# Peer Review File

# **Eliminating chemo-mechanical degradation of lithium solidstate battery cathodes during >4.5V cycling using amorphous ALD coatings**

Corresponding Author: Professor Neil Dasgupta

This manuscript has been previously reviewed at another journal. This document only contains reviewer comments, rebuttal and decision letters for versions considered at Nature Communications.

This file contains all reviewer reports in order by version, followed by all author rebuttals in order by version.

Version 0:

Reviewer comments:

Reviewer #1

#### (Remarks to the Author)

The authors have undertaken the suggested revisions, which has also involved additional work, and have also provided some arguments, which sound logical. Hence, in light of the significance of the results, as well as the extensive work done, I am happy to recommend publication of this manuscript in Nature Communications.

#### Reviewer #3

(Remarks to the Author)

This manuscript discusses the stability and performance enhancement of solid-state batteries (SSBs), specifically addressing the protection of the structural and chemical integrity of the cathode material of SSBs under high-voltage cycling (>4.5 V). As far as the reviewer is aware, the research topic has some value, but the content of the manuscript lacks some necessary analysis. Specific comments are given below. Based on these, I do not recommend this paper for publication. The authors also need to answer the following questions in the content of the manuscript, as commented below.

1. How did the atomic layer deposition (ALD) technique used in the study apply Nb2O5 coatings on single crystal NMC (LiNi0.5Mn0.3Co0.2O2) cathode particles? The authors should show more details on this.

2. The effect of monocrystalline and amorphous coatings on the charging rate needs to be elaborated by the authors. 3. What irreversible structural and chemical changes occur in the uncoated cathode materials mentioned in the article under high voltage cycling?

4. In the manuscript, the authors mention that it is the first time that Nb2O5 is used as a coating material for SSB cathodes with improved efficiency and cycling stability. On what technique were these results realized compared to other studies? 5. "Composite cathodes consisting of uncoated and Nb2O5-coated sc-NMC particles were prepared by mixing Li6PS5Cl (as the SE), graphitized carbon nanofibers (as the conducting additive), and PTFE (as the binder) in a ratio of 70:30:5:5." Is such a mixing ratio supported by the literature? Also, the proportions of the three materials are incorrectly indicated.

6. What are the results of the rate capability tests of the composite positive electrode at different voltage limits mentioned in the article, and how does the Nb2O5 coating affect this performance?

7. There are a large number of abbreviations in this paper that make reading and understanding of texts difficult. The parameters should be introduced in appendix section, their descriptions are omitted from the paper.

8. The analysis of the initial Coulomb efficiency was not specific enough. The results in Figure 2 are not sufficient to verify the high efficiency and stability of the Nb2O5 coating.

9. There are a large number of yellow-marked paragraphs in the main text content, which is not a professional representation.

10. The fonts of several images in the manuscript should all be appropriately enlarged to enhance readability.

Version 1:

Reviewer comments:

#### Reviewer #3

(Remarks to the Author)

The authors have revised the content of the manuscript in detail compared to the previous one, and the necessary analysis has enhanced the quality and rigor of the article. Therefore, this study on the stability and performance enhancement of solid-state batteries (SSBs) deserves to be published, provided that minor revisions are made to the following details. The specific comments are as follows.

1. The first occurrence of a term in the abstract should be explained in full, and the full name should be indicated in the SE to increase readability for the reader.

2. In the abstract, "Compared to uncoated samples at high voltages (≥4.5 V), the composite cathode with Nb2O5-coated CAM particles demonstrates a high initial Coulombic efficiency (91% vs. 82%)," the comparative representation of Coulombic efficiency in parentheses seems inappropriate, and a more standardized expression is suggested. 3. Units appearing in the manuscript should be examined in detail. For example, should 2 mS.cm-1 be revised to 2 mS·cm-1,

and should >275 mAh.g-1 be revised to >275 mAh·g-1?

4. "Recently, it has been shown that mechanical degradation (e.g., intergranular cracking) can be reduced by using single crystal (sc) NMC particles". Why is the abbreviation single crystal used here with a lowercase sc?

5. "This last requirement is often overlooked in the design of artificial SEI/CEI layers; however, it has recently been shown that amorphous coatings have the potential to enable fast charging rates". This sentence suggests a change.

6. "The composite SSB cathodes containing Nb2O5-coated sc-NMC particles, along with LPSC solid electrolyte, binder, and conducting additive, show significantly improved electrochemical performance under high voltage cycling (≥4.5 V) including initial Coulombic efficiency (CE. 91% vs. 83%)" where sc and CE; 91% vs. 83% are suggested to be modified. 7. The font size in Figure 4 is not consistent. For example, LTO/SE/NMC.

