

## Supporting Information

### Properties of the modular model of a two-component signal transduction system

First, we will show that in Eq. (2) (see main text),  $[R - P]$  (the concentration of phosphorylated regulator) approaches  $C_p$  in the limit of large  $[R]_{total}$  (total regulator concentration). Rewrite Eq. (2) as

$$2[R - P] = C_t + C_p + [R]_{total} - \sqrt{(C_t + C_p + [R]_{total})^2 - 4C_p[R]_{total}} \quad (S1)$$

(note that the quantities  $C_t$  and  $C_p$  are both positive).

Denote

$$a = C_t + C_p,$$

$$b = 4C_p,$$

$$y = a + [R]_{total}.$$

With this notation, from Eq. (S1) we get

$$\begin{aligned} 2[R - P] &= a + [R]_{total} - \sqrt{(a + [R]_{total})^2 - b[R]_{total}} = y - \sqrt{y^2 - b(y - a)} \\ &= y - \sqrt{y^2 - by + ab}. \end{aligned}$$

It follows that

$$\lim_{[R]_{total} \rightarrow \infty} 2[R - P] = \lim_{y \rightarrow \infty} \frac{1 - \sqrt{1 - b/y + ab/y^2}}{1/y} = \lim_{x \rightarrow 0} \frac{1 - \sqrt{1 - bx + abx^2}}{x}, \quad (S2)$$

where  $x = 1/y$ . Because both the numerator and the denominator in Eq. (S2) approach 0 as  $x \rightarrow 0$ , we use L'Hôpital's rule to calculate that limit. After differentiating both the numerator and the denominator in Eq. (S2), we get

$$\lim_{[R]_{total} \rightarrow \infty} 2[R - P] = \lim_{x \rightarrow 0} \frac{b - 2abx}{2\sqrt{1 - bx + abx^2}} = b/2 = 2C_p. \quad (S3)$$

This expression proves that  $[R - P] \rightarrow C_p$  in the limit of large  $[R]_{total}$ .

Next, we will show that the variable  $[R - P]$  in Eq. (2) (main text) is a monotonically increasing function of  $[R]_{total}$ . Write Eq. (2) as  $[R - P] = g([R]_{total})$ . We have that

$$g([R - P]) = a + [R]_{total} - \sqrt{(a + [R]_{total})^2 - 4C_p[R]_{total}};$$

$$g'([R - P]) = 1 - \frac{a + [R]_{total} - 2C_p}{\sqrt{(a + [R]_{total})^2 - 4C_p[R]_{total}}}.$$

If  $a + [R]_{total} \leq 2C_p$ , then  $g'([R - P]) \geq 1$ , and, therefore,  $g$  is monotonically increasing.

Let us assume that  $a + [R]_{total} > 2C_p$ . In this case,  $g'([R - P]) > 0$  will follow if

$$a + [R]_{total} - 2C_p < \sqrt{(a + [R]_{total})^2 - 4C_p[R]_{total}}$$

or, equivalently,

$$(a + [R]_{total} - 2C_p)^2 < (a + [R]_{total})^2 - 4C_p[R]_{total}.$$

After some algebra, this inequality is reduced to

$$-aC_p + C_p^2 < 0.$$

Because  $a = C_p + C_k > C_p$ , the inequality above holds, proving that  $[R - P]$  in Eq. (2) is a monotonically increasing function of  $[R]_{total}$ .

Now, we will prove that  $[R]_{total}$  is an increasing function of  $B$  in Eqs. (1)–(2). Let the pair  $\{[R]_{total} = R_0, [R - P] = P_0\}$  be the solution to Eqs. (1)–(2) for a certain value  $B = B_0$ .

Now, let  $B_1 > B_0$ , and let  $\{R_1, P_1\}$  be the solution to Eqs. (1)–(2) for  $B_1$ . We need to

prove that  $R_1 > R_0$ . Consider the functions  $[R]_{total} = f_B([R - P])$  and  $[R - P] = g([R]_{total})$

defined by Eq. (1) and Eq. (2), respectively. Because  $g$  is monotonically increasing,  $g^{-1}$

exists (and also is monotonically increasing), and Eq. (2) is equivalent to

$[R]_{total} = g^{-1}([R - P])$ . We have that  $g^{-1}(P_1) = f_{B_1}(P_1) = R_1$ . Further,

