

# Supporting Information for: Performance of a one-dimensional model of wave-driven nearshore alongshore tracer transport and decay with applications for dry weather coastal pollution

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## Supporting Information Available

### Determining dye parameters $k_P$ and $C_0$

A value for  $k_P$  was used for all 1D model runs based on dye concentrations from the SD Bight model, and  $C_0$  was tuned using an iterative search optimization method to maximize model performance for each 1D model run. The physical rate of dye loss was determined from  $k_P = k - k_B$ , where  $k$  is the total temporal rate of dye loss from the nearshore region of the SD Bight model. The total temporal rate of dye loss,  $k$ , assumed constant in time and space, was estimated using the decrease with  $y$  in time-averaged nearshore dye,  $\langle C_C \rangle$ . This decrease was exponential in  $\langle C_C \rangle$  north of  $y = 5$  km, or equivalently, linear in  $\ln \langle C_C \rangle$ . The total temporal decay rate,  $k$ , was related to the time-averaged spatial decay rate using a velocity scale,  $V$ ,

$$k = V \frac{d \ln \langle C_C \rangle}{dy}. \quad (\text{S1})$$

The velocity scale was chosen to be  $V = 0.1 \text{ms}^{-1}$ , the RMS of  $\bar{v}_C$  (Fig. S1). The mean of  $\bar{v}_C$  was not used because  $\bar{v}_C$  values occurred roughly symmetric around 0 (Fig. S1), such that the mean of  $\bar{v}_C$  was less than the typical velocity magnitude.

Beginning 5 km north of PB, the time-averaged SD Bight dye,  $\langle C_C \rangle$ , decays exponentially with  $y$  (Fig. 3a). The slope of  $\ln \langle C_C \rangle$  from the tuning period indicates an e-folding length scale of 7.9 km. This length scale was used to derive  $k_P = 1.3 \times 10^{-5} \text{s}^{-1}$ , an order of magnitude greater than  $k_B$  and slightly lower than the estimate of  $5 \times 10^{-5}$  determined for the region between the 4-m isobath and the surf zone edge in Grimes et al.<sup>1</sup>. The optimal Dirichlet boundary conditions for the 1D models were found to be  $C_0 = 0.008$  for the 1D model and  $C_0 = 0.011$  for the 1DC model. With these  $k_P$  and  $C_0$ , the 1D and 1DC models were able to reproduce time-averaged dye at alongshore locations with considerable skill.

## 27 Calculating velocity from wave properties

28 The 1D model alongshore-uniform wave-driven nearshore alongshore velocity,  $v_{1D}(t)$ , was es-  
 29 timated from wave properties at an offshore location (32.56957 N, -117.1688 E, 20-m isobath,  
 30 Fig. 1), the position of the Imperial Beach Nearshore Buoy operated by the Coastal Data  
 31 Information Program (CDIP). To make use of the established relationship between surf zone  
 32 alongshore currents and waves, (2),<sup>2-4</sup> the alongshore currents in the nearshore region are  
 33 presumed to be proportional to surf zone alongshore-mean alongshore currents.

34 To estimate  $v_{1D}$ , first the right hand side of (2) was simplified using a finite difference  
 35 approximation. Radiation stress begins decreasing in the surf zone where waves break, and  
 36  $S_{xy}$  decreases to zero at the shoreline. To average this wave forcing across the nearshore  
 37 domain, the change in  $S_{xy}$  to zero is divided by the cross-shore distance to the 5-m isobath  
 38  $L$ ,

$$\frac{\partial S_{xy}}{\partial x} \approx \frac{S_{xy}(t)}{L}. \quad (\text{S2})$$

39 For simplicity and generalizability to locations without well-known bathymetry, (S2) was  
 40 evaluated with a constant  $L$ , set to the mean of the tidally-varying distance to the 5-m  
 41 isobath. A narrow-banded representation of  $S_{xy}$  is used,<sup>2</sup>

$$S_{xy}(t) = E(t) \frac{c_g(t)}{c_p(t)} \cos \theta'(t) \sin \theta'(t), \quad (\text{S3})$$