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RE: Response to reviewer comments for manuscript entitled: Eliminating chemo-mechanical degradation of solid-state battery cathodes during >4.5V cycling using amorphous ALD coatings by Manoj K. Jangid, Tae H. Cho, Tao Ma, Daniel W. Liao, Hwangsun Kim, Younggyu Kim, Miaofang Chi, Neil P. Dasgupta.

#### **Dear Editorial Office,**

We thank the reviewers and greatly appreciate their valuable feedback. We have carefully addressed their comments through additional experiments, new analysis, and relevant references. Changes to the manuscript have been highlighted in the revised manuscript, SI, and response letter document below. Thank you for your consideration of this manuscript for publication in *Nature Communications*.

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#### **Reviewer #1:**

The authors have undertaken the suggested revisions, which has also involved additional work, and have also provided some arguments, which sound logical. Hence, in light of the significance of the results, as well as the extensive work done, I am happy to recommend publication of this manuscript in Nature Communications.

**Response:** We thank the reviewer for their supportive comments and for recommending publication of our research in *Nature Communications*. Your thorough feedback was invaluable in enhancing the quality of our manuscript.

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# **Reviewer #3:**

This manuscript discusses the stability and performance enhancement of solid-state batteries (SSBs), specifically addressing the protection of the structural and chemical integrity of the cathode material of SSBs under high-voltage cycling (>4.5 V). As far as the reviewer is aware, the research topic has some value, but the content of the manuscript lacks some necessary analysis. Specific comments are given below. Based on these, I do not recommend this paper for publication. The authors also need to answer the following questions in the content of the manuscript, as commented below.

**Response:** We thank the reviewer for their valuable feedback on our manuscript, and for commenting that the research topic has value. We have carefully considered the reviewer's specific comments and in response, we have provided detailed answers and have added significant new experiments, analysis, and discussion to the manuscript. We feel that this new content significantly increases the impact and depth of analysis in the paper.

**Comment 1:** How did the atomic layer deposition (ALD) technique used in the study apply Nb2O5 coatings on single crystal NMC (LiNi0.5Mn0.3Co0.2O2) cathode particles? The authors should show more details on this.

**Response:** We thank the reviewer for the comment. Unlike conventional ALD processes, which are performed on "static" substrates that are not moving, one of the important and novel aspects of this work is that the cathode powders were coated in a 'rotary bed' ALD mode. In this process, the cathode particles are constantly in motion and are suspended as they are agitated by the rotary-bed system. This is analogous to a clothes dryer, where the rotational motion of the machine causes the clothes to "tumble", exposing surface area and accelerating the drying process.

The rotary-bed ALD process was originally developed for powder metallurgy and ceramic engineering [*Surf. Coat. Technol.* **213** (2012) 183-191; *J. Vac. Sci. Technol. A* **38** (2020) 052403; *J. Vac. Sci. Technol. A* 25 (2007) 67–74], and it's use for solid-state battery cathode particles is a novel aspect of this work. The cathode powder is mixed with  $ZrO<sub>2</sub>$  balls and is placed in a tube inside the rotary vessel that is attached to a rotary motor. The rotary motor rotates the vessel, ensuring a conformal ALD coating on every particle in the powder.

In the ALD coating of powders, this agitation is critical to ensure that the ALD films are completely conformal along the entire particle surface. In contrast, if the powder bed was stagnant, there would be discontinuities/pinholes in the coatings at the particle-particle point contacts. For battery cathodes, these discontinuities become sites for unwanted surface reactions upon contact with electrolyte (SEI formation) and gas release at high voltage.

A detailed description of the ALD process parameters is provided in the 'Methods' section. To improve the clarity of the rotary-bed ALD process, in addition to Figure 1A, we have added a new detailed schematic of the ALD reactor equipped with a rotary bed attachment and the ALD process (Figure R1 below) in the revised SI as Figure S1. Briefly, one ALD cycle consists of an Nb pulse (1s), an Ar purge (20s), a DI water pulse (0.1s), and an Ar purge (20s). Thirty ALD cycles were repeated to achieve a  $\sim$ 5 nm thick Nb<sub>2</sub>O<sub>5</sub> coating on sc-NMC532 particles. The deposition was performed at a substrate temperature of 175 °C, avoiding the formation of any crystalline LiNbO<sub>x</sub> coating or Nb doping, as discussed in the manuscript.

