

Supporting Information

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SI Text

Methods. NO, NO₂, and HONO detection. A THERMO 42C chemiluminescence analyzer was used for NO and NO₂ detection. The latter is based on the reaction between nitric oxide (NO) and ozone (O₃), which produces a characteristic luminescence with an intensity that is linearly proportional to the NO concentration. Nitrogen dioxide is transformed into NO by means of a molybdenum NO₂-to-NO converter in order to be measured with the chemiluminescent reaction. As HONO is detected by the instrument as NO₂, a denuder tube (9 cm × 0.95 cm i.d.) containing K₂CO₃/Na₂CO₃ (Fluka) was introduced between the exit of the flow reactor and the detector. The denuder can be either bypassed leading to the detection of NO and NO₂ together with HONO; or it can be switched into the sample line along the experiment. In that case, only NO and NO₂ can be measured after HONO removal from the gas stream. Therefore, the HONO concentration can be obtained as the difference of the detector signal without and with the carbonate denuder in the sampling line (1).

Periodical calibrations of the NO₂ from the bottle were performed using the carbonate denuder. Only 3% of the total NO₂ (and possible contaminants) was trapped in the denuder, this value was then considered in the calculation of the uptake coefficients and products yield.

Estimation of NO₂ photodissociation. NO₂ may photodissociate with unit quantum yield in the wavelength region emitted by the lamps (300–420 nm), but its loss in the gas phase is negligible for the residence time of 6 seconds used in our experiments. An estimation of the photolysis rate constant, $J = 6.52 \times 10^{-4} \text{ s}^{-1}$ gives rise to a loss of 0.4% of the total NO₂ (g).

Uptake coefficient. The kinetic behaviour of the NO₂-soot heterogeneous reaction both in the dark and under irradiation can be well described by assuming a pseudo first-order reaction with respect to the gas-phase NO₂ concentration. The first-order rate constant, k_{obs} , derived from the experiment, is related to the geometric uptake coefficient (γ_g) by

$$\frac{d}{dt} \ln \frac{C_0}{C_i} = k_{\text{obs}} = \frac{\gamma_g \langle c_{\text{NO}_2} \rangle}{2r_{\text{tube}}} \quad [1]$$

where r_{tube} , γ_g , t , and $\langle c_{\text{NO}_2} \rangle$ are the flow-tube radius (0.547 cm), the geometric uptake coefficient, the exposure time, and the NO₂ average molecular velocity, respectively. C_0 is the NO₂ concentration when there is no contact between the soot surface and the reagent, whereas C_i is the trace gas concentration when the contact with NO₂ is allowed. The uptake coefficient is defined as the fraction of effective collisions between a gas phase reagent and a reactive surface that lead to the loss of the gas phase reagent due to chemical reaction. As γ_g is a mass dependent parameter (Fig. S2), it was transformed into a mass independent one, γ_{BET} , by taking into account the entire BET surface area of the soot sample instead of the geometric surface area of the glass substrate.

Equation I does not take into account possible diffusion limitations caused by the formation of a radial concentration gradient in the gas phase, which would occur if the loss at the surface is too fast to be recovered with the reagent supply. As a consequence, the Cooney–Kim–Davis method was used to correct the calculated uptake coefficients for gas-phase diffusion (2, 3). The diffusion coefficient, D , was calculated by using the formula proposed by Fuller et al. (4).

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3. Murphy DM, Fahey DW (1987) Mathematical treatment of the wall loss of a trace species in denuder and catalytic-converter tubes. *Anal Chem* 59:2753–2759.
4. Fuller EN, Ensley K, Giddings JC (1969) Diffusion of halogenated hydrocarbons in helium. The effect of structure on collision cross sections. *J Phys Chem* 73(11):3679–3685.

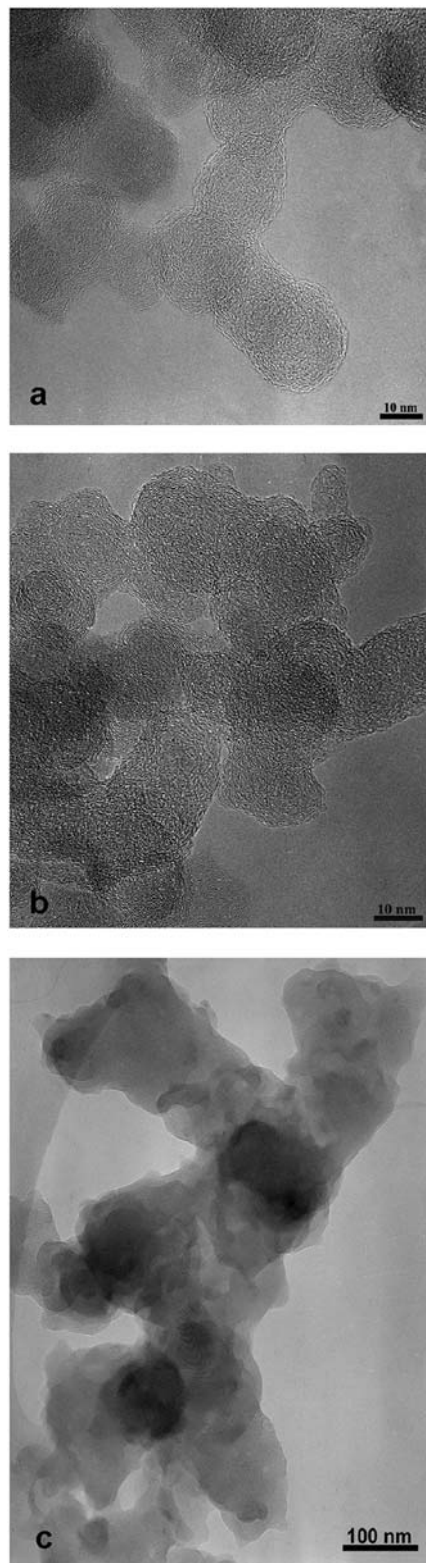


Fig. S1. TEM images of propane soot generated with a lean flame (a), a stoichiometric flame (b), and a rich flame (c).