42 where  $E$  is the wave energy,  $c_g$  is the group velocity,  $c_p$  is the phase velocity, and  $\theta'$  is the  
 43 difference between the mean wave direction,  $\theta$ , from shorenormal,  $\theta_{SN}$ . For these estimates of  
 44 alongshore-uniform wave-driven alongshore velocity,  $\theta_{SN}$  was a constant chosen to optimize  
 45 model performance. The 1D model was sensitive to the choice of  $\theta_{SN}$  because wave direction  
 46 is often near shorenormal, and the sign of  $\theta'$  determines the direction of the velocity. Over  
 47 the stretch of shoreline of interest, the mean shorenormal angle is 260°, varying from 240°  
 48 to 270°. Shorenormal angles are closest to 270° in center and decrease towards the domain  
 49 edges. Using uniform shorenormal angle  $\theta_{SN} = 263^\circ$  resulted in best R, NRMSE, and WSS

50 of  $v_{1D}$  out of one hundred  $\theta_{SN}$  values tested in the range  $240^\circ$  to  $270^\circ$ . The SD Bight model  
 51 alongshore-varying nearshore alongshore velocities  $v_C(t, y)$  used in the 1DC model and to  
 52 derive  $\bar{v}_C(t)$  were locally rotated using alongshore-varying shorenormal angles estimated from  
 53 the land mask in the grid.

54 The wave energy term in (S3),  $E$ , was determined using

$$E(t) = \frac{1}{16} \rho g H_s(t)^2, \quad (S4)$$

55 where  $g$  is gravitational acceleration,  $\rho$  is the mean seawater density, and  $H_s$  is the significant  
 56 wave height.

57 The standard deviation of the velocity vector  $\sigma_{\vec{u}}$  in (3) can be written out as a function  
 58 of  $H_s$  at the 5-m isobath. By definition,  $H_s = 4\sigma_\eta$ , where the  $\sigma_\eta$  is the standard deviation of  
 59 the sea surface height. Orbital velocities and sea surface elevation of shallow water gravity  
 60 waves have the same frequency, so  $\sigma_{\vec{u}}$  is proportional to  $\sigma_\eta$  by a scale factor of  $\sqrt{\frac{g}{h}}$  to change  
 61 the dimension. The resulting expression for  $\sigma_{\vec{u}}$  is,

$$\sigma_{\vec{u}}(t) = \sqrt{\frac{g}{h_{5m}}} \frac{H_{s,5m}(t)}{4}, \quad (S5)$$

62 where  $h$  is the constant depth of the water column.  $H_{s,5m}$  can be estimated from the sig-  
 63 nificant wave height at the offshore location of the wave buoy,  $H_{s,WB}$  using Snell's Law and  
 64 the conservation of wave energy flux given the difference in water depths. For this data  
 65 set,  $H_{s,5m} = 0.88H_{s,WB}$  on average. Combining (2), (3), (S2), and (S5) gives the following  
 66 equation for  $v_{1D}$ ,

$$v_{1D}(t) = -\frac{8}{3L\rho C_D} \sqrt{\frac{2h_{5m}}{\pi g}} \frac{S_{xy}(t)}{H_{s,5m}(t)}, \quad (S6)$$

67 where  $C_D$  has flexibility as a fitting parameter, calculated using a simple linear regression  
 68 (with intercept fixed to zero) between the wave-estimated velocity and  $\bar{v}_C$ .