The following new Figure has been added to the SI as Figure S1:



Figure S1: (A) Schematic of an ALD chamber with a rotary-bed attachment for conformal ALD coating at the particle scale on powders. (B) Schematic of the ALD process of Nb<sub>2</sub>O<sub>5</sub> coating on an individual singlecrystal NMC532 particle in the ALD chamber.

To provide further context for the powder ALD process, and its advantages compared to traditional (static) ALD modes, the following discussion and references have been added to the main text:

The procedure for depositing amorphous  $Nb<sub>2</sub>O<sub>5</sub>$  coatings onto sc-NMC particles using ALD is depicted schematically in Figure 1A and Figure S1. ALD was performed on sc-NMC particles (sized  $2$ -5  $\mu$ m) without any additional pretreatment. To ensure conformal coverage of the entire particle surface without the presence of discontinuities at particle-particle contact points, a rotary bed ALD reactor was used (Figure 1A and Figure S1)  $45,46$ . In this process, the cathode particles are constantly in motion and are suspended as they are agitated by the rotary-bed system. In contrast, if artificial CEI coatings are formed on powders that are sitting on a substrate or in a crucible, the coating will form pinholes at the contact points, which will serve as "hot spots" for electrolyte decomposition.

45. McCormick, J. A., Cloutier, B. L., Weimer, A. W. & George, S. M. Rotary Reactor for Atomic Layer Deposition on Large Quantities of Nanoparticles. *J Vac Sci Technol A* 25, 67–74 (2007).

46. Longrie, D., Deduytsche, D., Haemers, J., Driesen, K. & Detavernier, C. A Rotary Reactor for Thermal and Plasma-Enhanced Atomic Layer Deposi;on on Powders and Small Objects. *Surf Coat Technol* **213**, 183–191 (2012).

In addition, the following text has been added to the methods section, to point to this new schematic:

A detailed schematic of the ALD reactor with a rotary bed attachment and the ALD process is presented in Figure S1

### **Comment 2: The effect of monocrystalline and amorphous coatings on the charging rate needs to be elaborated by the authors.**

**Response:** We thank the reviewer for this comment and agree that it is important to clearly explain the benefits of using single-crystal particles and amorphous coatings in this study. In fact, it is the synergistic combination of these two characteristics (single-crystal vs. polycrystalline cathode particles, and amorphous vs. polycrystalline coatings) that distinguishes our work from previous efforts and enable the improved chemo-mechanical stability observed.

First, we will describe the importance of using single-crystal (sc) NMC in this study. As first described in the introduction section:

Recently, it has been shown that mechanical degradation (e.g., intergranular cracking) can be reduced by using single crystal (sc) NMC particles  $4-10$ .

This ability to eliminate intergranular fracture is one of the major motivations to use sc-NMC particles in this study. To further clarify this point, the following text was added to the discussion:

This chemo-mechanical behavior has been previously observed for single crystal NMC cathodes in liquid electrolyte systems, where the lattice gliding and fracture behavior of individual particles is distinct compared to polycrystalline NMC particles, where interparticle cracking commonly occurs <sup>68–73</sup>. As a consequence of these different fracture behaviors, single crystal NMC cathodes have been shown to exhibit significantly lower amounts of oxygen gas release at high voltages than their polycrystalline counterparts 6,7,20.

We have further emphasized this point in showing how both sc-NMC and the amorphous coating provide a synergistic benefit to avoid chemo-mechanical degradation:

To provide evidence for the improved mechanical stability, SEM analysis of the coated CAM particles after cycling to a 4.7 V was performed, and no particle cracking was observed throughout the electrode (Figure S20). This illustrates the synergistic benefits of using both sc-NMC particles and the amorphous ALD coating to mitigate chemo-mechanical failure of CAM particles at high voltages. As a consequence of this improved stability, the SE/CAM particle interface will be more well preserved, which is consistent with the improved rate capability and long-term cycling stability data of the coated particles (Figures 2,3,4).

The use of amorphous, as opposed to polycrystalline, coatings in this study is another novel and critical factor that differentiates our work from previous studies that have primarily focused on the crystalline LiNbO<sub>3</sub> phase. The amorphous coatings are chemically and structurally homogeneous. As a result, at the nanoscale, the coatings are free of current-focusing 'hot spots', which results in a more uniform distribution of interfacial kinetics and transport compared to polycrystalline coatings. The amorphous coatings are also mechanically compliant and are able to withstand the cyclic strains that occur in CAM particles during cycling, as shown by the *post mortem* TEM analysis in this paper. On the other hand, polycrystalline coatings will contain of grain boundaries, crystallographic defects, and spatial variations in topology and grain orientation. At the nanoscale, all of these factors will introduce local current focusing 'hot spots', which decreases the rate capability and stability of the cathode.

