

# Supporting Information

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## SI Text

**Derivation of Eq. 4.** At low temperature near  $T_K$  the RFOT theory of glasses predicts that the cooperatively rearranging regions (CRRs) in glass-forming liquids are compact. Away from  $T_K$ , CRRs need not be compact and string-like contiguous shapes, called lattice animals, have been observed in computer simulations and experiments. Accounting for the multiplicity of possible shapes of the CRRs (1) and using the landscape library arguments (2), the free energy of a CRR of  $N$  sites with  $b$  boundary interactions is

$$F(N, b, \sigma) = [f_{\text{eq}}(T) - \phi_{\text{in}}(T, \sigma)]N + v_{\text{int}}b - k_B T \ln \Omega(N, b) \quad [\text{S1}]$$

where  $f_{\text{eq}}(T)$  is the total bulk free energy per particle of an equilibrium state at temperature  $T$ ,  $\phi_{\text{in}}(T)$  is the internal free energy per particle of an initial glass state,  $v_{\text{int}} = (1/z)T_K(3/2)k_B \ln(\alpha_L a^2/\pi e)$  is a local interaction of pairs with  $z$  nearest neighbors, and  $\Omega(N, b)$  is the number of lattice animals of given  $N$  and  $b$ . The initial nonequilibrated free energy has an additional contribution due to stress

$$\phi_{\text{in}}(T, \sigma) = \phi_{\text{in}}^0(T) + \kappa \frac{\sigma^2}{2G} V_{\text{bead}} \quad [\text{S2}]$$

where  $\phi_{\text{in}}^0$  is an internal free energy of the initial state without any stress. The equilibrated bulk free energy at temperature  $T$  above  $T_K$  is the sum of the internal free energy of a state at the Kauzmann temperature  $T_K$  and the configurational entropy  $s_c$

$$f_{\text{eq}}(T) = \phi_K - \int_{T_K}^T dT' s_c(T') \quad [\text{S3}]$$

$$= \phi_K - \Delta c_p(T_g) T_g \left( \frac{T - T_K}{T_K} - \ln \frac{T}{T_K} \right) \quad [\text{S4}]$$

where we have used Angell's empirical form of the change in heat capacity upon vitrification  $\Delta c_p(T) = \Delta c_p(T_g)(T_g/T)$  and the thermodynamic relation,  $s_c(T) = \int_{T_K}^T dT' \frac{\Delta c_p(T')}{T'} = \Delta c_p(T_g) T_g (\frac{1}{T_K} - \frac{1}{T})$ . Note that  $f_{\text{eq}}(T_g) = \phi_g - T_g s_c(T_g)$ . The ideal glass state energy is equal to

$$\phi_K = \phi_g - \Delta c_p(T_g) T_g \ln \frac{T_g}{T_K}. \quad [\text{S5}]$$

Consider the first term on the right-hand side of Eq. S1 and let  $\phi_{\text{in}}^0(T)$  be the bulk energy at  $T_g$ . Then use the relation in Eq. S5 to obtain

$$f_{\text{eq}}(T) - \phi_{\text{in}}(T, \sigma) = -\Delta c_p(T_g) T_g \left\{ \frac{T - T_K}{T_K} + \ln \frac{T_g}{T} \right\} - \kappa \frac{\sigma^2}{2G} V_{\text{bead}}. \quad [\text{S6}]$$

Substitute this result back into Eq. S1. The free energy becomes

$$F(N, b, \sigma) = \left[ -\Delta c_p(T_g) T_g \left\{ \frac{T - T_K}{T_K} + \ln \frac{T_g}{T} \right\} - \kappa \frac{\sigma^2}{2G} V_{\text{bead}} \right] N + v_{\text{int}}b - k_B T \ln \Omega(N, b). \quad [\text{S7}]$$

If  $T$  is below  $T_K$ , the excess energy is frozen at the state  $T = T_K$  and the configurational entropy vanishes

$$F(N, b, \sigma) = \left[ -\Delta c_p(T_g) T_g \ln \frac{T_g}{T_K} - \kappa \frac{\sigma^2}{2G} V_{\text{bead}} \right] N + v_{\text{int}}b - k_B T \ln \Omega(N, b). \quad [\text{S8}]$$

