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Effect of thermal treatment at high temperature on phase stability and transformation of Yb_2O_3 and Y_2O_3 co-doped ZrO_2 ceramics

Zheng Cao^{1,2}, Shengli An^{1,2,3}✉ & Xiwen Song^{2,3}

Y_2O_3 doped ZrO_2 (YSZ) ceramic material is used to protect alloy components worked in high-temperature. But its phase transformation between tetragonal phase and monoclinic phase occurred at 1150 °C leads to YSZ invalid. Therefore, enhancing the phase stability of YSZ is necessary for meeting the demands of the development of thermal barrier coatings (TBC). In this study, X-ray diffraction and Raman spectra were used to explore the phase stability and phase transformation of Yb_2O_3 and Y_2O_3 co-doped ZrO_2 (YbYSZ) ceramics after heat treatment at 1300 °C with different times. The stability of tetragonal phase is improved by tetragonality decreasing with Yb^{3+} doped. Simultaneously, the incorporation of Yb^{3+} leads to O–O coupling, which is beneficial for increasing the concentration of oxygen vacancies near the substituted ions, thereby improving the stability of the crystal. The 6.5YbYSZ ceramic has the best stability after heat treatment at 1300 °C for different times.

More efficient engineering components for applications in the energy, automotive, aerospace, electronics, and power industries are desired in the current competitive world economy. Thermal barrier coatings (TBCs) are usually used to protect those components that operate in high-temperature, corrosion, or other harsh environments^{1,2}. TBCs are composed of two important layers: metal bond coat and ceramic top coat. Metal bond coat always uses MCrAlY (M = Ni, Co, Ni + Co, etc.) alloy to protect the components from oxidation and corrosion, while ceramic top coat acts as an insulator^{3,4}. Being in direct contact with the harsh working environment, ceramic top-coat should have lower thermal diffusivity, better performance on phase stability and thermal shock resistance during thermal cycling, as well as better oxidation and corrosion resistance^{5,6}. 6–8 wt% Y_2O_3 partially stabilized ZrO_2 (YSZ) as the most promising choice of ceramic top coat shows outstanding comprehensive performance in thermal conductivity, phase stability, and other aspects^{5,7,8}. However, when the operating ambient temperature exceeds 1200 °C, the tetragonal (t) phase transforms to the monoclinic (m) phase, which is accompanied by a volume expansion of 3–5%, leading to detrimental cracks in coatings^{9,10}. Moreover, at high temperatures (exceeds 1200 °C), the pores inside the YSZ coatings undergo shrinkage, particularly those perpendicular to the heat flow, thus resulting in a significant increase in the thermal conductivity of TBCs^{11–14}.

Therefore, the research and development of lower thermal conductivity and more stable top coat ceramic materials at high temperatures are urgently needed for the development of new-generation gas turbines. Numerous studies have shown that doping rare earth oxides (RE_2O_3) with different atomic masses or radii into YSZ systems is an effective method for improving thermal insulation performance and high-temperature phase stability^{15–19}. Stecura et al.²⁰ explored the thermal cycle life of Yb_2O_3 -stabilized ZrO_2 system at 1120 °C and found that the thermal cycle failure modes of Yb_2O_3 - ZrO_2 and Y_2O_3 - ZrO_2 were similar, but the thermal cycle life of Yb_2O_3 - ZrO_2 was significantly better than that of YSZ. By comparing the phase stability of Yb_2O_3 and Y_2O_3 co-stabilized ZrO_2 at 1450 °C, Caireny et al.²¹ found that the addition of Yb could efficiently improve the phase stability. Jing et al.²² studied 3–10 mol% Yb_2O_3 -stabilized ZrO_2 ceramics and found that the ceramics consisted with the metastable tetragonal phase (t') and had lower thermal conductivity. Leilei et al.²³ systematically studied the effects of Yb_2O_3 and Y_2O_3 co-doped in ZrO_2 on the phase stability and thermal conductivity. Their results

¹School of Metallurgy and Ecological Engineering, University of Science and Technology Beijing, 30 Xueyuan Road, Beijing 100083, China. ²Inner Mongolia Key Laboratory of Advanced Ceramic Materials and Devices, Inner Mongolia University of Science and Technology, 7 Arding Street, Baotou 014010, China. ³School of Materials and Metallurgy, Inner Mongolia University of Science and Technology, 7 Arding Street, Baotou 014010, China. ✉email: shengli_an@126.com

showed that co-doped ZrO_2 had better phase stability and lower thermal conductivity than those of Yb_2O_3 - or Y_2O_3 -doped ZrO_2 ceramics. Lei and his colleagues^{16,24,25} prepared 1 mol% RE_2O_3 (RE = La, Nd, Gd) and 1 mol% Yb_2O_3 -co-doped YSZ (1RE1Yb-YSZ) ceramics and 3.5 mol% RESZ (RE = Dy, Y, Er, Yb) ceramics by a chemical co-precipitation method. They found that all the prepared ceramics were composed of t' phase. The phase stability and thermal conductivity of 1RE1Yb-YSZ decreased with the increase of RE^{3+} ion radius, whereas the fracture toughness of 3.5 mol% RESZ showed the opposite trend. In addition, the corrosion resistance of a GdYb-YSZ ceramic was better than that of YSZ.

