- 1 Supplementary Information for
- 2 "The Extremely Brilliant Source storage ring of the European Synchrotron
- 3 Radiation Facility"

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#### 22 Supplementary Note 1: Low emittance principles

23 The photon beam brilliance is inversely proportional to the electron beam emittance  $\varepsilon_x^{-1}$ :

24 
$$\varepsilon_x = C_q \frac{\gamma^2}{J_x} \frac{I_5}{I_2} \quad J_x = 1 - \frac{I_4}{I_2}$$

with  $C_q$  a constant,  $J_x$  the horizontal damping partition number,  $\gamma$  the relativistic Lorentz factor and  $I_n$  the synchrotron radiation integrals defined as follows, respectively:

27 
$$I_4 = \oint \frac{\eta_x}{\rho} \left( \frac{1}{\rho^2} + 2k_1 \right) ds \qquad I_2 = \oint \frac{1}{\rho^2} ds \qquad I_5 = \oint \frac{\mathcal{H}_x}{|\rho|^3} ds$$

 $\rho$  is the bending radius of the dipoles,  $k_1$  the quadrupole strength and  $\eta_x$  the horizontal dispersion function. The integrals run over the whole lattice.  $\mathcal{H}_x$  is defined by the horizontal twiss parameters  $\beta_x$ ,  $\alpha_x$ , and  $\gamma_x$  and by  $\eta_x$  and  $\eta_x'$ , the horizontal dispersion function and its derivative along the beam trajectory <sup>1</sup>.

32 
$$\mathcal{H}_x = \beta_x \eta_x^{\prime 2} + 2\alpha_x \eta_x \eta_x^{\prime} + \gamma_x \eta_x^2$$

33

34 For a classic double-bend achromat  $^2$  these equations reduce to:

35

36 
$$\varepsilon_x^{DBA}[m.rad] = 5.036 * 10^{-13} E^2 [GeV^2] \theta^3 [deg^3]$$

37

38 where *E* is the electron beam energy and  $\Theta$  the average angle per dipole.

39 Low emittance can therefore be achieved with:

40 1) low  $\beta_x$ , and  $\eta_x$  at dipoles to reduce  $\mathcal{H}_x$ ,

41 2) a large number of low-angle ( $\theta$ ) dipoles and

42 3) combined function magnets with focusing gradient 
$$k_1$$
 and bending angle to increase  $J_x$ .

43

#### 45 Supplementary Note 2:

46 Supplementary Figures 1a-c shows a comparison of different synchrotron light source lattice 47 cells for storage rings with  $E_0 = 6$  GeV and 32 cells. The figures also show the electron beam 48 emittance ( $\varepsilon_x$ ) for the different lattice cells. The characteristics of the considered lattice cells 49 are given below.



56 Supplementary Figure 1: comparison of different synchrotron light source lattice cells 57 for storage rings with  $E_0 = 6$  GeV and 32 cells. Supplementary Figures 1a, b and c are for the 58 Double-Bend-Achromat (DBA), Multi-Bend-Achromat (MBA) and Hybrid-Multi-Bend-59 Achromat (HMBA) lattice cells, respectively.

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## 62 Double-Bend-Achromat (DBA) (first light in 1992). ε<sub>x</sub> ~ 4000 pm.rad

- 63 Characteristics:
- 64 1) small horizontal  $\beta$  and dispersion at dipoles (see Supplementary Note 1)
- 65 2) large dispersion at sextupoles.

