



Evidence for widespread thermal acclimation of canopy photosynthesis

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36 The SI contains 2 Supplementary Text, 3 Supplementary Tables, 9 Supplementary Figures, and
37 Supplementary References.

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40 **Supplementary Text 1. Farquhar-von Caemmerer-Berry model (FvCB) for estimating CO₂**
41 **assimilation rate**

42 We employ the standard FvCB model¹, which comprises the photosynthetic module of the
43 Breathing Earth System Simulator (BESS)^{2,3}, to estimate the canopy-scale CO₂ assimilation rate
44 (A) of C₃ plants in a big-leaf framework. Within the big-leaf framework, we assume the canopy
45 functions as a single bulk plane that serves as the source and sink for all mass and energy fluxes⁴.
46 The model determines A based on the slower rate of two biochemical processes: A_j , which is the
47 electron transport for ribulose-1,5-bisphosphate (RuBP) at low light and is dependent on the
48 capacity of the electron transport chain (J_{max} ; $\mu\text{mol m}^{-2} \text{s}^{-1}$), and A_c , which is the carboxylation of
49 RuBP and is dependent on ribulose-1,5-bisphosphate carboxylase/oxygenase (Rubisco) activities
50 (V_{cmax} ; $\mu\text{mol m}^{-2} \text{s}^{-1}$). Both A_j and A_c are influenced by intercellular CO₂ concentrations (C_i). For
51 non-optimality-based BESS versions (i.e., BESS_{PFT} and BESS_{LAI}), we assume a fixed ratio of C_i
52 to the ambient CO₂ concentration (C_a), which is referred to as χ and set at 0.7⁵. The eco-
53 evolutionary optimality (EEO) theory suggests that plants tend to maximize carbon gain and
54 minimize water loss by regulating stomatal conductance, which results in an optimal χ value⁶.
55 We use optimal χ for optimality-based BESS (BESS_{EEO}) (Supplementary Text 2).

$$56 \quad A_j = \frac{\alpha I J_{max}}{\alpha I + 2.1 J_{max}} \frac{(C_i - \Gamma^*)}{4(C_i + 2\Gamma^*)} \quad (1)$$

$$57 \quad A_c = \frac{V_{cmax}(C_i - \Gamma^*)}{C_i + K_c \left(1 + \frac{O}{K_o}\right)} \quad (2)$$

$$58 \quad A = \min(A_c, A_j) \quad (3)$$

59 where I ($\mu\text{mol photons m}^{-2} \text{s}^{-1}$) is incident photosynthetically photon flux density, α (mol mol^{-1})
60 is the intrinsic quantum yield based on incident light, Γ^* (Pa) is the CO₂ compensation point in
61 the absence of dark respiration, O (Pa) is oxygen partial pressure, and K_c (Pa) and K_o (Pa) are
62 Michaelis-Menten constants of Rubisco for CO₂ and O₂, respectively⁷.

63
64 In this study, we integrate the parameters characterizing acclimation and adaptation following
65 ref⁸ into the BESS code. An Arrhenius function is used to describe the temperature dependencies
66 of V_{cmax} and J_{max} for the baseline BESS⁹:

67
$$k = k^{25C} \times \exp \left[\frac{H_a \times 1000 \times (T - 298.15)}{298.15 \times R \times T} \right] \times \frac{\left[1 + \exp \left(\frac{298.15 \times S - H_d}{298.15 \times R} \right) \right]}{\left[1 + \exp \left(\frac{S \times T - H_d}{R \times T} \right) \right]} \quad (4)$$

68 where k^{25C} represents V_{cmax}^{25C} and J_{max}^{25C} , and R is the universal gas constant (8.31 J K⁻¹ mol⁻¹). T is
 69 the canopy temperature in °K. H_a, H_d and S are activation energy (kJ mol⁻¹), deactivation energy
 70 fixed at 200 kJ mol⁻¹, and entropy factor (kJ mol⁻¹ K⁻¹), respectively.

71
 72 We use three empirical approaches to estimate V_{cmax} variants at a reference temperature of 25 °C
 73 (V_{cmax}^{25C}) (see Methods), and calculate J_{max}^{25C} as a function of V_{cmax}^{25C} , home temperature (T_{home} , °C)
 74 and growth temperature ($\overline{T_{avr}}$, °C)⁸. Here, T_{home} is defined as the average air temperature of the
 75 warmest month over the measurement period following ref¹⁰. The values of H_a and S are
 76 estimated as functions of $\overline{T_{avr}}$ and T_{home} to account for acclimation, with a general form as:

77
$$H_a \text{ or } S = a\overline{T_{avr}} + bT_{home} + c(\overline{T_{avr}} - T_{home}) + d \quad (5)$$

78 where parameters a, b, c and d are set, following refs^{8,10} and can be found in Supplementary
 79 Table 2. T represents a key source of uncertainties in canopy-scale photosynthetic modelling¹⁰.

80 We test three approaches to estimate T, which assume that T is equivalent to either the air
 81 temperature (T_{air} , °K), the aerodynamic surface temperature (T_{aero} , °K), or the radiometric
 82 surface temperature of the big-leaf plane (T_{rad} , °K). T_{aero} is calculated as follows:

83
$$T_{aero} = T_{air} + \frac{H}{\rho G_{ah} c_p} \quad (6)$$

84 where H is the sensible heat flux (W m⁻²), ρ is the air density (kg m⁻³), G_{ah} is the aerodynamic
 85 conductance to heat transfer (m s⁻¹), and C_p is the heat capacity of dry air (J K⁻¹ kg⁻¹). G_{ah} is
 86 calculated as the sum of aerodynamic conductance to momentum transfer¹¹ and canopy boundary
 87 layer conductance to heat transfer¹². T_{rad} is calculated based on the physical principle that the
 88 longwave radiation emitted by an object is proportional to the fourth power of the object's
 89 temperature, stated by the Stephan-Boltzmann law:

90
$$T_{rad} = \left(\frac{LW_{out} - (1 - \epsilon)LW_{in}}{\sigma \epsilon} \right)^{\frac{1}{4}} \quad (7)$$

91 where LW_{out} and LW_{in} are the outgoing and incoming longwave radiation (W m⁻²), respectively.
 92 σ denotes the Stefan-Boltzmann constant (W m⁻² K⁻⁴). We set the emissivity of the surface, ε, to
 93 0.98. We compute T_{aero} and T_{rad} with R package bigleaf⁴. Note that the data availability for T_{rad}

94 and T_{aero} data is less than that for T_{air} , as their calculation depends on several variables (equation
 95 6 and 7). This is particularly significant given that LW_{out} and LW_{in} are available for only about
 96 74% of the sites. The estimated T_{aero} and T_{rad} show strong correlations with T_{air} , with R^2 values
 97 of 0.93 ± 0.10 and 0.78 ± 0.15 (mean ± 1 -SD, model: $T_{\text{air}} \sim T_{\text{aero}}$ or T_{rad}) over FLUXNET2015
 98 sites. In theory, T_{rad} and T_{aero} should more closely approximate the true canopy temperature (T)
 99 than T_{air} , potentially leading to better model performance when using them as T approximations.
 100 However, the three T approximations (i.e., T_{air} , T_{aero} and T_{rad}) yield highly similar results when
 101 estimating hourly A (Supplementary Fig. 8). It is important to note that eddy covariance GPP
 102 data are not independent of T_{air} , since both daytime and nighttime partitioning methods use T_{air}
 103 as an input¹³. This likely explains the comparable modelling performance between T_{air} and the
 104 other two T approximations. We finally choose T_{air} over T_{aero} and T_{rad} because the data are more
 105 frequently available. Detailed descriptions of other processes of the FvCB model in BESS and
 106 BESS's performance in estimating GPP over flux sites are given in refs^{2,3,9}.

