Selim Olcum^{a,b,1}, Nathan Cermak^{c,1}, Steven C. Wasserman^a, Kathleen S. Christine^{d,e}, Hiroshi Atsumi^f, Kristofor Payer^g, Wenjiang Shen^h, Jungchul Leeⁱ, Angela M. Belcher^{a,b,f}, Sangeeta N. Bhatia^{b,d,e,j,k}, Scott R. Manalis^{a,b,c,l,2}

^aDepartment of Biological Engineering, Massachusetts Institute of Technology, Cambridge, MA, 02139, USA ^bKoch Institute for Integrative Cancer Research, Massachusetts Institute of Technology, Cambridge, MA, 02139, USA.

^cComputational and Systems Biology Initiative, Massachusetts Institute of Technology, Cambridge, MA, 02139, USA ^dHarvard-MIT Health Sciences and Technology, Institute for Medical Engineering and Science, Massachusetts Institute of Technology, Cambridge, MA, 02139, USA

^eInstitute for Medical Engineering and Science, Massachusetts Institute of Technology, Cambridge, MA, 02139, USA ^fDepartment of Materials Science and Engineering, Massachusetts Institute of Technology, Cambridge, MA, 02139, USA

^gMicrosystems Technology Laboratories, Massachusetts Institute of Technology, Cambridge, MA, 02139 USA ^hInnovative Micro Technology, Santa Barbara, CA, 93117

ⁱDepartment of Mechanical Engineering, Sogang University, Seoul 121-742, Republic of Korea

^jDepartment of Electrical Engineering and Computer Science, Massachusetts Institute of Technology, Cambridge, MA, 02139, USA

^kHoward Hughes Medical Institute, Cambridge, Massachusetts 02139, USA

¹Department of Mechanical Engineering, Massachusetts Institute of Technology, Cambridge, MA, 02139, USA

¹ These authors contributed equally to this work.

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Туре	Device ID	Frequency (kHz)	Q factor	$\delta f/\delta m$ (mHz/ag)
0	S1	517	22,000	0.95
0	S3	545	14,000	0.95
0	S4	590	17,000	0.99
0	S6	577	24,000	1.08
1	41	1205	9,000	4
1	5B	1240	12,000	4.9
1	80	973	9,500	3.4
1	X4	1127	20,000	4
2	X6	2493	20,000	14.3
2	13L	1871	15,000	9.3
2	4K	2201	16,000	9.1
2	11M	1918	11,000	8.4
2	5J	2214	18,000	10.5
2	5M	2125	16,000	10.9
2	7A	2873	15,000	14
3	8N	2887	17,500	16
3	13M	2662	15,000	14.2
3	4J	3266	16,000	18
3	5N	2079	17,000	14
3	7B	3910	15,000	21.4

1 Device parameters

Table S1 Measured parameters of the cantilevers used in this study. The resonant frequencies and quality factors of the SNRs used in Figure 2 are measured by a lock-in amplifier (SRS-SR844) when the cantilevers are filled with ultra-pure deionized water. We measured the mass sensitivity of the cantilevers by weighing size-calibrated NIST traceable particles in each cantilever i.e. 30 nm gold (NIST SRM8012), 150 nm (Thermo Scientific 3150A), 200 nm (Thermo Scientific 3200A) and 220 nm (Thermo Scientific 3220A) polystyrene.

2 System operation

The cantilevers used in this work are operated in self-oscillation mode in a positive feedback loop. The image of the oscillator system is given in Fig. S1. The motion of the cantilever is converted to the deflection of a laser beam bounced off of the tip using an optical lever setup (Fig. 1a). We used an ultra-low noise diode lab laser module (Coherent 635 nm, 5 mW) as the laser source. We cleaned up and expanded the laser source by a spatial filter (0.5NA 13.86 mm aspherical lens, 20 μ m pinhole) and a collimating spherical lens (f=30 mm) to achieve a coherent ~3 mm-diameter filtered laser beam. Additionally, we used a film polarizer to tune the incident laser power on the cantilever. Increasing the laser power causes the temperature of the cantilever to fluctuate, which can be observed as frequency fluctuations of the oscillator. This is particularly the case for smaller cantilevers (Type 2 and 3). In all cases, we used the maximum laser power that can give the minimum frequency noise. The laser beam is focused on the cantilever tip using a 20X objective (Nikon LU Plan ELWD 0.4NA). The reflected laser beam is focused on the photodetector by an achromatic doublet lens (Thorlabs AC254-30-A). The spot size on the photodetector is adjusted by changing the distance of the focusing lens to the photodetector.

