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Insights into the Dielectric Loss Mechanism of Bianisotropic FeSi/SiC Composite Materials

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technique sheds new light on the ion diffusion mechanism in the metallic composite materials.

INTRODUCTION

The absorption of electromagnetic (EM) waves by the materials, especially coming from the RADAR is the crucial requirement for the development of the stealth technologies.^{1,2} In principle, the higher loss of the materials transformed the incident EM waves into heat energy.³ The typical household application of technology is a microwave oven. Here, orientational polarization of the electric dipoles of the water molecules generates heat energy within the food items because of the applied alternating EM field.⁴ However, over a long period silicon carbide was found to be the most suitable material for industrial applications because of its smaller absorption magnitude as well as the thinner width of the absorption.⁵ Nevertheless, these materials were widely used as a supplementary material because of their single absorption capacity. Hence, in the search for primary absorbing materials, they need to have higher permeability as well as higher dielectric loss. $^{6-10}$ Here, the role of the higher permeability forces the EM wave passes through the material compulsorily.¹¹ In contrast, the role of the higher dielectric loss is to convert the EM waves into other forms of energy, for instance, heat energy to absorb the EM wave completely.¹²⁻¹⁵

Several approaches have been taken to date to achieve the above criteria. For instance, Liu et al.¹⁶ chose FeSi powder as an absorbing material. They milled the spherical shape particles of FeSi alloy for several hours to achieve a flaky shape. Because of the flaky shape of the 12 h milled FeSi powder, they

reported an increase of permeability values. It also suggested mixing paraffin along with the FeSi powder to make a composite with having higher permeability along with the higher dielectric loss with the resonant frequency within the L-S band.¹⁷

Hence, ferromagnetic FeSi alloy is a perfect material for the primary absorbing material because of its higher permeability values with soft nature.^{18–20} However, Snoek's limit put constraints in increasing the permeability values as it directly affects the resonant frequency.²¹ Therefore, if we try to enhance the permeability values, it may result in the depletion of the resonant frequency sometimes under the microwave frequency. On the other hand, if we add SiC along with the FeSi alloy powder may result in higher dielectric loss along with the high permeability and high permittivity.

Hence, we investigated the dielectric effect of SiC on the flaky FeSi alloy composite powder within the phase limit using ball milling techniques to enhance its loss factor.

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EXPERIMENTAL DETAILS

Synthesis. FeSi powders synthesized commercially with gas atomization techniques were acquired as the primary absorbing material with a mesh size of 150. The composition study showed that it had 6.02 wt % silicon, 0.04 wt % chromium, and balance iron. The raw powders mixed with the SiC (99.9%, Alpha Chemika) with 2.5, 5.0, and 7.5 wt %, namely, FeSi@ 2.5%SiC, FeSi@5%SiC, and FeSi@7.5%SiC, respectively, within the phase purity limit. The mixed powders placed inside polyvinyl jars along with yttrium-stabilized ZrO₂ balls. The ball to powder ratio was maintained at a value of 25:1 and wet milling was performed in ethanol medium for 7 days at 150 rpm speed. After milling, wet powders were collected and washed several times with ethanol and finally dried in the final form in a hot air oven for 12 h at 60 °C temperature. Pellets with 1.1 cm diameter and 0.17 cm thickness obtained with a uniaxial pressing with 4 tons of pressure for 10 min.

Characterization. Bruker D8 Advance powder X-ray diffraction (XRD) was utilized to find the limit of phase purity of the materials within the $30^{\circ} \le 2\theta \le 80^{\circ}$ values. The indexing performed comparing with the PDF-2 (2018) database. The flaky shape of the particles along with the composite type of powders performed with scanning electron microscopy (SEM) techniques (Hitachi S 3500). The pellets painted with the silver paste. The dielectric and impedance properties determined with a Hioki IM3536 LCR meter within the 4 Hz to 8 MHz range of frequencies.

RESULTS AND DISCUSSION

The XRD patterns for the pure and composite powders are shown in Figure 1. The reflection peaks were obtained for the



Figure 1. XRD pattern for the FeSi/SiC composite powders.

(110) and (200) miller indices planes only.¹⁶ This suggests a high crystallinity nature along with the absence of any spurious secondary peaks up to 7.5 wt % for the FeSi@7.5%SiC composite powder. It also suggests that long hours of the milling process did not initiate any chemical decomposition in the composite matrices. However, with the increase of the SiC content peak broadening along with the reduced intensity of the peaks are visible. The peaks also shifted to the high value of Bragg angles with the SiC content. These suggested that a lower atomic radii of Si (1.18 Å) than that of the Fe (1.24 Å) and caused distortion because of the shrinkage of the lattice

structure. Hence, the increased defect density may be responsible for the peak shifting as well as the peak broadening phenomenon. The $D \cdot \beta \cos \theta = n\lambda$ formula of Debye–Scherrer was utilized to determine the distribution of the particle size from the intensity peaks of the XRD data.²² Here, diffraction peak width β obtained from the full width at half-maximum value of the (110) plane and $\lambda = 1.5418$ Å. The distribution result suggests 10.46, 28.2, and 60.33% presence of the D10, D50, and D90 size of the particles. The obtained value of the bulk density was found to be 3.92 g/cm³ for the FeSi in good agreement with the literature.²³

The SEM-energy-dispersive X-ray (EDX) analysis of the samples is presented in Figure 2. The brittle nature of the FeSi



Figure 2. SEM-EDX analysis for (a) FeSi and (b) FeSi@5%SiC powders.

alloy powder is visible here with heterogeneous sizes because of long hours of milling. The composite nature of the FeSi@ 5%SiC powder was observed at the inset of Figure 2b. Here, the SiC particles provided a lamellar outer layer sandwiched with FeSi central cores. The presence of the SiC was also detected in the elemental analysis with EDX. The same has not been observed in the XRD till the 7.5 wt % of SiC because of the high degree of crystallinity of the FeSi primary phases. The presence of the secondary SiC phases around the surface of the FeSi primary phases also initiated shape bianisotropy.²⁴ Hence,

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it may lead to the quick magnetization as well as the effects the complex permittivity of the composite powders.