107

108 **Supplementary Text 2. EEO-based estimate of leaf photosynthetic capacity**

109

110 The coordination hypothesis posits that leaf A_c (equation 2) tends to be equal to A_j (equation 1)
 111 over intermediate time scales, meaning that photosynthesis operates at a co-limitation point of A_c
 112 and A_j ^{14,15}. We apply the findings from this study on PFT-dependent optimal time scales for
 113 acclimation (Fig. 2) to represent the growth conditions of plants. To account for the effect of
 114 finite J_{max} ^{6,16}, we modify equation (1) using a non-rectangular hyperbola function¹⁷:

$$115 \quad A_j = \frac{\alpha I}{\sqrt{1 + \left(\frac{\alpha I}{J_{\text{max}}}\right)^2}} \frac{(C_i - \Gamma^*)}{(C_i + 2\Gamma^*)} \quad (8)$$

$$116 \quad \alpha = \frac{a_L b_L}{4} \Phi_{\text{PSII,max}} M \quad (9)$$

117 where $a_L = 0.8$ represents the leaf absorptance, $b_L = 0.5$ represents the fraction of absorbed light
 118 for photosystem II (PSII), and the factor 4 accounts for the number of electron equivalents
 119 required to assimilate one CO_2 molecule. The constant $M = 12$ (g) represents the weight of 1 mol
 120 carbon. $\Phi_{\text{PSII,max}}$ represents the maximum quantum yield of PSII for a representative light-
 121 adapted leaf, and is dependent on T ¹⁸:

122
$$\Phi_{PSII,max} = 0.352 + 0.022T - 0.00034T^2 \quad (10)$$

123 The least-cost theory proposes that plants can optimize χ by minimizing the combined unit costs
 124 per carbon assimilation of maintaining carbon assimilation and water transpiration (E)¹⁹:

125
$$e \frac{\partial(E/A)}{\partial\chi} = -f \frac{\partial(V_{cmax}/A)}{\partial\chi} \quad (11)$$

126 where e and f (unitless) are the unit costs for E and A, respectively. One optimal χ value can be
 127 resolved from equation (10) through an application of Fick's law of diffusion for H₂O and CO₂¹⁹:

128
$$\chi = \frac{\sqrt{\beta \frac{K + \Gamma^*}{1.6\eta^*} + \frac{\Gamma^* \sqrt{VPD}}{C_a}}}{\sqrt{\beta \frac{K + \Gamma^*}{1.6\eta^*} + \sqrt{VPD}}} \quad (12)$$

129 where VPD (Pa) is the vapor pressure deficit, and K (Pa) is the effective Michaelis-Menten
 130 coefficient of Rubisco²⁰. η^* (Pa s), which represents the viscosity of water at 25 °C, can be
 131 estimated using a T dependence function⁶. The parameter β is the ratio of the unit costs a and b
 132 (equation 9) when standardized to their values at 25 °C, and is fixed at 146 based on an updated
 133 isotope-derived χ database^{6,16}.

134
 135 Furthermore, we assume that the optimal J_{max} value maximizes the difference between carbon
 136 gain (A_j) and the cost of $c \times J_{max}$, where c (unitless) is a cost factor. We estimate c to be 0.103
 137 based on a typical value of $J_{max}/V_{cmax} = 1.88$ ^{6,21}. By establishing an equivalence between
 138 equations (2) and (7), we can solve for an EEO-based leaf-scale V_{cmax} value (V_{cmax_EEO}):

139
$$V_{cmax_EEO} = \alpha I \frac{C_i + K}{C_i + 2\Gamma^*} \sqrt{1 - \left[\frac{4c(C_i + 2\Gamma^*)}{C_i - \Gamma^*} \right]^{\frac{2}{3}}} \quad (13)$$

140 For the seasonally-fixed V_{cmax}^{25C} ($V_{cmax_PFT}^{25C}$) and phenology-based V_{cmax}^{25C} ($V_{cmax_LAI}^{25C}$), they are
 141 derived for the top leaves. When calculating $V_{cmax_EEO}^{25C}$, we assume a fraction of 1 for absorbed
 142 photosynthetically active radiation to represent leaves located at the top of a canopy. This
 143 assumption ensures consistency in the derivation of canopy V_{cmax}^{25C} among the three BESS
 144 variants.

145

146 To convert top-leaf V_{cmax}^{25C} ($V_{cmax,top}^{25C}$) to representative-leaf V_{cmax}^{25C} ($V_{cmax,ave}^{25C}$), we use a satellite-
147 based clumping index (k_n , unitless) derived from a global map²², which indicates the non-
148 randomness of leaf distribution⁷:

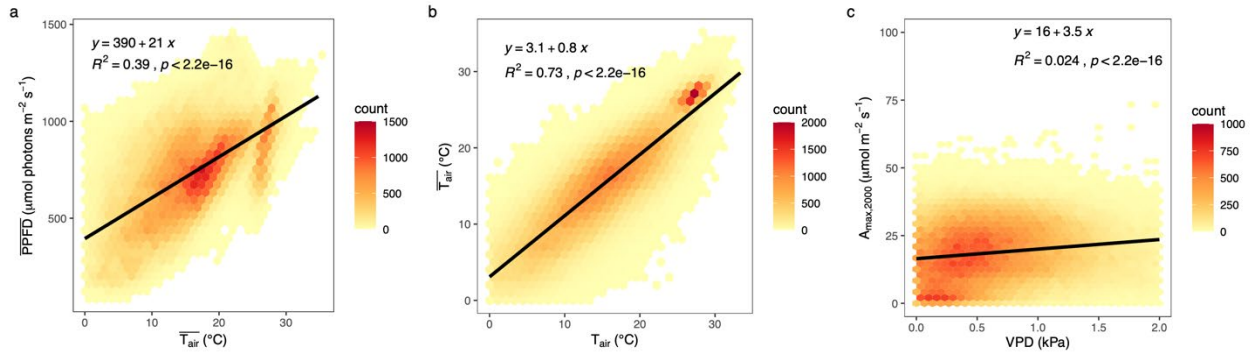
$$149 \quad V_{cmax,ave}^{25C} = V_{cmax,top}^{25C} \times \frac{1 - e^{-k_n}}{k_n} \quad (14)$$

150 We calculate canopy-scale representative V_{cmax}^{25C} ($V_{cmax,canopy}^{25C}$) following:

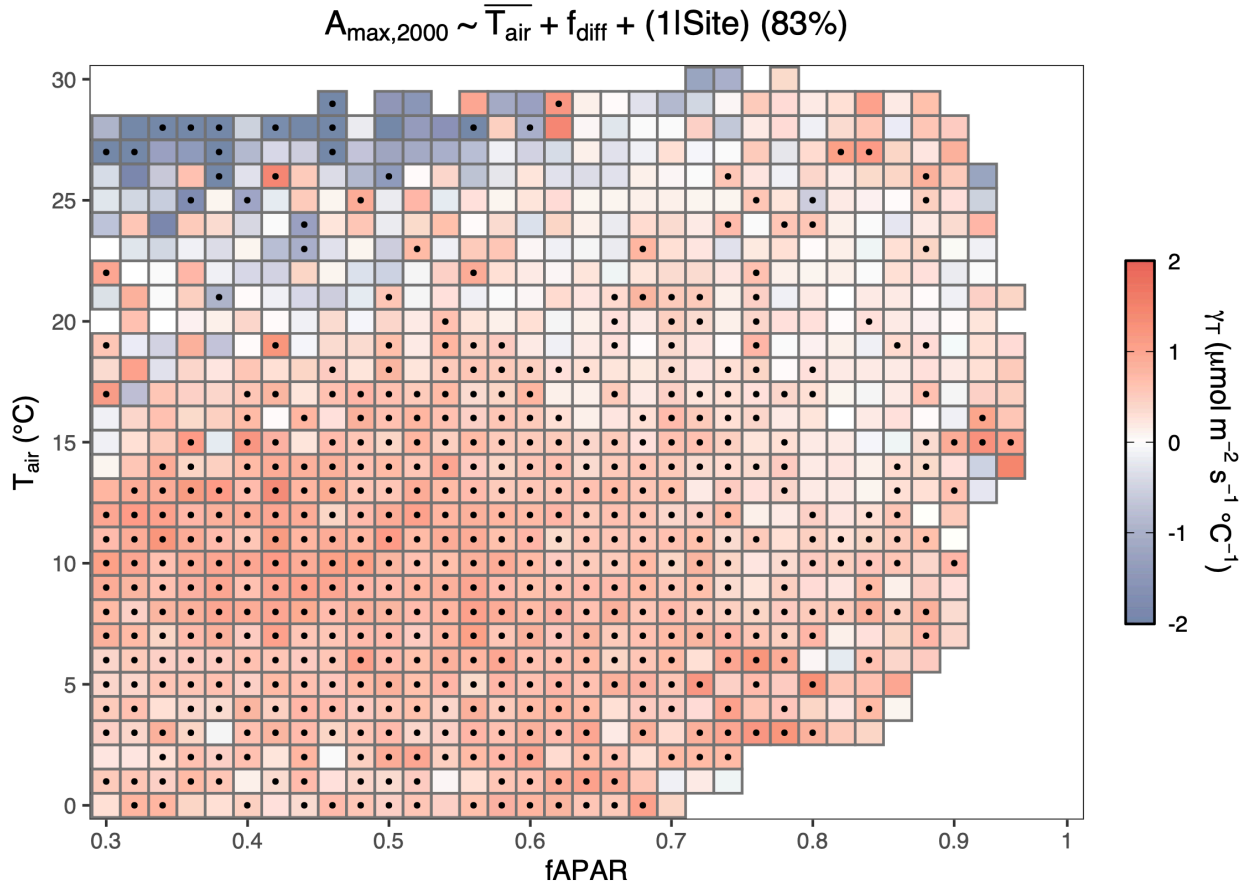
$$151 \quad V_{cmax,canopy}^{25C} = V_{cmax,ave}^{25C} \times LAI \quad (15)$$

