

# Supporting Text

## 1 Dynamic Structure Factor

For the fits to the dynamic light-scattering data we use an expression for the dynamic structure factor derived from the single-polymer transverse mean square displacement (MSD) of a point on the contour (1). By a normal mode analysis as outlined in *Methods*, one finds for the MSD (1–3):

$$\delta r_{\perp}^2(t) = \langle [\mathbf{r}_{\perp}(s, t) - \mathbf{r}_{\perp}(s, 0)]^2 \rangle \quad [5]$$

$$\approx \frac{4L^3}{\pi^4 \ell_p} \int_0^{L/a} dn \frac{1 - \exp[-(t/\tilde{\tau}_n)\tilde{h}(k_n)]}{n^4}, \quad [6]$$

where  $k_n = \pi n/L$ ,  $\tau_n = 4\pi\eta/\kappa k_n^4$ , and

$$\tilde{\tau}_n = \begin{cases} \tau_n & (n > \ell), \\ \tau_n \exp[\mathcal{E}(l/n - 1)] & (n < \ell), \end{cases} \quad (\ell = L/\Lambda) \quad [7]$$

is the relaxation time of the glassy wormlike chain and  $\tilde{h}(k) = 4\pi\eta h(k)$  is the Fourier transform of the (“Rotne-Prager”) mobility function,

$$\tilde{h}(k) = \gamma_{RP} - \log(ka) + \mathcal{O}(k^2 a^2), \quad [8]$$

which represents a dimensionless refining factor to the simple “free-draining” approximation with a constant friction coefficient  $\zeta_{\perp}$  employed in *Methods*. This factor depends on the hydrodynamic constant  $\gamma_{RP}$  and on the backbone diameter  $a$  of the filament.

For  $n > \ell$  the following approximation to the integral Eq. 6 is used:

$$\delta r_{\perp, \Lambda}^2(t) = \frac{4\Lambda^3}{3\ell_p\pi^4} \left[ 1 - \frac{3}{4} \left( \frac{t}{\tau_\Lambda} \right)^{3/4} \left\{ -\log [e^{-B} a/\ell_\perp(t)] \right\}^{3/4} \right. \\ \left. \Gamma(-3/4, (t/\tau_\Lambda) \left\{ -\log [e^{-B} a/\ell_\perp(t)] \right\}) \right]. \quad [9]$$

Here,  $\tau_\Lambda \equiv \tau_\ell = (4\pi\eta/\kappa)(\Lambda/\pi)^4$  is the relaxation time of a mode of (half) wavelength  $\Lambda$ . The length  $\ell_\perp(t) = (\kappa t/4\pi\eta)^{1/4}$  is the transverse elastohydrodynamic correlation length. The constant  $B$  is defined as  $B = \gamma_{RP} - \log(\tilde{n}_0)$  where  $\tilde{n}_0$  is a numerically determined mode number. The (approximated) integral for  $n < \ell$ ,

$$r_{\perp}^{2,G}(t) = \frac{4L^3}{\ell_p\pi^4} \int_0^\ell dn \frac{1 - \exp(-(t/\tau_1)n^4 \exp[-\mathcal{E}(l/n - 1)] \{B - \log[a/\ell_\perp(t)]\})}{n^4} \quad [10]$$

is evaluated numerically (an analytic approximation is given in ref. 4). The dynamic structure factor in the limit  $t \gg \tau_q = 4\pi\eta/\kappa q^4$  immediately follows (1),

$$S(q, t)/S(q, 0) = \exp(-q^2[\delta r_{\perp}^{2,G}(t) + \delta r_{\perp, \Lambda}^2(t)]/4). \quad [11]$$

To produce the fits of Eq. 11 to the DLS data in Fig. 5 of the main text, we used the constants  $\ell_p = 9 \mu\text{m}$  and  $a = 9 \text{ nm}$  (5). The free parameters were the stretching parameter  $\mathcal{E}$ , the interaction length  $\Lambda$ , and the hydrodynamic constant  $B$ . The values obtained for  $c = 17 \mu\text{M}$  and different values of the scattering vector  $q$  are given in SI Figs. 7-9.

The applicability of single-polymer theory (1) becomes questionable for low values of  $q$  comparable to the inverse mesh size  $\xi^{-1}$ . As  $\xi^{-1} = 2.6 \mu\text{m}^{-1}$  for  $c = 17 \mu\text{M}$ , a quantitative evaluation of the fits should focus on the largest measurable  $q \gg 2.6 \mu\text{m}^{-1}$ . The data in SI Figs. 7-9 suggest that (at least) the values obtained

for  $q \lesssim 10 \mu\text{m}^{-1}$  have to be discarded as meaningless, while those obtained for  $10 \mu\text{m}^{-1} \lesssim q \lesssim 15 \mu\text{m}^{-1}$  still exhibit some small but noticeable systematic errors.

