### **Supplementary Information**

# Carbon nanolayer-mounted single metal sites enable dipole polarization loss under electromagnetic field

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### **1. Supplementary Figures**

The precursor HMoO<sub>3</sub>@polypyrrole (HMO@PPy) was prepared according to our previous reported literature, followed by pyrolysis at 700°C to form HMO@Nitrogendoped carbon (HMO@NC) (**Supplementary Fig. 1a**). As shown in **Supplementary Fig. 1b-e**, transmission electron microscopy (TEM) images of HMO@NC show that all of HMO@NC exhibit elongated nanorods with core-shell morphology and the carbon layer thickness thickens with increasing pyrrole ratio (mass ratios: HMO/pyrrole = 2:1; 1:1; 1:2). However, HMO@NC material has almost no EWM absorbing properties (**Supplementary Fig. 1f-1h**).



**Supplementary Fig. 1** | HMO@NC preparation and characterization: a) Schematic diagram of the preparation of HMO@NC. TEM image of HMO@NC with different mass ratios of PPy: b) 2:1, c) 1:1 and c, d) 1:2. f) EWM absorption performance diagram of HMO@NC-0.5, g) HMO@NC and h) HMO@NC-2.



Supplementary Fig. 2 | X-ray diffraction (XRD) patterns of the samples.



Supplementary Fig. 3 | Raman patterns of the samples.



**Supplementary Fig. 4** | EDS mapping images of sNi(N<sub>4</sub>)@NC-1.



Supplementary Fig. 5 | HAADF-STEM and corresponding EDS mapping images of  $sNi(N_4)@NC-2$ .



**Supplementary Fig. 6** | HAADF-STEM and corresponding EDS mapping images of sNi(N<sub>4</sub>)@NC.



Supplementary Fig. 7 | HAADF-STEM and corresponding EDS mapping images of  $sNi(N_4)@NC-3$ .



**Supplementary Fig. 8** | EDX spectrum and corresponding element proportion statistics of a) sNi(N<sub>4</sub>)@NC-1, b) sNi(N<sub>4</sub>)@NC-2 c) sNi(N<sub>4</sub>)@NC and d) sNi(N<sub>4</sub>)@NC-3.



**Supplementary Fig. 9** | Aberration-corrected high-angle annular dark-field scanning TEM images: a) sNi(N<sub>4</sub>)@NC-1, b) sNi(N<sub>4</sub>)@NC-2, c) sNi(N<sub>4</sub>)@NC.



Supplementary Fig. 10 | ICP-OES spectrum of  $sNi(N_4)@NC-1$ ,  $sNi(N_4)@NC-2$ ,  $sNi(N_4)@NC$  and  $sNi(N_4)@NC-3$ . (Data are presented as mean  $\pm$  SD (n = 3 independent samples)



Supplementary Fig. 11 | Ni 2p XPS spectrum of  $sNi(N_4)@NC$ .



**Supplementary Fig. 12** | a) XANES spectrum at the Ni K-edge, (b) EXAFS spectra in reciprocal space. EXAFS fitting results of c) sNi(N<sub>4</sub>)@NC-2, d) sNi(N<sub>4</sub>)@NC, and e) sNi(N<sub>4</sub>)@NC-3.



Supplementary Fig. 13 | N 1s XPS spectrum of sNi(N<sub>4</sub>)@NC-1 and sNi(N<sub>4</sub>)@PPy.



Supplementary Fig. 14 | Electron paramagnetic resonance and Ramman spectra measurement: a) EPR pattern of  $sNi(N_4)@NC-1$  and HMO@NC. b) Deconvoluted C 1s spectra, c) Deconvoluted Raman spectra of  $sNi(N_4)@NC-1$ .

The C 1*s* spectra were deconvoluted into graphitic carbon (C–C) at 284.7 eV, defective carbon at 285.2 eV, C=N/C–O at 286.2 eV, and C–N/C=O at 289.3 eV. Raman peaks can be deconvoluted into five bands (polyenes at 1200 cm<sup>-1</sup> for the  $D_4$  band, graphene edges at 1350 cm<sup>-1</sup> for the  $D_1$  band, topological defects at 1500 cm<sup>-1</sup> for the  $D_3$  band, graphitic lattice at 1580 cm<sup>-1</sup> for the G band, and surface graphene layers at 1620 cm<sup>-1</sup> for the  $D_2$  band).



