

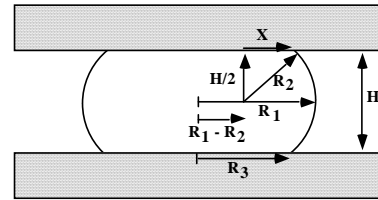


**Aggregate compression.** The inner chamber is filled with pre-warmed CO<sub>2</sub>-independent tissue culture medium (Gibco/BRL, NY). Aggregates ranging in size from about 200-300 μ are positioned on the lower compression plate. The upper compression plate (UCP) is positioned above the aggregate and allowed to settle, establishing a pre-compression apparent UCP weight baseline. The LCP is raised until the aggregate is compressed against the UCP. Adjusting the height of the inner core of the lower apparatus controls different degrees of compression. Compression is monitored by observation through a dissecting microscope equipped with a CCD video camera. Aggregate images are captured, digitized, and analyzed using ImageJ software. Apparent UCP weight change is continuously recorded on a strip chart recorder, achievement of shape equilibrium being denoted by the leveling-off of the Cahn balance's voltage output. Each aggregate is subjected to 2 different degrees of compression, the second greater than the first.

**Calculation of aggregate cohesivity.** At shape equilibrium, the cohesivity of an aggregate of cells compressed between parallel plates to which it does not adhere can be obtained from the Young-Laplace equation (Eqn. S1, Fig. S2), where  $\sigma$  is cohesivity,  $F$  is the force acting to compress the aggregate,  $\pi r^2_3$  is the area of the surface of the aggregate upon which force  $F$  is exerted, and  $R_2$  and  $R_3$  are, respectively, the radius of the equator of the compressed aggregate and the radius of an arc defining its surface profile normal to the compressing plates and extending between them. Measuring the compressive force and geometry at force and shape equilibrium and applying these measurements to the Young-Laplace equation generates numerical values of *apparent* tissue surface tension. Upon reaching equilibrium and calculation of  $\sigma_1$ , aggregates will be decompressed and allowed to approach a second equilibrium  $\sigma_2$  will be calculated as described above.

$$\text{Eqn. S1} \quad \sigma = \frac{F}{\pi R_3^2} \left( \frac{1}{R_1} + \frac{1}{R_2} \right)^{-1}$$

Fig. S2



**Confirmation of aggregate liquidity.** The two likely material states to be considered as they apply to tissue aggregates are liquidity and elasticity. The calculated surface tension of a liquid aggregate, when subjected to two different compressions will remain constant. In such aggregates the ratio of  $\sigma_2/\sigma_1$  will be equal to 1 and will be less than the ratio of the force applied at each successive compression ( $F_2/F_1$ ). In contrast, the calculated surface tension of an elastic aggregate will obey Hooke's law and increase proportionately to the applied force. For elastic aggregates the ratio of  $\sigma_2/\sigma_1$  will not be equal to 1 but will instead approach the ratio of  $F_2/F_1$ . The surface tension of liquid aggregates will also be independent of aggregate size (2, 3). Only measurements in which surface tension is independent of the applied force and size are used to calculate average  $\sigma$  for each cell line.

**Validation of TST measurements.** In order to confirm the validity of our TST measurements, the tissue surface tensiometer was calibrated by compressing an air bubble in culture medium and comparing the calculated surface tension with that obtained by the de Noüy ring method. Surface tension measured by TST and by the de Noüy technique were essentially identical and within 5% of the published value (2).

## References Cited

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2. Foty RA, Forgacs G, Pflieger CM, Steinberg MS. Liquid properties of embryonic tissues: Measurement of interfacial tensions. *Phys Rev Lett* 1994;72(14):2298-2301.
3. Foty RA, Pflieger CM, Forgacs G, Steinberg MS. Surface tensions of embryonic tissues predict their mutual envelopment behavior. *Development* 1996;122(5):1611-1620.