152 Detailed deduction of V_{cmax_EEO} can be found in ref²³. Additionally, we test the sensitivity of
153 $V_{cmax_EEO}^{25C}$ to the selection of the time scale for acclimation (τ) by examining its relative change
154 when setting $\tau = 14$ days compared to other τ values (Supplementary Fig. 9). Overall, $V_{cmax_EEO}^{25C}$
155 changes by $0.17 \pm 2.59 \%$, $0.28 \pm 1.37 \%$, $0.14 \pm 0.78 \%$, $0.01 \pm 0.85 \%$, $0.37 \pm 1.79 \%$ and 1.34
156 $\pm 3.01 \%$ (mean ± 1 -SD) across flux sites when τ is set to 3, 7, 10, 20, 30 and 45 days,
157 respectively. This finding indicates that τ has a relatively limited impact on $V_{cmax_EEO}^{25C}$
158 estimation, particularly when τ is selected within the range of 7 to 30 days, a period commonly
159 used in previous studies²³⁻²⁵.

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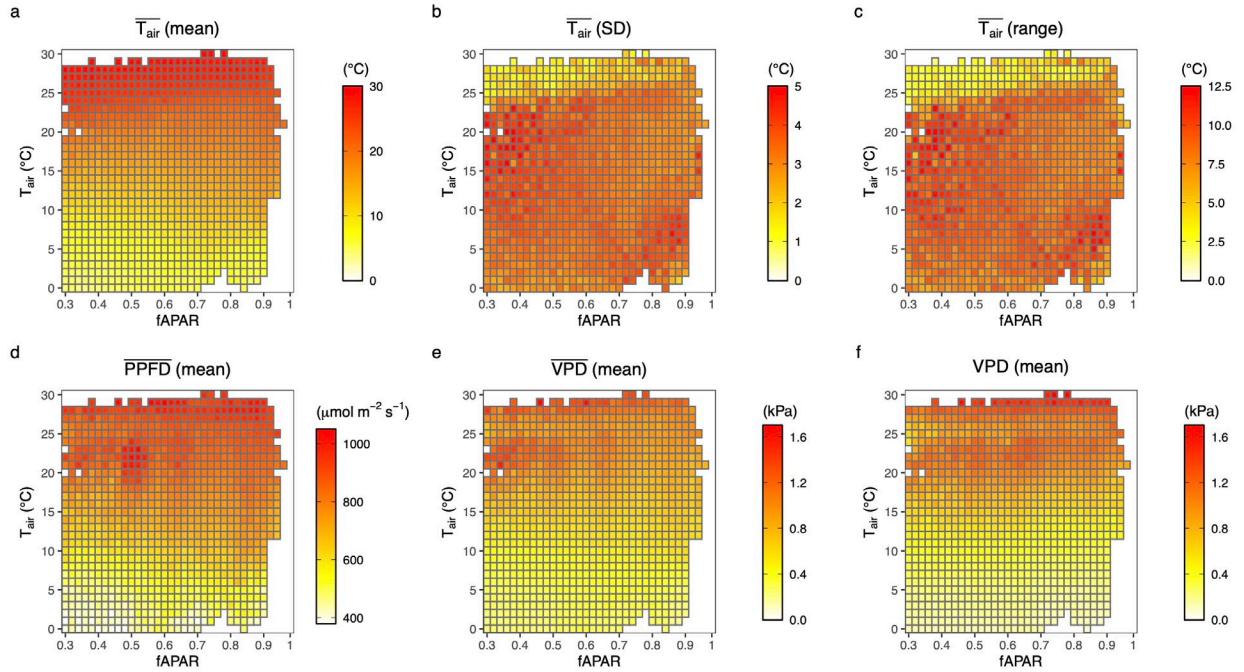


161
 162 **Supplementary Fig. 1: Relationships among environmental variables and $A_{max,2000}$.** a–c, The
 163 relationships between $\overline{T_{air}}$ and \overline{PPFD} (a), between $\overline{T_{air}}$ and T_{air} (b) and between $A_{max,2000}$ and
 164 VPD (c). Black lines represent linear fits ($Y \sim X$).
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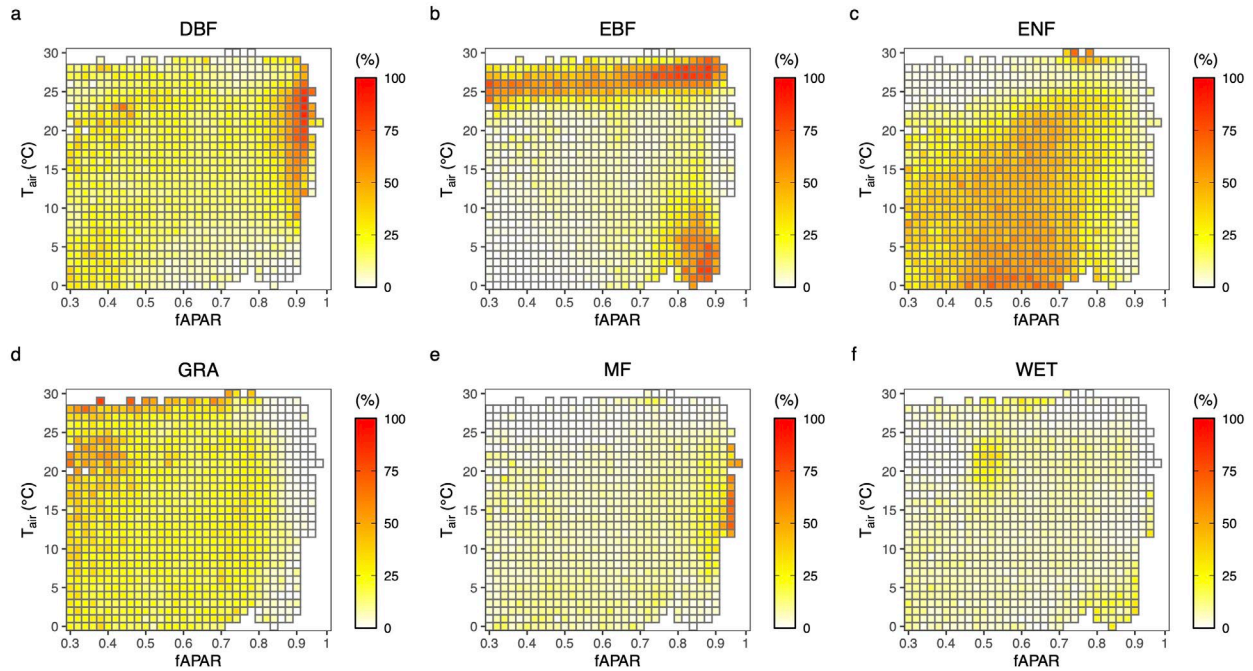
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Supplementary Fig. 2: The partial effect of $\overline{T_{avr}}$ on $A_{\max,2000}$ over fAPAR and T_{air} bins. Diffuse fraction (f_{diff}) is incorporated in the modelling ($A_{\max,2000} \sim \overline{T_{avr}} + f_{\text{diff}} + (1 | \text{Site})$). Site-level f_{diff} is estimated by an artificial neural network model²⁶, due to limited data availability of observed f_{diff} . Numbers (%) in parentheses represent the detectability of positive partial correlation coefficients, which is defined as the percentage of the number of bins displaying a positive partial correlation coefficient over the total number of bins. Black dots indicate significant (two-sided, $P < 0.05$) correlations.