Supplementary Fig. 15 | a) Real and b) Imaginary part of permeability.



Supplementary Fig. 16 | Magnetic loss angular tangent of the samples.



Supplementary Fig. 17 | Electromagnetic parameters tests: a) Real ( $\epsilon'$ ) and imaginary ( $\epsilon''$ ) part of permittivity, b) Tan  $\delta\epsilon$ , c) conduction loss ( $\epsilon_c''$ ) and d) Polarization relaxation loss ( $\epsilon_p''$ ) of HMO@NC, sNi(N<sub>4</sub>)@NC-1, sNi(N<sub>4</sub>)@NC-2, sNi(N<sub>4</sub>)@NC and sNi(N<sub>4</sub>)@NC-3.



Supplementary Fig. 18 | Cole-Cole semicircles of a) HMO@NC, b) sNi(N<sub>4</sub>)@NC-1,
c) sNi(N<sub>4</sub>)@NC-2, d) sNi(N<sub>4</sub>)@NC and e) sNi(N<sub>4</sub>)@NC-3.

Polarization relaxation is evaluated through Cole-Cole semicircles. Following Debye relaxation theory, the related equations of  $\varepsilon'$  and  $\varepsilon''$  are as follows: <sup>1,2</sup>

$$\varepsilon' = \varepsilon_{\infty} + \frac{\varepsilon_{s} - \varepsilon_{\infty}}{1 + \omega^{2} \tau^{2}} \qquad (Equ.S1)$$

$$\varepsilon'' = \frac{\varepsilon_{s} - \varepsilon_{\infty}}{1 + \omega^{2} \tau^{2}} + \frac{\sigma}{\omega\varepsilon_{0}} \qquad (Equ.S2)$$

$$(\varepsilon' - \frac{\varepsilon_{s} + \varepsilon_{\infty}}{2})^{2} + (\varepsilon'')^{2} = (\frac{\varepsilon_{s} - \varepsilon_{\infty}}{2})^{2} \qquad (Equ.S3)$$

where  $\varepsilon_s$ ,  $\varepsilon_{\infty}$ ,  $\omega$  and  $\tau$  are static permittivity, optical dielectric constant, angular frequency and polarization relaxation time, respectively.  $\sigma$  and  $\varepsilon_0$  correspond to conductivity and the permittivity in a vacuum.



Supplementary Fig. 19 | a) Conductivity (Data are presented as mean  $\pm$  SD (n = 3 independent samples) and b) Impedance matching of HMO@NC,  $sNi(N_4)@NC-1$ ,  $sNi(N_4)@NC-2$ ,  $sNi(N_4)@NC$  and  $sNi(N_4)@NC-3$ .



Supplementary Fig. 20 | 3D RL plots of a) sNi(N<sub>4</sub>)@NC-1, b) sNi(N<sub>4</sub>)@NC-2 and c) sNi(N<sub>4</sub>)@NC-3.



Supplementary Fig. 21 | 2D RL plots of a) sNi(N<sub>4</sub>)@NC-1, b) sNi(N<sub>4</sub>)@NC-2 and c) sNi(N<sub>4</sub>)@NC-3.



Supplementary Fig. 22 | a) Summary of EAB and  $RL_{min}$  for all the samples. b) As the reaction temperature increases, the content of Ni increases.



Supplementary Fig. 23 | Correlation analysis of between electronegativity difference and  $RL_{min}$ .



Supplementary Fig. 24 | Magnetic loss mechanism analysis. a) Real and b) Imaginary part of permeability, c) Tan  $\delta_{\mu}$  of sM(N<sub>4</sub>)@NC-1 (M= Ni, Cu, Co and Ni/Cu). d) Real and e) Imaginary part of permeability, f) Tan  $\delta_{\mu}$  of sM(N<sub>4</sub>)@NC-3 (M= Ni, Cu, Co and Ni/Cu).