## To clarify these points, the following text in the 'Introduction' section has been modified and highlighted:

Ideally, the coating would be chemically and structurally homogenous to avoid local current focusing at 'hot spots' such as grain/phase boundaries, crystallographic defects, and spatial variations in chemical composition, topology, and grain orientation of the coating. This last requirement is often overlooked in the design of artificial SEI/CEI layers; however, it has recently been shown that amorphous coatings have the potential to enable fast charging rates, which is attributed to a more uniform distribution of interfacial kinetics and transport compared to the 'natural' SEI layer that forms based on electrolyte decomposition  $^{28,29}$ . Hot spots can also arise if the coating is not perfectly conformal and continuous (pinhole-free), which requires precise synthesis methods such as atomic layer deposition (ALD) <sup>13,28,30</sup>. Finally, the coating must be sufficiently mechanically compliant to withstand the cyclic strains that occur in CAM particles during cycling.

To further prove the benefits of using an amorphous-phase coating over the traditional polycrystalline LiNbO<sub>3</sub> coatings, we have performed new experiments comparing our ALD-coated cathode particles to those using the state-of-the-art solution processed LiNbO<sub>3</sub> coatings. we deposited polycrystalline LiNbO<sub>3</sub> coatings on the sc-NMC532 powders used in this study. The LiNbO<sub>3</sub> coating was applied using a solution processing method that includes a high-temperature annealing step at 425 °C, resulting in a polycrystalline coating  $5,33,41$ .

The rate capabilities of composite cathodes having amorphous ALD  $Nb<sub>2</sub>O<sub>5</sub>$ , and crystalline LiNbO<sub>3</sub> coatings at 4.3 V and 4.7 V are compared in Figure R2 below and the same has been added to the SI as Figure S11. The comparison clearly shows that although the crystalline LiNbO $_3$ -coated cathodes perform better than the uncoated cathode, they are still significantly inferior to the amorphous  $Nb<sub>2</sub>O<sub>5</sub>$ -coated cathodes. For example, at 2C with a 4.3 V cutoff, the accessible capacities were 0.22, 1.16, and 1.64 mAh.cm<sup>-2</sup>, respectively for uncoated, LiNbO<sub>3</sub>, and Nb<sub>2</sub>O<sub>5</sub>coated cathodes. When the rate capability is performed at a higher cutoff voltage (4.7 V), the difference between LiNbO<sub>3</sub> and Nb<sub>2</sub>O<sub>5</sub> electrodes gets further contrasted. With a 4.7 V cutoff, the LiNbO<sub>3</sub>-coated cathode showed a significant capacity loss, retaining only 0.45 mAh.cm<sup>-2</sup> but the accessible capacity of the  $Nb<sub>2</sub>O<sub>5</sub>$ -coated cathode remained fairly stable with a 1.49 mAh.cm<sup>-2</sup>. The performance of the uncoated cathode almost vanished.

To clarify, the following Figure has been added to the SI as Figure S11:



Figure R2: Rate capability trends of uncoated, ALD  $Nb<sub>2</sub>O<sub>5</sub>$  coated, and solution-processed LiNbO<sub>3</sub> coated sc-NMC composite cathodes at (A) 4.3 V and (B) 4.7 V cutoff voltages.

To clarify, the following text has been added to the main text:

To provide a comparison to state-of-the-art coatings, solution-processed LiNbO<sub>3</sub> coatings were also applied to sc-NMC cathodes  $5,33,41$ . The rate capability of ALD Nb<sub>2</sub>O<sub>5</sub>-coated cathodes cycled to 4.3 V and 4.7 V cutoff voltages is consistently higher than those of LiNbO<sub>3</sub>-coated cathodes. It is important to highlight that the solution processing method involves a high-temperature annealing step, resulting in a polycrystalline coating with microstructural heterogeneity. The superior performance of the  $Nb<sub>2</sub>O<sub>5</sub>$  coating underscores the benefits of an amorphous coating.

