## Supplementary Information For

Microfluidic oscillators with widely tunable periods



Sung-Jin Kim, Ryuji Yokokawa, and Shuichi Takayama

Fig. S1 Top and bottom pressure of valves 1 and 2. The values were obtained from a theoretical model. The difference between  $P_{T1}$  and  $P_{B2}$  or between  $P_{T2}$  and  $P_{B1}$  is ~5% in the valve-open state. Thus, we can approximate  $P_{B2}$  as  $P_{T1}$  and  $P_{B1}$  as  $P_{T2}$  to measure threshold pressure.  $C_i$ ,  $C_e$ ,  $P_{th\text{-close}}$ ,  $P_{\text{th-close}}$ , and  $Q_i$  are  $1.8 \times 10^{-13} \text{ m}^5 \text{ N}^{-1}$ ,  $8.5 \times 10^{-13} \text{ m}^5 \text{ N}^{-1}$ ,  $-1 \text{ kPa}$ ,  $7.9 \text{ kPa}$ , and  $10 \mu \text{L min}^{-1}$ , respectively.



Fig. S2. (A) Valve dimensions used for estimating  $C_i$ . *a* is a measure of valve length, *b* is valve width, and *h* is membrane thickness. *C*<sub>i</sub> of each valve is calculated by  $C_i = \frac{\partial V}{\partial P} = \frac{a^4}{4\pi^4}$  $4\pi^4D$ ab  $\frac{du}{3+3n^4+2n^2}$ , where *D* is  $Eh^3$  $\frac{Eh}{12(1-v^2)}$ , and *V* and *P* are the volume and pressure, respectively (ref. S1). *C*<sub>i</sub> is estimated under the condition that the valve's membrane did not touch the valve's bottom floor. (B) Theoretical membrane deflection by  $P_T - P_B$  change. The graph shows how the small heights of the valves limit the extent of membrane deflection, *d*, thus reducing the effective *C*<sub>i</sub>. When the valve is closed, its membrane deflects downward as  $P_T - P_B$  increases. This deflection continues until  $P_T - P_B > P_{th-open}$ .  $P_{th-open}$ s were measured between 9 and 40 kPa depending on the valve type. At  $P_T - P_B = 3$  kPa, which is  $\lt P_{th-open}$ (i.e. close valve state), even the membrane of the smallest valve having  $C_i = 1.78 \times 10^{-14}$  m<sup>5</sup> N<sup>-1</sup> deflects more than the valve height of 75 µm. In other words, the valve's membrane can touch the valve's bottom floor before the valve opens. This contact greatly decreases the effective *C*<sup>i</sup> value. Thus, to make  $C_i$  constantly larger than  $C_e$ , for example a valve having a constantly large  $C_i = 1.67 \times 10^{-11}$  m<sup>5</sup> N<sup>-1</sup> was prepared by making the valve height  $\sim$  2 mm so the membrane does not touch the bottom. It should be noted that the contact does not affect the oscillation of the small size valves (the first three valves in the table of Fig. S2A) having 75  $\mu$ m valve height, because the contact rather increases  $C_e/C_i$  through the decrease of effective  $C_i$  and thus the condition of  $C_e/C_i > 1$  is kept. *d* is calculated from  $d =$ 

$$
((P_{\rm T} - P_{\rm B})\frac{a^4}{JEh})^{1/3}
$$
, where  $J = \frac{\pi^6}{32(1-v^2)} \left[ \frac{9+2n^2+9n^4}{256} + \frac{\{4+n+n^2+4n^3-3\nu n(n+1)\}^2}{2\{81\pi^2(1+n^2)+128(1+\nu)n-9\pi^2\nu(1+n^2)\}} \right]^{1/3}$  and *n* is  $a/b$  (ref. S2). *E* and *v* are 3.5 MPa and 0.5, respectively.

## **References**

- (S1) A. C. Ugural in Stresses in plates and shells (McGraw-Hill, Boston, 1981), pp. 90-92.
- (S2) O. Tabata, K . Kawahata, S. Sugiyama and Igarashi I, *Sens. Actuators* 1989, **20**, 135–141.