# 66 Multi-Bend-Achromat (MBA) (first light in 2015). ε<sub>x</sub> ~ 300 pm.rad

- 67 Characteristics:
- 68 1) more dipoles with less field (see Supplementary Note 1)
- 69 2) dipole-quadrupoles ( $J_x > 1$ ), 3) octupoles (see Supplementary Note 1).
- 70 Hybrid-Multi-Bend-Achromat (HMBA) (first light 2019). ε<sub>x</sub> ~ 133 pm.rad
- 71 Characteristics:
- 72 1) all features of MBA
- 2) two large localized dispersion bumps as in DBA to increase sextupole efficiency
- 3) almost exact -*I* transformation (see Supplementary Note 4) between sextupoles pairs to
- 75 locally cancel sextupolar aberrations
- 76 4) longitudinal gradient dipoles to increase dispersion at sextupoles
- 5) increased dipole filling ratio.
- 78

#### 79 Supplementary Note 3: Natural chromaticity correction

Given a lattice layout (DBA, MBA, HMBA) with dipoles and quadrupoles, the sextupoles are set such that the natural chromaticity  $\xi_{x,y}$  introduced by the integrated quadrupole strengths  $(b_2L)$  is neutralized or overcompensated using sextupoles with integrated strength  $b_3L$  to allow as large as possible off-momentum phase space stability and thus long lifetimes and stable high charge bunches. In this case the chromaticity is defined as

85 
$$\xi_{x,y} = \frac{1}{4\pi} \left( \sum_{n=1}^{N_{sext}} 2b_3 L \eta_{x,y} \beta_{x,y} - \sum_{n=1}^{N_{quad}} b_2 L \beta_{x,y} \right),$$

86 where  $\eta_{x,y}$  and  $\beta_{x,y}$  are the horizontal and vertical dispersion and  $\beta$ -functions and  $N_{sext}$  and 87  $N_{quad}$  the number of sextupoles and quadrupoles present in the lattice. This determines the 88 sextupole strengths,  $(b_3L)$  excluding further non-linear optimization, that are inversely 89 proportional to the dispersion and  $\beta$ -functions at sextupoles. Large  $\beta$ -functions and dispersion 90 at the sextupoles will therefore allow to reduce their strengths <sup>1</sup>.

For the specific case of low emittance lattices that generally feature small dispersion (low dipole fields) and small  $\beta$ -functions, this can lead to strong sextupole strength, potentially reaching technological limits.

#### 95 Supplementary Note 4: The -I transformation between sextupoles

96 With  $b_3L$  the sextupole integrated strength and x, x', y, y' the position and angle in the 97 horizontal and vertical planes, the electron-optical effect of a sextupole can be 98 represented as a coordinates transformation by the transfer matrix  $\mathcal{M}_s$ :

99 
$$\binom{x}{y'}_{y'} = \mathcal{M}_s \binom{x_0}{y_0}, \binom{x}{x'}_{y'} = \binom{1}{0} \begin{pmatrix} 0 & 0 & 0 \\ -0.5b_3Lx_0 & 1 & 0.5b_3Ly_0 & 0 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & b_3Lx_0 & 1 \end{pmatrix} \binom{x_0}{y_0},$$

100

101 If the matrix representing the region of the lattice between two consecutive sextupoles is 102 exactly -I (minus identity), as shown in supplementary Fig. 2, and we neglect the 103 presence of other sextupoles, then

104 
$$\mathcal{M}_t = \mathcal{M}_s(x_0, y_0). (-\mathbb{I}). \mathcal{M}_s(-x_0, y_0) = -I$$

105 the distortions introduced by the first sextupole at first order are cancelled by the 106 sextupole with identical field at the other side of the -I region.

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108

109 Supplementary Figure 2: Lattice functions and magnet layout for the Hybrid Multi-Bend

110 Achromat (HMBA) Synchrotron standard cell. The Dipoles, quadrupoles, sextupoles, 111 multipoles and diagnostic elements along the cell (position s) are shown as violet, pink, light

- 112 green, dark green and black symbols respectively. The  $\beta_x$ ,  $\beta_z$ , and  $\eta_x$  parameters are shown as
- 113 blue, red and orange lines respectively. Reproduced by permission <sup>3</sup>.
- 114

115 The -I transformation is obtained by tuning the quadrupoles gradients such that the 116 optics phase advance is an odd multiple of  $\pi (\phi_x=3\pi, \phi_y=\pi)$ . The effect of the -I117 transformation between sextupole pairs is shown by electron beam tracking simulation

118 for the HMBA cell in the figure below (Supplementary Fig. 3).