Supplementary Fig. 25 | Dielectric loss mechanism analysis. a) Real and imaginary part of permittivity, and b) Tan  $\delta_{\epsilon}$  of sM(N<sub>4</sub>)@NC-1 (M= Ni, Cu, Co and Ni/Cu). c) Real and imaginary part of permittivity, and d) Tan  $\delta_{\epsilon}$  of sM(N<sub>4</sub>)@NC-3 (M= Ni, Cu, Co and Ni/Cu).



Supplementary Fig. 26 | Cole-Cole semicircles of a)  $sNi(N_4)@NC-1$ , b)  $sCu(N_4)@NC-1$ , c)  $sCo(N_4)@NC-1$ , d)  $sNi/Cu(N_4)@NC-1$ , e)  $sNi(N_4)@NC-3$ , f)  $sCu(N_4)@NC-3$ , g)  $sCo(N_4)@NC-3$  and h)  $sNi/Cu(N_4)@NC-3$ .



Supplementary Fig. 27 | a) Conductivity (Data are presented as mean  $\pm$  SD (n = 3 independent samples), b) Conduction loss and c) Polarization relaxation loss of  $sM(N_4)@NC-1$  (M=Ni, Cu, Co, Ni/Cu).

Since the material has no significant magnetization, the contribution of magnetic losses to the material is negligible (Supplementary Fig. 24). Among them, the minimum reflection loss of HMO@NC,  $sNi(N_4)@NC$ ,  $sCu(N_4)@NC$ ,  $sCo(N_4)@NC$ , and  $sNi/Cu(N_4)@NC$  is -9.3, -17.8, -38.6, -55.9, and -51.7 dB, respectively; the maximum absorption bandwidth is 0, 4.7, 4.6, 4.8, and 6.44, respectively. The results of the EWM absorbing properties are consistent with the pattern of their dielectric constant and dielectric loss curves (Supplementary Fig. 25). The  $sM(N_4)@NC$  and  $sM(N_4)@NC-3$ 

materials exhibit multiple polarization relaxation processes (Supplementary Fig. 26). Polarization loss is stripped out by its conductive loss, it is found that  $sCo(N_4)@NC$  exhibits a higher polarization loss capacity, which aligns perfectly with its minimal reflection loss (Supplementary Fig. 27).



Supplementary Fig. 28 | a) Impedance matching and b) Attenuation constant of  $sM(N_4)@NC-1$  (M=Ni, Cu, Co and Ni/Cu), c) Impedance matching and d) Attenuation constant of  $sM(N_4)@NC-3$  (M=Ni, Cu, Co and Ni/Cu).

The attenuation ability can be revealed by the attenuation constant ( $\alpha$ ), which can be calculated via following equations: <sup>3,4</sup>

$$\alpha = \frac{\sqrt{2}\pi f}{c} \times \sqrt{(\mu''\epsilon'' - \mu'\epsilon') + \sqrt{(\mu''\epsilon'' - \mu'\epsilon')^2 + (\mu'\epsilon'' - \mu''\epsilon')^2}} \qquad (Equ.S4)$$

where  $Z_0$  and  $Z_{in}$  embody the input impedance of the air and absorber, d is the thickness of absorber, f is the frequency of an electromagnetic wave and c represents the velocity of light in a vacuum.



Supplementary Fig. 29 | Theoretical calculation: a) Atomic structure models and b, c) Differential charge density (From left to right, the order is HMO@NC,  $sNi(N_4)@NC-1$ ,  $sCu(N_4)@NC-1$  and  $sCo(N_4)@NC-1$ .



**Supplementary Fig. 30** | a, b, c) Tafel plots of prepared samples and d, e) Electrochemical impedance spectra of prepared samples.



**Supplementary Fig. 31** | Density of polarizability of a)  $sNi(N_4)@NC$  and b)  $sCu(N_4)@NC$  (The red and solid line parts represent areas where the electric field leads to an increase in density, while the blue and dashed lines correspond to areas where the density decreases).



Supplementary Fig. 32 | The average value of  $\varepsilon'$  and  $\varepsilon''$  of all samples.



**Supplementary Fig. 33** | The remaining energy after one-time EWM penetration. a-i) COMSOL Multiphysics simulation of all samples.