$f_{B_0}(P_1) < f_{B_1}(P_1) = g^{-1}(P_1)$ , which follows from the definition of the function  $f_B$ . At the

same time,  $g^{-1}(0) = 0 < f_{B_0}(0) = \tau B_0$ . Therefore, due to the continuity of  $g^{-1}$  and  $f_{B_0}$ ,

these functions attain the same value  $X$  for some  $[R - P]_X \in (0, P_1)$ . Therefore, the pair

$\{X, [R - P]_X\}$  is the solution to Eqs. (1)–(2) for  $B = B_0$ . Because this solution is unique

(see Supplementary Information in Ref. 1),  $X = R_0$  and  $[R - P]_X = P_0$ . This implies that

$P_0 < P_1$ . Because  $g^{-1}$  is a monotonically increasing function,  $R_0 = g^{-1}(P_0) < g^{-1}(P_1) = R_1$ ,

Q.E.D.

## Parameter values for the models

For the modular model of two-component signal transduction (Eqs. (1)–(2)), we used the following parameter values (taken from Ref. 1):  $D = 40$ ,  $C_t = 1$ , and  $C_p$ ,  $\tau_A$ , and  $\tau_B$  as indicated in the main text. For the simple model of positive autoregulation (Eqs. (3)–(4)) we used the following parameter values (taken from Ref. 2):  $k_{-a} = 20 \text{ min}^{-1}$ ,  $H = 2$ ,  $K = 5 \text{ }\mu\text{M}^{-2}$ ,  $k_d = 0.08 \text{ min}^{-1}$ , and  $k_1$ ,  $k_2$ ,  $k_a$  as indicated in the main text.

## References

1. Miyashiro, T. & Goulian, M. (2008). High stimulus unmasks positive feedback in an autoregulated bacterial signaling circuit. *Proc Natl Acad Sci USA* **105**, 17457-17462.
2. Mitrophanov, A. Y. & Groisman, E. A. (2008). Positive feedback in cellular control processes. *Bioessays* **30**, 542-555.
3. Shin, D. & Groisman, E. A. (2005). Signal-dependent binding of the response regulators PhoP and PmrA to their target promoters *in vivo*. *J Biol Chem* **280**, 4089-4094.
4. Perez, J. C., Shin, D., Zwir, I., Latifi, T., Hadley, T. J. & Groisman, E. A. (2009). Evolution of a bacterial regulon controlling virulence and  $\text{Mg}^{2+}$  homeostasis. *PLoS Genetics* **5**, Art. No. e1000428.

5. Shin, D., Lee, J., Huang, H. & Groisman, E. A. (2006). A positive feedback loop promotes transcription surge that jump-starts *Salmonella* virulence circuit. *Science* **314**, 1607-1609.

Table S1. Bacterial strains used in this study.

<b>Strain</b>	<b>Description</b>	<b>Source</b>
EG13918	<i>phoP</i> -HA	Ref. 3
EG14338	Deletion of PhoP box in EG13918	Ref. 4
EG14943	Replacement of the PhoP box with -35 hexamer in EG13918	Ref. 5

Table S2. Primers used for RT-PCR.

Primer No.	Target genes	Sequences (5' - 3')
4443	<i>mgtA</i> forward	TAATTGCCACAAAACCTTATG
4446	<i>mgtA</i> reverse	TCGCGGGAGAGGGGTGGGTT
4485	<i>mgtC</i> forward	GCGGGATTACGCACTAATGC
4486	<i>mgtC</i> reverse	GTCATGGAGCTCAGAATAAAAACG
6964	<i>pagC</i> forward	AAAAGATTAAATCGGAGCGGGA
6965	<i>pagC</i> reverse	TGACGCTCCATCCGCAATA
7013	<i>pagD</i> forward	ACATCATGCTTTTATGCTTTGGTC
7017	<i>pagD</i> reverse	AAACCAGAACAATGGCCTGAA
4489	<i>phoP</i> forward	GATGAAGACGGCCTTTCCTTAA
4490	<i>phoP</i> reverse	GAACCGGCAGTGAAACATCA
7108	<i>ugtL</i> forward	CGATTAGCTGACGGCTTTGTTT
7114	<i>ugtL</i> reverse	GATTTCTTCATTTTGAGCCTCCTC
7116	<i>yobG</i> forward	TGAAAAAATTTTCGATGGGTCG
7118	<i>yobG</i> reverse	TGATATTAACACCTGCGCCC
3023	<i>rrs</i> forward	CCAGCAGCCGCGGTAAT
3024	<i>rrs</i> reverse	TTTACGCCAGTAATTCCGATT