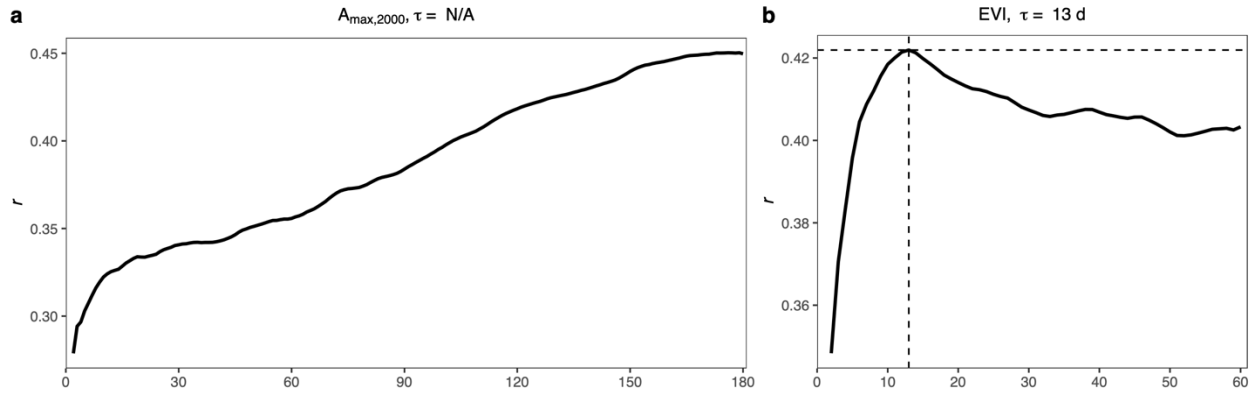


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 176 **Supplementary Fig. 3: Averages (mean), standard deviations (SD) and ranges of**
 177 **environmental variables in the fPAR-T_{air} bin pairs for the cross-site analysis. a–c, The mean**
 178 **(a), SD (b) and range (c) of $\overline{T_{air}}$ (°C), d, the mean of \overline{PPFD} (μmol m⁻² s⁻¹), and e–f, the mean of**
 179 **\overline{VPD} (kPa) and VPD (kPa) in each fPAR-T_{air} bin pair.**

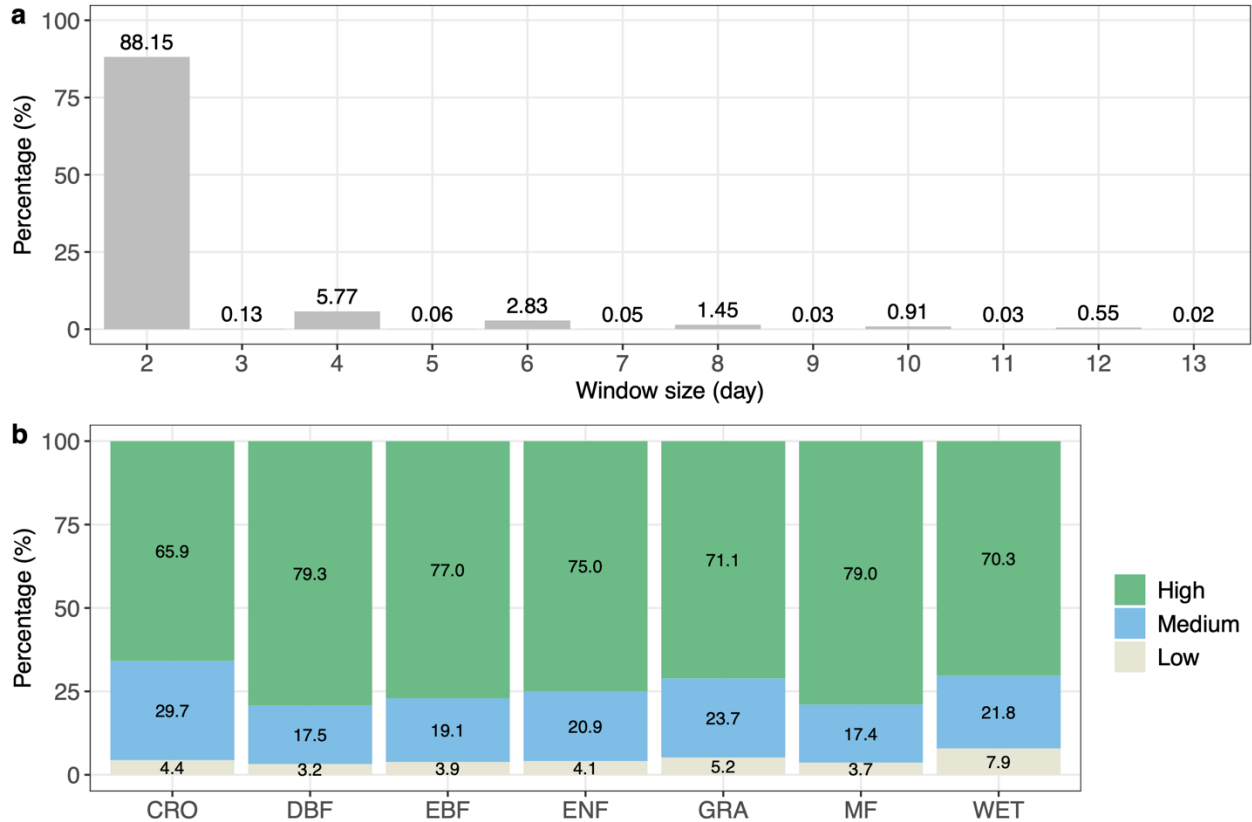
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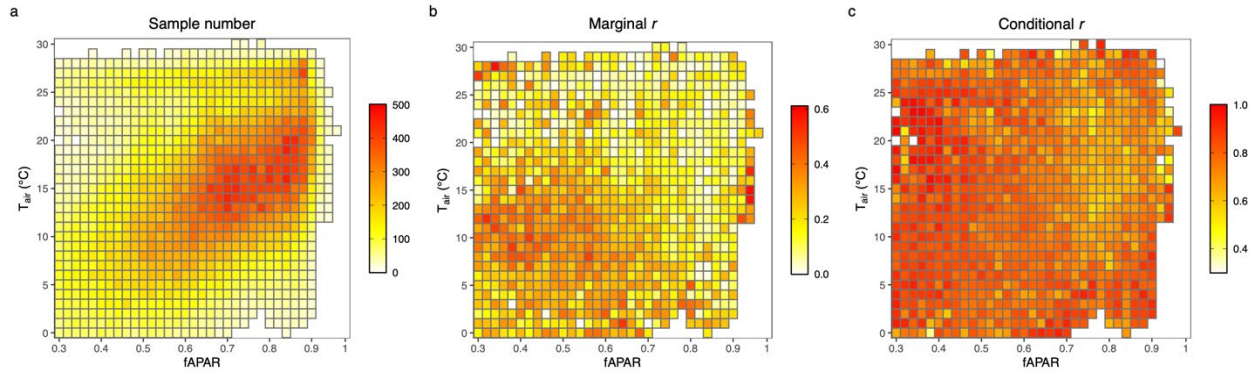
182
 183 **Supplementary Fig. 4: Percentage of each plant functional type (PFT) in fPAR-T_{air} bin**
 184 **pairs for the cross-site analysis. a–f, The ratio (%) of the number of each PFT to the total**
 185 **sampling number in each fPAR-T_{air} bin pair, for deciduous broadleaf forests (DBF) (a),**
 186 **evergreen broadleaf forests (EBF) (b), evergreen needle-leaf forests (ENF) (c), grasslands**
 187 **(GRA) (d), mixed forests (MF) (e), and wetlands (WET) (f).**