The MSD given by Eq. 6 exhibits a remarkable symmetry. It is straightforward to check that upon simultaneously rescaling  $\Lambda \rightarrow \Lambda' = \gamma\Lambda$  and  $\mathcal{E} \rightarrow \mathcal{E}' = \gamma\mathcal{E}$ , the long-time tails of the original MSD  $\delta r_{\perp}^2$  and the MSD of the rescaled variables,  $\delta r'_{\perp}{}^2$ , can be superimposed, that is,  $\delta r'_{\perp}{}^2(t) = \delta r_{\perp}^2(\alpha t)$  for  $t \gg \tau_{\Lambda}, \tau_{\Lambda'}$  with  $\alpha = \exp[\mathcal{E}(\gamma-1)]$  (the weak mode-number dependence of the mobility function is neglected). Inset of Fig. 5 in the main text demonstrates that this symmetry is well obeyed for  $q = 8.04 \mu\text{m}^{-1}$ .

## 2 Linear Viscoelastic Modulus of a Glassy wormlike Chain

In the theory of Soft Glassy Rheology (SGR) (6), the noise temperature  $1 < x < 2$  is directly monitored by the power-law exponent  $x - 1$  of the linear viscoelastic moduli for low frequencies ( $G'(\omega), G''(\omega) \sim \omega^{x-1}$ ). In this section,  $x$  will be compared to the stretching parameter  $\mathcal{E}$  of a glassy wormlike chain (GWLC).

By applying the the prescription of the GWLC to the high-frequency limiting form of the dynamical shear modulus of a wormlike chain (7), we calculate the macrorheological modulus of a GWLC (4). Its expression for vanishing prestress is

$$G(\omega) = \frac{1}{5}\Lambda/\xi^2\alpha(\omega), \quad [12]$$

here  $\xi = \sqrt{3/c_p L}$  is the mesh size and

$$\alpha(\omega) = \alpha_L \sum_{n=1}^{\infty} \frac{1}{n^4 + i\omega\tilde{\tau}_n/2} \quad [13]$$

with the prefactor  $\alpha_L = L^4/(kT\pi^4\ell_p^2)$  is the susceptibility of the GWLC to a point force at the ends. The relaxation times  $\tilde{\tau}_n$  are modified as described in section 1. By an analytic approximation it is possible to determine the functional dependence of  $G(\omega)$  on the frequency and the stretching parameter  $\mathcal{E}$ . The viscoelastic modulus of a GWLC is not a simple power law but a function that depends essentially logarithmically on frequency. An approximation to the storage modulus valid for  $\omega\tau_\Lambda \ll 1$ ,  $\mathcal{E} \gg 1$  is

$$G'(\omega) = \frac{\Lambda}{5\xi^2\alpha_\Lambda} \frac{3}{\left(1 - \frac{4}{\mathcal{E}} \log \left[ \frac{4}{\mathcal{E}} \left(\frac{\omega\tau_\Lambda}{2}\right)^{1/4} \right] - \frac{4}{\mathcal{E}} \log \left\{ \frac{\mathcal{E}}{4} - \log \left[ \left(\frac{\omega\tau_\Lambda}{2}\right)^{1/4} \right] \right\} \right)^3} \quad [14]$$

From Eq. 14 it is straightforward to derive the local power law exponent of the elastic modulus for  $\mathcal{E} \gg 1$  at a fixed frequency. Asymptotically for  $\mathcal{E} \rightarrow \infty$  (at fixed  $\omega$ ) the result is  $x - 1 = 3/\mathcal{E}$  (note that the limits  $\mathcal{E} \rightarrow \infty$  and  $\omega \rightarrow 0$  do not commute). This result and the exact slope valid for all  $\mathcal{E}$  are shown in SI Fig. 10.

A similar analysis can be carried out for the loss angle  $\delta = \arctan(G''/G')$ . The exact value as a function of  $\mathcal{E}$  at a fixed frequency and the asymptotic analytical approximation  $\delta = \arctan(5/\mathcal{E}) \approx 5/\mathcal{E}$  (valid for  $\mathcal{E} \rightarrow \infty$  at  $\mathcal{E}\omega/\omega_\Lambda = \text{const.} \ll 1$ ) are given in SI Fig. 10. Our result ( $5(x - 1)/3 = \delta$ ) is compatible with power-law rheology, where the exact relation  $(\pi/2)(x - 1) = \delta$  is expected (8). The deviation of our factor from the exact value is an artefact of the analytical approximations made.

## References

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