We used a custom-made low-noise photodetector circuit to transform the angular deflection acquired from the optical lever setup to an electrical signal by a high-speed split PIN photo-diode (Hamamatsu S4204). We used ultra-low-noise transimpedance amplifiers (OPA847) with 5 MHz 3 dB-bandwidth followed by a high speed instrumentation amplifier (AD8130) to convert the differential optical deflection signal on the split photodiode to a voltage signal. The generated voltage signal is amplified by an automatic gain control (AGC) stage to achieve constant amplitude at the output of the photodetector. The output amplitude can be tuned by a DC input voltage connected to the AGC stage.

The optimal delay required in the loop for stable self-oscillation is introduced by a field programmable gate array (FPGA, Altera Cyclone IV on DE2-115). The analog signal in the loop is interfaced with the digital signal in the FPGA using the Terasic AD/DA conversion board at 100 MSPS with 14-bit convertors. The FPGA and the conversion board run on an external 100 MHz oven controlled crystal oscillator clock (Abracon AOCJY2-E-H1C). The delay algorithm in the FPGA is capable of achieving sub-clock delays (39 ps minimum) using numerical interpolation, which converts to less than 0.1 degree resolution for adjusting the phase shift of



Figure S1 Photograph of the oscillator system. The incident laser path onto the cantilever is indicated with a red line. The orange line shows the reflected laser path from the cantilever.

the highest frequency oscillators used in this work (4 MHz).

Since the amplitude of photodetector output is kept constant by the AGC, the oscillation amplitude of a cantilever can be adjusted by the FPGA independently. The output of the FPGA is amplified with a gain of 15 dB using an amplifier utilizing a high current OPAMP (LT1210) output stage, which drives a piezoceramic actuator (American Piezo Co. APC841, 7x7x0.2 mm) integrated underneath the SNR chip.

The frequency of oscillation is measured by period counting at 100 MHz using a digital heterodyne mixer and a low-pass filter coded in the FPGA. The signal is mixed with a reference sinusoid generated by a numerically-controlled oscillator (NCO). The heterodyned signal is then filtered using a 3-stage cascaded integrator comb (CIC) filter with a width of 500 data points (5 μ s) and then up-sampled (1st-order hold) back to 100 MHz. The number of clock cycles in between zero crossings of the resulting signal is counted to infer the period. Note that the difference of the reference frequency and the oscillation frequency determines the RF measurement bandwidth.

The FPGA communicates with a control computer via Ethernet. The computer is used to control the delay in the loop and the amplitude of oscillation as well as the bandwidth of the frequency measurement algorithm. Measured oscillation frequency waveform (baseband signal) is recorded by the control computer for post-processing.

3 Detector noise

For performing an analysis on the noise sources limiting the noise performance of the SNRs, we first measured the voltage noise power spectrum density of the photodetector output, $S_V^{pd}(V^2/Hz)$ in our optical lever setup using a spectrum analyzer (HP 4395A) when the water-filled cantilevers were driven only by the thermal energy due to the non-zero ambient temperature, T (~300K). The displacement noise spectral density of a cantilever due to thermal energy, S_x^{th} (m²/Hz) as a function of frequency, ω is given by(1):

$$S_{\chi}^{th}(\omega) = \frac{4\omega_0^3 k_B T}{kQ} \frac{1}{(\omega_0^2 - \omega^2)^2 + (\omega\omega_0/Q)^2}$$
(1)

where, k_B , k, Q and ω_0 are Boltzmann constant and stiffness, quality factor and resonant frequency of the cantilever. At the resonant frequency, above equation reduces to $4k_BTQ/\omega_0k$, which can be used to calculate the responsivity (V/m) of the optical lever setup as follows:

$$R = \sqrt{\frac{S_V^{pd}(\omega_0) - S_V^{pd}(\omega \neq \omega_0)}{S_x^{th}(\omega_0)}} = \sqrt{\frac{S_V^{pd}(\omega_0) - S_V^{pd}(\omega \neq \omega_0)}{4k_B T Q/\omega_0 k}}$$
(2)