This study is based on the better performance of YbYSZ system. X-ray diffraction and Raman spectra are used to explore the phase composition and phase transformation of ceramic samples heat-treated at 1300 °C for different times.

Experimental procedure

Material preparation. x mol% $\text{YbO}_{1.5} - (8.5-x)$ mol% $\text{YO}_{1.5} - \text{ZrO}_2$ ($x=0, 2.5, 4.5, 6.5,$ and 8.5 , denoted as $x\text{YbYSZ}$) ceramics were prepared by a solid-state reaction method. Y_2O_3 , Yb_2O_3 , and ZrO_2 (99.9%, Zhongnuo New Material Technology Co. Ltd.) were used as raw materials. All oxide powders were calcined at 800 °C for 5 h to eliminate the influence of absorbed water before mixed. Then, the oxides weighed with stoichiometric ratios were milled by two steps. First step was to mix-up all raw materials and pulverize the oxides to micron scale by ball milling. The second step was to further refine the precursor mixed oxide slurry, which was milled in a high-energy ball mill at 2300 rpm, 2500 rpm, and 2700 rpm for 3 h respectively to obtain a nanoscale mixture. The slurry after two grinding steps was completely dried at 80 °C and then sintered at 1450 °C for 3 h to obtain the initial ceramic samples.

Experiment of heat treatment. All initial ceramic samples were heat-treated in a muffle furnace at 1300 °C for 9, 33, 93, 143, 208, 287 and 358 h and then cooled to room temperature at a rate of 10°/min.

Structural characterization and analysis. X-ray diffraction (XRD, Rigaku Smart Lab II, Japan) and Raman spectroscopy (Raman, Horiba, Japan) were used to identify the phase composition and structure of initial ceramic samples and heat-treated ceramic samples. The XRD scans from 20° to 80° at a scan rate of 5°/min with Cu K α radiation ($\lambda=0.15418$ nm). The Raman scans from 100/60 cm^{-1} to 800 cm^{-1} with a green laser (532 nm).

Results and discussion

Phase composition and structure of initial ceramic samples. The XRD patterns of $x\text{YbYSZ}$ ($x=0, 2.5, 4.5, 6.5,$ and 8.5) ceramics are presented in Fig. 1. As shown in Fig. 1a, the diffraction peaks correspond to two different tetragonal-related PDF cards (PDF Nos. 70-4426 and 70-4430). The PDF cards can be defined as metastable (PDF#4430, t') and stable (PDF#4426, t) tetragonal zirconia phase due to the difference in lattice parameters^{26,27}. Therefore, the XRD patterns suggest that Yb^{3+} and Y^{3+} have completely dissolved into ZrO_2 lattice and formed t and t' phases. In addition, the positions of the diffraction peaks shift to high angles with the content of Yb^{3+} increasing (Fig. 1b), which means cell shrinkage. To further investigate the effect of Yb and Y co-doped on phase composition and crystal structure, GSAS software was applied to refine the XRD patterns^{28,29}. By comparing the phase content of t phase and t' phase shown in Fig. 1c, the content of t' phase increased from 47.5 to 55.5% with the increase of Yb^{3+} . The increase of t' phase is beneficial for improving phase stability of ceramics. Figure 1d displays the tetragonality of t and t' phase, it can be found that the tetragonality of t and t' phase showed an opposite trend with the increase of Yb^{3+} , and the addition of Yb^{3+} has a greater influence on the tetragonality of t phase. The reduction of tetragonality of t phase is beneficial to inhibit the phase transition from the t phase to the m -phase.

Raman spectra is sensitive to chemical bonds and other short-range ordered structures in the crystal³⁰. Therefore, Raman spectra of $x\text{YbYSZ}$ ($x=0, 2.5, 4.5, 6.5,$ and 8.5) ceramics showed in Fig. 2 is used to analyze the lattice distortion of samples. Raman spectra of all ceramic samples consist of six vibration modes related with tetragonal phase and metastable tetragonal phase, and no monoclinic phase was detected^{26,31,32}. Table 1 displays Raman shift of all ceramics. The incorporation of Yb^{3+} has a greater effect on Raman shift of I_5 , and the coexistence of Yb^{3+} and Y^{3+} ceramic samples have much lower Raman shift. I_5 is related with chemical bond vibration mode of O–O coupling. Therefore, the $x\text{YbYSZ}$ ($x=2.5, 4.5$ and 6.5) ceramics samples are easier to form larger-scale defect clusters, which can improve the resistance of phase transformation controlled by diffusion.