## 69 **Calibrating $C_d$ and velocity fit**

70 Calibration of  $v_{1D}$  was done by fitting  $C_d$  using a linear regression with  $\bar{v}_C$  for the tuning  
71 period to a slope of 1 with no intercept (Fig. S1c). The resulting  $v_{1D}$  had strong agreement  
72 ( $R > 0.8$ ) with  $\bar{v}_C$  (Fig. S1). The drag coefficient fit value was  $C_D = 0.004$ , consistent with  
73 the value of 0.0033 found for the surf zone in Feddersen<sup>3</sup>. The resulting wave-driven  $v_{1D}$   
74 captured the time variations in  $\bar{v}_C$  (Fig. S1b). During the biggest southerly waves in winter  
75 (spikes between Jan 1 and Mar 1 in Fig. S1b),  $v_{1D}$  overestimated  $\bar{v}_C$ .

76 Historic wave forcing was used to compare the 1D model with water samples, which re-  
77 quired recalibrating  $C_d$ . As before,  $C_d$  was used as a fitting parameter between alongshore  
78 velocity estimated from wave observations at the Imperial Beach Nearshore Buoy 155 man-  
79 aged by Coastal Data Information Program at Scripps Institution of Oceanography (SIO)  
80 and velocity measured by an acoustic Doppler current profiler (ADCP) deployed near Impe-  
81 rial Beach by the Coastal Processes Group at SIO. Velocities were measured from November  
82 18, 2019 to December 4, 2019 at 16 Hz at 32.57291 N, -117.13597 E. To identify alongcoast  
83 currents, velocities were smoothed with an hour-long moving average, then tidally-filtered,<sup>5</sup>  
84 and finally rotated to the principal axis.<sup>6</sup> Waves were observed half-hourly at the 21 m iso-  
85 bath at 32.56968 N, -117.16895 E. Data from Buoy 155 is available during twelve deployments  
86 from November 2, 2007 to current day as of writing, with the sixth buoy deployment from  
87 August 24, 2018 to March 20, 2020 overlapping the full ADCP deployment. Correlation of  
88 measured and wave-estimated velocities was  $R = 0.34$ , consistent with previous wave model  
89 performance near Imperial Beach.<sup>7</sup> The tuned drag coefficient was  $C_d = 0.004$ , consistent  
90 with the model-model fit in this study and previous literature.<sup>3</sup>

## 91 Willmott Skill Score

92 Willmott Skill Score (WSS) is a comprehensive model agreement metric that scales the mean  
93 square error by the potential error for a data set,<sup>8</sup>

$$\text{WSS} = 1 - \frac{\sum_{i=1}^{i=N} (m_i - o_i)^2}{\sum_{i=1}^{i=N} (|m_i - \langle o \rangle| + |o_i - \langle o \rangle|)^2} \quad (\text{S7})$$

94 where  $m$  is the 1D model value,  $o$  is the SD Bight model value, and  $N$  is the number of data  
95 points. WSS ranges from 0 to 1, with 1 being best.

## 96 Impact of Neglecting Alongshore Diffusivity

97 The 1D model equation used here (1) did not include alongshore diffusivity, unlike similar 1D  
98 models of nearshore alongshore advection.<sup>1,9</sup> This is because numerical alongshore diffusivity  
99 arising from the upwind advection scheme provided adequate alongshore diffusivity expected  
100 for this environment. The numerical alongshore diffusivity,  $K_{yy}^*$ , was estimated using a scale  
101 analysis,

$$K_{yy}^* \approx \frac{V \Delta y}{2} \quad (\text{S8})$$

102 where  $\Delta y = 30$  m was the grid cell length and  $V = 0.1 \text{ ms}^{-1}$  was a typical velocity scale,  
103 chosen to be the RMS of  $\bar{v}_C$  as before. For this 1D model, the numerical  $K_{yy}^* = 1.5 \text{ m}^2\text{s}^{-1}$ . Es-  
104 timation of expected alongshore diffusivity follows Spydell et al.<sup>10</sup>, who calculated nearshore  
105 alongshore diffusivity using drifters at Huntington Beach, CA and Torrey Pines, CA over  
106 a nearshore domain which extended beyond the surf zone to an offshore distance of 160 m.  
107 Spydell et al.<sup>10</sup> used two scaling estimates of  $K_{yy}$ . The first calculation used mixing length  
108 arguments,<sup>11</sup>

