides to spread the scintillation photons. Timing resolution, depth of interaction resolution, and the effect of event rate on detector performance were measured at the bias voltage determined to be optimal for the flood histograms. Performance obtained with and without the noise-blocking Schottky diodes was also compared. The results showed that all crystals in the LYSO array can be clearly resolved, and performance improved when using diodes to block noise, and at the lower temperature. The average energy resolution, flood histogram quality, timing resolution and DOI resolution were $23.8 \pm 2.0 \%$, 1.54 ± 0.17 , $1.78 \pm 0.09 \text{ ns}$ and $2.81 \pm 0.13 \text{ mm}$ respectively, obtained at a bias voltage of 30.0 V and a temperature of 5 °C using the diode readout method. The event rate experiments showed that the flood histogram and energy resolution of the detector were not significantly degraded for an event rate of up to 150 000 counts/s.

1 Introduction

High resolution and high sensitivity positron emission tomography (PET) scanners are powerful functional and molecular imaging tools to image biological processes *in vivo* (Tai *et al* 2003 and Slomka *et al* 2016). Most PET detectors are based on scintillator arrays coupled to photodetector (Lewellen 2008). To simultaneously achieve high spatial resolution and high sensitivity, long crystals with small cross-sectional area are required, and the detectors are best located close to the subject to cover a large solid angle and reduce effect of

the non-colinearity of the gamma photons on spatial resolution (Stickel and Cherry 2004). However, PET scanners with compact geometry and long crystals suffer from the parallax error (mispositioning of the line of response), which can be mitigated using detectors with depth-of-interaction (DOI) encoding capability (Stickel and Cherry 2004, Yang *et al* 2008 and Shao *et al* 2014).

Various approaches have been proposed to obtain DOI information from PET detectors, including multi-layer crystals, custom reflector designs, the use of the light distribution in monolithic crystals and the dual-ended readout method (Joung *et al* 2002, Yang *et al* 2006, Du *et al* 2008, Thompson and Goertzen 2011, Kolb *et al* 2014 and Lee and Lee 2015). Compared to other methods, reading out the scintillators from both ends maximizes overall light collection and provides extremely good high DOI resolution, as well as continuous DOI information, by using the energy ratio of the two photodetector signals (Yang *et al* 2006). The dual-ended readout method has been successfully implemented in several prototype PET scanners where the uniformity of the spatial resolution was significantly improved (Yang *et al* 2008 and Shao *et al* 2014).

Silicon photomultipliers (SiPMs) are the most suitable photodetectors for dual-ended readout PET detectors due to their compact size and high gain, compared to photomultiplier tubes (PMTs) and avalanche photodiodes (APDs). DOI detector modules using SiPM arrays or position sensitive SiPMs (PS-SiPM) with small dimensions $< 16 \times 16 \text{ mm}^2$ have been widely investigated (Schmall *et al* 2013, Shao *et al* 2014, Du *et al* 2015 and Du *et al* 2018). The packing fraction of these SiPM array based detectors is low, however, due to the edge effect (the SiPM arrays need to be larger than the crystal array to decode the edge crystals), resulting in large dead space between modules when constructing PET scanners. A high packing fraction can be achieved using PS-SiPMs, however, it is difficult to build large-area ($>20 \times 20 \text{ mm}^2$) PS-SiPMs and the capacitance of such large-area devices is problematic (Schmall *et al* 2013 and Du *et al* 2018).

One way to build higher packing fraction DOI detector modules is using large-area SiPM arrays. In this paper, a DOI detector module based on a 12×12 array ($50.2 \times 50.2 \text{ mm}^2$) of SiPMs coupled to both ends of a 46×46 array of polished LYSO crystals with 1 mm pitch was designed and evaluated. The proposed detector module has a packing fraction of 84%, and requires just 9 electronic channels for further processing, 8 for position information and 1 for timing information, to read out the 25cm^2 detector area. Performance in terms of flood histogram quality, energy resolution and signal-to-noise ratio (SNR) were measured at different bias voltages (26.0 to 31.0 V in 0.5 V intervals) and at two temperatures (5 °C and 20 °C). Timing resolution and DOI resolution were measured at the bias voltage determined to be optimal for the flood histograms. One concern for large-area detectors is the high singles rate that the module must handle without incurring significant dead time losses or mispositioning due to pile up. Therefore, the performance of the module was also evaluated as a function of event rate (Du *et al* 2015 and Du *et al* 2018).

2 Materials and Methods

2.1. DOI detector module

The DOI detector module (figure 1) consists of two 12×12 arrays of $3 \times 3 \text{ mm}^2$ C-series SiPMs (MicroFB-30035-SMT) (SensL, Inc), and a 46×46 array of $0.945 \times 0.945 \times 20 \text{ mm}^3$ polished LYSO crystals (Crystal Photonics, Inc). The total area of the SiPM arrays is $50.2 \times 50.2 \text{ mm}^2$, and the center-to-center distance of two SiPMs is 4.2 mm, leaving a 1.2 mm dead space between SiPMs, as shown in figure 2 (a) and (b). Each SiPM pixel has an active area of $3.0 \times 3.0 \text{ mm}^2$ and contains 4,774 microcells ($35 \mu\text{m}$) with a 64% fill factor. The C-series SiPMs are fabricated using a p-on-n structure that significantly improves photon detection efficiency (PDE) for blue light. They have a 41% PDE at 420 nm and an over-voltage of 5.0 V (SensL 2014), matching well the emission spectra of widely-used LSO or LYSO crystals in PET (Saoudi *et al* 1999 and Du *et al* 2009). The pitch size of the LYSO array is 1.0 mm and Toray reflector (Toray industries, Inc.) was used to optically isolate the crystals.

To create light sharing among SiPMs, clear acrylic slabs with a thickness of 2.0 mm were used as light guides and coupled between the scintillator arrays and SiPM surface using optical grease BC-630 (Saint-Gobain). 2.0 mm thick clear acrylic slabs were selected by comparing the results obtained using clear acrylic slabs with thicknesses ranging from 1.5 mm to 3.0 mm. The SiPM arrays, crystal array and clear acrylic slabs were assembled together using a 3D printed holder to maintain the relative position of components for different experiments (figure 1).

2.2. Signal multiplexing circuit

Each SiPM pixel has two outputs, a fast output and a standard output (SensL 2014). As the detector was built to achieve high spatial resolution, to simplify the readout electronics, only the standard outputs were used and the fast outputs were left floating. In our custom front-end electronics (figures 1 and 3), the standard outputs were individually amplified. Two different preamplifier circuits were designed and compared, as shown in figure 4. The first one is the standard readout method and the second is the diode readout method. As each SiPM array has 144 elements distributed over a large area, and during any given gamma interaction only a subset of the SiPMs detect scintillation photons, Schottky diodes (NSR0320, ON Semiconductor) were used to block noise from the SiPMs with negligible signals (Anderson and Anderson 2017 and Rudan 2017). To compensate the forward voltage of the diodes, a diode bias voltage of 125 mV was applied (ON Semiconductor 2011). This value was chosen by investigating several diode bias voltages to determine the tradeoff between signal loss and noise reduction.

For each SiPM array, the amplified SiPM signals were summed into rows and columns, generating 12 row signals and 12 column signals. The row/column signals were weighted by applying a gain to each row and column proportional to its location along each axis, generating four position signals (Popov 2011). The 8 position signals of one detector module were further amplified and shaped by a spectroscopy amplifier (N586B, CAEN) and digitized by a PowerDAQ board (PD2MFS, United Electronic Industries). The gamma

photon interaction position x and y , deposited energy E and DOI information were calculated using the following functions:

$$x = \frac{1}{2} \left(\frac{X_1^+ - X_1^-}{X_1^+ + X_1^-} + \frac{X_2^+ - X_2^-}{X_2^+ + X_2^-} \right), y = \frac{1}{2} \left(\frac{Y_1^+ - Y_1^-}{Y_1^+ + Y_1^-} + \frac{Y_2^+ - Y_2^-}{Y_2^+ + Y_2^-} \right) \quad (1)$$

$$E = X_1^+ + X_1^- + Y_1^+ + Y_1^- + X_2^+ + X_2^- + Y_2^+ + Y_2^- \quad (2)$$

$$DOI = \frac{(X_1^+ + X_1^- + Y_1^+ + Y_1^-) - (X_2^+ + X_2^- + Y_2^+ + Y_2^-)}{X_1^+ + X_1^- + Y_1^+ + Y_1^- + X_2^+ + X_2^- + Y_2^+ + Y_2^-} \quad (3)$$

where X_i^+ , X_i^- , Y_i^+ , Y_i^- ($i = 1, 2$) are the four position signals from SiPM array 1 and 2 respectively.

The 24 row signals and 24 column signals were summed together to form one global timing signal and sent to a constant fraction discriminator (CFD) (584, ORTEC) to generate a time stamp and to generate a trigger for the DAQ board.

2.3 Experimental methods

2.3.1 Flood histograms—A 0.5 mm diameter, 50 μCi ^{68}Ge point source, located 150 mm above one end of the LYSO array, was used to irradiate the LYSO crystals. To determine the settings to achieve the best flood histograms, these histograms were measured at different bias voltages (from 26.5 V to 31.0V, in 0.5 V intervals) and a 250 – 750 keV energy window was applied to each crystal to select events. To quantitatively compare the flood histogram quality at different bias voltages, a flood histogram quality metric was calculated following the method described in Du *et al* 2016. Briefly, the flood histogram quality parameter k_j was calculated for all 2,116 crystals in the LYSO array based on the ratio of the crystal separation to the spot size, and the flood histogram was quantified using the geometric mean and the standard deviation for all k_j using the following function,

$$k = \sqrt[2116]{\prod_{i=1}^{2116} k_i}, \quad \sigma_k = \sqrt{\frac{1}{2116} \sum_{i=1}^{2116} (k_i - k)^2} \quad (4)$$

2.3.2 Signal to noise ratio and energy resolution—The data used to generate the flood histogram were also used to calculate the SNR and energy resolution. The signal amplitude for each individual crystal was quantified as the centroid of the Gaussian fit to the 511 keV photopeak of the energy spectrum. The energy resolution was the FWHM to the centroid of the Gaussian fit. The average signal amplitude and the average energy resolution of all crystals in the LYSO array were taken as a measure of the signal and the energy resolution for the whole crystal array respectively (Du *et al* 2018).