Phase composition of $x\text{YbYSZ}$ ($x=0, 2.5, 4.5, 6.5,$ and 8.5) after heat treatment for different times. Figure 3 represents the variation of XRD patterns and Raman spectra of 8.5YSZ ceramics after heat-treated with 33, 93, 143, 208, 278 and 358 h. According to Fig. 3a, the intensities of $m(-111)$ and $m(111)$ peaks increased dramatically after heat treatment for 143–208 h. Furthermore, after heat treatment for 208 h, the characteristic peaks of t and t' phases of the tetragonal phase were hardly observed (see Fig. 3b). According to the phase diagram of Y_2O_3 - ZrO_2 ³³, 8.5YSZ was located in the coexisting phase region of the t and c phases. Therefore, the metastable t' phase is decomposed to the equilibrium t and c phases, and then the t phase transforms to the m phase when the ceramics were heat-treated for a long time. The Raman spectra shown in Fig. 3c further displays that the relative peaks of m phase are appeared with the passage of heat treatment time.

According to the previous discussion on the influence of the coexistence of Yb^{3+} and Y^{3+} on the crystal, 6.5YbYSZ ceramic sample is special compared with other ceramic samples. Therefore, Fig. 4 exhibits the variation of XRD patterns and Raman spectra of 6.5YbYSZ ceramic sample after heat-treated different time. It can be seen from Fig. 4 that the changes of XRD patterns and Raman spectra of 6.5YbYSZ ceramic sample are the same

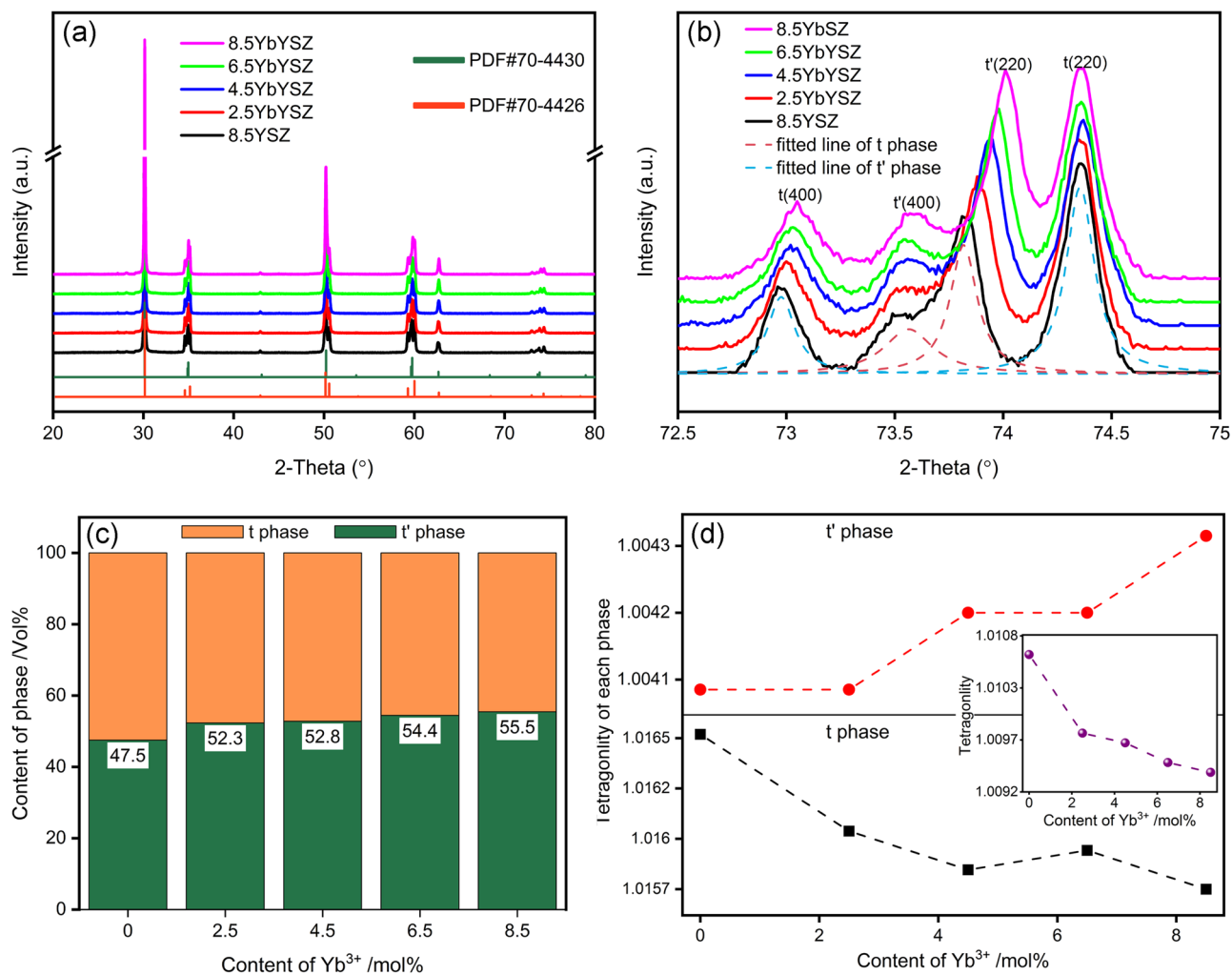


Figure 1. XRD patterns of $x\text{YbYSZ}$ ($x=0, 2.5, 4.5, 6.5, \text{ and } 8.5$): (a) $2\theta=20^{\circ}\text{--}80^{\circ}$ at a scan rate of $5^{\circ}/\text{min}$, (b) $2\theta=72.5^{\circ}\text{--}75^{\circ}$ at a scan rate of $1^{\circ}/\text{min}$; (c) phase content and (d) tetragonality of t phase and t' phase.