119

#### 120 Supplementary Figure 3: electron beam tracking simulation for the HMBA cell

121 When moving away from the phase advances  $(\phi_x=3\pi, \phi_y=\pi)$  generating the -I122 transformation, either the Touschek lifetime <sup>4</sup> or the injection efficiency are negatively 123 affected. The presence of interleaved sextupoles, makes the optimum phase advances 124 deviate slightly from the theoretical  $(\phi_x=3\pi, \phi_y=\pi)$ .

#### 126 Supplementary Note 5: Undulator radiation

127

128 Undulators create a periodic magnetic field perpendicular to the electron path, which introduces 129 by the *Lorentz* force a periodic transverse undulation of the electron trajectory. The radiations 130 emitted at each period interfere. This leads to a photon spectrum with narrow intense peaks. In 131 such case, the photon spectrum shows narrow intense peaks <sup>5, 6, 7</sup> (harmonics) at specific photon

132 energies. An undulator is characterised by its deflection parameter, defined as

133 
$$K = \frac{eB_0\lambda_0}{2\pi mc}$$

where *e* is the elementary charge,  $B_0$  and  $\lambda_0$  are the undulator peak magnetic field and period length, *m* the electron mass and *c* the speed of light. The resonant wavelength on-axis is

136 
$$\lambda = \frac{\lambda_0}{2\gamma^2 n} \left( 1 + \frac{K^2}{2} \right)$$

137 *n* being the harmonic number and  $\gamma$  the relativistic Lorentz factor. The photon flux reaches a 138 maximum at  $K \approx 1.2$  for the fundamental and at higher *K* values for higher harmonics. For a 139 Gaussian photon beam and a single electron, the *diffraction limited* X-ray source size and 140 divergence are respectively

141 
$$\sigma_n = \sqrt{\lambda L/\pi}$$
 and  $\sigma'_n = \sqrt{\lambda/2L}$ 

142 *L* being the undulator length and  $\lambda$  the X-ray wavelength.

143

#### 145 Supplementary Note 6: Spectral flux, coherence and brilliance

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147 A single electron produces transversally coherent radiation.

148 However, the finite electron bunch size

149 
$$\sigma_{x,y} = \sqrt{\epsilon_{x,y} \beta_{x,y} + \eta_{x,y}^2 \delta_E^2}$$

150

151 
$$\sigma'_{x,y} = \sqrt{\varepsilon_{x,y} \gamma_{x,y} + \eta'_{x,y}^2 \delta_E^2}$$

152  $\delta_{\epsilon}$  being the energy spread of the electron beam, result in partially coherent radiation <sup>8</sup> with

153 photon source size 
$$\Sigma_{X,Y} = \sqrt{\sigma_n^2 + \sigma_{X,Y}^2}$$
 and divergence  $\Sigma'_{X,Y} = \sqrt{\sigma'_n^2 + \sigma'_{X,Y}^2}$ .

154 In practice, the radiation is coherent in the vertical plane and partially coherent in the horizontal

155 plane, due to the ellipsoidal shape of the electron beam.

156 The apparent brilliance of the source, defined as  $=\frac{F}{\Sigma_X \Sigma'_X \Sigma'_Y \Sigma'_Y}$ , combines the spectral flux *F* and 157 the source sizes and divergences: high brilliance means a large number of photons in a small 158 phase space volume, i.e. a large coherent flux. The brilliance can be interpreted as the 159 distribution of photons in the phase space and is linked to the Wigner distribution of the electric 160 field <sup>9, 10, 11, 12, 13, 14, 15, 16, 17.</sup>

#### 162 Supplementary Note 7: Sources of errors in storage rings

164 The design of a particle accelerator is based on an ideal model that assumes a perfectly aligned 165 machine without magnetic field errors. In reality, misalignments and field errors, mostly 166 determined by the mechanical tolerances of the magnets and the calibration of the current-to-167 field transfer functions, cannot be avoided. These are estimated during the design phase and 168 the so-called design parameters represent the average of multiple seeds of errors.