**Supplementary Fig. 34** | Radar cross section (RCS) simulation by FEKO software. a) The sample coating thickness of 3 mm for metal back models and the monitor frequency was set as 9.04 GHz. Corresponding RCS simulation of a1) PEC, a2) HMO@NC, a3)  $sNi(N_4)@NC$ , a4)  $sCu(N_4)@NC$ , a5)  $sCo(N_4)@NC$  and a6)  $sNi/Cu(N_4)@NC$ , and a7) comparison of RCS simulation curves. b) The Predator 2 model simulated radar transmission angles of 0°, 45° and 90° at 9.04 GHz frequency, (b1, b4, b7) PEC; (b2, b5, b8)  $sCo(N_4)@NC$ ; (b3, b6, b9) RCS polar summary diagram.



**Supplementary Fig. 35** | RCS simulation: a) The sample coating thickness of 4.4 mm for metal back models and the monitor frequency was set as 6.08 GHz. Corresponding RCS simulation of a1) PEC, a2) HMO@NC, a3)  $sNi(N_4)@NC$ , a4)  $sCu(N_4)@NC$ , a5)  $sCo(N_4)@NC$  and a6)  $sNi/Cu(N_4)@NC$ , and a7) comparison of RCS simulation curves.

To verify the effective enhancement of EMW absorption performance of  $sM(N_4)@NC$  by surface modification of  $sM(N_4)$ , the radar cross section (RCS) simulation was performed using FEKO software. The metal back (PEC) (Supplementary Fig. 34a) and Predator 2 (Supplementary Fig. 34b) were selected as the simulation model. First, the metal-back simulation model consists of a bottom PEC

plate (200 mm x 200 mm x 1 mm) and an upper coating (HMO@NC and sM(N<sub>4</sub>)@NC-1, 3.00 mm), and the RCS signals of different surface coatings are obtained through the FEKO software (Supplementary Fig. 34a1-34a6). From the summarized 2D plot (Supplementary Fig. 34a7 and Supplementary Table 10), it can be clearly seen that the RCS values of the samples at 0° are ranked from high to low as follows: PEC (12.62 dBsm) > HMO@NC (12.62 dBsm) >  $sNi(N_4)@NC-1$  (5.28 dBsm) >  $sCu(N_4)@NC-1$  $(-0.23 \text{ dBsm}) > sNi/Cu(N_4)@NC-1 (-8.69 \text{ dBsm}) > sCo(N_4)@NC-1 (-53.61 \text{ dBsm}).$ This indicates that surface modification of sNi(N<sub>4</sub>) can significantly enhance the electromagnetic loss capability of HMO@NC on metal backplates. In addition, we can modulate the RCS value of the sample at 0° by adjusting the coating thickness (Supplementary Fig. 35). To comprehensively evaluate the application potential of sCo(N<sub>4</sub>)@NC-1 in real-world scenarios, we employed the Predator 2 model to simulate radar transmission angles of  $0^{\circ}$ ,  $45^{\circ}$ , and  $90^{\circ}$  at a frequency of 9.04 GHz. In this way, we can more accurately predict the material's performance in actual applications and provide strong support for further applied research. From Supplementary Fig. 34b1-34b3, When the radar transmission angle is  $0^{\circ}$ , there is almost no radar scattering signal on the upper layer of the aircraft, and the  $\Delta RCS$  value can reach -49.59 dBsm (Supplementary Table 11). When the transmission angle is adjusted to 45° and 90°, the radar scattering signal range on the aircraft surface changes significantly compared to 0°. After coating with sCo(N<sub>4</sub>)@NC-1, the radar scattering signal on the upper layer of the aircraft also significantly weakens (Supplementary Fig. 34b4-34b9). The results show that the Predator 2 coated with sCo(N4)@NC-1 exhibits excellent RCS attenuation capability regardless of incidence angle.

## 3. Supplementary Tables

Samula	The metal content of
Sample	Ni (wt%)
sNi(N4)@NC-1	0.17
sNi(N <sub>4</sub> )@NC-2	0.19
sNi(N4)@NC	0.23
sNi(N4)@NC-3	0.28

Supplementary Table 1 | The content of Ni in different samples measured by ICP-OES.

Supplementary Table 2 | Parameters of the Ni K-edge EXAFS fitting results for sample.