For calculating the responsivity of the optical lever setup we used the measured parameters of the cantilever under test. The resonant frequencies and the quality factors are given in Table S1. The stiffness of a cantilever is calculated using the measured mass sensitivity values in the same table using the following relation:

$$\frac{\delta f}{\delta m} = -\frac{f_0}{2m^*} = -\frac{2\pi^2 f_0^3}{k}$$
(3)

where m^* is the effective mass of the cantilever. Using the above relations and measured cantilever parameters, we calculated the displacement noise power spectral density for different types of SNRs used in this work. The results are given in Figure S2. The red circles are

the spectrum analyzer (HP 4395A) measurements referred to displacement domain performed at 3 Hz resolution bandwidth with 100 averages. The dashed black curves are calculated using equation (1) and the dashed green lines are the calculated noise density of the photodetector referred to the displacement domain. We measured the photodetector noise floor between 90-140 fm/\sqrt{Hz} for all types of cantilevers. The noise of the optical lever setup is limited by the thermomechanical vibrations of the cantilevers at the vicinity of their resonant frequencies and by the photodetector noise floor at frequencies away from the resonant frequency.

For investigating the effect of the displacement noise on the oscillator performance we measured the root-mean-square (RMS) frequency noise of the cantilevers when they were oscillating in feedback. We then compared the acquired noise measurements to the RMS frequency noise due to thermal energy and detector noise, which can be calculated following the analysis given by Albrecht et al.(1) as:



$$\langle \delta \omega^2 \rangle = \frac{k_B T}{k \langle x_c^2 \rangle} \frac{\omega_0 B}{Q} + \frac{B^3 S_x^{pd}}{12 \langle x_c^2 \rangle} \tag{4}$$

Figure S2 Displacement noise density of SNRs of different types. The red circles are calculated by referring the measured voltage power spectral density of the cantilevers due to thermal vibrations to displacement domain. The dashed black lines are the calculated displacement noise density of the cantilevers due to thermal vibrations using equation (1). The green dashed lines are the calculated displacement noise floor of the photodetector. The spectrum measurements are performed using 3 Hz resolution bandwidth and 100 averages.

where *B* is the RF measurement bandwidth, S_x^{pd} is the photodetector power spectral density referred to the displacement domain in m²/Hz and $\langle x_c \rangle$ is the RMS displacement of the cantilever tip. The first term in this equation is due to the thermal energy and the second term is due to the photodetector noise. The RMS displacements of the cantilevers used in this work are limited by the mechanical nonlinearity. We used the approximate displacement expression given by Arlett et al.(2) converted to RMS at the onset of nonlinearity as

$$\langle x_c \rangle = 5.46 \frac{L}{\sqrt{2Q}} \tag{5}$$

where L is the length of the cantilever. The calculated RMS noise values as a function of measurement bandwidth are given in Figure S3. The red dots are the measured RMS frequency noise in 1 second intervals as a function of measurement bandwidth and when the cantilevers are in self-oscillation at their onset of nonlinearity. The dashed black lines are the estimated noise due to the thermal energy and the black solid curves are the estimated noise due to the combination of thermal energy and the photodetector noise as given in equation (4).



Figure S3 Root-mean-square frequency noise of the oscillators are measured as a function of measurement bandwidth for different types of SNRs and plotted as red circles. The dashed black lines are the RMS frequency noise due to thermal energy calculated using the first term in equation (4). The solid black lines are the calculated RMS noise due to the detector noise floor and thermal energy. Each red circle is calculated using 1 second of frequency noise measurement.

