## **Supporting information**

Nanoparticle-based Tough Polymers with Crack-propagation Resistance

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## **Experimental Details**



Figure S1. Schematic illustration of the preparation of the tear test specimens.

## **Results and Discussion**



**Figure S2.** Representative DSC curve (second heating) for an EM microparticle at a heating rate of 10 °C/min.  $T_g$  was calculated from the cross-point of tangents to the baseline and inflection point.



**Figure S3.** AFM height images of the EM and EM-R*X* (*X* = 0.001, 0.01, 0.05, 0.2) microparticles dried on a glass substrate and their determined sizes (FWHM and the maximum height).



**Figure S4.** TEM images of EM and EM-R*X* (*X* = 0.001, 0.01, 0.02, 0.05, 0.2) as well as EM-H*Y*  $(Y = 0.1, 0.2)$  microparticles dried on the copper grid.





**Figure S5** (a) Weight of the soluble mass  $(w_1)$  and original mass  $(w_2)$  obtained from the Soxhlet extraction of EM and EM-R $X$  ( $X = 0.001$ , 0.01, 0.02, 0.05, 0.2) microparticles. (b) Molecularweight distribution of the soluble fraction of EM microparticles acquired from GPC measurements.



**Figure S6.** Photograph of a EM-R0.4 film. The EM-R0.4 microparticles formed a brittle film.



**Figure S7.** (a) Photographs and (b) SEM images (surface) of the EM and EM-R*X* (*X* = 0.001, 0.01, 0.05, 0.2) films.



**Figure S8.** Time-lapse photographs the tear tests of the (a) EM-R0.001, (b) EM-R0.01, (c) EM-

R0.05, and (d) EM-R0.2 films. The initial crack length *c* and elongation rate were fixed at 2 mm and 10 mm/min, respectively.



**Figure S9.** (a) *σ*-*λ* curves for the notched and unnotched EM-R0.05 latex films. (b) The Young's modulus *E*, maximum extension ratio  $\lambda_{\text{max}}$ , and maximum stress  $\sigma_{\text{max}}$  values obtained from the  $\sigma$ - $\lambda$ curves.



**Figure S10.** (a) Chemical structure of 1,6-hexanediol dimethacrylate (HDD), which was selected as a conventional chemical crosslinker. (b) Stress-extension ratio curves of tear tests for HDDcrosslinked EM-H films. Elongation rate was fixed at 10 mm/min. Elongation-rate dependence of (c) stress-extension ratio curves and (d) photographs of latex films just before fracture at various rates.



**Figure S11.** SAXS scattering intensity in the high-*q* range for EM and EM-R films.



(b)		Energy density function $U/MJ \text{ m}^{-3}$	E/MPa	Young's modulus Maximum strain Maximum stress $\varepsilon_{\text{max}}$ / $\%$	$\sigma_{\rm max}$ / MPa
	ΕM	$16.9 \pm 3.9$	$8.9 \pm 6.6$	$789.3 \pm 108.7$	$3.5 \pm 0.6$
	EM-R0.001	$19.4 \pm 2.0$	$4.1 \pm 2.3$	$959.2 \pm 44.8$	$3.7 \pm 0.2$
	<b>EM-R0.01</b>	$34.4 \pm 5.1$	$8.2 \pm 2.4$	$932.3 \pm 99.8$	$7.8 \pm 1.5$
	$EM-R0.02$	$43.3 \pm 4.3$	$12.2 \pm 1.2$	$954.3 \pm 22.5$	$10.0 \pm 1.3$
	<b>EM-R0.05</b>	$23.3 \pm 4.9$	$8.1 \pm 3.1$	$925.6 \pm 78.3$	$5.2 \pm 0.6$
	$EM-R0.2$	$14.9 \pm 1.8$	$9.4 \pm 14.7$	$592.2 \pm 29.7$	$3.4 \pm 0.5$

**Figure S12.** (a) Stress-strain curves for the EM and EM-R $X(X=0.001, 0.01, 0.02, 0.05, 0.2)$  films obtained from tensile test measurements. (b) The Energy density function *U*, Young's modulus *E*, maximum strain  $\varepsilon_{\text{max}}$ , and maximum stress  $\sigma_{\text{max}}$  values obtained from the stress-strain curves. The tensile speed was fixed at 10 mm/min. Each curve was extracted from those close to its mean (*N*   $= 3$ ).



**Figure S13.** (a,c,e,g) Stress-extension ratio curves for the EM-R*X* latex films obtained from tear tests conducted at various elongation rates. (b,d,f,h) Photographs of the EM-R*X* latex films just before fracture at various elongation rates.

**Movie S1.** The fracture behavior of an EM film during a tear test at an elongation rate of 10 mm/min. Note that this video has been modified to 50x speed.

**Movie S2.** The fracture behavior of an EM-R0.02 film during a tear test at an elongation rate of 10 mm/min. Note that this video has been modified to 50x speed.