The SNR was calculated following the methods described in Yang *et al* 2011 and Du *et al* 2013. Briefly, the noise was measured by periodically triggering the DAQ board using the computer clock and the FWHM of histogram of the summed 8 position signals was treated as the noise. The average SNR was calculated as the ratio of the average signal amplitude to the noise.

2.3.3 DOI measurements—The DOI resolution was measured using a reference detector consisting of a PMT and a $20 \times 20 \times 0.5 \text{ mm}^3$ LSO slab wrapped with teflon tape. A $0.5 \text{ mm } ^{68}\text{Ge}$ point source was mounted on a translation table with the reference detector to irradiate the crystals from the side at different depths (Du *et al* 2018). The distance from the point source to the LSO slab was 100 mm and the distance from the point source to the surface of the LYSO array was 80 mm (figure 5 (a)). Due to the large size of the LYSO array, only part of the crystal array can be irradiated and used for DOI analysis, as shown in figure 5. The 276 crystals (12 rows \times 23 columns) in the white rectangle (figure 5) were used. The DOI resolution was measured at five depths (from 2 mm to 18 mm, in 4 mm steps) and at two temperatures (5 °C and 20 °C). The bias voltage was the optimal bias voltage determined for the flood histogram (30.0 V for the diode readout method and 28.0 V for the standard readout method). A 250–750 keV energy window was applied to each crystal to select events, and no correction for the source size or beam geometry was made.

2.3.4 Timing measurements—Timing resolution was also measured at a bias voltage of 30.0 V when the diode readout method was used and 28.0 V when the standard readout method was used, and at 5 °C and 20 °C. A $16 \times 16 \times 16 \text{ mm}^3$ LYSO crystal (wrapped with Teflon) coupled to a Hamamatsu PMT R12844–10 was used as a reference detector. The timing signals from the reference detector and the DOI detector were sent to a time-amplitude converter (TAC) and used as a start and stop signal respectively. The TAC output was digitized by the PowerDAQ board together with position signals. The timing resolution of two identical reference detectors was $480 \text{ ps} \pm 16 \text{ ps}$.

The FWHM of the timing spectrum of each crystal was used as the timing resolution and a 250–750 keV energy window was also applied to each crystal to select events. The estimated coincidence timing resolution of two DOI detector modules was calculated by subtracting in quadrature the contribution of the reference detector using the following equation (Du *et al* 2018):

$$CTR = \sqrt{2} \sqrt{CTR_{measured}^2 - CTR_{reference_detector}^2} / 2 \quad (5)$$

2.3.5 Effect of event rate—A large-area detector with high detection efficiency and multiplexing electronics must be able to handle the relatively high single event rates that will be encountered in dynamic PET scanning, especially in the early time points immediately after injection. The performance of the proposed detector was measured using a 4 mCi ^{18}F source with a size of $16 \times 16 \times 8 \text{ mm}^3$, located 120 mm from the entry face of the LYSO array. Coincidence event data were acquired using a reference detector, consisting of a PMT R12844–10 and a $16 \times 16 \times 32 \text{ mm}^3$ LYSO. Flood histograms and energy resolution were

measured at different event rates and at a temperature of 5 °C. The SiPM bias voltage was 30.0 V and 28.0 V for the diode readout method and standard readout method, respectively.

3. Results

3.1 Flood histograms

The flood histograms obtained using the diode readout method and standard readout method are shown in figure 6, and the position profile for the 22nd crystal row are shown in figure 7(a). The bias voltages were set to 30.0 V and 28.0 V for the diode readout method and standard readout method respectively, based on the plot of flood histogram quality versus bias voltage shown in figure 7 (b). Better flood histograms were consistently obtained using the diode readout method, especially for the edge crystals, which were more clearly separated (figure 7). The highest flood histogram quality values for each temperature and readout method are listed in Table I. The flood histograms obtained at 20 °C using the diode readout method was almost the same as that achieved at 5 °C for the standard readout method.

3.2 Signal-to-noise ratio

The noise, average signal amplitude and average SNR of all crystals in the array are shown in figure 8. The noise and signal both increase with increasing bias voltage. The noise obtained at 20 °C was higher than that obtained at 5 °C using the same readout method. The noise (figure 8 (a)) obtained using the diode readout method was smaller than that obtained using the standard readout method, showing that the noise, as expected, was reduced by the Schottky diodes.

The signals obtained using the diode readout method were also smaller than these obtained using standard readout method, because the signals were truncated by the forward voltage of diode (ON Semiconductor 2011). Using the standard readout method, the signals obtained at 20 °C were smaller than these obtained at 5 °C at the same bias voltage, as the breakdown voltage of SiPMs increases with increasing temperature (SensL 2014). The over-voltage (voltage over breakdown voltage) was lower at the higher temperature when the same bias voltage was applied. However, using the diode readout method, the signal obtained at the two temperatures was almost the same, because the forward voltage of the diode was also lower at the higher temperature and for the lower signals (ON Semiconductor 2011).

The SNR increases and then decreases with increasing bias voltage except the one obtained at 5 °C using the diode readout method, which is just reaching its maximum at the high end of the tested bias voltage range. The diode method, as well as lower temperatures, reduce noise, allowing operation at higher bias voltages before the noise dominates the SNR. The SNR obtained using the diode readout was higher than that obtained using standard readout method. The best SNR was obtained at 31.0 V using the diode readout method at 5 °C.

3.3 Energy resolution

The average energy resolutions versus bias voltage are shown in figure 9 (a). In addition, the average energy resolution obtained at the optimal bias voltage for the flood histogram (30.0

V and 28.0 V for the diode readout method and standard readout method respectively) are listed in Table II. The energy resolution decreases with increasing bias voltage since the photon detection efficiency increases as bias voltage increases (SensL 2014). The energy resolution obtained using the standard readout method was better than that obtained using the diode readout method. Energy resolution obtained at 5 °C was better than that obtained at 20 °C, but the temperature effect was very small.

The average FWHM of the 511 keV photopeak of all crystals are shown in figure 9 (b). The FWHM obtained using the diode readout method was smaller than that obtained using the standard readout method, which means the apparent degradation in energy resolution obtained using the diode readout method is mainly due to the truncation of the signal caused by the forward voltage of the diode, which reduces the denominator in the energy resolution calculation.

3.4 DOI resolution

The DOI response for an edge crystal, calculated using equation 3, is shown in figure 10 (a). The average DOI resolution across the five depths for each crystal measured (see white rectangle in figure 5) is shown in figure 10 (b). These results were obtained using a bias voltage of 28.0 V, temperature of 5 °C and the standard readout method. Figure 11 shows the average DOI resolution across all five depths and all crystals in the same column versus the crystal column order. The DOI resolution degrades as the crystal column order increases, due to the increased detection of scattered photons and divergence of the collimating beam with increasing penetration into the crystal array. The DOI resolution obtained using the diode readout method was worse than that obtained using the standard readout method, due to the effect of the forward bias voltage of the diodes on the SiPM signals (figure 11). The average DOI resolution of all crystals in the first column obtained under different conditions are reported in Table II. The average DOI resolution was < 3 mm.

3.5 Timing resolution

The timing spectra for a corner, edge and center crystal are shown in figure 12. These measurements were obtained at a bias voltage of 30.0 V and a temperature of 5 °C using the diode readout method. The peak positions of the timing spectra were crystal dependent due to the location of the crystals and the different trace length of the signal lines.

The average timing resolution across all crystals in the LYSO array are listed in Table III. The timing resolution was improved at the lower temperature and using diode readout method, as noise was reduced (figure 8 (a)).

3.6 Event rate effects

The flood histograms obtained at different event rates are shown in figure 13, and the flood histogram quality metric and energy resolution versus event rate are plotted in figure 14 and figure 15 respectively. As expected, pile up causes the flood histograms and energy resolution to deteriorate at higher event rates, however all crystals can be identified (flood histogram quality > 1) up to an event rate of approximately 150,000 counts per second. The

diode readout method provides better flood histograms than the standard readout method except at the very highest event rates studied where pileup effects dominate both methods.

4. Discussion

The results showed that better performance was obtained at lower temperatures and selection of bias voltage was important to optimize detector performance. Better flood histograms and timing resolution were obtained using the diode readout method, which removed the influence of SiPMs measuring negligible signals. However, better energy resolution and DOI resolution was obtained using the standard readout method.

The flood histogram showed that all the crystals in the LYSO array could be clearly identified (figure 6). The average energy resolution obtained at the optimal bias voltage was less than 25 %, and the DOI resolution was less than 3 mm. The DOI resolution was not as good as that previously obtained using position-sensitive avalanche photodiodes (PS-APDs) (Yang *et al* 2006 and Ren *et al* 2014), however, it was not worse than that obtained using other PS-SiPMs or SiPM arrays (Du *et al* 2018). Further studies are ongoing to investigate why the DOI resolution was not as good as these obtained using PS-APDs.