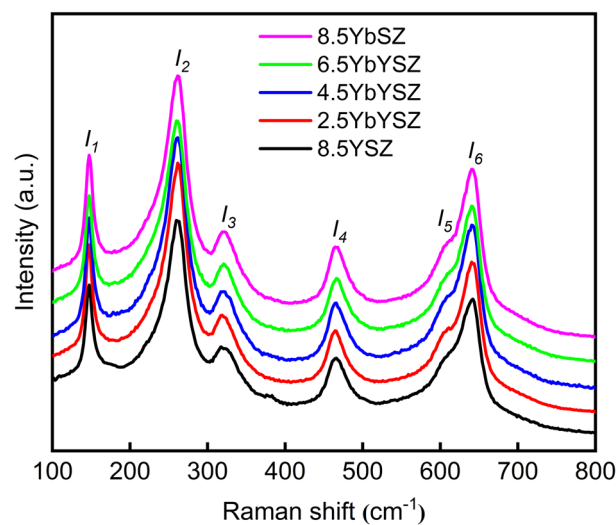


Figure 2. Raman spectra of $x\text{YbYSZ}$ ($x=0, 2.5, 4.5, 6.5, \text{ and } 8.5$) ceramics.

Samples	Raman shift (cm ⁻¹)					
	I ₁	I ₂	I ₃	I ₄	I ₅	I ₆
8.5YSZ	147	260	325	467	620	642
2.5YbYSZ	147	260	325	467	618	642
4.5YbYSZ	147	259	324	467	617	642
6.5YbYSZ	147	259	324	465	613	642
8.5YbSZ	147	260	325	467	619	642

Table 1. Raman shift of xYbYSZ (x = 0, 2.5, 4.5, 6.5, and 8.5) ceramic samples.

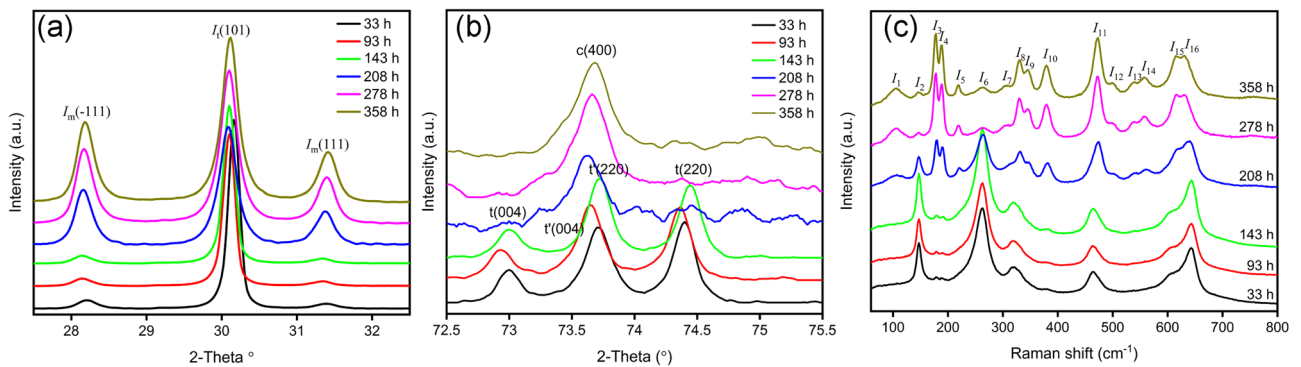


Figure 3. XRD patterns (a) $2\theta = 27.5^\circ - 32.5^\circ$, (b) $2\theta = 72.5^\circ - 75.5^\circ$, and (c) Raman spectra of 8.5YSZ ceramics after heat treatment for different times.

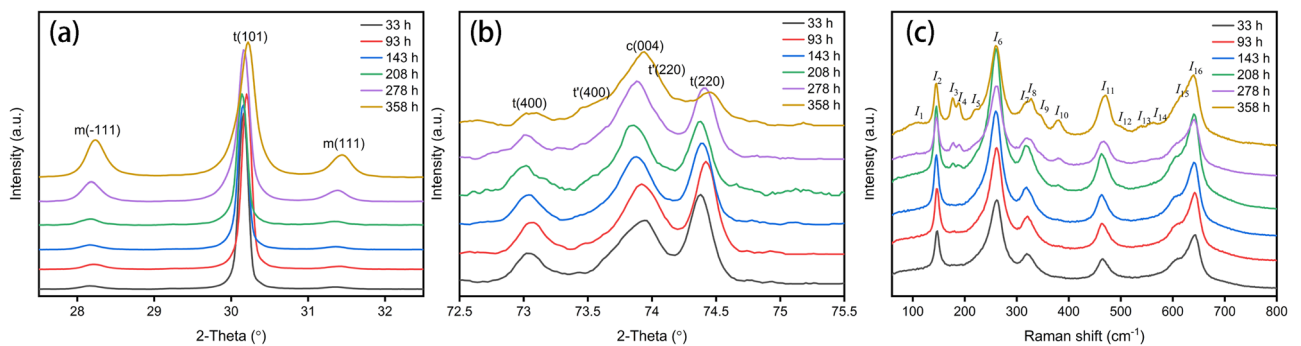


Figure 4. XRD patterns (a) $2\theta = 27.5^\circ - 32.5^\circ$, (b) $2\theta = 72.5^\circ - 75.5^\circ$, and (c) Raman spectra of 6.5YbYSZ ceramics after heat treatment for different times.