From Figure S3, we can see that all types of cantilevers are limited by the photodetector noise at wide measurement bandwidths. Increased noise at wide measurement bandwidth limits the throughput for better mass resolution cases. Approximately flat RMS frequency noise at narrower bandwidth operation is also observed in Allan deviation curves in Fig. 2 as the flicker noise region. Especially for device types 2 and 3, if the displacement noise floor of the motion detector can be reduced, the throughput of the device can be increased up to 10-fold without sacrificing mass resolution.

4 Thermal noise limit on Allan deviation

In order to calculate the fundamental noise limit on frequency stability in terms of Allan deviation due to the thermal noise on the cantilever, we treat the cantilever as a damped harmonic oscillator. The spectral density of the random displacements of the cantilever, $S_{\chi}^{th}(\omega)$ was given in equation (1), which is used here to calculate the spectral density of the phase fluctuations, $S_{\varphi}^{th}(\omega)$:

$$S_{\varphi}^{th}(\omega) = \frac{S_x^{th}(\omega)}{\langle x_c \rangle^2} = \frac{4\omega_0^3 k_B T}{k \langle x_c \rangle^2 Q} \frac{1}{(\omega_0^2 - \omega^2)^2 + (\omega\omega_0/Q)^2}$$
(6)

Equation (6) can be approximated as follows (1) for very high Q oscillators:

$$S_{\varphi}^{th}(\omega) \approx \frac{\omega_0 k_B T}{k \langle x_c \rangle^2 Q} \frac{1}{(\omega - \omega_0)^2}$$
(7)

If we convert the above relation to baseband around the carrier frequency ω_0 by defining a modulation frequency $\omega_m = \omega - \omega_0$, we get the phase noise density as:

$$S_{\varphi}^{th}(\omega_m) \approx \frac{\omega_0 k_B T}{k \langle x_c \rangle^2 Q} \frac{1}{\omega_m^2} = \frac{\omega_0 k_B T}{E_C Q} \frac{1}{\omega_m^2}$$
(8)

where E_c is the carrier energy defined as $k\langle x_c \rangle^2$. The Allan variance due to the phase noise density of an oscillator is calculated using the following relation (3):

$$\sigma_A^2(\tau) = 2\left(\frac{2}{\omega_0\tau}\right)^2 \int_0^\infty S_{\varphi}(\omega) \sin^4(\omega\tau/2) \, d\omega \tag{9}$$

If we evaluate the integral above using the phase noise density in equation (8), we get:

$$\sigma_A^{th}(\tau) = \sqrt{\frac{\pi k_B T}{\tau E_C Q \omega_0}} = \sqrt{\frac{k_B T}{2 \tau E_C Q f_0}}$$
(10)

Since the cantilevers in this work are driven at their onsets of nonlinearity, we use the approximate expression given in equation (5) as the RMS displacement to calculate the nonlinearity limited Allan deviation due to thermal noise,

$$\sigma_{A,non}^{th}(\tau) = \frac{1}{5.46L} \sqrt{\frac{k_B T}{\tau \ k \ f_0}}$$
(11)

which is independent of the quality factor. Therefore, as long as an oscillator is driven at its onset of nonlinearity, the lowest Allan deviation that can be achieved does not depend on the quality factor of the resonator. In that case the practically achievable stability would be limited by the coupling efficiency of the actuator or the power handling capability of the resonator. The fundamental limits on the Allan deviation of the oscillators used in this work, which are plotted

in Figure 2 of the manuscript as a function of gate time, τ , are calculated using equation (11) and the design parameters given in Table 1 of the manuscript.