A coincidence timing resolution of ~1.6 to 1.8 ns was obtained using a constant fraction discriminator and without any dark count suppression technique. This timing resolution is similar or better compared with other recent work using large-area SiPM array and comparable readout methods (Shao *et al* 2015 and Stolin *et al* 2014). Better timing resolution could be obtained by optimizing the setup and bias voltage according to the timing resolution, which will be studied in future.

This detector module can handle event rates of ~150,000 counts/s without significant performance degradation (figures 13, 14). Higher event rate capability is expected by using the latest J-series SiPMs from SensL, as the signal pulse shape is shorter (SensL 2014, 2017). The event rate can also be increased by using pile-up recovery electronics and more complicated readout (Wang *et al* 2003), such as reading out each SiPM signals individually. For most of the envisaged applications, the current counting rate capability already is sufficient.

Our work shows the possibility of developing dual-ended readout detectors based on large-area SiPM arrays and crystal arrays with a pitch size of 1.0 mm (for high resolution) and a length of 20 mm (for high sensitivity). Detector modules developed by others either use SiPM arrays with smaller size or crystal array with larger pitch size or shorter length (e.g. Shao *et al* 2015 and Stolin *et al* 2014). Monolithic crystal-based PET detectors with similar size also have been developed and are an attractive approach, however, complicated positioning algorithms, such as neural networks or maximum likelihood, are used to calculate the gamma photon interaction position, and training data or reference data are required (Borghi *et al* 2016 and Pierce *et al* 2018). Compared to the monolithic crystal-based PET detectors, detectors based on arrays of pixelated crystals are relatively easy to use and calibrate, and the simple center-of-gravity position algorithms can easily be implemented inside hardware, such as FPGAs.

5. Conclusions

The performance of a DOI encoding PET detector module based on large-area SiPM arrays was characterized in detail with a view to their use in high resolution dedicated organ PET scanners (brain or breast) and small animal PET scanners. The multiplexed readout electronics reduced the 288 SiPM signals to 9 signals, 8 signals for position information and 1 signal for timing information, greatly simplified the subsequent acquisition electronics.

With the attractive performance parameters measured here, relatively cost-effective and simple high-resolution small-animal PET and dedicated scanners for breast and brain imaging could be developed based upon these modules. Our next step is to develop detector modules and electronics that can be tiled on all four sides to eliminate gaps between modules and to develop a partial prototype human brain PET scanner to evaluate the performance at a system level.

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References

- Anderson B and Anderson R 2017 *Fundamentals of Semiconductor Devices* (2nd) McGraw-Hill Education.
- Borghi G, Jan Peet B, Tabacchini V and Schaart DR 2016 32 mm × 32 mm × 22 mm monolithic LYSO:Ce detector with dual-sided digital photon counter readout for ultrahigh-performance TOF-PET and TOF-PET/MRI *Phys. Med. Biol.* 61 4929–4949. [PubMed: 27286232]
- Du H, Yang Y, Glodo J, Wu Y, Shah K and Cherry SR 2008 Continuous depth-of-interaction encoding using phosphor-coated scintillators *Phys. Med. Biol.* 54:1757–1771.
- Du J, Bai X, Gola A, Ferri A, Piemonte C, Yang Y and Cherry SR 2018 Performance of a high-resolution depth-encoding PET detector module using linearly-graded SiPM *Phys. Med. Biol.* 63:035035. [PubMed: 29324437]
- Du J, Schmall J, Yang Y, Di K, Dokhale P, Shah K and Cherry SR 2013 A simple capacitive charge-division readout for position-sensitive solid-state photomultiplier array *IEEE Trans. Nucl. Sci.* 60:3188–3197. [PubMed: 25558081]
- Du J, Schmall J, Yang Y, Di K, Roncali E, Mitchell G, Buckley S, Jackson C and Cherry SR 2015 Evaluation of Matrix9 silicon photomultiplier array for small-animal PET *Med. Phys.* 42:585–599. [PubMed: 25652479]
- Du J, Wang Y, Zhang L, Zhou Z, Xu Z and Wang X 2009 Physical properties of LYSO scintillator for NN-PET detectors *Proceedings of the 2009 2nd International Conference on Biomedical Engineering and Informatics* 1:314–318.
- Du J, Yang Y, Bai X, Gola A, Ferri A, Zorzi N, Piemonte C and Cherry SR 2015 Evaluation of linearly-graded SiPMs for high resolution small-animal PET *Biomedical Physics & Engineering Express* 1:045008.
- Du J, Yang Y, Bai X, Judenhofer M, Berg E, Di K, Buckley S, Jackson C and Cherry SR 2016 Characterization of large-area SiPM array for PET applications *IEEE Trans. Nucl. Sci.* 63:8–16. [PubMed: 27182077]
- Joung J, Miyaoka R and Lewellen T 2002 cMiCE: a high resolution animal PET using continuous LSO with a statistics based positioning scheme *Nucl. Instrum. Methods A* 489:584–598.
- Kolb A, Parl C, Mantlik F, Liu C, Lorenz E, Renker D and Pichler B 2014 Development of a novel depth of interaction PET detector using highly multiplexed GAPD cross-strip encoding *Med. Phys.* 41:081916. [PubMed: 25086547]

- Lee M and Lee J 2015 Depth-of-interaction measurement in a single-layer crystal array with a single-ended readout using digital silicon photomultiplier *Phys. Med. Biol* 60:6495–6514. [PubMed: 26247294]
- Lewellen TK 2008 Recent developments in PET detector technology *Phys. Med. Biol* 53: R287–R317. [PubMed: 18695301]
- ON Semiconductor. NSR0320MW2T1G, NSVR0320MW2T1G, NSR0320MW2T3G. Datasheet. 2011. http://www.onsemi.com/pub_link/Collateral/NSR0320MW2T1-D.PDF.
- Pierce L, Pedemonte S, DeWitt D, MacDonald L, Hunter W, Van Leemput K and Miyaoka R 2018 Characterization of highly multiplexed monolithic PET / gamma camera detector modules *Phys. Med. Biol* 63 075017 [PubMed: 29498361]
- Popov V 2011 Advanced data readout technique for multianode position sensitive photomultiplier tube applicable in radiation imaging detectors *JINST* 6:C01061.
- Ren S, Yang Y and Cherry SR 2014 Effects of reflector and crystal surface on the performance of a depth-encoding PET detector with dual-ended readout *Med. Phys* 41:072503. [PubMed: 24989406]
- Rudan M 2017 *Physics of Semiconductor Devices* (2nd) Springer.
- Saoudi A, Pepin C, Pékpin C, Houde D and Lecomte R 1999 Scintillation light emission studies of LSO scintillators *IEEE Trans. Nucl. Sci* 46:1925–1928.
- Schmall J, Du J, Yang Y, Dokhale P, McClish M, Christian J, Shah K and Cherry SR 2013 Comparison of large-area position-sensitive solid-state photomultipliers for small animal PET *Phys. Med. Biol* 57:8119–8134.
- SensL. C-series low noise, blue-sensitive silicon photomultipliers. Datasheet. 2014. <http://sensl.com/downloads/ds/DS-MicroCseries.pdf>.
- SensL. J-series high PDE and timing resolution, TSV package. Datasheet. 2017. <http://sensl.com/downloads/ds/DS-MicroJseries.pdf>.
- Shao Y, Sun X and Lou K 2015 Development of compact DOI-measurable PET detectors for simultaneous PET/MR Imaging *EJNMMI Physics* 2:A2. [PubMed: 26956275]
- Shao Y, Sun X, Lan K, Bircher C, Lou K and Deng Z 2014 Development of a prototype PET scanner with depth-of-interaction measurement using solid-state photomultiplier arrays and parallel readout electronics *Phys. Med. Biol* 59:1223–1238. [PubMed: 24556629]
- Slomka P, Pan T, Germano G 2016 Recent advances and future progress in PET instrumentation *Seminars in Nuclear Medicine* 46:5–19. [PubMed: 26687853]
- Stickel J and Cherry SR 2004 High-resolution PET detector design: modelling components of intrinsic spatial resolution *Phys. Med. Biol* 50:179–195.
- Stolin A, Majewski S, Jaliparthi G, Raylman R and Proffitt J 2014 Evaluation of imaging modules based on SensL array SB-8 for nuclear medicine applications *IEEE Trans. Nucl. Sci* 61:2433–2438.
- Tai Y, Chatziioannou A, Yang Y, Silverman R, Meadors K, Siegel S, Newport D, Stickel J and Cherry SR 2003 MicroPET II: design, development and initial performance of an improved microPET scanner for small-animal imaging *Phys. Med. Biol* 48:1519–1537. [PubMed: 12817935]
- Thompson C and Goertzen A 2011 Evaluation of a 16:3 signal multiplexor to acquire signals from a SiPM array with dual and single layer LYSO crystal blocks *IEEE Trans. Nucl. Sci* 58:2175–2180.
- Wang Y, Li H, Liu Y, Xing T, Uribe J, Baghaei H, Farrell R and Wong W 2003 A modular low dead-time coincidence system for high-resolution PET cameras *IEEE Trans. Nucl. Sci* 50:1386–1391.
- Yang Y, Dokhale P, Silverman R, Shah K, McClish M, Farrell R, Entine G and Cherry SR 2006 Depth of interaction resolution measurements for a high resolution PET detector using position sensitive avalanche photodiodes *Phys. Med. Biol* 51:2131–2140. [PubMed: 16625031]
- Yang Y, Wu Y, Farrell R, Dokhale P, Shah K and Cherry SR 2011 Signal and noise properties of position-sensitive avalanche photodiodes *Phys. Med. Biol* 56:6327–6336. [PubMed: 21896961]
- Yang Y, Wu Y, Qi J, James S, Du H, Dokhale P, Shah K, Farrel R and Cherry SR 2008 A prototype PET scanner with DOI-encoding detectors *J. Nucl. Med* 49:1132–1140. [PubMed: 18552140]



Figure 1. Photograph of the DOI detector module with readout electronics, which reduce the 288 SiPM signals to 9 signals (8 for position information and 1 for timing information).