The graph of the real and imaginary parts of permittivity at room temperature with the frequency is presented in Figure 3.



Figure 3. (a) Real and (b) imaginary parts of permittivity vs frequency for FeSi/SiC powders. The solid lines represent the fitting of the dielectric data with the Cole–Cole relaxation model.

The composite materials here show more enhanced dielectric properties than the pure FeSi alloy. In general, the lowfrequency dielectric constants directly depend on the orientational polarization mechanism, whereas the atomic and electronic contribution to the dielectric constant comes at the optical frequency regions. Hence, with an application of the alternating field at a low-frequency region, the electric dipoles try to follow toward the direction of the field. The addition of SiC in the composite material generates additional dipole presence inside the material. At the same time, the pure FeSi powder contains a single dipolar mechanism. Therefore, the real part of permittivity at lower frequencies for the FeSi@5% SiC and FeSi@7.5%SiC materials exhibited nearly 10⁴ times higher permittivity than that of the pure FeSi powders. When the applied alternating electric field changes direction, the dipoles also try to change the direction with the applied field known as the relaxation mechanism.²⁵ This leads to the loss inside the material. The presence of the distributed relaxation mechanism leads to the higher loss inside the material; hence, in this work, FeSi@7.5%SiC exhibited maximum dielectric loss.

With the increase of the frequencies, the dipoles failed to align themselves with the alternating electric field; hence, the orientational polarization contribution to the dielectric behavior also minimizes.

The single relaxation mechanism of the pure FeSi powders is represented by the Debye $model^{26}$

$$\varepsilon^* = \frac{\varepsilon_0' - \varepsilon_{\infty}'}{1 + i\omega\tau} + \varepsilon_{\infty}' \tag{1}$$

Whereas the distributed relaxation mechanism for the composite bianisotropic material follows the Cole–Cole model^{27}

$$\varepsilon^* = \frac{\varepsilon'_0 - \varepsilon'_{\infty}}{1 + (i\omega\tau)^{1-\gamma}} + \varepsilon'_{\infty}$$
⁽²⁾

Here, the stretching component of the relaxation behavior expressed with the $1 - \gamma$ terms in the equation. The resonance phenomenon is said to happen if the magnitude of the $1 - \gamma$ term exceeds the value of unity. To fit the dielectric data of the composite material, the eq 2 is extended to its trigonometric form as²⁸

$$e^{*} = \frac{(\varepsilon_{0}' - \varepsilon_{\infty}') \left((\omega \tau)^{1-\gamma} \sin\left(\frac{\pi \gamma}{2}\right) + 1 \right)}{1 + 2(\omega \tau)^{1-\gamma} \sin\left(\frac{\pi \gamma}{2}\right) + (\omega \tau)^{2(1-\gamma)}} + \varepsilon_{\infty}'$$
(3)

Hence, we fitted the composite material dielectric data with the eq 3. The fitting results indicated that the value of the stretching component equals to the 0.58, 0.62, and 0.68 for the FeSi@2.5%SiC, FeSi@5%SiC, and FeSi@7.5%SiC, respectively. This indicates that the spectra are within the relaxation mode and can be extendable to GHz frequency for the spectra to behave in the resonance mode. They are indicating well below the Snoek's limit. Hence, the bianisotropic composite material can have high permeability and high permittivity well below the Snoek's limit.

Moreover, the impedance characteristics of the pure and composite material are presented in Figure 4. It is observed



Figure 4. (a) Impedance characteristics of the pure and composite materials. Inset shows the fitting result obtained with (b) equivalent circuit for the FeSi@7.5%SiC samples.

that the pure FeSi resulted in a poorly resolved semicircle impedance spectrum. However, with the addition of SiC the semicircle arcs start forming and finally resolved into a clear semicircular arc for the FeSi@7.5%SiC samples. Here, the proposed equivalent circuit for the FeSi@7.5%SiC samples is shown in Figure 4b. The significance of the R_2 term is purely ohmic resistance where the dispersion behavior resulted because of the constant phase element part. The Warburg element signifies diffusive nature.²⁹ Hence, impedance data fitted well for the diffusive contribution of the SiC material in the FeSi@7.5%SiC samples, as shown in the inset of Figure 4a. Hence, the diffusion of ions resulted in a higher loss in the FeSi@7.5%SiC material.

CONCLUSIONS

In summary, FeSi/SiC composite materials were prepared with a mechanical ball milling method along with commercially available FeSi alloy powders. The uniform dispersion of the FeSi alloy into the SiC materials formed a bianisotropic nature into the composite materials. The SiC particles provided a lamellar outer layer sandwiched with FeSi central cores. The incorporation of additional SiC electric dipoles and ion diffusion mechanism into the composite resulted in 10⁴ times of dielectric loss inside the material with respect to the pure FeSi alloy powder. Hence, the material can absorb a broad part of the EM wave to transform it into the heat energy efficiently. The Cole-Cole relaxation mechanism confirms the presence of the stretching component well below the resonance within the Snoek's limit. The presence of the Warburg capacitance leads to the ion diffusion through the FeSi/SiC composite materials for higher losses. Hence, it is possible to obtain a high magnitude of permeability and permittivity FeSi/SiC materials for the efficient absorption of EM waves to tackle the EM pollution.

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Notes

The authors declare no competing financial interest.

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