as 8.5YSZ. Meanwhile, the characteristic peaks of t and t' phases shown in Fig. 4 can also be observed after heat treatment for 358 h. Therefore, 6.5YbYSZ ceramic has better phase stability than 8.5YSZ. This result is consistent with above discussion about crystal.

Variation of monoclinic phase composition of xYbYSZ (x = 0, 2.5, 4.5, 6.5, and 8.5) after heat treatment for different times. Monoclinic phase is an important factor to estimate the stability of YSZ ceramic materials. XRD is often used to detect the existence of m phase according to Garvie and Nicholson's equation^{34,35}:

$$X_m = \frac{I_m(\bar{1}11) + I_m(111)}{I_m(\bar{1}11) + I_m(111) + I_t(101)} \quad (1)$$

where I_p^{hkl} is the area of the diffraction peak related to the (hkl) crystal plane.

Figure 5 is the variation of monoclinic phase of xYbYSZ (x = 0, 2.5, 4.5, 6.5, and 8.5) ceramic samples after heat treatment at 1300 °C for 9, 33, 93, 143, 208, 278, and 358 h. It's obvious seen that the addition of Yb³⁺ is beneficial for improving phase stability and 6.5YbYSZ ceramic sample has the best behavior. What's more, the

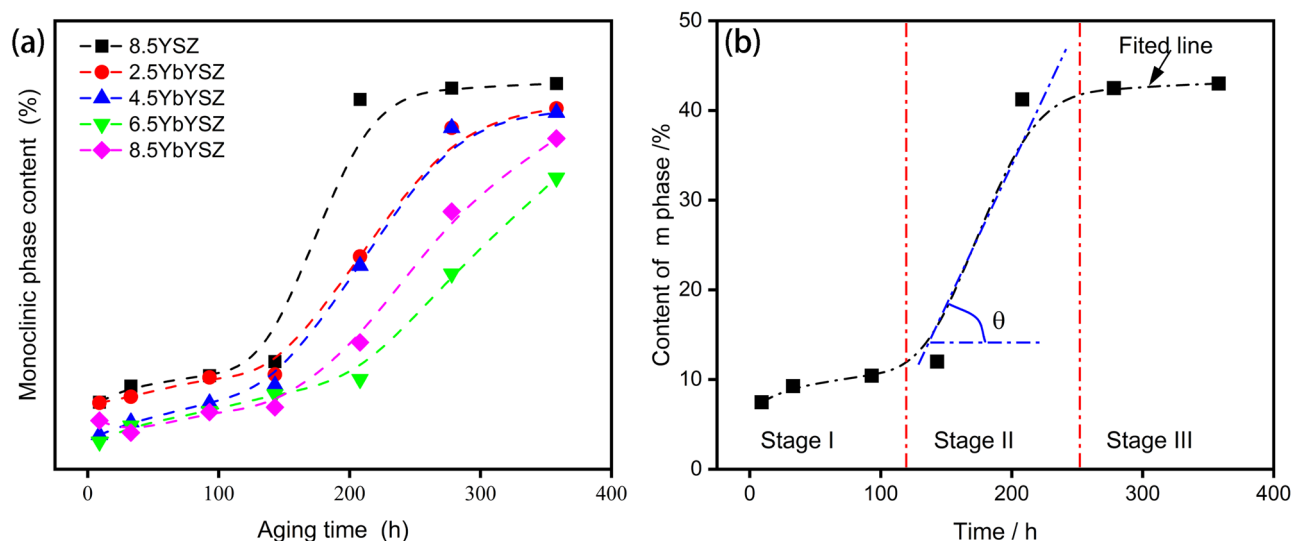


Figure 5. The variation of m phase content of xYbYSZ ceramics (a) and fitted line of the m phase content of 8.5YSZ ceramic (b) after heat treatment at 1300 °C for 9, 33, 93, 143, 208, 278, and 358 h.

relationship between the content of the monoclinic phase and the heat-treated time presents an “S” curve. And the change of monoclinic phase content with different heat-treated time can be divided into three stages (as shown in Fig. 5b): (I) slow increase stage, (II) approximately linear increase stage, and (III) saturation stage. By comparing phase composition of xYbYSZ ($x=0, 2.5, 4.5, 6.5,$ and 8.5) ceramic samples after heat treatment for 33, 93, 143, 208, 278, and 358 h shown in Figs. 3 and 4, all ceramic samples have similarity transition process.