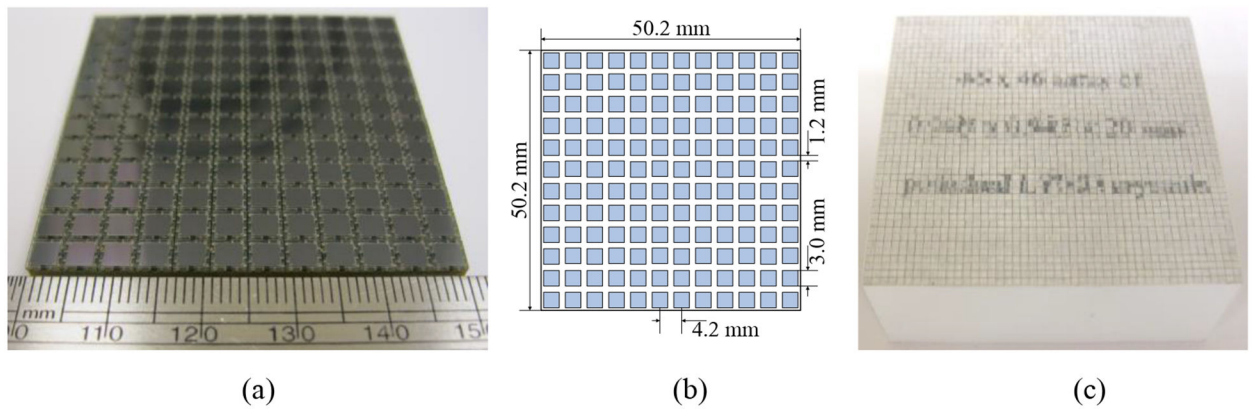


Figure 2.

(a) Photograph and (b) diagram of the 12×12 SiPM array. The light blue squares in (b) indicate the active area of SiPMs. (c) photograph of the LYSO array. The two ends of the LYSO array were left open.

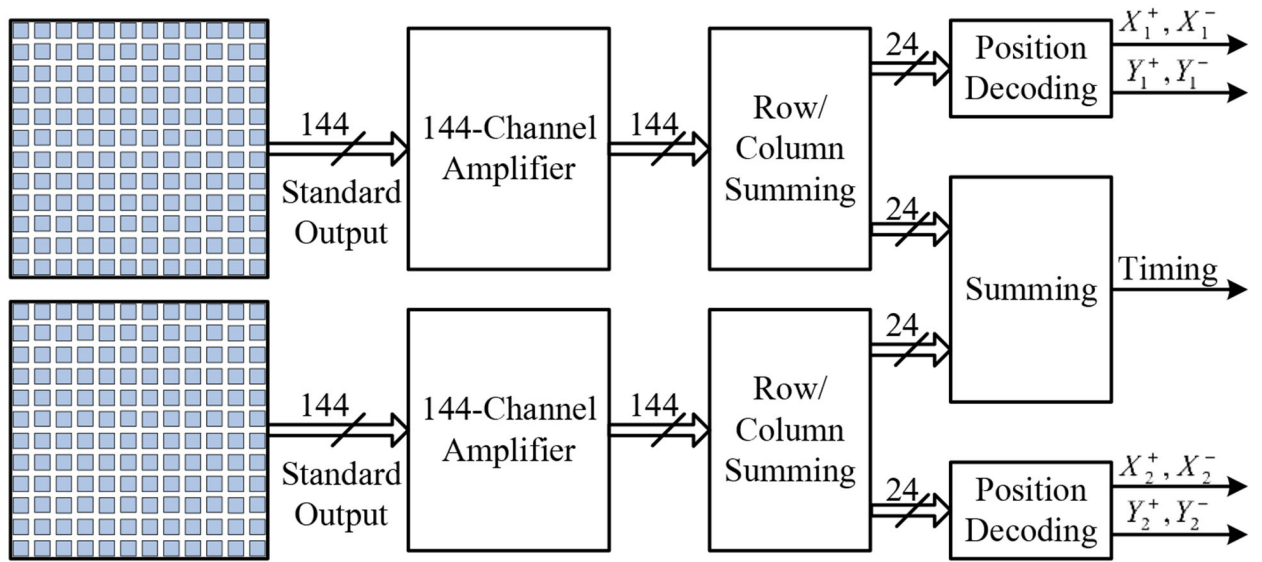


Figure 3.
Block diagram of the readout electronics.

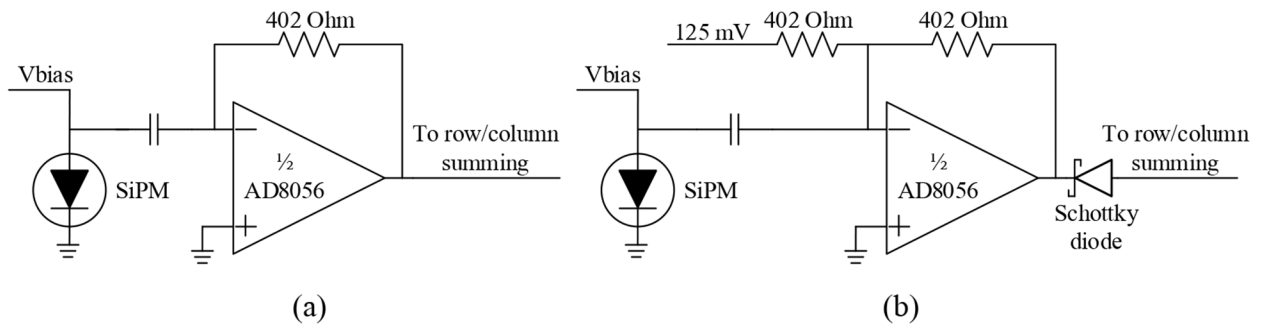


Figure 4. Schematic of the amplifier circuit for a single SiPM pixel. (a) standard readout method and (b) diode readout method. All the 288 SiPMs have their own identical amplifier circuit.

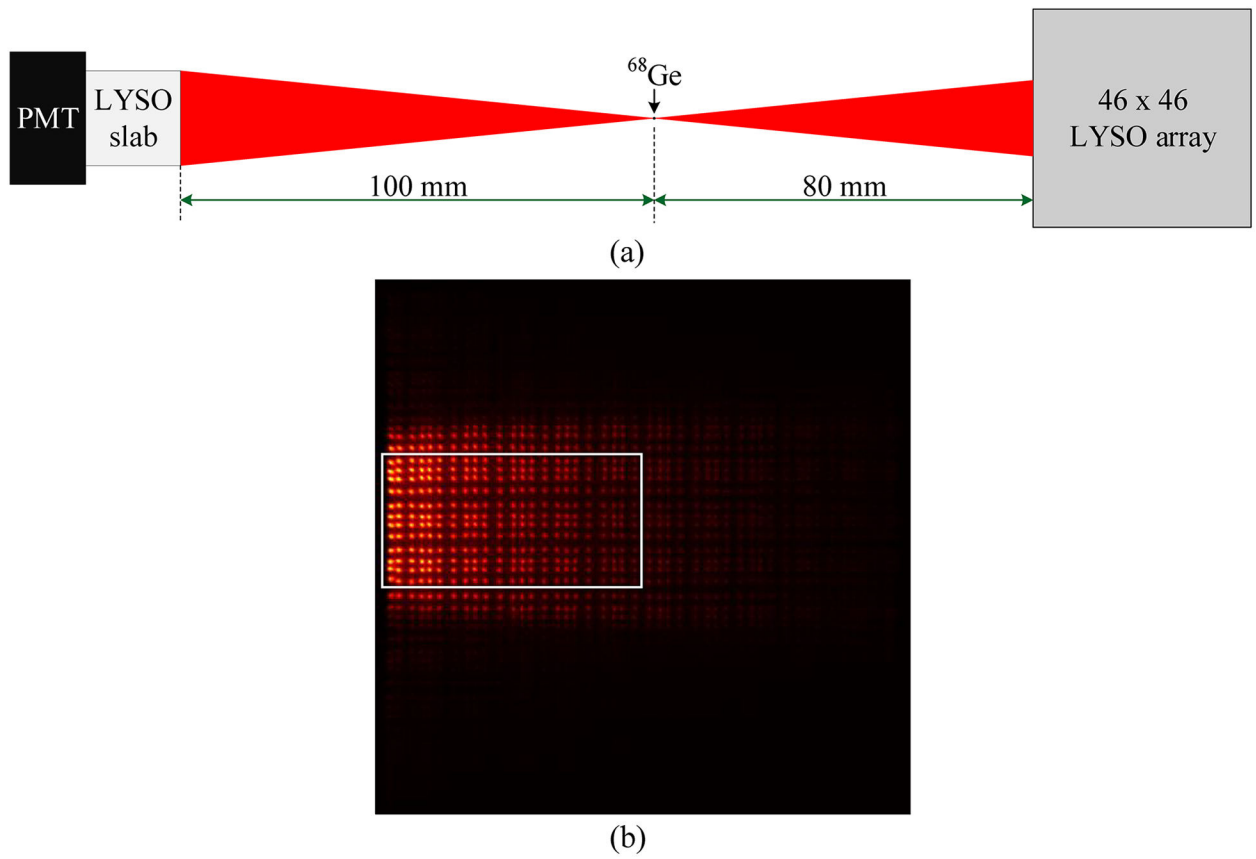


Figure 5. (a) schematic of the DOI setup and (b) flood histogram obtained during DOI resolution measurements. The 276 crystals in the white rectangle were used as being representative of the entire array.