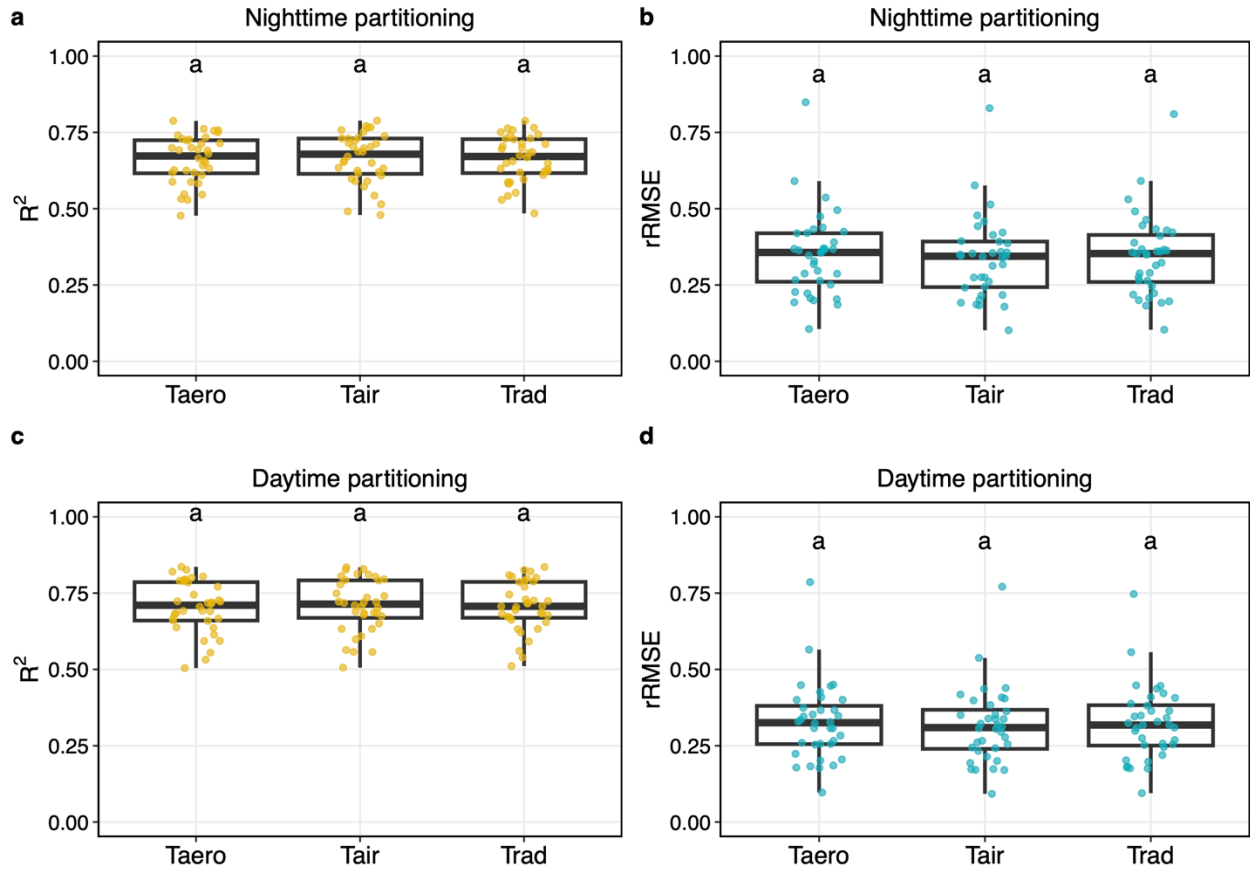
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 189 **Supplementary Fig. 5: Responses of the 5-d moving average of correlation (r) between**
 190 **photosynthetic capacity metrics and $\overline{T_{air}}$ to the number of days used for averaging daytime**
 191 **T_{air} for evergreen broadleaf forests (EBF). a-b, $A_{max,2000}$ (a) and enhanced vegetation index**
 192 **(EVI) (b) are used to indicate canopy photosynthetic capacity. Daily EVI for each EBF flux site**
 193 **is derived from MODIS MCD43A4.**
 194



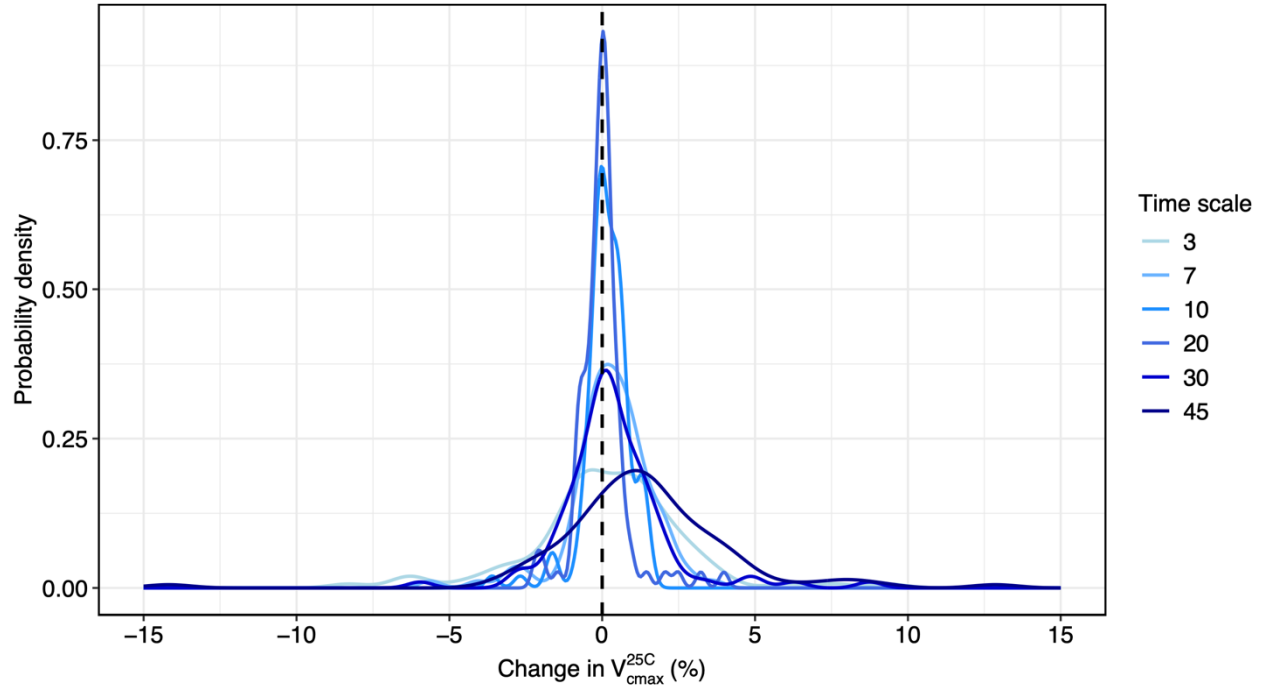
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 196 **Supplementary Fig. 6: Percentages of window sizes (a) and quality flags (b) for the fitted**
 197 **light response curves.** A "low" quality flag indicates that curve fitting cannot be well
 198 constrained with the available data within 14 days. A "medium" quality flag means the curve
 199 fitting can be constrained but the fitting parameters show unreasonable ranges. A "high" quality
 200 flag indicates that the curve fitting is well-constrained and the fitting parameters are within
 201 reasonable ranges. The reasonable range for each parameter is provided in ref.²⁷.
 202



203
 204 **Supplementary Fig. 7: Statistical metrics for the cross-site analysis. a–c,** The sampling
 205 number **(a)**, marginal correlation coefficient (marginal r) **(b)**, and conditional correlation
 206 coefficient (conditional r) **(c)** for the cross-site analysis using linear mix-effect models ($A_{\max,2000}$
 207 $\sim \overline{T_{air}} + (1 | \text{Site})$).
 208



209
 210 **Supplementary Fig. 8: Comparison of model performance in estimating hourly GPP using**
 211 **three temperature approximations. a–d,** Model performance is evaluated based on the
 212 coefficient of determination (R^2 , golden yellow) and GPP partitioned by the nighttime (a) and
 213 daytime (c) methods, as well as relative root mean square error (rRMSE, teal) and GPP
 214 partitioned by the nighttime (b) and daytime (d) methods. The temperature approximations
 215 include aerodynamic surface temperature (T_{aero}), air temperature (T_{air}), and radiometric surface
 216 temperature (T_{rad}). In the box plots, the central lines represent the median values, the upper and
 217 lower box limits represent the 75th and 25th percentiles, and the upper and lower whiskers
 218 extend to 1.5 times the interquartile range, respectively. Identical letters indicate no statistically
 219 significant differences between the average values of the metrics, according to Tukey’s HSD test
 220 (two-sided, $P > 0.05$). The analysis includes only non-cropland, non-dryland, C_3 sites with
 221 acceptable performance (see Supplementary Table 2) and with available data for incoming and
 222 outgoing longwave radiation needed for T_{rad} calculations ($n = 36$).
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Supplementary Fig. 9: Relative change in V_{cmax}^{25C} estimated using a 14-day time scale for acclimation compared to other time scales. The probability density function for the relative change in V_{cmax}^{25C} is estimated using kernel density estimation, based on data from 105 long-term (observational length greater than three years), non-cropland, and C₃ sites.