5 Limit of detection

We calculated limits of mass detection of the SNRs by taking measurements of instrument noise (the same data as used for Fig. 2), filtering with an FIR filter, h_T , and calculating the standard deviation, σ_T of the remaining signal, illustrated in Figure S4. The filter h_T was defined as the peak shape given in Dohn et al.(4) for a peak of width T, with the mean subtracted and then the amplitude normalized such that the gain for a peak of the same width was unity. This approach deviates slightly from the truly optimal (in terms of signal-to-noise ratio) FIR filter for detecting a signal s, which is given by



Figure S4 Illustration of the method used for calculating limits of detection using matched filters of varying peak widths. Raw noise is filtered with a filter shaped like the signal generated by a particle transiting the cantilever, with the mean subtracted. The filters are normalized such that a 1 Hz peak input yields a 1 Hz peak out.

$$h = \alpha R^{-1} s \tag{12}$$

where *h* is the vector of filter coefficients (taps), α is a normalization constant, and *R* is the covariance matrix of the noise. Because our noise has long correlation times (a defining characteristic of 1/f and 1/f² noise) leading to extremely long optimal FIR filters, instead of multiplying our signal by R⁻¹, we approximate the true matched filter by simply subtracting off the mean (DC component) of our peak shape (shown in second row of Figure S4). This effectively includes a high-pass component in our filter that should reject frequencies below those in our peak. After filtering, we calculate the standard deviation σ of the resulting signal, and define our limit of detection as 3σ , shown in Figure S5.



Figure S5 Limits of mass detection for the devices considered in this study. Limits of detection are calculated based on applying approximately matched filters of varying widths and calculating three times the resulting noise standard deviation. The apparent independence of limit of detection and peak width over the range from 20-500 mHz results from the dominating 1/f noise, which has equal power in every decade of the spectrum.

6 Mass Sensitivity Calibration



Figure S6 Mass sensitivity calibration of SNRs. We calibrated the mass sensitivity of the cantilevers by running gold nanoparticles (RM-8012, NIST) as reference before the actual experiment. We calculate the sensitivity of a cantilever such that the mean diameter of the measurement is 26.5 nm, which is the mean of the estimated diameter of the nanoparticles by AFM, SEM and TEM measurements in the reference material datasheet. (a) Buoyant mass histogram of reference gold nanoparticles. 3,600 particles are measured in a 20-minute experiment. (b) Histogram of the estimated diameter of weighed particles by assuming a spherical shape and uniform gold density of 19.3 g/cm³.

7 Dynamic light scattering measurements of gold nanoparticles

For comparing the performance of SNRs to dynamic light scattering (DLS), we measured the gold nanoparticle populations used in the experiment given in Fig. 3 using a Malvern ZEN3690 DLS instrument. First, we analyzed 10 nm, 15 nm and 20 nm gold nanoparticles, separately. The results of the measurements are given in Table S2, below.

		DLS		SNR (from the mixture)		Datasheet	
Sample		Mean (nm)	CV(%)	Mean (nm)	CV(%)	Mean (nm)	CV(%)
1	10 nm AuNP	12.68	10.2	9.9	7.4	9.9	
2	15 nm AuNP	15.99	13.4	14.4	5.3	14.3	< 8%
3	20 nm AuNP	22.07	15.6	19.7	4.9	20.4	< 8%
4	Mixture	18.77	24.8				

Table S2 DLS measurements of the gold nanoparticles used in this work. Samples 1, 2 and 3 are monodisperse populations of gold nanoparticles used in sample 4, which was weighed in the SNR and the results were given in Fig. 3.

For the mono-disperse gold nanoparticle populations, the mean diameters measured by the DLS are slightly higher than what were measured by SNR or reported in the datasheets of the particles. The measured coefficients of variances (CV's) by the DLS are also higher than SNR measurements. More importantly, DLS detects the mixture of these particles as a single peak around 18.77 nm with a relatively broader coefficient of variance (24.8%) compared to the single particle measurements.

8 Dynamic range in size

We demonstrate the dynamic range of SNRs by weighing a mixture of equal concentration 150 nm, 200 nm and 220 nm polystyrene beads (NIST traceable Thermo Scientific). The same cantilever and detection and estimation parameters that were used for gold nanoparticle mixture that was shown in Fig. 3 were used to weigh the polystyrene nanoparticle mixture. The three populations were successfully identified by measuring more than 12,500 particles in less than 30 minutes. We estimated the average transit time for a single particle as 30 ms. The estimated diameters in Figure S7b is calculated by assuming a spherical shape and uniform polystyrene density of 1.05 g/cm³. Calculated coefficient of variations and the mean sizes for the three populations are 2.3% around 149.8nm, 1.7% around 199.9nm and 1.2% around 217.2nm, respectively.