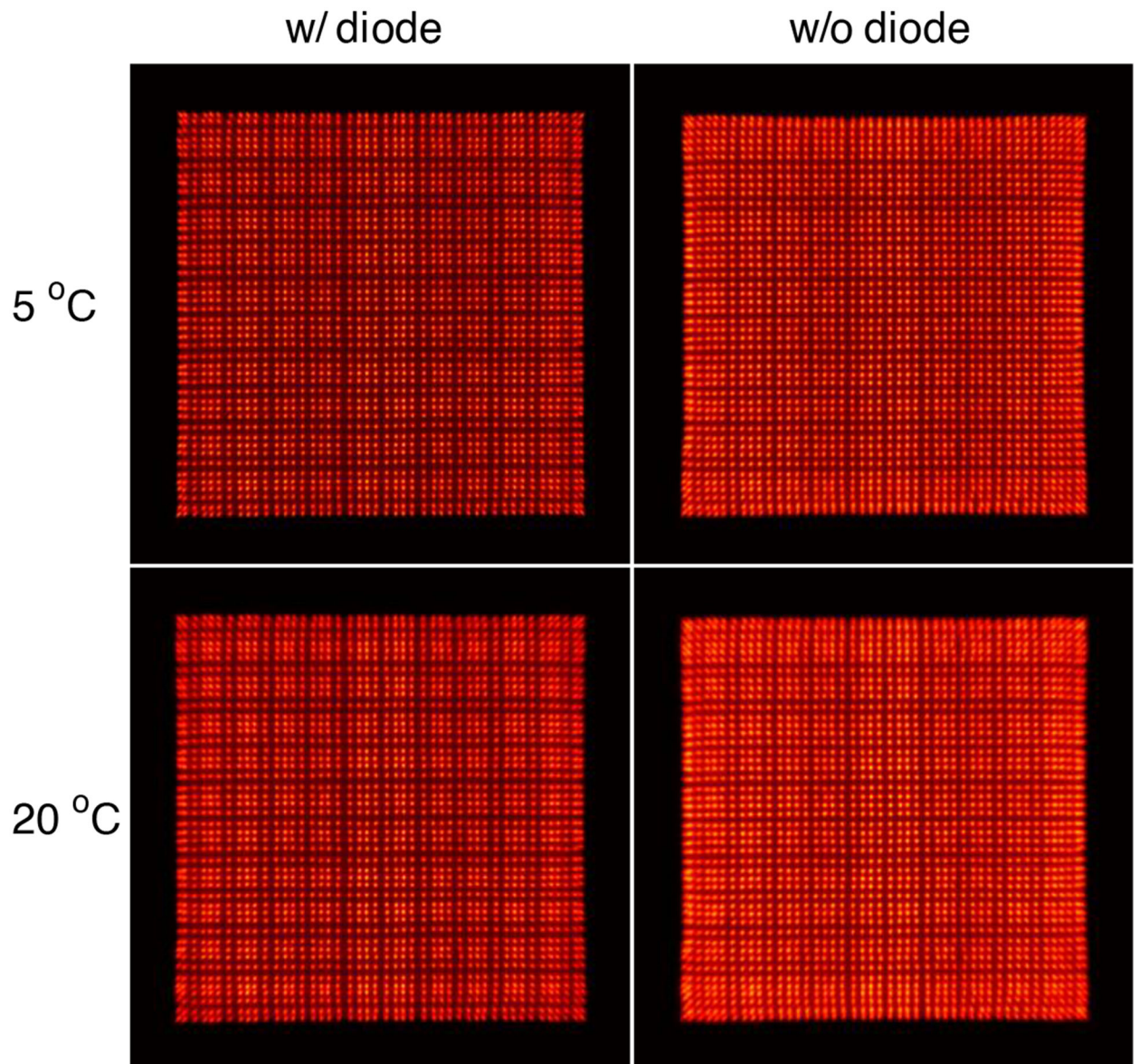
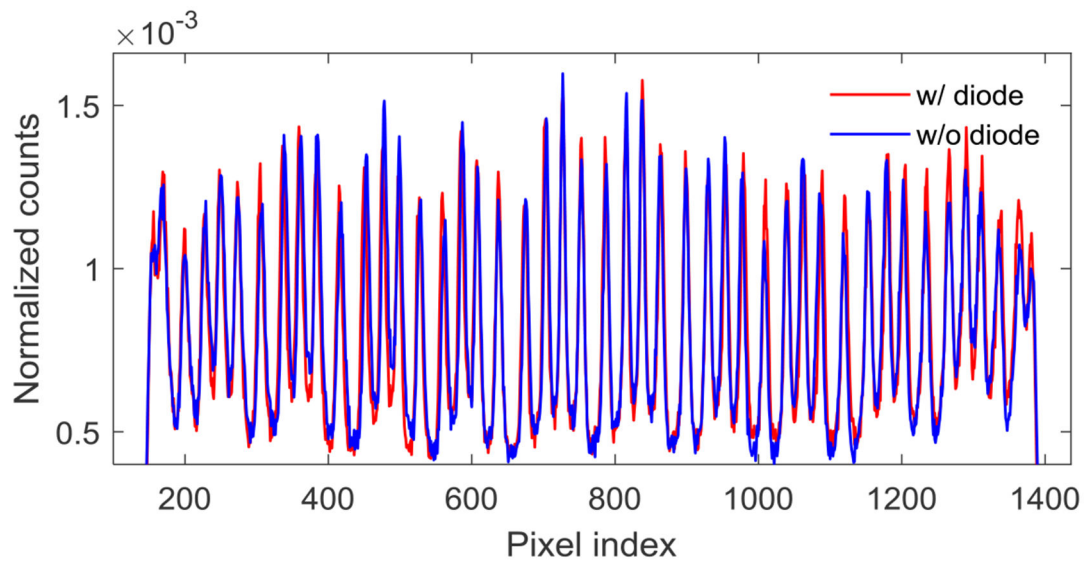
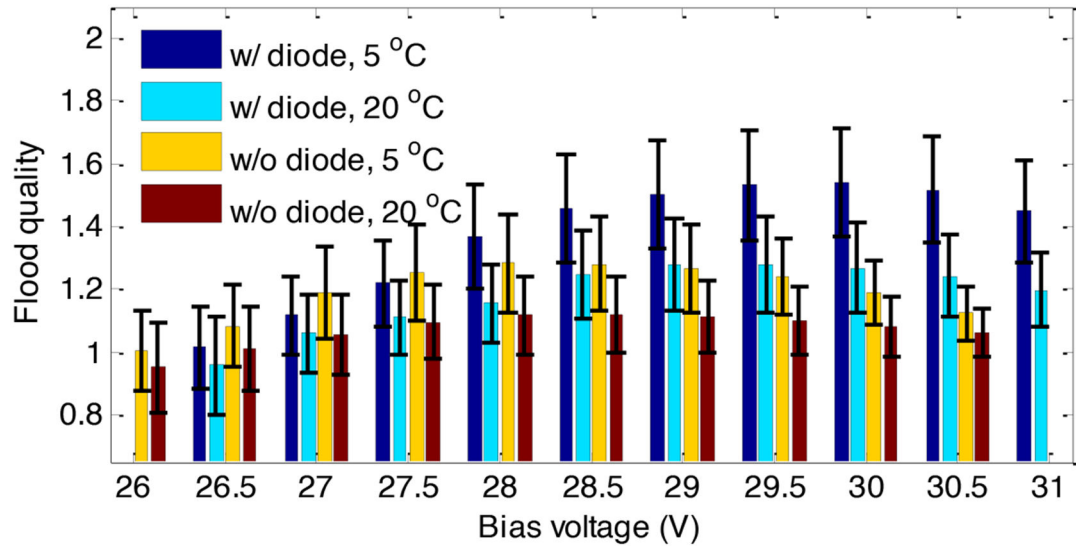


Figure 6. Flood histograms obtained at two different temperatures and using the two different readout methods.



(a)



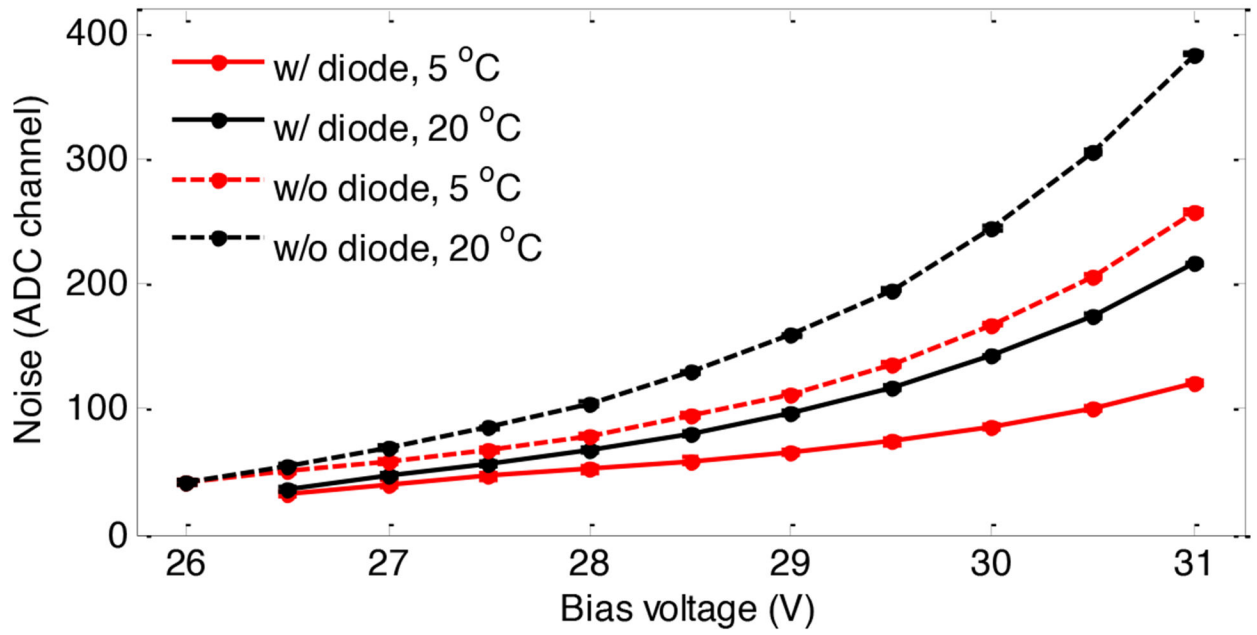
(b)

Figure 7.