Therefore, monoclinic phase variation of 8.5YSZ ceramic sample was discussed to explore the formation reason of “S” curve. Comparing the XRD patterns of 8.5YSZ shown in Fig. 5b, Stage I was processed with two transition processes. One is the transition from t' phase to t and c phase, and the other one is the transition from initial t phase to m phase. Therefore, Stage I is controlled by the stability of t' phase and t phase. Therefore, the content of m phase in Stage I gradually increases with the prolongation of heat treatment time. The characteristic peaks of t' phase vanished and c phase appeared. While in Stage II, the content of m phase sharply increases, and the characteristic peaks of t phase disappear. The characteristic peaks of c phase have little difference in this stage due to t' phase exhausted in Stage I. Therefore, Stage II is major occurred transition from t phase to m phase, which belongs to martensitic transformation. In Stage III, all transformable phases are exhausted. The content of m phase gets maximized, and Stage III is almost horizontal.

According to previous discussion about crystal structure, the incorporation of Yb^{3+} has effects on O–O coupling, which leads to form large-scale defect clusters difficult to move at high temperature. Meanwhile, the addition of Yb^{3+} is benefit for decreasing the tetragonality of initial t phase, which can improve the stability of t phase. The content of m phase in Stage I of xYbYSZ ($x=2.5, 4.5, 6.5,$ and 8.5) ceramic samples is lower than that of 8.5YSZ ceramic sample. And the duration of Stage I of xYbYSZ ($x=2.5, 4.5, 6.5,$ and 8.5) ceramic samples is longer than that of 8.5YSZ ceramic sample because of the formation of large-scale defect clusters. In Stage II, the content of the m phase transformed from t phase can be fitted as a line, and the slope of fitted line can reflect indirectly the transformability of t phase. As shown in Fig. 6, the slope of fitted line in Stage II is decrease with Yb^{3+} doped, and 6.5YbYSZ ceramic sample has the lowest slope. The transformable t phase comes from two sources, one is the initial t phase after sintered and the other comes from the transformation of t' phase. The initial t phase of 6.5YbYSZ ceramic has better stability. Therefore, only the stability of the t -phase derived from the t' -phase transition needs to be discussed. The enhancement of O–O coupling in 6.5YbYSZ ceramics leads to the redistribution of oxygen vacancies in the crystal. Above all, 6.5YbYSZ has the best phase stability after heat treatment at 1300 °C.

Conclusions

$\text{Yb}_x\text{Y}_{0.085-x}\text{Zr}_{0.915}\text{O}_{2-1.5x}$ ($x=0, 0.025, 0.045, 0.065,$ and 0.085) ceramics were prepared using a solid-state reaction method. The content of t' phase and the tetragonality of t' phase increase with Yb^{3+} incorporation. What's more, the addition of Yb^{3+} is good for enhancing O–O coupling, which leads to formation of large-scale defect clusters.

After the xYbYSZ ($x=0, 2.5, 4.5, 6.5,$ and 8.5) ceramic samples were heat-treated at 1300 °C for 33, 93, 143, 208, 278 and 358 h, the phase stability of the coexisting Yb^{3+} and Y^{3+} ceramic samples was better, and the m phase change showed an “S”-shaped curve. The “S” curve can be divided into three stages.

The decrease of tetragonality of t phase and O–O coupling was beneficial for improving the phase stability. 6.5YbYSZ ceramic showed the best stability performance after heat treatment at 1300 °C.

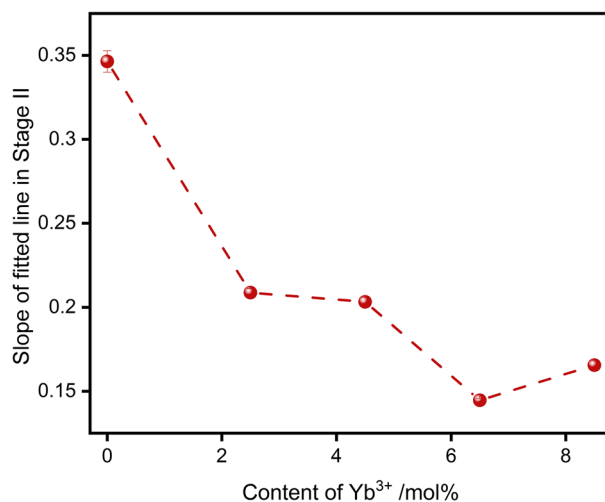


Figure 6. The slope of fitted line in Stage II.

Data availability

All data generated or analyzed during this study are included in this published article, and the datasets used and analyzed during the current study are available from the corresponding author on reasonable request.