In percolation clusters (3), for large  $N$ , the number of lattice animals is approximately

$$\Omega_{\text{perc}} \equiv \left( \frac{(\alpha + 1)^{\alpha+1}}{\alpha^\alpha} \right)^N \exp \left( -\frac{N^{2\phi}}{2B^2} (\alpha - \alpha_e)^2 \right) \quad [\text{S9}]$$

where  $\alpha = t/N$ , and  $t$  is the number of unoccupied sites bounding the occupied cluster. Follow the analysis by Stevenson, Schmalian, and Wolynes (1) in which  $v_{\text{int}}b$  and  $k_B T \ln \Omega_{\text{perc}}$  are carried out explicitly, we take the exponent  $\phi$  at mean field value of 1/2 and a lattice constant  $B = 1.124$ . The number of bonds  $b$  is directly related to  $t$  and should linearly depend on coordination number  $b \approx 1.68t/z_{\text{SC}}$  (4), where  $z_{\text{SC}}$  is the coordination number for the simple cubic lattice. Recall that the interaction energy  $v_{\text{int}} = (1/z)T_K(3/2)k_B \ln(\alpha_L a^2/\pi e) = 3.6907k_B T_K/z$ . The free energy in Eq. S8 is now a function of  $N$  and  $t$ . Minimize this function with respect to  $t$ , the most probable value of  $t$  is  $\bar{t} = \bar{\alpha}N$ , where  $\bar{\alpha} = 3.10$  at  $T = T_K$ . At this most probable value,  $\Omega_{\text{perc}}$  becomes a simple exponential function,  $\Omega_{\text{perc}} \sim \lambda^N$ , where  $\lambda = 6.82$ . Each term in Eq. S8 is now proportional to  $N$ , and we can write

$$F(N, b, \sigma) = \left[ -\Delta c_p(T_g) T_g \ln \frac{T_g}{T_K} - \kappa \frac{\sigma^2}{2G} V_{\text{bead}} \right] N + v_{\text{int}} 1.68 \frac{z_{\text{fc}}}{z_{\text{SC}}} \bar{\alpha} N - k_B T N \ln \lambda \quad [\text{S10}]$$

$$= k_B T N \left\{ \left[ -\frac{\Delta c_p(T_g)}{k_B} \frac{T_g}{T} \left\{ \ln \frac{T_g}{T_K} \right\} - \frac{1}{k_B T} \frac{\kappa \sigma^2}{2G} V_{\text{bead}} \right] + \frac{v_{\text{int}}}{k_B T} 1.68 \frac{z_{\text{fc.c.}}}{z_{\text{SC}}} \bar{\alpha} - \ln \lambda \right\}. \quad [\text{S11}]$$

At the thresholding stress  $\sigma^*$  where  $F(N, \sigma^*) = 0$ , one finds

$$\sigma^* = \sqrt{\frac{2Gk_B T}{\kappa V_{\text{bead}}} \left( \left[ \frac{v_{\text{int}}}{k_B T} 1.68 \frac{z_{\text{fc.c.}}}{z_{\text{SC}}} \bar{\alpha} - \ln \lambda \right] - \frac{\Delta c_p(T_g)}{k_B} \frac{T_g}{T} \ln \frac{T_g}{T_K} \right)}, \quad [\text{S12}]$$

or

$$\sigma^* = \sqrt{\frac{2Gk_B T}{\kappa V_{\text{bead}} k_B T} \left( 1.68 \frac{z_{\text{fc.c.}}}{z_{\text{SC}}} \bar{\alpha} - \left[ \ln \lambda + \frac{\Delta c_p(T_g)}{k_B} \frac{T_g}{T} \ln \frac{T_g}{T_K} \right] \frac{k_B T}{v_{\text{int}}} \right)}. \quad [\text{S13}]$$

Substituting the numbers in the previous paragraph, we finally obtain Eq. 4

$$\sigma^* = \sqrt{\frac{2Gk_B T}{\kappa V_{\text{bead}}} \left( \left[ 3.20 \frac{T_K}{T} - 1.91 \right] - \frac{\Delta c_p(T_g)}{k_B} \frac{T_g}{T} \ln \frac{T_g}{T_K} \right)}. \quad [\text{S14}]$$