To clarify, the following text has been added to the 'Methods' section:

#### **Solution-processed LiNbO<sub>3</sub> coating on sc-NMC532 powders:**

A 3 wt% LiNbO<sub>3</sub> coating was deposited on sc-NMC532 powders using the solution processing method, following the published literature  $5,33,41$ . A solution of 5% (w/v) lithium niobium ethoxide in ethanol (Thermo Scientific Chemicals) was added to 0.5 g of sc-NMC532 powder, stirred for 1 h, and dried at 70 °C for 12 h under Ar flow. Finally, this dried powder was annealed in an oxygen atmosphere at 425 °C for 1.5 h, resulting in a LiNbO<sub>3</sub> coating on sc-NMC532 particles.

### **Comment 3: What irreversible structural and chemical changes occur in the uncoated cathode**  materials mentioned in the article under high voltage cycling?

**Response**: Thank you for the comments. We have shown and discussed multiple irreversible structural and chemical changes and their impact on the performance of the uncoated cathode during high-voltage cycling. For example, Figure 2G-I and Figure S13 highlight the evolution of higher interfacial impedance contributed by more CEI formation and irreversible structural changes. In Figure 5 and Figure S18, HRTEM images and XRD plots after cycling at different cutoff voltages reveal irreversible structural changes, highlighting the formation of a kinetically less active rock-salt phase. Furthermore, in Figure 6, lattice/planner gliding, and sub-surface and intraparticle cracking in uncoated NCM particles have been demonstrated.





Figure 3: (G) Nyquist impedance plots of uncoated and  $Nb<sub>2</sub>O<sub>5</sub>$ -coated cathodes after the rate capability tests. (H) Zoomed-in view showing Nyquist impedance plots of Nb<sub>2</sub>O<sub>5</sub>-coated cathodes. (I) Comparison of interfacial impedance for uncoated and  $Nb_2O_5$ -coated cathodes after the rate capability tests.



Figure S13: (A) Intermittent EIS measurement at specific voltage points during the charging cycle (at C/10 rate) of uncoated and Nb<sub>2</sub>O<sub>5</sub>-coated cathodes against a Li-metal anode. Zoomed-in view of Nyquist plots

obtained at different voltage points during the charging cycle are presented for (B) uncoated and (D) Nb2O5-coated cathodes, with insets providing a zoomed-out view of the Nyquist plots. (C) Comparison of total interfacial impedance at different voltage points during charging.



Figure 5: (A) Schematic showing structural changes occurring in uncoated sc-NMC532 particles when cycled to different voltage limits. Upon repeated cycling to high voltage limits (>4.3 V), uncoated particles undergo irreversible structural changes (spinel and rock-salt phase formations), and (sub)surface and intraparticle cracking. HAADF-STEM images after 500 cycles at 1C rate for (B) uncoated cycled at 4.3 V and (C) uncoated cycled at 4.7 V are presented. FFT patterns and zoomed-in views of marked regions are also presented as insets. (D-F) *Ex-situ* XRD scans (zoomed-in) of uncoated samples before cycling obtained from samples after rate capability test at 4.3 V and 4.7 V limits.



Figure 6: (A) Schematic showing the onset of lattice gliding, subsequent microcrack formation, and its growth in (sub)surface and intra-particle cracking. (B) HAADF-STEM image of uncoated sc-NMC particle after 500 cycles at 1C rate and 4.7 V shows serrated surface resulting from lattice gliding and (sub)surface cracking. (C) Zoomed-in images of the cracks highlighted by white box in (B) and FFTs from different marked regions. FIB-SEM cross-section images of uncoated sc-NMC electrode after 500 cycles at 1C rate and 4.7 V showing (D) (sub)surface and (E) intra-particle cracks.

# **Comment 4: In the manuscript, the authors mention that it is the first time that Nb2O5 is used** as a coating material for SSB cathodes with improved efficiency and cycling stability. On what **technique were these results realized compared to other studies?**

**Response:** We thank the Reviewer for the comment. To the best of our knowledge, this is the first demonstration of fabrication of a pin-hole free conformal niobium oxide coating by ALD method for SSB cathodes. The coatings have a Nb:O atomic ratio of 2:5 (i.e.,  $Nb<sub>2</sub>O<sub>5</sub>$ ) and amorphous phase (Figure 1B,C and Figure S4). We confirmed its composition by multiple techniques (XPS and TEM-EDS) (Table S1 and Figure S2). The ALD process allowed precisely tuning the composition while low-temperature processing (175 °C) enabled amorphous nature, preventing the formation of crystalline phase and any Nb-doping to NMC (Figure S6).