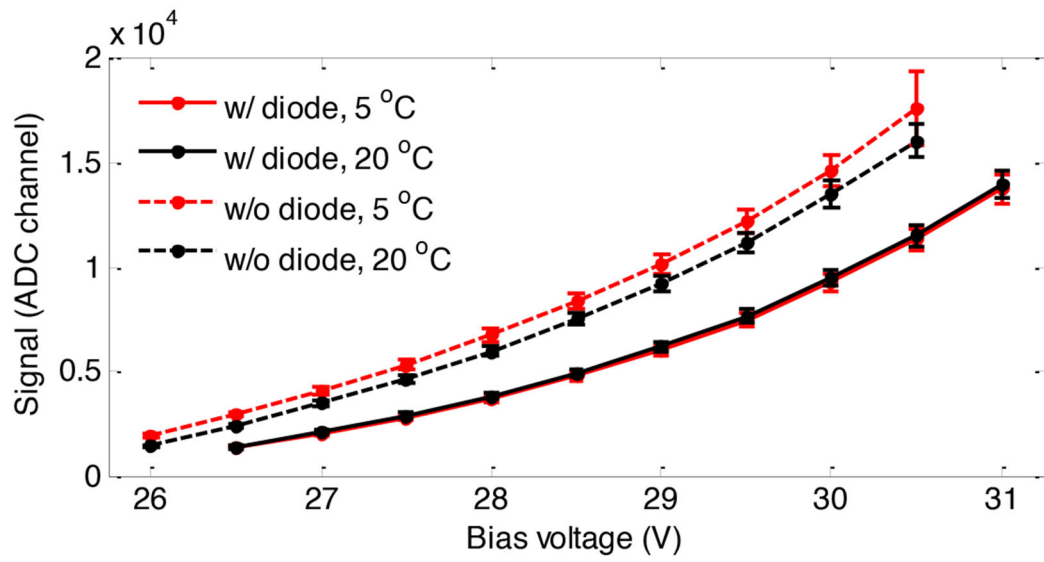
(a) position profile of the 22nd crystal row of the flood histograms at 5 °C shown in figure 6

and (b) the flood histogram quality versus bias voltage, temperature and readout method.

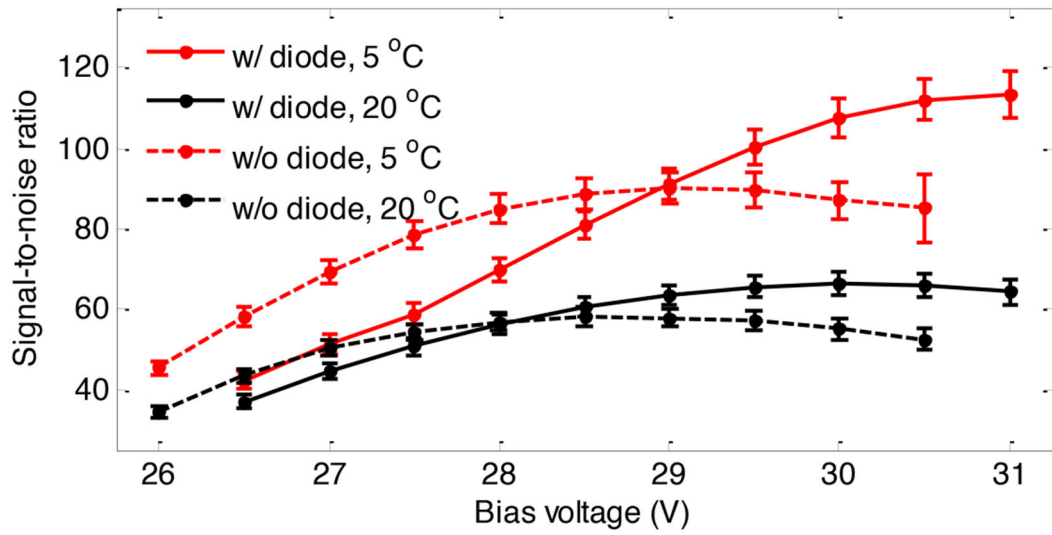
The error bars represent the standard deviation across all the crystals.



(a)

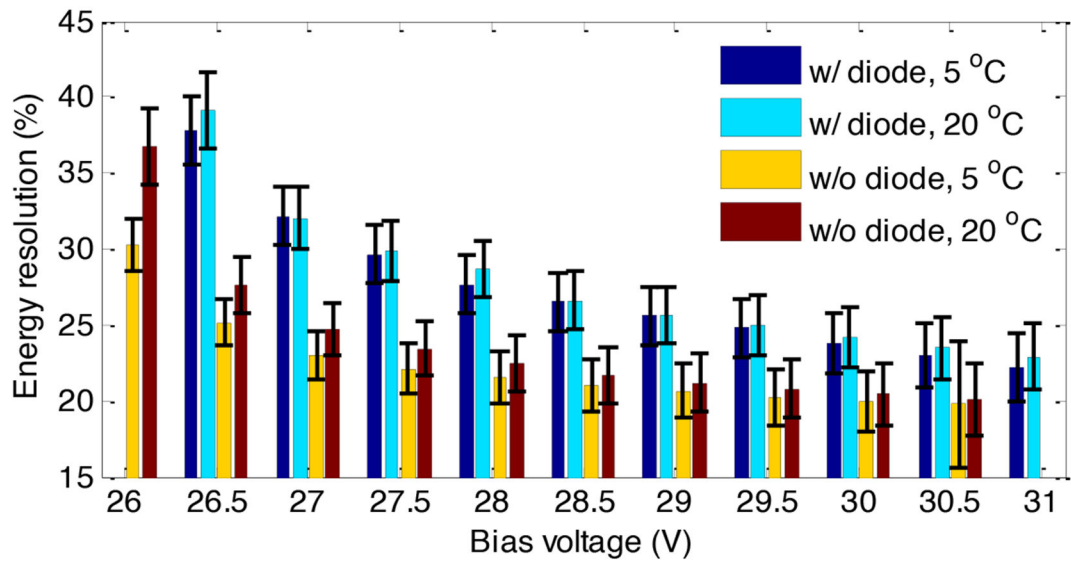


(b)

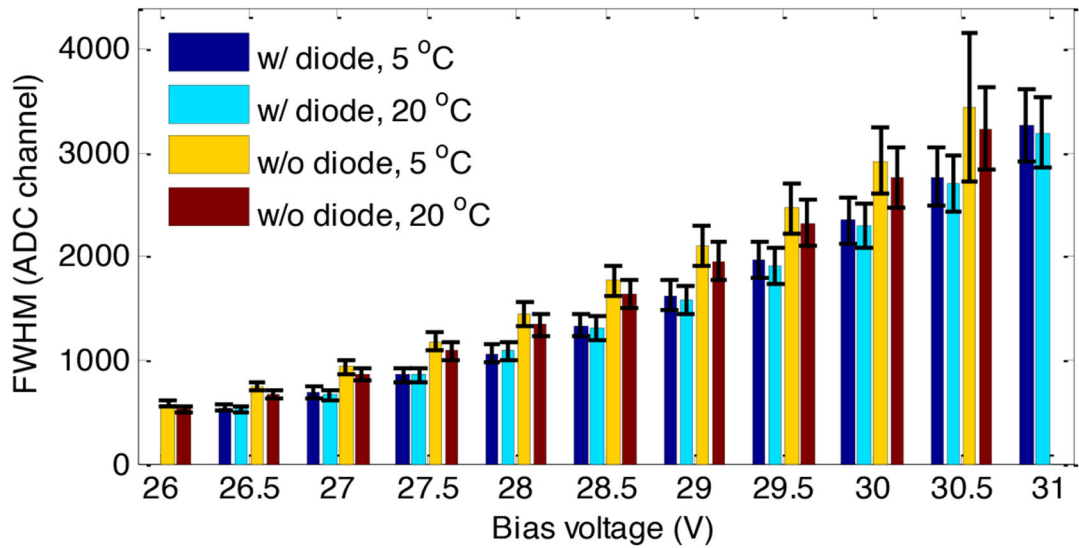


(c)

Figure 8. (a) noise, (b) signal and (c) SNR versus bias voltage, temperature and readout method.