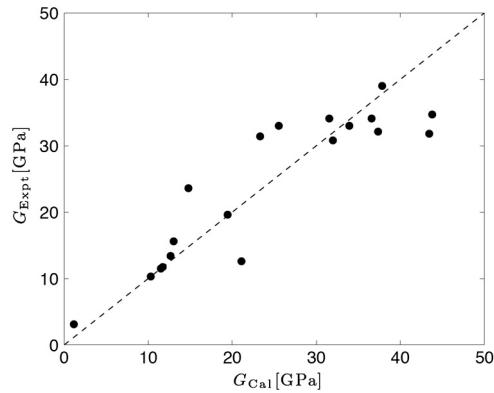
**Experimental Data and Numerical Prediction.** In Table S1 we summarize the input thermodynamic data and measured strengths as well as their sources in the literature. The bead count is

1. Stevenson JD, Schmalian J, Wolynes PG (2006) The shapes of cooperatively rearranging regions in glass-forming liquids. *Nat Phys* 2:268–274.
2. Lubchenko V, Wolynes PG (2004) Theory of aging in structural glasses. *J Chem Phys* 121:2852–2865.
3. Leath PL (1976) Cluster size and boundary distribution near percolation threshold. *Phys Rev B* 14:5046–5055.

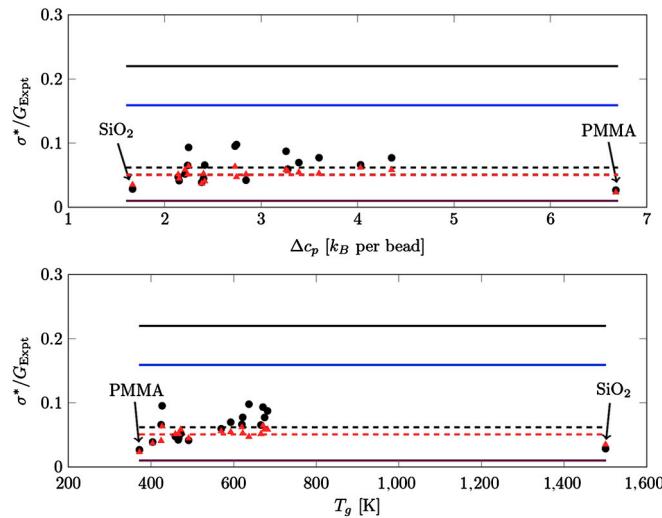
obtained as described by Lubchenko and Wolynes (5) and Stevenson and Wolynes (4) using the melting entropy. All strength measurements were all made at room temperature 300 K.

We also show here in Fig. S1 the comparison of measured elastic moduli with those predicted via the relation  $G_{\text{cal}} = 24.9k_B T_m/V_{\text{bead}}$  from thermodynamic data along with the Lindemann relation and the assignment  $T_A \approx T_m$ . The predictions for strength use the measured  $G$  when available but use the value from Lindemann relation and  $T_A \approx T_m$ .

4. Stevenson JD, Wolynes PG (2005) Thermodynamic-kinetic correlations in supercooled liquids: A critical survey of experimental data and predictions of the random first-order transition theory of glasses. *J Phys Chem B* 109:15093–15097.
5. Lubchenko V, Wolynes PG (2003) Barrier softening near the onset of nonactivated transport in supercooled liquids: Implications for establishing detailed connection between thermodynamic and kinetic anomalies in supercooled liquids. *J Chem Phys* 119:9088–9105.



**Fig. S1.** Comparison between the measured elastic moduli and those calculated using the Lindemann criterion.



**Fig. S2.** The ratio between strength and shear moduli versus heat capacity change at  $T_g$  and the glass transition temperature  $T_g$ . The black circles are the RFOT theory predictions, and the red triangles are the measured values. Typical value of crystal strength (violet solid line), Frenkel strength (blue solid line), and strength in the limit  $T \rightarrow 0, T_g \rightarrow T_K$  (black solid line) are also shown in comparison.

**Table S1. Experimental data and theoretical results of 19 glasses: density  $\rho$ (kg/m<sup>3</sup>), latent heat of fusion  $\Delta H_M$ (kJ/mol K), number of bead  $N_{\text{bead}}$ , Kauzmann temperature  $T_K$ (K), glass transition temperature  $T_g$ (K), melting temperature  $T_M$ (K), heat capacity change at glass transition temperature  $\Delta c_p$ (J/mol K), experimental shear modulus  $G_{\text{expt}}$ (GPa), measured strength  $\sigma_{\text{expt}}^*$ (GPa), and theoretical estimated strength  $\sigma_{\text{pred}}^*$ (GPa)**