Figure S7 Dynamic range of SNRs. (a) Buoyant mass histogram of a mixed population of 150 nm, 200 nm and 220 nm polystyrene nanoparticles. **(b)** Estimated diameters of weighed nanoparticles. Black curves are Gaussian fits to the histograms.

9 Accuracy of concentration estimation

The concentration of particles in a solution is estimated by the ratio of the number of particles detected and the estimated total analyte volume. The amount of analyte flowing through the cantilever is calculated using the transit time estimates of the particles and the cantilever dimensions. Concentration accuracy is affected by the error in the particle count and the error in the estimated analyte volume.



Figure S8 Accuracy of the concentration estimates. (a) Probability of a particle being detected (vs being coincident with another particle) as a function of sample concentration. **(b)** Estimated concentration as a function of actual concentration when there are no other error sources. **(c)** Probability of detection of a particle as a function of buoyant mass. The vertical dashed line is the limit of detection (5 ag) for the cantilever under consideration. The red circles are the simulation results using the detection algorithm when simulated particle peaks are inserted in real frequency noise data.

Erroneous particle counts are caused by two primary factors – coincident (overlapping) particles in the cantilever, and failure to detect particles that are close to the limit of detection. Coincidence occurs if two particles transit the cantilever close together enough that they cannot be distinguished from a single, larger particle. Here, we conservatively consider particles to be coincident if the distance between two particles in the cantilever channel is less than half the cantilever length. Using the channel dimensions and assuming particle arrival follows a Poisson process, we calculate the probability of any given particle being sufficiently spaced from its neighbors to be detected, as a function of the particle concentration (Figure S8a). This allows us to predict the relationship between actual and observed concentrations (Figure S8b). For Type 3 devices, the error in the concentration estimate of a sample with 10¹⁰ particles/ml is about 15%, and is higher for the longer devices.

Another contribution to the particle count error comes from the probability of detecting a particle passing through the buried channel. The probability of detection of a particle with a buoyant mass at the detection threshold given in Figure S5 is 50% due to the inherent noise of the system. We calculated the probability of detection as a function of particle buoyant mass by integrating the frequency noise distribution converted to mass around the limit of detection. For a cantilever with 5 ag limit of detection, the probability of detection as a function of the buoyant mass is given in Figure S8c. The solid line is the calculated theoretical detection probability whereas the red circles are the results of the detection of simulated particle signals superimposed on a measured noise waveform. A total of 600 particles were injected in the measured noise waveform of 10 minutes and the detection algorithm was used to detect the superimposed particle signals. The simulation results and the theoretical estimations agree well.

Estimating the flow rate of the fluid passing through the buried channel using the pressure difference across the cantilever and the channel dimensions does not provide satisfactory results since the flow rate during an experiment may vary due to partial clogging or surface adhesion. So we use the particle transit time through the cantilever as an estimate of the linear flow velocity. Coupled with the cantilever dimensions, we can use this to estimate the volumetric flow rate. To assess the accuracy of this method, we simulate the performance of our detection algorithm on estimating the transit time of the particles. We inject 600 particles with 100 ms transit time to a measured frequency noise waveform of Type 2 device with 5 ag limit of detection. As expected, the variance of the transit time estimates increases as the particle mass approaches to the limit of detection. We calculated the standard deviation of the transit time estimates as 20.5 ms around a mean of 95.2 ms for 10 ag particles. Although individual particles show a large variance the error on the mean value for 600 particles is less than 5% and gets smaller for higher number of measured particles. The variance of the transit time estimates reduces very quickly as the signal to noise ratio improves. For example, the error of transit time estimate using 100 ag particles (600 particles) is less than 1% with a standard deviation of 1.8 ms.