To emphasize the novel aspects of our methods compared to previous studies, we revised the title of the paper as follows:

### **Eliminating chemo-mechanical degradation of solid-state battery cathodes during >4.5V cycling using amorphous ALD coatings**

On the other hand, the majority of prior reports to date on niobium-based coatings have used different methods including wet-chemical, ALD followed by heat treatment, or solid-state reactions. Importantly, these techniques have typically included a high-temperature annealing step either during or after the coating synthesis on the cathode particles, which leads to the formation of crystalline Li<sub>x</sub>NbO<sub>y</sub>. We have provided a comprehensive survey of different coating materials for high-voltage cathodes, their synthesis methods, and electrochemical performance in Table S4 in the SI.

#### For your reference, Table S4 is revisited below.

**Table S4:** Comparison of electrochemical performance of layered cathode materials having different coatings in solid electrolyte and liquid electrolyte systems.







# **Comment 5: "Composite cathodes consisting of uncoated and Nb2O5-coated sc-NMC particles** were prepared by mixing Li6PS5Cl (as the SE), graphitized carbon nanofibers (as the conducting additive), and PTFE (as the binder) in a ratio of 70:30:5:5." Is such a mixing ratio supported by the literature? Also, the proportions of the three materials are incorrectly indicated.

Response: We thank the Reviewer for raising this point. The composition of an SSB cathode greatly affects its microstructure, and electronic and ionic percolation pathways, critically influencing the energy and power densities. To provide a balance between energy and power density, composite SSB cathodes are often composited cathode active material and solid electrolyte in a weight ratio of approximately 70:30, in addition to other phases (conducting additive and binder) that has been widely used in the literature [Commun. Mater. 2 (2021) 112; *Chem. Mater.* **33** (2021) 2624–2634; *Batteries & Supercaps* **5** (2022) e202100397].

We conducted a systematic study on the effect of cathode composition on the rate performance of the uncoated cathode (Figure R3) and chose the 70:30:5:5 composition. This convention of expressing the relative loadings is commonly used in the literature; however, we understand the Reviewer's point that an alternative expression may be to express then as a percentage, rather than a ratio. Therefore, we have now clarified the corresponding weight ratio of this mixture:

To clarify, the following text has been modified in the main text:

Composite cathodes consisting of uncoated and  $Nb<sub>2</sub>O<sub>5</sub>$ -coated sc-NMC particles were prepared by mixing Li<sub>6</sub>PS<sub>5</sub>Cl (as the SE), graphitized carbon nanofibers (as the conducting additive), and PTFE (as the binder) in a weight ratio of 70:30:5:5 (or weight % ratio of  $63.6:27.3:4.6:4.6$ ).

To understand the role of mixing ration on performance, we performed an optimization study of cathodes with varying ratios, as shown in Fig. R3 below. The results showed that the cathodes with higher solid electrolyte content (e.g., 30:70:5:5 or 50:50:5:5) exhibited greater accessible capacity and high-rate capability. In contrast, the cathodes with higher active material content (e.g.,  $80:20:5:5$  and  $90:10:5:5$ ) experienced more significant rate limitations.



Figure R3: Effect of cathode composition on rate capability

To clarify, the following text has been modified in the 'Methods' section:

For composite cathode preparation, NMC powders (uncoated or coated; Li-capacity 165 mAh.g<sup>-1</sup> at 4.3V), Li<sub>6</sub>PS<sub>5</sub>Cl SE phase (≤1µm size; MSE Supplies), PTFE binder (Sigma Aldrich) and graphitized carbon nanofibers conductive additive (Sigma Aldrich) were mixed in a weight ratio of 70:30:5:5 (or weight % ratio of  $63.6:27.3:4.6:4.6$ ).

# **Comment 6: What are the results of the rate capability tests of the composite positive electrode** at different voltage limits mentioned in the article, and how does the Nb2O5 coating affect this **performance?**

**Response:** The rate capability results from uncoated and Nb<sub>2</sub>O<sub>5</sub>-coated cathodes, cycled to different cutoff voltages (4.3 V, 4.5 V, 4.7 V), including accessible capacities, impedance (before and after the rate capability tests), and polarization (derived from the  $dQ/dV$  plots), were presented in Figure 3, Figure S7 and Figure S9 (now Figure S9 and Figure S12 in the revised SI). These results have been discussed in 'Effect on Rate Capability' and 'Effect on Cell Polarization and Impedance Evolution' sections.