Sample	shell	CN	<b>R</b> (Å)	ΔE <sub>0</sub> (eV)	$\sigma^2 \times 10^3 (\text{\AA}^2)$	<b>R-factor</b>
SNi(N4)@NC-1	Ni-N	3.9	1.87	0.70	3.533	0.022
SNi(N4)@NC-2	Ni-N	3.6	1.86	2.67	12.6	0.032
SNi(N4)@NC	Ni-N	3.7	1.91	4.80	15.6	0.026
SNi(N4)@NC-3	Ni-N	4.0	1.89	5.25	-18.3	0.008

CN, coordination number; R, distance between absorber and backscatter atoms;  $\Delta E_0$ , the inner potential correction;  $\sigma^2$ , Debye–Waller factor to describe the variance due to disorder (both lattice and thermal); R-factor is used to evaluate the quality of the fitting and the smaller value means more satisfied fitting; Fitting R-range=1-2.3; Fitting k-range=3-11.2.

N1c	Binding	Area ratio	
1115	energy (eV)	(%)	
Pyridinic N	398.8	32.4	
Pyrrolic N	400.7	23.8	
Graphtie N	401.5	19.7	
Mo-N	397.3	24.1	

Supplementary Table 3 | Fitting data of N 1s Spectrum.

Supplementary Table 4 | Comparison of EMW absorption performance of  $sNi(N_4)@NC$  and  $sNi(N_4)@NC-X$  (X= 1, 2, 3) samples prepared at different temperatures.

Absorbors	Thickness	EAB	<b>RL</b> min
Absorbers	(mm)	(GHz)	(dB)
sNi(N4)@NC-1	2.3	4.7	-17.8
sNi(N4)@NC-2	2.3	5.6	-36.2
sNi(N4)@NC	2.3	6.08	-52.7
sNi(N4)@NC-3	2.3	5.68	-32.9

Abaaubaur	Thickness	EAB	<b>RL</b> min
Absorbers	(mm)	(GHz)	(dB)
sNi(N4)@NC-1	2.3	4.7	-17.8
sCu(N4)@NC-1	2.1	4.6	-38.6
sCo(N <sub>4</sub> )@NC-1	2.0	4.8	-55.9
sNi/Cu(N4)@NC-1	2.1	6.44	-51.8
sNi(N4)@NC-3	2.3	5.68	-32.9
sCu(N <sub>4</sub> )@NC-3	2.1	5.1	-34.1
sCo(N <sub>4</sub> )@NC-3	2.0	5.0	-49.8
sNi/Cu(N <sub>4</sub> )@NC-3	2.3	6.2	-45.4

**Supplementary Table 5** | Comparison of EMW absorption performance of the different sM(N<sub>4</sub>) samples.

**Supplementary Table 6** | Comparison of EMW absorption performance of some representative carbon-based absorbers.

Absorbors	Thickness	EAB	<b>RL</b> min	Dof
Absorbers	(mm)	(GHz)	(dB)	Kei
CoMoO4@C	5.0	3.45	-26.0	[5]
C@NiCo2O4@ Fe3O4	3.4	2.10	-43.0	[6]
Fe <sub>3</sub> O <sub>4</sub> @PANI	2.0	3.75	-23.7	[7]
Co-C/MWCNTS	2.5	3.60	-50.0	[8]
C@NiCo2O4	1.5	4.16	-39.0	[9]

Fe <sub>3</sub> O <sub>4</sub> @C	4.0	5.80	-43.5	[10]
sCo(N4)@NC-1	2.0	4.80	-55.9	This work
sNi/Cu(N4)@NC-1	2.1	6.44	-51.7	This work

**Supplementary Table 7** | Mulliken charge (local of NC and MN4 structure) for all the samples.

	NC	Ni	Cu	Со
С	0.370	0.0252	0.234	0.243
Ν	-0.370	-0.321	-0.424	-0.551
MN <sub>4</sub>		0.070	0.190	0.307

**Supplementary Table 8** | The dipole moment calculations of HMO@NC,  $sNi(N_4)@NC$ ,  $sCu(N_4)@NC$  and  $sCo(N_4)@NC$ , and their corresponding values to the  $\mu(x, y, z)$  component of the dipole vector.  $\mu$  is the magnitude of each vector. All values are in units of Debye.