$$K_{yy} \approx \gamma V L, \quad (\text{S9})$$

109 where  $\gamma$  is a fitting parameter, found in Spydell et al.<sup>10</sup> to be  $\gamma = 0.52 \pm 0.08$ . The second  
110 calculation used shear dispersion in a pipe,<sup>12,13</sup>

$$K_{yy} \approx V^2 T_0, \quad (\text{S10})$$

111 where  $T_0$  is the timescale of mixing, found in Spydell et al.<sup>10</sup> to be  $T_0 = 154 \pm 13$  s. Using  
112  $V$  and  $L$  in this study results in  $K_{yy}$  estimates of 10 and  $1.5 \text{ m}^2\text{s}^{-1}$  for the mixing length  
113 and pipe shear dispersion arguments, respectively. This range is consistent with the range  
114 of  $K_{yy} = 1 - 10 \text{ m}^2\text{s}^{-1}$  estimated in Grimes et al.<sup>1</sup>. Grant et al.<sup>9</sup> found significantly higher  
115 estimates of  $K_{yy} = 40 - 80 \text{ m}^2\text{s}^{-1}$  in their field observations at Huntington Beach, CA,  
116 but Grant et al.<sup>9</sup> considered only the well-mixed region of the surf zone extending to 50  
117 m offshore. The numerical diffusivity  $K_{yy}^*$  falls within the range of expected alongshore  
118 diffusivity found here,  $K_{yy} = 1.5 - 10 \text{ m}^2\text{s}^{-1}$ . Inclusion of additional prescribed alongshore  
119 diffusivity was tested using  $K_{yy}$  ranging from 1 to  $10 \text{ m}^2\text{s}^{-1}$ , but model performance metrics  
120 varied by at most 3% of their original values. This justified neglecting additional alongshore  
121 diffusivity beyond numerical alongshore diffusivity.

## 122 **Example data from binary analysis**

123 The binary analysis converted tracer concentrations from the 1D and SD Bight models to  
124 Boolean using a tracer threshold. The two Boolean data series in time and  $y$  were then  
125 compared to generate a data series of True Positives, True Negatives, False Positives, and  
126 False Negatives. These four conditions were normalized as fractions of all time steps as a  
127 function of  $y$ . Example values from the alongshore location of four beaches, listed from most  
128 northern (HdC) to most southern (PTJ), are in Table S1. At all locations, True Negatives  
129 make up a majority of time steps and the fraction of True Negatives increases with  $y$ . The  
130 largest fraction of True Positives is found at Playas Tijuana (PTJ), comprising 15.42% of  
131 time steps.

Table S1: Example data comparing Boolean dye threshold exceedance between 1D model and SD Bight model at four alongshore locations corresponding to public beaches (locations illustrated in Fig. 1).

Location	% True Positive	% False Positive	% True Negative	% False Negative
HdC	0.72	2.56	95.84	0.89
SS	3.75	3.02	91.37	1.85
IB	6.79	6.14	82.54	4.53
PTJ	15.42	7.90	69.21	7.48

132

133 To further interpret these results, the Sensitivity and Specificity were calculated. Sensi-  
 134 tivity  $> 0.6$  for all beaches except HdC, the northernmost beach, and Specificity  $> 0.9$  for  
 135 all beaches (Table S1), improving slightly with  $y$ .

Table S2: Sensitivity and Specificity of 1D model predictions of Boolean threshold exceedance of SD Bight model dye at four alongshore locations corresponding to public beaches (locations illustrated in Fig. 1).