For the Reviewer's reference, we are revisiting these figures below:



Figure 3: Rate capability trends of (A) uncoated and (B)  $Nb_2O_5$  coated composite cathodes (vs. LTO anode). Voltage profiles of (C) uncoated and (D)  $Nb<sub>2</sub>O<sub>5</sub>$  coated cathodes at different c-rates (C/10, C/5, C/2, 1C, 2C) at a cutoff voltage of 4.7V. Comparison of polarization estimated from dQ/dV analysis of voltage profiles at different c-rates for (E) uncoated and (F) Nb<sub>2</sub>O<sub>5</sub> coated electrodes. (G) Nyquist impedance plots of uncoated and  $Nb<sub>2</sub>O<sub>5</sub>$ -coated cathodes after the rate capability tests. (H) Zoomed-in view showing Nyquist impedance plots of  $Nb<sub>2</sub>O<sub>5</sub>$ -coated cathodes. (I) Comparison of interfacial impedance for uncoated and  $Nb<sub>2</sub>O<sub>5</sub>$ -coated cathodes after the rate capability tests.



Figure S9: Voltage profiles at different c-rates (C/10, C/5, C/2, 1C, 2C) for (A-C) uncoated and (D-F*)* Nb2O5 coated sc-NMC composite cathodes cycled at different cutoff voltages.



Figure  $S12$ :  $dQ/dV$  vs V plots obtained from the voltage profiles during rate capability tests of (A-C) uncoated and (D-F) Nb<sub>2</sub>O<sub>5</sub> coated sc-NMC composite cathodes cycled at different cutoff voltages.

**Comment 7: There are a large number of abbreviations in this paper that make reading and** understanding of texts difficult. The parameters should be introduced in appendix section, their descriptions are omitted from the paper.

**Response:** We thank the Reviewer for this suggestion. For more clarity and better readability, we now summarized the abbreviations in Table S5 in the SI.

To clarify, the following table has been added to the SI as Table S5:

Table S5: List of abbreviations used in the study



# **Comment 8: The analysis of the initial Coulomb efficiency was not specific enough. The results** in Figure 2 are not sufficient to verify the high efficiency and stability of the Nb2O5 coating.

**Response:** We thank the Reviewer for the comment, and would like to discuss the initial Coulombic efficiency (ICE) further. Figure 2 presents the average ICE from three sets of samples at each condition with error bars, demonstrating the repeatability of our results and the superior performance of  $Nb<sub>2</sub>O<sub>5</sub>$ -coated samples starting from the formation cycling. The high ICE significantly results in improved rate capability (at high current densities) and long-term cycling stability.

To provide further analysis of ICE, we have now added new analysis of the detailed voltage traces and corresponding  $dQ/dV$  plots during the first formation cycles of the cathode samples cycled to different cutoff voltages (4.3 V, 4.5 V, 4.7 V) in Figure R4 below. For the uncoated samples, the voltage traces appear more sloped and reach the cutoff voltage early during the discharge cycle. On the other hand, the voltage traces of  $Nb<sub>2</sub>O<sub>s</sub>$ -coated samples appear relatively less sloped and take more time to reach the cutoff voltage during the discharge cycle. Additionally, the uncoated samples exhibit higher higher cell polarization during the discharge cycles compared to the coated samples. Furthermore, the dQ/dV plots show inferior reversibility for the uncoated samples and greater accessibility and reversibility for the coated samples.



Figure 2: Initial Coulombic efficiency of uncoated and Nb<sub>2</sub>O<sub>5</sub> coated cathodes cycled to different cutoff voltages during the first formation cycle.

To clarify, the following Figure has been added in the SI as Figure S8:



Figure R4: First formation cycle voltage profiles and corresponding dQ/dV vs V plots at different cutoff voltages for  $(A,C)$  uncoated and  $(B,D)$  Nb<sub>2</sub>O<sub>5</sub> coated sc-NMC composite cathodes, respectively.

#### To clarify, the following text has been added to the main text:

The voltage traces during the first formation cycle of the uncoated samples exhibit higher cell polarization and appear more sloped, reaching the cutoff voltage earlier during the discharge cycle (Figure S8).

**Comment 9: There are a large number of yellow-marked paragraphs in the main text content,**  which is not a professional representation.

**Response:** We apologize for the confusion caused due to the yellow-marked paragraphs in the manuscript provided. These yellow highlights were responses to previous reviewer comments from an earlier submission.

# **Comment 10. The fonts of several images in the manuscript should all be appropriately enlarged to enhance readability.**

**Response:** Thank you for your feedback. We have appropriately enlarged the fonts in the figures in the revised manuscript to enhance readability and overall clarity.

Thank you for your consideration of this article for publication.