Sample	$\mu_{x}$	$\mu_y$	$\mu_z$	μ
HMO@NC	1.4505	2.2213	-0.0234	2.6529
sNi(N4)@NC	0.9850	1.1210	-0.02442	1.4925
sCu(N4)@NC	1.3299	1.7386	0.000556	2.1890
sCo(N4)@NC	1.7613	2.4557	0.01403	3.0220

**Supplementary Table 9** | The RCS values at  $\theta = 0^{\circ}$ .

	RCS value (dBsm)
PEC	12.627
HMO@NC	12.623
sNi(N4)@NC-1	5.285
sCu(N <sub>4</sub> )@NC-1	-0.236
sCo(N4)@NC-1	-53.618
sNi/Cu(N4)@NC-1	-8.695

detection angle	ΔRCS (dBsm)
0°	-8.01
45°	-14.96
90°	-15.25

Supplementary Table 10 | The average  $\triangle$ RCS of different detection angles.

Electromagnetic parameter	Physical significance	
	Complex permittivity (the material's ability	
ε <sub>r</sub>	to respond to an electric field)	
	Complex permeability (the materials'	
μr	response to a magnetic field)	
$\epsilon'$ and $\mu'$	Real part ( the ability to store energy)	
$\epsilon''$ and $\mu''$	imaginary part ( the ability to lose energy)	
$Z_{in}$	impedance of absorbers	
$Z_0$	impedance of free-space	
f	incident EMW frequency	
d	thickness of absorbers	
с	velocity of light	
ε <sub>s</sub>	static permittivity	
$\epsilon_{\infty}$	optical dielectric constant	
ω	angular frequency	
τ	polarization relaxation time	
α	attenuation constant	

Supplementary Table 11 | Electromagnetic parameters and physical significance.

Supplementary Table 12 |  $\epsilon'$ ,  $\epsilon''$ ,  $\epsilon_c$ ,  $\epsilon_p$  average values of HMO@NC,  $sNi(N_4)@NC$ ,  $sNi(N_4)@NC-1$ ,  $sNi(N_4)@NC-2$  and  $sNi(N_4)@NC-3$ .

	ε' <sub>av</sub>	ε" <sub>av</sub>	Ec, av	Ep, av
HMO@NC	5.47	1.24	0.41	0.81
sNi(N4)@NC	5.52	2.05	0.58	1.47
sNi(N4)@NC-1	6.46	2.90	0.62	2.28
sNi(N <sub>4</sub> )@NC-2	6.55	3.31	0.68	2.63
sNi(N4)@NC-3	6.67	2.81	0.81	2.0

Supplementary Table 13 |  $\epsilon'$ ,  $\epsilon''$ ,  $\epsilon_c$ ,  $\epsilon_p$  average values of HMO@NC,  $sNi(N_4)@NC$ ,  $sCu(N_4)@NC$ ,  $sCo(N_4)@NC$  and  $sNi/Cu(N_4)@NC$ .

	ε' <sub>av</sub>	ε" <sub>av</sub>	Ec, av	Ep, av
HMO@NC	5.47	1.24	0.41	0.81
sNi(N4)@NC	5.52	2.05	0.58	1.47
sCu(N <sub>4</sub> )@NC	6.94	2.60	0.77	1.82
sCo(N4)@NC	8.19	3.80	0.81	3.0
sNi/Cu(N4)@NC	6.33	2.75	0.72	1.87

Supplementary Table 14 |  $\epsilon'$ ,  $\epsilon''$  average values of HMO@NC,  $sNi(N_4)@NC-3$ ,  $sCu(N_4)@NC-3$ ,  $sCo(N_4)@NC-3$  and  $sNi/Cu(N_4)@NC-3$ .

	$\epsilon'_{av}$	$\epsilon''_{av}$
HMO@NC	5.47	1.24
sNi(N4)@NC-3	6.35	2.71
sCu(N <sub>4</sub> )@NC-3	7.13	2.84
sCo(N4)@NC-3	8.36	4.15
sNi/Cu(N4)@NC-3	6.22	2.91

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