230 **Supplementary Table 1: Relationships between the site-level observed diffuse fraction and**
 231 **$\overline{T_{avr}}$ for the flux sites where diffuse PAR and direct PAR are available.** The diffuse fraction
 232 is calculated as the ratio of diffuse PAR to the sum of diffuse and direct PAR. The relationship
 233 between the diffuse fraction and $\overline{T_{avr}}$ is modelled as a linear function (diffuse fraction $\sim \overline{T_{avr}}$).
 234 Diffuse fraction and $\overline{T_{avr}}$ show a significant positive relationship at only one of the 41 sites.
 235

Site	IGBP ^a	slope	R ²	p-value
AT-Neu	GRA	-0.0033	0.0295	< 0.05
BE-Bra	MF	-0.0031	0.0293	< 0.05
CA-Gro	MF	-0.0022	0.0198	< 0.05
CA-Obs	ENF	8.00E-04	0.0029	< 0.05
CA-Qfo	ENF	-0.0013	0.0062	< 0.05
CG-Tch	SAV	-0.0242	0.1631	< 0.05
CH-Oe1	GRA	-6.00E-04	0.001	> 0.05
CH-Oe2	CRO	3.00E-04	3.00E-04	> 0.05
CZ-BK1	ENF	-0.0029	0.016	< 0.05
CZ-BK2	GRA	-0.0042	0.0139	> 0.05
DE-Geb	CRO	-0.0065	0.0869	< 0.05
DE-Hai	DBF	-0.0085	0.1278	< 0.05
DE-Tha	ENF	-0.003	0.0455	< 0.05
ES-Ln2	OSH	1.00E-04	0.003	> 0.05
FI-Hyy	ENF	-0.0017	0.0129	< 0.05
FI-Lom	WET	-0.3004	0.0167	< 0.05
FR-Gri	CRO	-0.005	0.0938	< 0.05
FR-LBr	ENF	-0.0036	0.0416	< 0.05
FR-Pue	EBF	-0.0045	0.0568	< 0.05
GF-Guy	EBF	-0.0622	0.1985	< 0.05
GH-Ank	EBF	-0.0237	0.318	< 0.05
IT-BCi	CRO	-0.0073	0.1796	< 0.05
IT-Col	DBF	-0.0055	0.0817	< 0.05
IT-MBo	GRA	-0.0019	0.0076	< 0.05
IT-PT1	DBF	0.0064	0.0126	> 0.05
IT-Ro2	DBF	-0.0068	0.1393	< 0.05
IT-SR2	ENF	-0.008	0.1565	< 0.05
IT-SRo	ENF	-0.0055	0.1152	< 0.05
NL-Loo	ENF	-0.0046	0.0915	< 0.05
RU-Ha1	GRA	-0.008	0.2058	< 0.05
US-Me1	ENF	-0.0046	0.0407	< 0.05
US-Me2	ENF	-0.0064	0.0938	< 0.05
US-MMS	DBF	-0.0027	0.0375	< 0.05
US-Ne1	CRO	-0.0023	0.0341	< 0.05
US-Ne2	CRO	-0.0017	0.0193	< 0.05
US-Ne3	CRO	-0.0019	0.024	< 0.05
US-Syv	MF	-0.0037	0.055	< 0.05
US-UMB	DBF	-0.0042	0.075	< 0.05
US-UMd	DBF	-0.0031	0.0415	< 0.05
US-Var	GRA	-0.0069	0.1031	< 0.05
US-WCr	DBF	8.00E-04	0.001	> 0.05

236 ^aThe land cover classification defined by The International Geosphere–Biosphere Programme
 237 (IGBP) (definitions are as in Fig. 2)
 238

Supplementary Table 2: Site information of the FLUXNET2015 database

Site	Latitude	Longitude	IGBP ^a	Period	Model ^b	DOI
AR-SLu	-33.4648	-66.4598	MF	2009-2011	No	10.18140/FLX/1440191
AR-Vir	-28.2395	-56.1886	ENF	2009-2012	No	10.18140/FLX/1440192
AT-Neu	47.11667	11.3175	GRA	2002-2012	Yes	10.18140/FLX/1440121
AU-Ade	-13.0769	131.1178	WSA	2007-2009	No	10.18140/FLX/1440193
AU-ASM	-22.283	133.249	SAV	2010-2014	No	10.18140/FLX/1440194
AU-Cpr	-34.0021	140.5891	SAV	2010-2014	No	10.18140/FLX/1440195
AU-Cum	-33.61518	150.72362	EBF	2012-2014	No	10.18140/FLX/1440196
AU-DaP	-14.0633	131.3181	GRA	2007-2013	Yes	10.18140/FLX/1440123
AU-DaS	-14.1593	131.3881	SAV	2008-2014	No	10.18140/FLX/1440122
AU-Dry	-15.2588	132.3706	SAV	2008-2014	No	10.18140/FLX/1440197
AU-Emr	-23.8587	148.4746	GRA	2011-2013	No	10.18140/FLX/1440198
AU-Fog	-12.5452	131.3072	WET	2006-2008	No	10.18140/FLX/1440124
AU-Gin	-31.3764	115.7138	WSA	2011-2014	No	10.18140/FLX/1440199
AU-GWW	-30.1913	120.6541	SAV	2013-2014	No	10.18140/FLX/1440200
AU-How	-12.4943	131.1523	WSA	2001-2014	No	10.18140/FLX/1440125
AU-Lox	-34.4704	140.6551	DBF	2008-2009	Yes	10.18140/FLX/1440247
AU-RDF	-14.5636	132.4776	WSA	2011-2013	No	10.18140/FLX/1440201
AU-Rig	-36.6499	145.5759	GRA	2011-2014	Yes	10.18140/FLX/1440202
AU-Rob	-17.1175	145.6301	EBF	2014-2014	No	10.18140/FLX/1440203
AU-Stp	-17.1507	133.3502	GRA	2008-2014	No	10.18140/FLX/1440204
AU-TTE	-22.287	133.64	GRA	2012-2014	No	10.18140/FLX/1440205
AU-Tum	-35.6566	148.1517	EBF	2001-2014	No	10.18140/FLX/1440126
AU-Wac	-37.4259	145.1878	EBF	2005-2008	No	10.18140/FLX/1440127
AU-Whr	-36.6732	145.0294	EBF	2011-2014	No	10.18140/FLX/1440206
AU-Wom	-37.4222	144.0944	EBF	2010-2014	No	10.18140/FLX/1440207
AU-Ync	-34.9893	146.2907	GRA	2012-2014	Yes	10.18140/FLX/1440208
BE-Bra	51.30761	4.51984	MF	1996-2014	No	10.18140/FLX/1440128
BE-Lon	50.55162	4.74623	CRO	2004-2014	No	10.18140/FLX/1440129
BE-Vie	50.30493	5.99812	MF	1996-2014	No	10.18140/FLX/1440130
BR-Sa1	-2.85667	-54.95889	EBF	2002-2011	No	10.18140/FLX/1440032
BR-Sa3	-3.01803	-54.97144	EBF	2000-2004	No	10.18140/FLX/1440033
CA-Gro	48.2167	-82.1556	MF	2003-2014	Yes	10.18140/FLX/1440034
CA-Man	55.87962	-98.48081	ENF	1994-2008	No	10.18140/FLX/1440035
CA-NS1	55.87917	-98.48389	ENF	2001-2005	Yes	10.18140/FLX/1440036
CA-NS2	55.90583	-98.52472	ENF	2001-2005	Yes	10.18140/FLX/1440037
CA-NS3	55.91167	-98.38222	ENF	2001-2005	Yes	10.18140/FLX/1440038
CA-NS4	55.91437	-98.380645	ENF	2002-2005	Yes	10.18140/FLX/1440039
CA-NS5	55.86306	-98.485	ENF	2001-2005	Yes	10.18140/FLX/1440040
CA-NS6	55.91667	-98.96444	OSH	2001-2005	No	10.18140/FLX/1440041
CA-NS7	56.63583	-99.94833	OSH	2002-2005	No	10.18140/FLX/1440042
CA-Oas	53.62889	-106.19779	DBF	1996-2010	Yes	10.18140/FLX/1440043
CA-Obs	53.98717	-105.11779	ENF	1997-2010	Yes	10.18140/FLX/1440044
CA-Qfo	49.6925	-74.34206	ENF	2003-2010	Yes	10.18140/FLX/1440045
CA-SF1	54.48503	-105.81757	ENF	2003-2006	No	10.18140/FLX/1440046
CA-SF2	54.25392	-105.8775	ENF	2001-2005	Yes	10.18140/FLX/1440047
CA-SF3	54.09156	-106.00526	OSH	2001-2006	No	10.18140/FLX/1440048
CA-TP1	42.6609361	-80.559519	ENF	2002-2014	No	10.18140/FLX/1440050
CA-TP2	42.7744194	-80.458775	ENF	2002-2007	No	10.18140/FLX/1440051
CA-TP3	42.7068111	-80.348314	ENF	2002-2014	No	10.18140/FLX/1440052
CA-TP4	42.710161	-80.357376	ENF	2002-2014	Yes	10.18140/FLX/1440053
CA-TPD	42.635328	-80.557731	DBF	2012-2014	Yes	10.18140/FLX/1440112
CG-Tch	-4.28917	11.65642	SAV	2006-2009	No	10.18140/FLX/1440142
CH-Cha	47.21022	8.41044	GRA	2005-2014	No	10.18140/FLX/1440131
CH-Dav	46.81533	9.85591	ENF	1997-2014	No	10.18140/FLX/1440132