Glasses	$\rho$	$\Delta H_M$	$N_{\text{bead}}$	$T_K$	$T_g$	$T_M$	$\Delta c_p$	$G_{\text{expt}}$	$\sigma_{\text{expt}}^*$	$\sigma_{\text{pred}}^*$	Refs.
PMMA	1188	4.64	0.84	337	372	397	6.68	3.10	0.07	0.08	(1–7)
$\text{SiO}_2$	2648	9.6	0.78	876	1500	1995	1.67	31.40	1.1	0.90	(8–12)
$\text{Mg}_{65}\text{Cu}_{25}\text{Y}_{10}$	3978	8.65	0.66	325	424	771	2.41	19.60	0.8	1.29	(13–20)
$\text{Mg}_{65}\text{Cu}_{20}\text{Zn}_5\text{Y}_{10}$	3284	7.77	0.79	325	404	702	2.38	23.60	0.88	0.92	(15, 21)
$\text{Mg}_{80}\text{Cu}_{10}\text{Y}_{10}$	—	7.21	0.69	—	427	746	2.73	—	0.8	0.96	(15, 22, 23)
$\text{La}_{55}\text{Al}_{25}\text{Ni}_{20}$	6140	7.48	0.75	337	491	712	2.15	13.40	0.6	0.52	(15, 18, 19, 24, 25)
$\text{La}_{55}\text{Al}_{25}\text{Cu}_5\text{Ni}_{15}$	6050	7.51	0.82	328	472	660	2.21	—	0.6	0.47	(15, 18, 24)
$\text{La}_{55}\text{Al}_{25}\text{Cu}_{10}\text{Ni}_{10}$	5930	6.84	0.74	332	467	662	2.40	—	0.6	0.48	(15, 18, 24)
$\text{La}_{55}\text{Al}_{25}\text{Cu}_{15}\text{Ni}_5$	6370	7.21	0.78	320	459	663	2.14	—	0.6	0.52	(15, 18, 24)
$\text{La}_{55}\text{Al}_{25}\text{Co}_5\text{Cu}_{10}\text{Ni}_5$	6000	6.09	0.66	363	466	661	2.84	15.60	0.8	0.67	(15, 18, 24, 26)
$\text{Pd}_{40}\text{Ni}_{40}\text{P}_{20}$	8951	7.39	0.60	487	570	884	3.28	39	2.19	2.33	(13, 15, 18, 19, 27, 28)
$\text{P}_{40}\text{Cu}_{30}\text{Ni}_{10}\text{P}_{20}$	9300	6.84	0.61	497	593	798	3.39	33.00	1.8	2.30	(13, 15, 18, 19, 26, 29)
$\text{Pd}_{77}\text{Cu}_6\text{Si}_{17}$	10400	8.55	0.58	553	637	1058	2.74	31.80	1.5	3.11	(16, 30–32)
$\text{Zr}_{11}\text{Cu}_{27}\text{Ni}_8\text{Ti}_{34}$	6850	11.3	0.72	537	671	1128	2.25	—	2.2	3.20	(13, 18, 32–34)
$\text{Zr}_{41.2}\text{Ti}_{13.8}\text{Ni}_{10}\text{Cu}_{12.5}\text{Be}_{22.5}$	6125	8.2	0.63	553	620	937	4.03	34.10	2.12	2.26	(13, 15, 18, 2635–37)
$\text{Zr}_{46.25}\text{Ti}_{8.25}\text{Ni}_{10}\text{Cu}_{7.5}\text{Be}_{27.5}$	6014	9.4	0.57	550	622	1185	3.60	34.70	1.83	2.68	(13, 14, 16, 31, 32, 36, 38, 39)
$\text{Zr}_{52.5}\text{Cu}_{17.9}\text{Ni}_{14.6}\text{Al}_{10}\text{Ti}_5$	6730	8.2	0.55	633	675	1072	4.35	32.12	1.88	2.48	(15, 16, 18, 34, 37, 40)
$\text{Zr}_{57}\text{Cu}_{15.4}\text{Ni}_{12.6}\text{Al}_{10}\text{Nb}_5$	6690	9.4	0.62	656	682	1091	3.26	30.80	1.8	2.69	(15, 16, 18, 34, 40)
$\text{Zr}_{65}\text{Al}_{7.5}\text{Cu}_{27.5}$	6744	12.8	0.8	517	666	1150	2.24	33.00	1.7	2.16	(15, 18, 25)

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