Location	Sensitivity	Specificity
HdC	0.45	0.97
SS	0.67	0.97
IB	0.60	0.93
PTJ	0.67	0.90

136

## 137 **Comparison of 1D model to microbial source tracking**

138 Nearshore 1D model prediction of two SADB WTP microbial source tracking sampling cam-  
 139 paigns from Zimmer-Faust et al.<sup>14</sup> were evaluated with a best linear fit in log space, found  
 140 by minimizing squared error between log model dye to log DNA copies. Slopes, intercepts,  
 141 and correlation coefficients ( $R^2$ ) are given below for three genetic markers, HF183, Lachno3,  
 142 and *Enterococcus*, by sampling campaign. Sensitivity and Specificity were calculated using  
 143 the BAC threshold for model dye and a 1 copy/mL threshold for genetic marker. Since  
 144 nondetects were rare, sampling campaigns were consolidated in Sensitivity and Specificity



145 calculations. *Enterococcus* was detected in every sample, so no Specificity could be calcu-  
 146 lated. Consistent detection of *Enterococcus* may be because *Enterococcus* can also originate  
 147 from animal and environmental sources, unlike HF183 and Lachno3 which are human-specific  
 148 indicators.

Table S3: Data on the best linear fit between log of nearshore model prediction and log of Zimmer-Faust et al.<sup>14</sup> microbial sampling for three water quality indicators in two campaigns ("C1" = first sampling campaign on Oct 2–4, "C2" = second sampling campaign on Oct 27–29). Sensitivity and Specificity calculated using detects and nondetects per indicator for both C1 and C2.

Indicator	Slope (C1, C2)	Intercept (C1, C2)	R <sup>2</sup> (C1, C2)	Sensitivity	Specificity
HF183	8.3, 3.5	52, 29	0.42, 0.40	0.94	0.42
Lachno3	5.0, 3.6	33, 30	0.21, 0.39	0.82	0.22
<i>Enterococcus</i>	3.8, 2.6	29, 26	0.18, 0.54	0.82	N/A

150 **Supporting Information Figures**

Figure S1: a) SD Bight model alongshore-varying alongshore velocity,  $v_C$ , as a function of time during tuning period and  $y$ , with alongshore beach locations on right side (compare with Fig. 1). b) Time series of  $\bar{v}_C$  (black) with  $v_{1D}$  (blue), c) scatter plot of hourly  $\bar{v}_C$  vs  $v_{1D}$ , best fit line (black dashed line) has slope = 1.02, intercept =  $-0.0022$ , and  $R = 0.89$ . One-to-one line (magenta) for comparison with best fit in c). RMS of  $\bar{v}_C$  is  $0.1 \text{ m s}^{-1}$ .