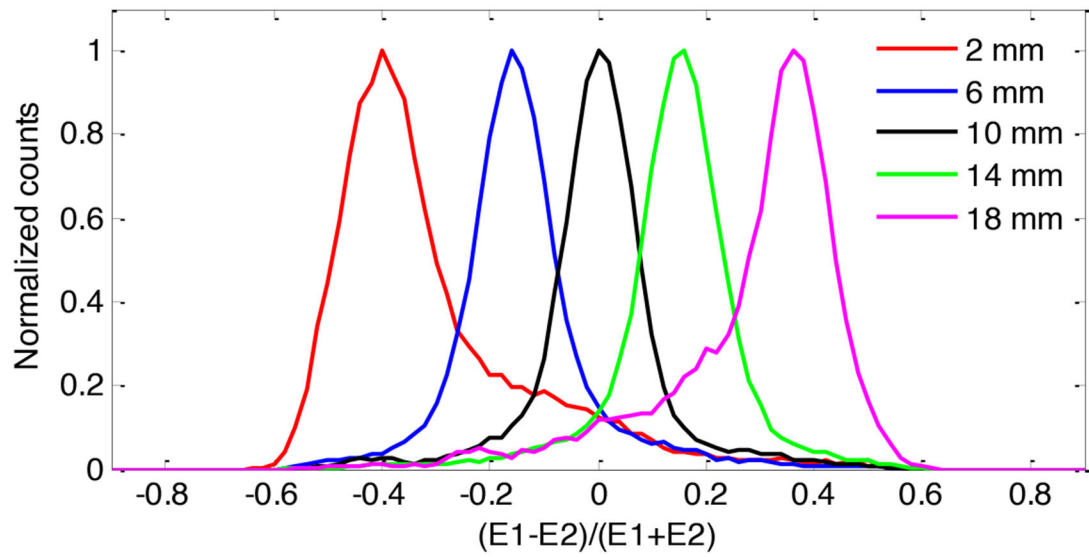


(a)

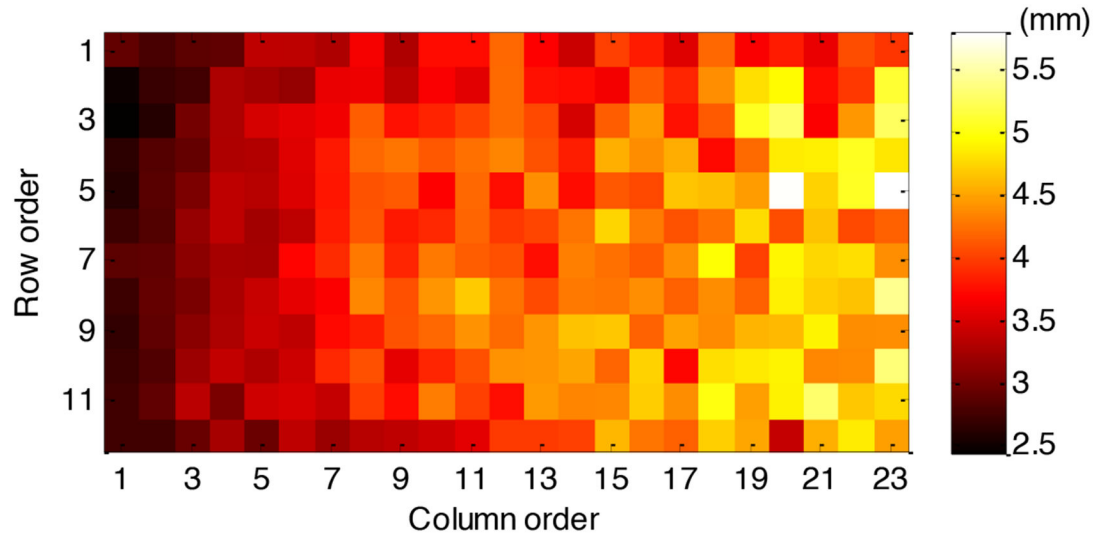


(b)

Figure 9. (a) energy resolution and (b) average FWHM versus bias voltage, temperature and readout method.



(a)



(b)

Figure 10.

(a) Histogram of DOI ratio of an edge crystal for different depths, and (b) DOI resolution measured for each crystal.

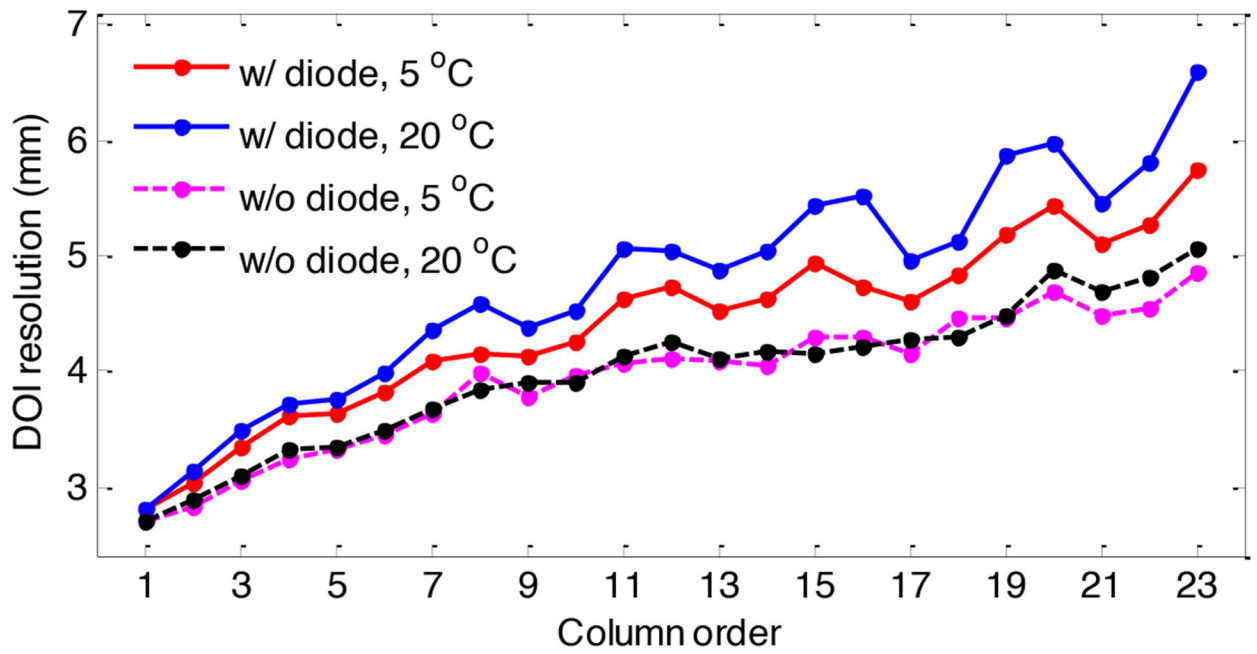


Figure 11.
Average DOI resolution for all 23 crystal columns measured.

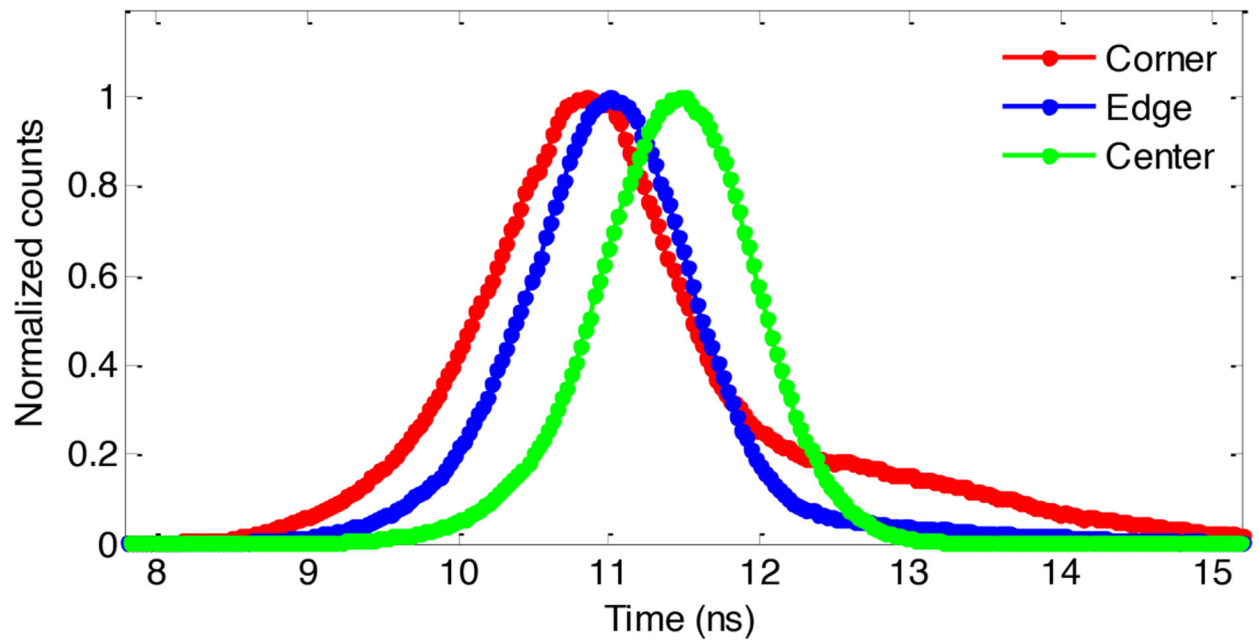


Figure 12.
Timing spectra of three crystals, obtained at a bias voltage of 30.0 V and a temperature of 5 °C using the diode readout method.