CH-Fru	47.11583	8.53778	GRA	2005-2014	No	10.18140/FLX/1440133
CH-Lae	47.47833	8.36439	MF	2004-2014	No	10.18140/FLX/1440134
CH-Oe1	47.28583	7.73194	GRA	2002-2008	No	10.18140/FLX/1440135
CH-Oe2	47.28642	7.73375	CRO	2004-2014	No	10.18140/FLX/1440136
CN-Cha	42.4025	128.0958	MF	2003-2005	No	10.18140/FLX/1440137
CN-Cng	44.5934	123.5092	GRA	2007-2010	Yes	10.18140/FLX/1440209
CN-Dan	30.4978	91.0664	GRA	2004-2005	No	10.18140/FLX/1440138
CN-Din	23.1733	112.5361	EBF	2003-2005	No	10.18140/FLX/1440139
CN-Du2	42.0467	116.2836	GRA	2006-2008	Yes	10.18140/FLX/1440140
CN-Du3	42.0551	116.2809	GRA	2009-2010	Yes	10.18140/FLX/1440210
CN-Ha2	37.6086	101.3269	WET	2003-2005	No	10.18140/FLX/1440211
CN-HaM	37.37	101.18	GRA	2002-2004	Yes	10.18140/FLX/1440190
CN-Qia	26.7414	115.0581	ENF	2003-2005	No	10.18140/FLX/1440141
CN-Sw2	41.7902	111.8971	GRA	2010-2012	No	10.18140/FLX/1440212
CZ-BK1	49.50208	18.53688	ENF	2004-2014	No	10.18140/FLX/1440143
CZ-BK2	49.49443	18.54285	GRA	2004-2012	No	10.18140/FLX/1440144
CZ-wet	49.02465	14.77035	WET	2006-2014	Yes	10.18140/FLX/1440145
DE-Akm	53.86617	13.68342	WET	2009-2014	No	10.18140/FLX/1440213
DE-Geb	51.09973	10.91463	CRO	2001-2014	No	10.18140/FLX/1440146
DE-Gri	50.95004	13.51259	GRA	2004-2014	No	10.18140/FLX/1440147
DE-Hai	51.07921	10.45217	DBF	2000-2012	Yes	10.18140/FLX/1440148
DE-Kli	50.89306	13.52238	CRO	2004-2014	No	10.18140/FLX/1440149
DE-Lkb	49.09962	13.30467	ENF	2009-2013	No	10.18140/FLX/1440214
DE-Lnf	51.32822	10.3678	DBF	2002-2012	Yes	10.18140/FLX/1440150
DE-Obe	50.78666	13.72129	ENF	2008-2014	No	10.18140/FLX/1440151
DE-RuR	50.62191	6.30413	GRA	2011-2014	No	10.18140/FLX/1440215
DE-RuS	50.86591	6.44714	CRO	2011-2014	No	10.18140/FLX/1440216
DE-Seh	50.87062	6.44965	CRO	2007-2010	No	10.18140/FLX/1440217
DE-SfN	47.80639	11.3275	WET	2012-2014	Yes	10.18140/FLX/1440219
DE-Spw	51.89225	14.03369	WET	2010-2014	Yes	10.18140/FLX/1440220
DE-Tha	50.96256	13.56515	ENF	1996-2014	Yes	10.18140/FLX/1440152
DE-Zrk	53.87594	12.88901	WET	2013-2014	Yes	10.18140/FLX/1440221
DK-Eng	55.69053	12.19175	GRA	2005-2008	No	10.18140/FLX/1440153
DK-Fou	56.4842	9.58722	CRO	2005-2005	No	10.18140/FLX/1440154
DK-Sor	55.48587	11.64464	DBF	1996-2014	Yes	10.18140/FLX/1440155
ES-Amo	36.83361	-2.25232	OSH	2007-2012	No	10.18140/FLX/1440156
ES-LgS	37.09794	-2.96583	OSH	2007-2009	No	10.18140/FLX/1440225
ES-LJu	36.92659	-2.75212	OSH	2004-2013	No	10.18140/FLX/1440157
ES-Ln2	36.9695	-3.47582	OSH	2009-2009	No	10.18140/FLX/1440226
FI-Hyy	61.84741	24.29477	ENF	1996-2014	Yes	10.18140/FLX/1440158
FI-Jok	60.8986	23.51345	CRO	2000-2003	No	10.18140/FLX/1440159
FI-Let	60.64183	23.95952	ENF	2009-2012	Yes	10.18140/FLX/1440227
FI-Lom	67.99724	24.20918	WET	2007-2009	Yes	10.18140/FLX/1440228
FI-Sod	67.36239	26.63859	ENF	2001-2014	Yes	10.18140/FLX/1440160
FR-Fon	48.47636	2.7801	DBF	2005-2014	Yes	10.18140/FLX/1440161
FR-Gri	48.84422	1.95191	CRO	2004-2014	No	10.18140/FLX/1440162
FR-LBr	44.71711	-0.7693	ENF	1996-2008	No	10.18140/FLX/1440163
FR-Pue	43.7413	3.5957	EBF	2000-2014	No	10.18140/FLX/1440164
GF-Guy	5.27877	-52.92486	EBF	2004-2014	No	10.18140/FLX/1440165
GH-Ank	5.26854	-2.69421	EBF	2011-2014	No	10.18140/FLX/1440229
GL-NuF	64.13083	-51.38611	WET	2008-2014	No	10.18140/FLX/1440222
GL-ZaF	74.48143	-20.55452	WET	2008-2011	No	10.18140/FLX/1440223
GL-ZaH	74.47328	-20.5503	GRA	2000-2014	No	10.18140/FLX/1440224
IT-BCi	40.52375	14.95744	CRO	2004-2014	No	10.18140/FLX/1440166
IT-CA1	42.38041	12.02656	DBF	2011-2014	No	10.18140/FLX/1440230
IT-CA2	42.37722	12.02604	CRO	2011-2014	No	10.18140/FLX/1440231