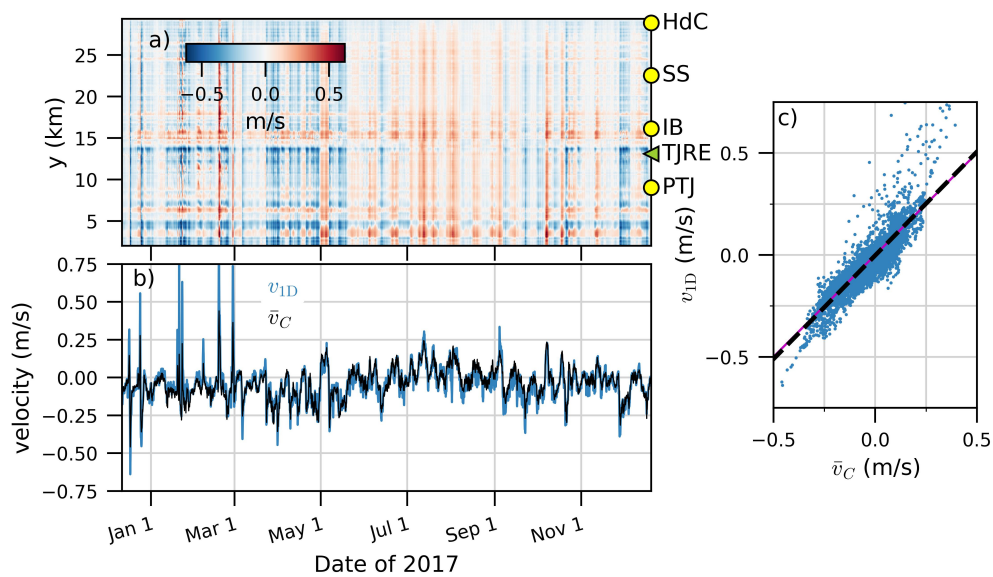
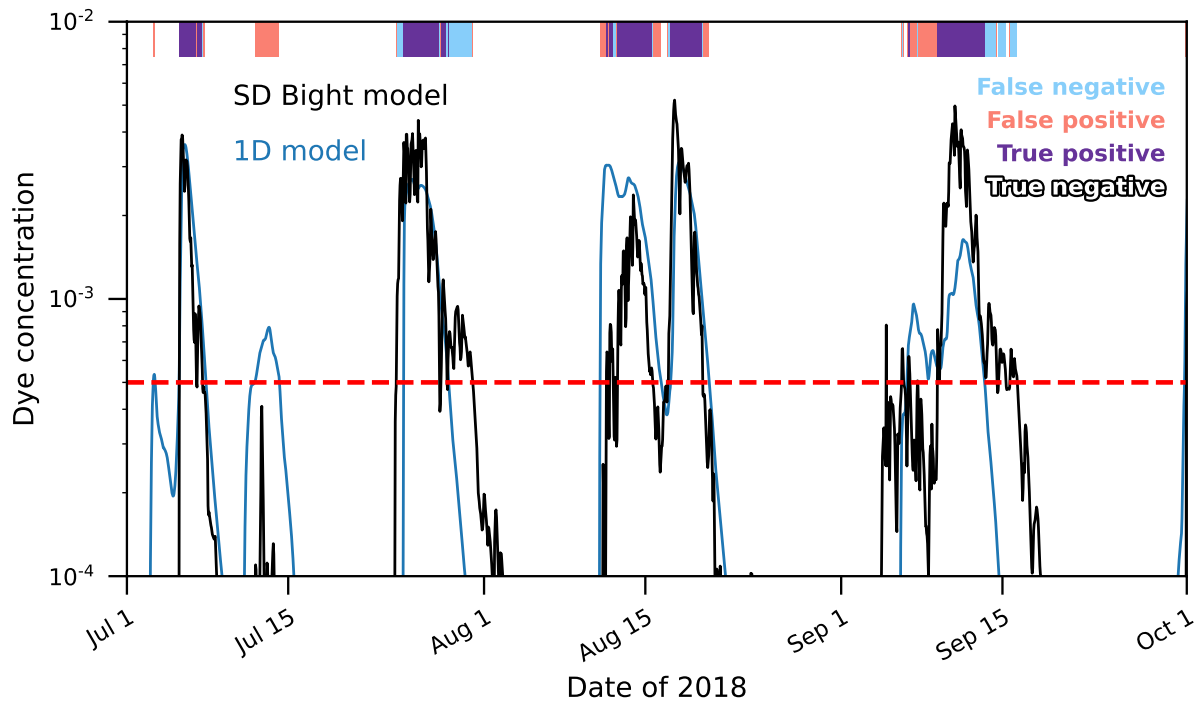


Figure S2: Dye concentrations at Imperial Beach (yellow circle labelled IB in Fig. 1) over three late summer months during model evaluation period from the SD Bight model (black solid line) and 1D model (blue solid line). The dashed red line indicates  $C_{\text{BAC}} = 5 \times 10^{-4}$ . Colored bars at top of figure depict True Positive, (purple), False Positive (orange), False Negative (blue), or True Negative (white). Four conditions defined in manuscript text.



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