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References

- Mondal, K., Nuñez, L., Downey, C. M. & Van Rooyen, I. J. Thermal barrier coatings overview: Design, manufacturing, and applications in high-temperature industries. *Ind. Eng. Chem. Res.* **60**(17), 6061. <https://doi.org/10.1021/acs.iecr.1c00788> (2021).
- Mondal, K., Nuñez, L., Downey, C. M. & van Rooyen, I. J. Recent advances in the thermal barrier coatings for extreme environments. *Mater. Sci. Energy. Technol.* **4**, 208. <https://doi.org/10.1016/j.mset.2021.06.006> (2021).
- Wu, S. *et al.* Research progresses on ceramic materials of thermal barrier coatings on gas turbine. *Coatings* **11**(1), 1. <https://doi.org/10.3390/coatings11010079> (2021).
- Chellaganesh, D., Khan, M. A. & Jappes, J. T. W. Thermal barrier coatings for high temperature applications—A short review. *Mater. Today Proc.* **45**, 1529. <https://doi.org/10.1016/j.matpr.2020.08.017> (2021).
- Cao, X., Vassen, R. & Stoeber, D. Ceramic materials for thermal barrier coatings. *J. Eur. Ceram. Soc.* **24**, 1. [https://doi.org/10.1016/S0955-2219\(03\)00129-8](https://doi.org/10.1016/S0955-2219(03)00129-8) (2004).
- Clarke, D. R. & Levi, C. G. Materials design for the next generation thermal barrier coatings. *Annu. Rev. Mater. Res.* **33**, 383. <https://doi.org/10.1146/annurev.matsci.33.011403.113718> (2003).
- Vaßen, R., Jarligo, M. O., Steinke, T., Mack, D. E. & Stöver, D. Overview on advanced thermal barrier coatings. *Surf. Coat. Technol.* **205**(4), 938. <https://doi.org/10.1016/j.surfcoat.2010.08.151> (2010).
- Clarke, D. R., Oechsner, M. & Padture, N. P. Thermal-barrier coatings for more efficient gas-turbine engines. *Mrs. Bull.* **37**(10), 891. <https://doi.org/10.1557/mrs.2012.232> (2012).
- Di Girolamo, G., Blasi, C., Brentari, A. & Schioppa, M. Microstructural, mechanical and thermal characteristics of zirconia-based thermal barrier coatings deposited by plasma spraying. *Ceram. Int.* **41**, 11776. <https://doi.org/10.1016/j.ceramint.2015.05.145> (2015).
- Mamivand, M., Zaeem, M. A., El Kadiri, H. & Chen, L. Q. Phase field modeling of the tetragonal-to-monoclinic phase transformation in zirconia. *Acta Mater.* **61**(14), 5223. <https://doi.org/10.1016/j.actamat.2013.05.015> (2013).
- Yi, H., Che, J., Liang, G. & Liu, X. Effect of rare earth elements on stability and sintering resistance of tetragonal zirconia for advanced thermal barrier coatings. *Curr. Comput.-Aided Drug Des.* **11**(3), 287. <https://doi.org/10.3390/cryst11030287> (2021).
- Li, G. *et al.* A comprehensive sintering mechanism for TBCs-Part I: An overall evolution with two-stage kinetics. *J. Am. Ceram. Soc.* **100**, 2176. <https://doi.org/10.1111/jace.14784> (2017).
- Li, G. *et al.* A comprehensive sintering mechanism for TBCs-Part II: Multiscale multipoint interconnection-enhanced initial kinetics. *J. Am. Ceram. Soc.* **100**, 4240. <https://doi.org/10.1111/jace.14940> (2017).
- Che, J., Wang, X., Liu, X., Liang, G. & Zhang, S. Outstanding sintering resistance in pyrochlore-type La₂(Zr_{0.7}Ce_{0.3})₂O₇ for thermal barrier coatings material. *Ceram. Int.* **47**(5), 6996. <https://doi.org/10.1016/j.ceramint.2020.11.050> (2021).
- Li, Q. *et al.* Synthesis and phase stability of scandia, gadolinia, and ytterbia co-doped zirconia for thermal barrier coating application. *J. Therm. Spray. Technol.* **24**(1–2), 136. <https://doi.org/10.1007/s11666-014-0158-2> (2014).
- Guo, L., Li, M. & Ye, F. Phase stability and thermal conductivity of RE₂O₃ (RE=La, Nd, Gd, Yb) and Yb₂O₃ co-doped Y₂O₃ stabilized ZrO₂ ceramics. *Ceram. Int.* **42**(6), 7360. <https://doi.org/10.1016/j.ceramint.2016.01.138> (2016).
- Khor, K. A. & Yang, J. Transformability of t-ZrO₂ and lattice parameters in plasma sprayed rare-earth oxides stabilized zirconia coatings. *Scripta Mater.* **37**(9), 1279. [https://doi.org/10.1016/S1359-6462\(97\)00262-5](https://doi.org/10.1016/S1359-6462(97)00262-5) (1997).
- Zhu, D., Nesbitt, J. A., Barrett, C. A., Mccue, T. R. & Miller, R. A. Furnace cyclic oxidation behavior of multicomponent low conductivity thermal barrier coatings. *J. Therm. Spray Technol.* **13**(1), 84. <https://doi.org/10.1361/10599630418185> (2004).
- Sun, L., Guo, H., Peng, H., Gong, S. & Xu, H. Influence of partial substitution of Sc₂O₃ with Gd₂O₃ on the phase stability and thermal conductivity of Sc₂O₃-doped ZrO₂. *Ceram. Int.* **39**(3), 3447. <https://doi.org/10.1016/j.ceramint.2012.09.100> (2013).
- Stecura, S. New ZrO₂-Yb₂O₃ plasma-sprayed coatings for thermal barrier applications. *Thin Solid Films* **150**(1), 15. [https://doi.org/10.1016/0040-6090\(87\)90305-1](https://doi.org/10.1016/0040-6090(87)90305-1) (1987).
- Cairney, J. M., Rebollo, N. R., Rühle, M. & Levi, C. G. Phase stability of thermal barrier oxides: A comparative study of Y and Yb additions. *Z. Metallkd/Mater. Res. Adv. Tech.* **98**(12), 1177. <https://doi.org/10.3139/146.101595> (2007).