IT-CA3	42.38	12.0222	DBF	2011-2014	No	10.18140/FLX/1440232
IT-Col	41.84936	13.58814	DBF	1996-2014	Yes	10.18140/FLX/1440167
IT-Cp2	41.70427	12.35729	EBF	2012-2014	No	10.18140/FLX/1440233
IT-Cpz	41.70525	12.37611	EBF	1997-2009	No	10.18140/FLX/1440168
IT-Isp	45.81264	8.63358	DBF	2013-2014	Yes	10.18140/FLX/1440234
IT-La2	45.9542	11.2853	ENF	2000-2002	No	10.18140/FLX/1440235
IT-Lav	45.9562	11.28132	ENF	2003-2014	No	10.18140/FLX/1440169
IT-MBo	46.01468	11.04583	GRA	2003-2013	Yes	10.18140/FLX/1440170
IT-Noe	40.60618	8.15169	CSH	2004-2014	No	10.18140/FLX/1440171
IT-PT1	45.20087	9.06104	DBF	2002-2004	Yes	10.18140/FLX/1440172
IT-Ren	46.58686	11.43369	ENF	1998-2013	No	10.18140/FLX/1440173
IT-Ro1	42.40812	11.93001	DBF	2000-2008	Yes	10.18140/FLX/1440174
IT-Ro2	42.39026	11.92093	DBF	2002-2012	No	10.18140/FLX/1440175
IT-SR2	43.73202	10.29091	ENF	2013-2014	No	10.18140/FLX/1440236
IT-SRo	43.72786	10.28444	ENF	1999-2012	No	10.18140/FLX/1440176
IT-Tor	45.84444	7.57806	GRA	2008-2014	Yes	10.18140/FLX/1440237
JP-MBF	44.3869	142.3186	DBF	2003-2005	Yes	10.18140/FLX/1440238
JP-SMF	35.2617	137.0788	MF	2002-2006	No	10.18140/FLX/1440239
MY-PSO	2.973	102.3062	EBF	2003-2009	No	10.18140/FLX/1440240
NL-Hor	52.24035	5.0713	GRA	2004-2011	Yes	10.18140/FLX/1440177
NL-Loo	52.16658	5.74356	ENF	1996-2014	No	10.18140/FLX/1440178
PA-SPn	9.31814	-79.6346	DBF	2007-2009	No	10.18140/FLX/1440180
PA-SPs	9.31378	-79.63143	GRA	2007-2009	No	10.18140/FLX/1440179
RU-Che	68.61304	161.34143	WET	2002-2005	Yes	10.18140/FLX/1440181
RU-Cok	70.82914	147.49428	OSH	2003-2014	No	10.18140/FLX/1440182
RU-Fyo	56.46153	32.92208	ENF	1998-2014	No	10.18140/FLX/1440183
RU-Ha1	54.72517	90.00215	GRA	2002-2004	Yes	10.18140/FLX/1440184
SD-Dem	13.2829	30.4783	SAV	2005-2009	No	10.18140/FLX/1440186
SJ-Adv	78.186	15.923	WET	2011-2014	No	10.18140/FLX/1440241
SJ-Blv	78.92163	11.83109	SNO	2008-2009	No	10.18140/FLX/1440242
SN-Dhr	15.40278	-15.43222	SAV	2010-2013	No	10.18140/FLX/1440246
US-AR1	36.4267	-99.42	GRA	2009-2012	No	10.18140/FLX/1440103
US-AR2	36.6358	-99.5975	GRA	2009-2012	No	10.18140/FLX/1440104
US-ARb	35.5497	-98.0402	GRA	2005-2006	Yes	10.18140/FLX/1440064
US-ARc	35.54649	-98.04	GRA	2005-2006	Yes	10.18140/FLX/1440065
US-ARM	36.6058	-97.4888	CRO	2003-2012	No	10.18140/FLX/1440066
US-Atq	70.4696	-157.4089	WET	2003-2008	No	10.18140/FLX/1440067
US-Blo	38.8953	-120.6328	ENF	1997-2007	No	10.18140/FLX/1440068
US-Cop	38.09	-109.39	GRA	2001-2007	No	10.18140/FLX/1440100
US-CRT	41.628495	-83.347086	CRO	2011-2013	No	10.18140/FLX/1440117
US-GBT	41.36579	-106.2397	ENF	1999-2006	Yes	10.18140/FLX/1440118
US-GLE	41.36653	-106.2399	ENF	2004-2014	Yes	10.18140/FLX/1440069
US-Goo	34.2547	-89.8735	GRA	2002-2006	No	10.18140/FLX/1440070
US-Ha1	42.5378	-72.1715	DBF	1991-2012	Yes	10.18140/FLX/1440071
US-IB2	41.84062	-88.24103	GRA	2004-2011	Yes	10.18140/FLX/1440072
US-Ivo	68.4865	-155.7503	WET	2004-2007	Yes	10.18140/FLX/1440073
US-KS1	28.4583	-80.6709	ENF	2002-2002	No	10.18140/FLX/1440074
US-KS2	28.6086	-80.6715	CSH	2003-2006	No	10.18140/FLX/1440075
US-Lin	36.3566	-119.8423	CRO	2009-2010	No	10.18140/FLX/1440107
US-Los	46.0827	-89.9792	WET	2000-2014	Yes	10.18140/FLX/1440076
US-LWW	34.9604	-97.9789	GRA	1997-1998	No	10.18140/FLX/1440077
US-Me1	44.5794	-121.5	ENF	2004-2005	No	10.18140/FLX/1440078
US-Me2	44.4523	-121.5574	ENF	2002-2014	No	10.18140/FLX/1440079
US-Me3	44.3154	-121.6078	ENF	2004-2009	No	10.18140/FLX/1440080
US-Me4	44.4992	-121.6224	ENF	1996-2000	No	10.18140/FLX/1440081
US-Me5	44.43719	-121.56676	ENF	2000-2002	No	10.18140/FLX/1440082

US-Me6	44.3232842	-121.6078	ENF	2010-2014	No	10.18140/FLX/1440099
US-MMS	39.3232	-86.4131	DBF	1999-2014	Yes	10.18140/FLX/1440083
US-Myb	38.049861	-121.76498	WET	2010-2014	No	10.18140/FLX/1440105
US-Ne1	41.16506	-96.47664	CRO	2001-2013	No	10.18140/FLX/1440084
US-Ne2	41.16487	-96.4701	CRO	2001-2013	No	10.18140/FLX/1440085
US-Ne3	41.17967	-96.43965	CRO	2001-2013	No	10.18140/FLX/1440086
US-NR1	40.0329	-105.5464	ENF	1998-2014	Yes	10.18140/FLX/1440087
US-Oho	41.5545	-83.8438	DBF	2004-2013	Yes	10.18140/FLX/1440088
US-ORv	40.0201	-83.0183	WET	2011-2011	No	10.18140/FLX/1440102
US-PFa	45.9459	-90.2723	MF	1995-2014	No	10.18140/FLX/1440089
US-Prr	65.12367	-147.48756	ENF	2010-2014	Yes	10.18140/FLX/1440113
US-SRC	31.9083	-110.8395	MF	2008-2014	No	10.18140/FLX/1440098
US-SRG	31.789379	-110.82768	GRA	2008-2014	No	10.18140/FLX/1440114
US-SRM	31.8214	-110.8661	WSA	2004-2014	No	10.18140/FLX/1440090
US-Sta	41.3966	-106.8024	OSH	2005-2009	No	10.18140/FLX/1440115
US-Syv	46.242	-89.3477	MF	2001-2014	No	10.18140/FLX/1440091
US-Ton	38.4316	-120.96598	WSA	2001-2014	No	10.18140/FLX/1440092
US-Tw1	38.1074	-121.6469	WET	2012-2014	No	10.18140/FLX/1440108
US-Tw2	38.1047	-121.6433	CRO	2012-2013	No	10.18140/FLX/1440109
US-Tw3	38.1159	-121.6467	CRO	2013-2014	No	10.18140/FLX/1440110
US-Tw4	38.10298	-121.6414	WET	2013-2014	No	10.18140/FLX/1440111
US-Twt	38.1087204	-121.6531	CRO	2009-2014	No	10.18140/FLX/1440106
US-UMB	45.5598	-84.7138	DBF	2000-2014	Yes	10.18140/FLX/1440093
US-UMd	45.5625	-84.6975	DBF	2007-2014	Yes	10.18140/FLX/1440101
US-Var	38.4133	-120.9507	GRA	2000-2014	Yes	10.18140/FLX/1440094
US-WCr	45.8059	-90.0799	DBF	1999-2014	Yes	10.18140/FLX/1440095
US-Whs	31.7438	-110.0522	OSH	2007-2014	No	10.18140/FLX/1440097
US-Wi0	46.618778	-91.081444	ENF	2002-2002	Yes	10.18140/FLX/1440055
US-Wi1	46.730472	-91.232944	DBF	2003-2003	Yes	10.18140/FLX/1440054
US-Wi2	46.686889	-91.152833	ENF	2003-2003	No	10.18140/FLX/1440056
US-Wi3	46.634722	-91.098667	DBF	2002-2004	Yes	10.18140/FLX/1440057
US-Wi4	46.739333	-91.16625	ENF	2002-2005	No	10.18140/FLX/1440058
US-Wi5	46.653083	-91.085806	ENF	2004-2004	Yes	10.18140/FLX/1440059
US-Wi6	46.624889	-91.298222	OSH	2002-2003	No	10.18140/FLX/1440060
US-Wi7	46.649111	-91.069278	OSH	2005-2005	No	10.18140/FLX/1440061
US-Wi8	46.722333	-91.252417	DBF	2002-2002	Yes	10.18140/FLX/1440062
US-Wi9	46.618778	-91.081444	ENF	2004-2005	No	10.18140/FLX/1440063
US-Wkg	31.7365	-109.9419	GRA	2004-2014	No	10.18140/FLX/1440096
US-WPT	41.464639	-82.996157	WET	2011-2013	No	10.18140/FLX/1440116
ZM-Mon	-15.4391	23.2525	DBF	2000-2009	No	10.18140/FLX/1440189

240 ^aThe land cover classification defined by The International Geosphere–Biosphere Programme

241 (IGBP) (definitions are as in Fig. 1)

242 ^bIf the site is C₃, non-cropland and non-dryland, and demonstrates acceptable model performance

243 ($R^2 > 0.5$) across all three model variants

244 **Supplementary Table 3: Parameter values for temperature dependency functions of V_{cmax}**
 245 **and J_{max} (equation 5)**

246

Parameters	$H_{a,v}$ ^a	$H_{a,j}$ ^b	S_v ^c	S_j ^d	b_{jv} ^e
a	1.14	0	-0.38	0	0
b	0	0	0	-0.84	-0.0375
c	0	0	0	-0.52	-0.0202
d	42.6	40.71	645.13	658.77	2.56

247 ^aActivation energy of V_{cmax}

248 ^bActivation energy of J_{max}

249 ^cEntropy term of V_{cmax}

250 ^dEntropy term of J_{max}

251 ^eThe ratio of J_{max}^{25C} to V_{cmax}^{25C}

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253

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