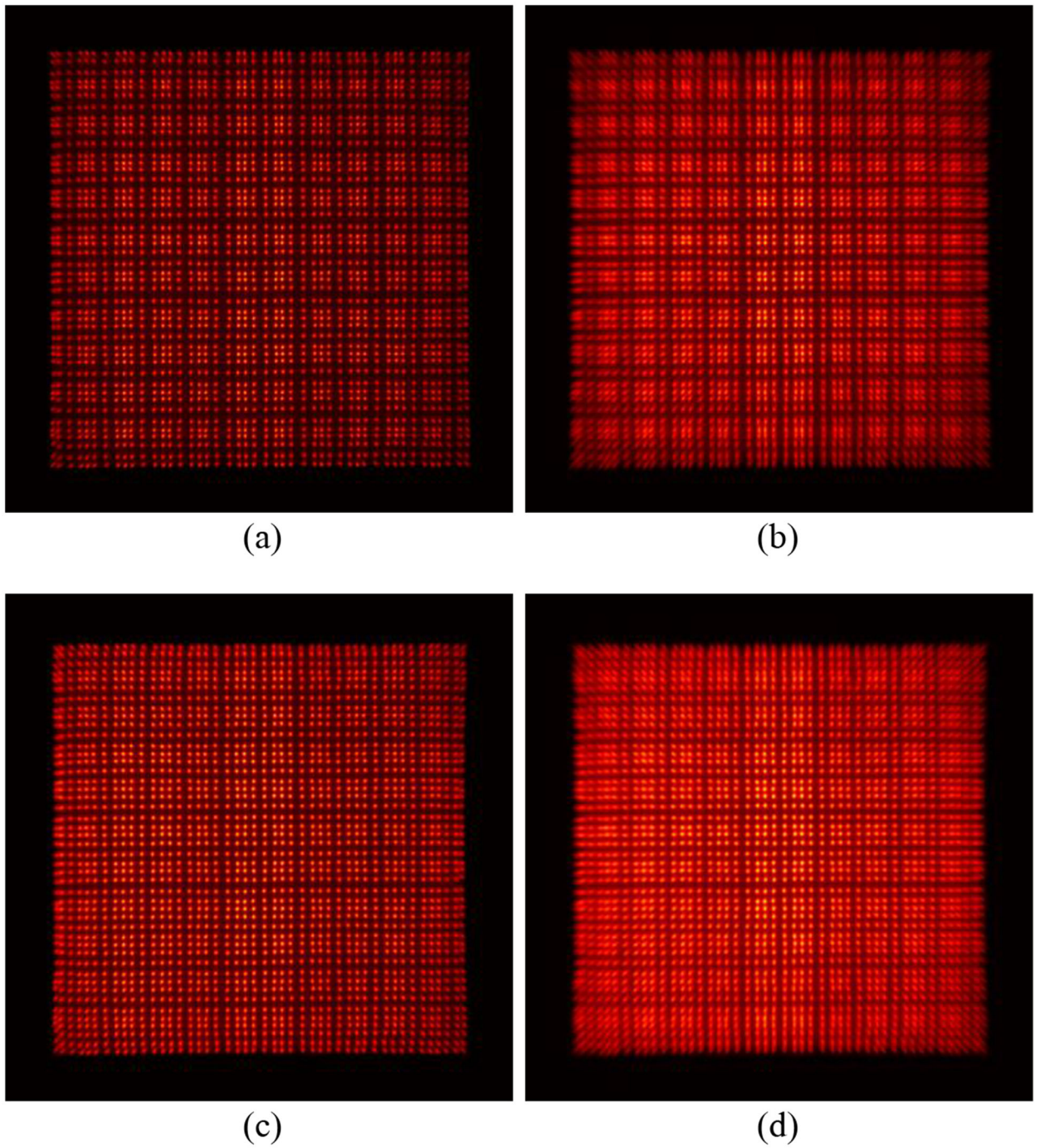


Figure 13. Flood histograms obtained at event rates of (a) 39.8 k/s and (b) 142.0 k/s using diode readout method. Flood histograms obtained at event rates of (c) 29.6 k/s and (d) 131.8 k/s using standard readout method.

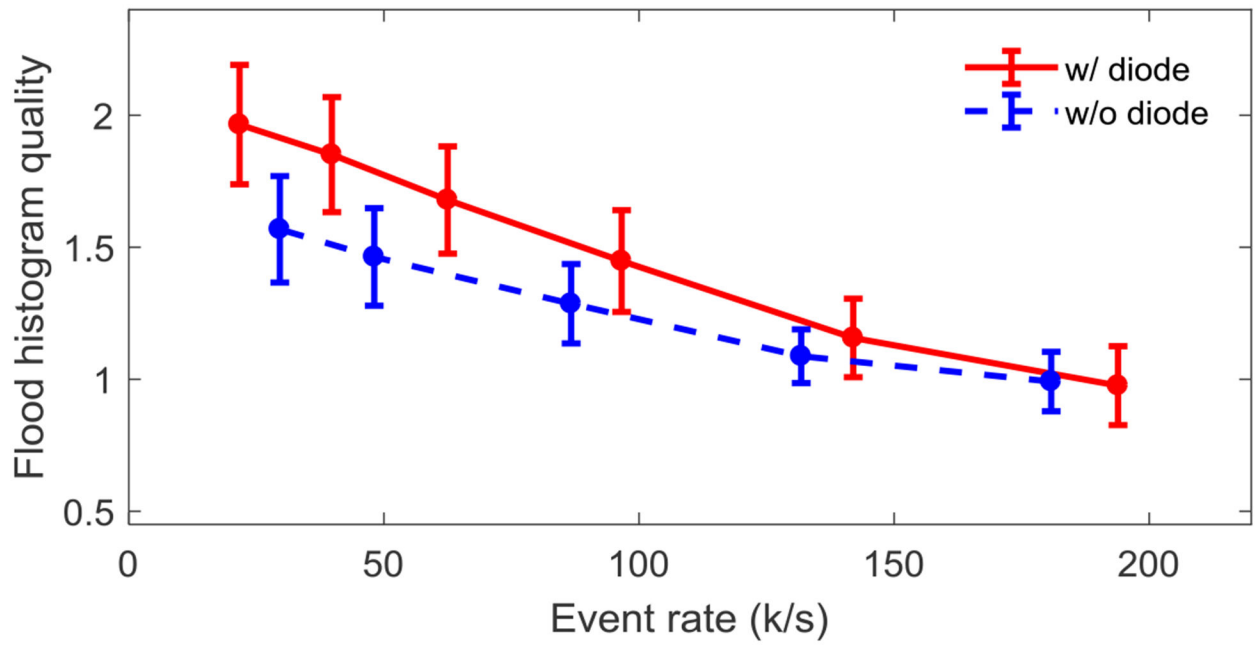


Figure 14.
Flood histogram quality versus event rate.

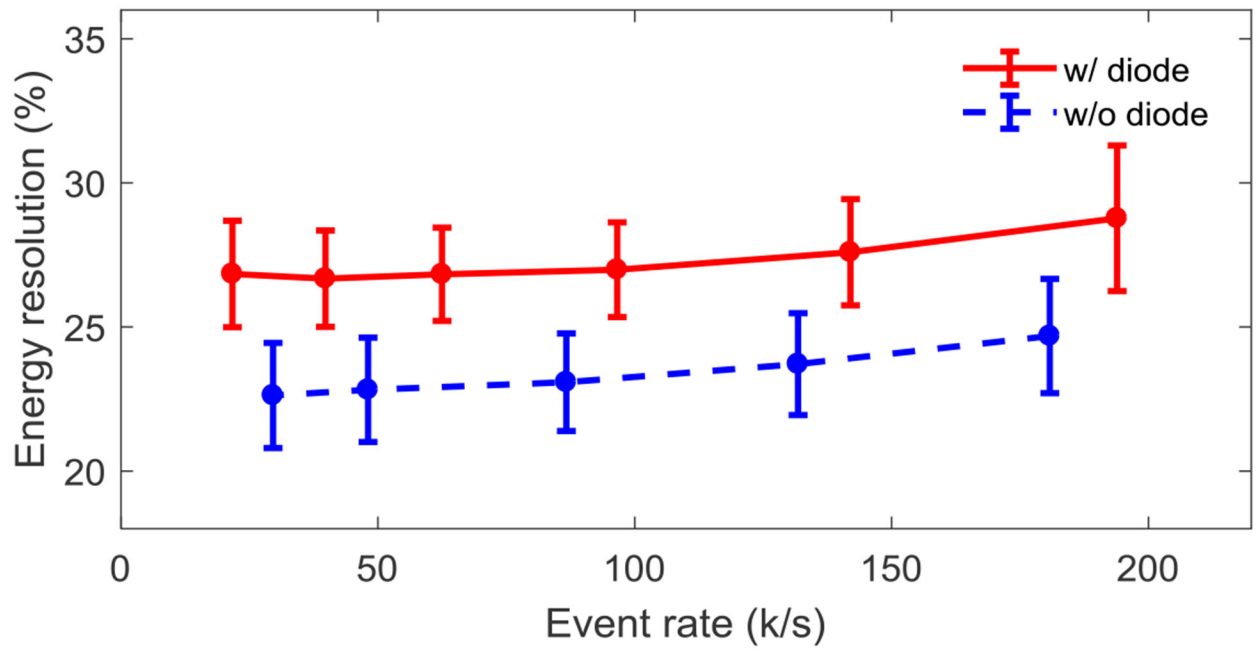


Figure 15.
Energy resolution versus event rate.

Table I.

Flood histogram quality

Temperature (°C)	Flood histogram quality	
	w/ diode	w/o diode
5	1.54 ± 0.17	1.29 ± 0.16
20	1.28 ± 0.15	1.13 ± 0.12

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Table II.

Average energy resolution obtained at the optimal bias voltage for the flood histogram.

Temperature (°C)	Average energy resolution (%)	
	w/ diode	w/o diode
5	23.82 ± 2.0	21.52 ± 1.74
20	24.21 ± 2.0	22.44 ± 1.82

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Table III.

Average DOI resolution of crystals in the first column

Temperature (°C)	Average DOI resolution (mm)	
	w/ diode	w/o diode
5	2.81 ± 0.13	2.69 ± 0.14
20	2.82 ± 0.13	2.71 ± 0.09

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Table IV.

Average timing resolution

Temperature (°C)	Average timing resolution (ns)	
	w/ diode	w/o diode
5	1.63 ± 0.08	1.75 ± 0.17
20	1.78 ± 0.09	2.04 ± 0.18

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