22. Feng, J., Ren, X., Wang, X., Zhou, R. & Pan, W. Thermal conductivity of ytterbia-stabilized zirconia. *Scripta Mater.* **66**(1), 41. <https://doi.org/10.1016/j.scriptamat.2011.09.038> (2012).
23. Sun, L., Guo, H., Peng, H., Gong, S. & Xu, H. Phase stability and thermal conductivity of ytterbia and yttria co-doped zirconia. *Prog. Nat. Sci.* **23**(4), 440. <https://doi.org/10.1016/j.pnsc.2013.06.013> (2013).
24. Guo, L. *et al.* Hot corrosion evaluation of Gd₂O₃-Yb₂O₃ co-doped Y₂O₃ stabilized ZrO₂ thermal barrier oxides exposed to Na₂SO₄+V₂O₅ molten salt. *Ceram. Int.* **43**(2), 2780. <https://doi.org/10.1016/j.ceramint.2016.11.109> (2017).
25. Guo, L., Li, M., Zhang, C., Huang, X. & Ye, F. Dy₂O₃ stabilized ZrO₂ as a toughening agent for Gd₂Zr₂O₇ ceramic. *Mater. Lett.* **188**, 142. <https://doi.org/10.1016/j.matlet.2016.11.038> (2017).
26. Bouvier, P., Gupta, H. C. & Lucazeau, G. Zone center phonon frequencies in tetragonal zirconia: Lattice dynamical study and new assignment proposition. *J. Phys. Chem. Solids.* **62**(5), 873. [https://doi.org/10.1016/S0022-3697\(00\)00243-2](https://doi.org/10.1016/S0022-3697(00)00243-2) (2001).
27. Viazzi, C., Bonino, J. P., Ansart, F. & Barnabé, A. Structural study of metastable tetragonal YSZ powders produced via a sol-gel route. *J. Alloy Compd.* **452**(2), 377. <https://doi.org/10.1016/j.jallcom.2006.10.155> (2008).
28. Toby, B. H. & Von Dreele, R. B. GSAS-II: The genesis of a modern open-source all purpose crystallography software package. *J. Appl. Crystallogr.* **46**(2), 544. <https://doi.org/10.1107/S0021889813003531> (2013).
29. Naumenko, A. P. *et al.* Vibrational analysis and Raman spectra of tetragonal zirconia. *Phys. Chem. Solid State.* **9**(1), 121 (2008).
30. Toby, B. H. EXPGUI, a graphical user interface for GSAS. *J. Appl. Crystallogr.* **34**(2), 210. <https://doi.org/10.1107/S0021889801002242> (2001).
31. Zyuzin, D. A. *et al.* X-ray, Raman and FTIRS studies of the microstructural evolution of zirconia particles caused by the thermal treatment. *J. Solid State Chem.* **179**(10), 2965. <https://doi.org/10.1016/j.jssc.2006.04.057> (2006).
32. Bouvier, P. & Lucazeau, G. Raman spectra and vibrational analysis of nanometric tetragonal zirconia under high pressure. *J. Phys. Chem. Solids.* **61**(4), 569. [https://doi.org/10.1016/S0022-3697\(99\)00242-5](https://doi.org/10.1016/S0022-3697(99)00242-5) (2000).
33. Garvie, R. C. & Nicholson, P. S. Phase analysis in zirconia systems. *J. Am. Ceram. Soc.* **55**(6), 303. <https://doi.org/10.1111/j.1151-2916.1972.tb11290.x> (1972).
34. Weng, W. *et al.* Review of zirconia-based biomimetic scaffolds for bone tissue engineering. *J. Mater. Sci.* **56**(14), 8309. <https://doi.org/10.1007/s10853-021-05824-2> (2021).
35. Witz, G., Shklover, V., Steurer, W., Bachegowda, S. & Bossmann, H. P. Phase evolution in yttria-stabilized zirconia thermal barrier coatings studied by rietveld refinement of X-ray powder diffraction patterns. *J. Am. Ceram. Soc.* **90**(9), 2935. <https://doi.org/10.1111/j.1551-2916.2007.01785.x> (2007).

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Author contributions

C.Z. conceived, designed, and analyzed the work and wrote the manuscript. S.A. and X.S. helped with the revision and editing. All authors reviewed the manuscript.

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Competing interests

The authors declare no competing interests.

Additional information

Correspondence and requests for materials should be addressed to S.A.

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