We generally classify machine imperfections from the multipoles excited by such errors, andconsequently the magnet type used to correct them:

171

163

172 173 • dipole errors will introduce beam displacements throughout the storage ring that can be described as follows <sup>1</sup>:

$$\Delta u = \sum_{k} M_{12}(s_m | s_k) \Theta_k$$

175 176 where  $\Delta u$  is the displacement of the beam at the location  $s_m$  due to many dipole-field errors 177  $\Theta_k$  at locations  $s_k$ , and  $M_{12}$  is the transfer matrix from the perturbation  $s_k$  to the observation 178 point  $s_m$ . The main contribution to dipole-field errors are unwanted dipole-field components, 179 quadrupole misalignments or beam offset in quadrupole magnets.

180

181 Quadrupole-field errors will introduce a betatron tune shift and linear optics 182 perturbations that will break the lattice properties described in the previous section and 183 consequently degrade the lifetime, injection efficiency and emittance of the machine. The main 184 contributors to quadrupole-field errors are unwanted quadrupole field components, sextupole 185 misalignments or beam offset in sextupole magnets.

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187 Reducing these errors enables the storage ring to operate closer to the ideal model, and thus 188 improve performance. The strength of the corrections applied to bring the machine towards its 189 ideal model is therefore a good indicator of how well the components have been manufactured 190 and the storage ring assembled.

#### 192 Supplementary Note 8: Orbit and optics correction

193 Good control of the closed orbit and linear optics are essential to achieve the design 194 performance of the accelerator. The closed orbit is measured using beam position monitors and 195 then minimized using dipole correctors. To do so, Single Value Decomposition inversion <sup>18</sup> is 196 used to minimize to sum of the squares of the orbit distortions at the beam position monitors<sup>1</sup>:

197 
$$(u_m - \Delta u_m)_{min}^2 = (u_m - M \Theta_n)_{min}^2$$

where  $u_m$  is the measured position at monitor m, M is the orbit response matrix of all the

199 correctors n and  $\Theta_n$  are the vectors of the strength applied to the dipole correctors to minimize 200 perturbations. Similarly, linear optics are corrected using quadrupole correctors by inverting a 201 matrix of the beam response to quadrupole perturbations.





The figure shows the magnetic corrections applied to the ESRF-EBS storage ring. All corrections are below the expected values from the error model as shown in Supplementary Table 3.

### 207 Supplementary Table 3:

	unit	Measured	Model
Gradient corr.	[m <sup>-1</sup> ]	1.7 10-3	2.6 10-3
Dipole corr. [H/V]	μrad	65/30	160/120
β-beating	%	1-2 ±2	1
Closed orbit [H/V]	μm	55/55	140/80

#### 208 Measured and model rms corrections, closed orbit and optics errors.

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210 211 212

# Supplementary Figure 5: Undulator deflection parameter versus period, for different undulator technologies. In a first approximation, the peak magnetic field varies as

 $B \propto Exp((-\pi g) / \lambda_0)$ , where g is the magnetic gap. The parameter K varies with  $\lambda_0$ , 215 resulting in small deflections, limited flux and poor tunability at short periods. At the ESRF, 216 217 most of the undulators are installed around a 10 mm vacuum chamber with a minimum gap of 218 11 mm. Prototype vacuum chambers with 8 mm thickness will be installed for tests, allowing 219 the installation of undulators with a gap of 9 mm. The CPMUs are operated at gaps in the 5 to 220 6 mm range, depending on their length. Operated at 77 K in most cases, they compete with 221 Super-Conducting Undulators operated at helium temperature due to their smaller magnetic 222 gaps. Reducing the vertical size of the beam by means of a mini- $\beta$  setup would allow to install 223 devices with ultra-small gap. The minimum gap of such devices is not determined yet but is 224 expected to be at least in the 3.5 to 4 mm range. 225

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228