Sincerely,

Veil Dasgyster

Neil Dasgupta Associate Professor, Miller Faculty Scholar Department of Mechanical Engineering Department of Materials Science & Engineering University of Michigan, Ann Arbor

We thank the Reviewer for their positive feedback. We have carefully addressed all comments and made necessary changes to the manuscript that are highlighted in the revised manuscript, SI, and response letter below. Thank you again for your consideration of this manuscript for publication in *Nature Communications*.

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#### **Reviewer #3:**

The authors have revised the content of the manuscript in detail compared to the previous one, and the necessary analysis has enhanced the quality and rigor of the article. Therefore, this study on the stability and performance enhancement of solid-state batteries (SSBs) deserves to be published, provided that minor revisions are made to the following details. The specific comments are as follows.

**Response:** We thank the reviewer for the positive feedback, recognizing our efforts and enhanced quality of the revised manuscript and recommending it for publication in *Nature Communications*. Below, we provide point-by-point responses to the specific questions.

**Comment 1:** The first occurrence of a term in the abstract should be explained in full, and the full name should be indicated in the SE to increase readability for the reader.

**Response:** We have now defined SE at its first occurrence in the abstract.

**Comment 2:** In the abstract, "Compared to uncoated samples at high voltages (≥4.5 V), the composite cathode with Nb2O5-coated CAM particles demonstrates a high initial Coulombic efficiency (91% vs. 82%)," the comparative representation of Coulombic efficiency in parentheses seems inappropriate, and a more standardized expression is suggested.

**Response:** We thank the Reviewer for the suggestion. We have revised the statement to ensure scientific clarity.

To clarify the following text has been modified in the abstract:

At high-voltages ( $\geq$ 4.5 V), the composite cathode with Nb<sub>2</sub>O<sub>5</sub>-coated CAM particles demonstrates a higher initial Coulombic efficiency of 91% compared to 82% for the uncoated samples, along with improved rate capability (10x higher accessible capacity at 2C rate) and remarkable capacity retention during extended high-voltage cycling (99.4% after 500 cycles at 4.7 V).

**Comment 3:** Units appearing in the manuscript should be examined in detail. For example, should 2 mS.cm-1 be revised to 2 mS·cm-1, and should >275 mAh.g-1 be revised to >275 mAh·g- $1?$ 

**Response:** We have revised the format of the units throughout the main text and SI.

**Comment 4:** "Recently, it has been shown that mechanical degradation (e.g., intergranular cracking) can be reduced by using single crystal (sc) NMC particles". Why is the abbreviation single crystal used here with a lowercase sc?

**Response:** We have replaced this abbreviation with uppercase SC throughout the main text and SI.

**Comment 5:** "This last requirement is often overlooked in the design of artificial SEI/CEI layers; however, it has recently been shown that amorphous coatings have the potential to enable fast charging rates". This sentence suggests a change.

**Response:** We thank the Reviewer for the feedback. This sentence has been modified as follows:

The importance of chemical and structural homogeneity of the coating is often overlooked in the design of artificial SEI/CEI layers. However, recent studies have shown that amorphous coatings can enable fast-charging capabilities, which is attributed to a more uniform distribution of interfacial kinetics and transport compared to the composite 'natural' SEI layer that forms based on electrolyte decomposition 28,29

**Comment 6:** "The composite SSB cathodes containing Nb2O5-coated sc-NMC particles, along with LPSC solid electrolyte, binder, and conducting additive, show significantly improved electrochemical performance under high voltage cycling (≥4.5 V) including initial Coulombic efficiency (CE. 91% vs. 83%)" where sc and CE; 91% vs. 83% are suggested to be modified.

**Response:** This sentence is now modified in the introduction, as provided below:

The composite SSB cathodes containing  $Nb<sub>2</sub>O<sub>5</sub>-coated SC-NMC$  particles show significantly improved electrochemical performance under high-voltage cycling (≥4.5 V) including a higher initial Coulombic efficiency of 91% compared to 82% for the uncoated samples, improved rate capability (10x higher accessible capacity at 2C rate), and long-term cycling stability (99.4% after 500 cycles) compared to uncoated SSB cathodes.

**Comment 7:** The font size in Figure 4 is not consistent. For example, LTO/SE/NMC.

**Response:** We have corrected and revised the figure in the main text.

sincerely,<br>Veil Dasgypter

Neil Dasgupta Associate Professor, Miller Faculty Scholar Department of Mechanical Engineering Department of Materials Science & Engineering University of Michigan, Ann Arbor