10 Exosome diameter estimation



Figure S9 Estimated size distribution (kernel density estimates) of fibroblast (red) and hepatocyte (black) exosomes for different assumed exosome densities. The data used for size estimation is the buoyant mass measurements in Fig. 4. Two extreme cases for the mean exosome density are considered; 1.13 g/ml (solid), and 1.19 g/ml (dashed). All exosomes are assumed to be spherical.

11 Dynamic light scattering measurements of exosomes

We performed DLS measurements of different types of exosome populations for comparison. The mean of the dominant mode (in concentration) detected by the DLS is 44.6 nm and 44.1 nm for fibroblast and hepatocyte exosomes with standard deviations of 12.9 nm and 6.3 nm, respectively. The DLS measurements, similar to SNR measurements, estimate a broader distribution for the fibroblast exosomes compared to hepatocyte exosomes. However, DLS does not provide information about the shape of the distribution or absolute concentration. In addition, we note that the information gathered from the DLS is not very reliable for heterogeneous samples like exosomes, due to the fact that DLS is biased towards the detection of larger particles (5).

Exosomes		DLS			
		Mean (nm)	Std (nm)		
1	Fibroblast	44.6	12.9		
2	Hepatocyte	44.1	6.3		

Table S3 DLS measurements of the exosome populations analyzed in this work.Malvern ZEN3690DLS instrument is used for the measurements.



12 Repeated exosome measurements

Figure S10 Distribution of buoyant mass measurements (kernel density estimates) of exosomal vesicles derived from fibroblast (red) and hepatocyte (black) cells. The thinner dashed lines are the results of the repeated measurements using a second batch of purified fibroblast and hepatocyte exosomes and using a different cantilever. The vertical line close to 5 ag depicts the limit of detection of the measurements. The inset shows the estimation of exosome diameter by assuming a spherical shape and uniform density of 1.16 g/ml.



13 Preparation of DNA covered gold nanoparticles

Figure S11 Preparation of DNA-covered gold nanoparticle. (a) Schematic illustration of a DNA-covered gold nanoparticle. (i) Gold nanoparticles were incubated with bis(p-sulfonatophenyl)-phenylphosphine (BSPP) at room temperature overnight. (ii) The phosphinated gold nanoparticle solution was incubated with activated thiol-DNA at room temperature overnight. (b) UV spectra of a bare gold nanoparticle (black, $\lambda_{max} = 519.5$ nm) and a phosphinated gold nanoparticle (red, $\lambda_{max} = 522.5$ nm). Phosphination of a gold nanoparticle causes the change of environment on its surface and λ_{max} of the phosphinated gold nanoparticle shifts by 3 nm. (c) Agarose gel analysis identifies phosphinated (left) and DNA-covered (right) gold nanoparticles. (d) A photograph of phosphinated gold nanoparticles (left) and DNA-covered gold nanoparticles (right) under high salt conditions. Gold nanoparticles not covered by DNA aggregate under high salt solution.

14 Design of DNA origami scaffold



Figure S12 Design and AFM images of DNA origami scaffold. (a) Design of the DNA origami. Each color shows individual single stranded DNAs. The constructed DNA origami scaffold was examined by AFM. Scale: **(b)** $5.0 \,\mu$ m x $5.0 \,\mu$ m; **(c)** $839.8 \,$ mm x $839.8 \,$ mm.



15 Design and preparation of gold covered DNA origami

Figure S13 Design and preparation of gold nanoparticles-embedded DNA origami. (a) The design of DNA origami structures with two (i) and three (ii) binding sites for DNA-modified gold nanoparticles. (b) Agarose gel analysis and AFM images of the gold nanoparticles-embedded DNA origami. Annealed products of DNA origami with gold nanoparticles were loaded on 1% Sybr safestained agarose gel containing 10 mM MgCl₂ (running buffer TBE (0.5X), loading buffer 40% glycerol, 15 V/cm, 30 minutes, room temperature). Lane 1 contains 15 nm gold nanoparticles fully covered by DNA. Lane 2 contains DNA origami with one binding site and the DNA-modified gold nanoparticles. (origami:gold = 1:1) Lane 3 contains DNA origami with two binding sites and the DNA-modified gold nanoparticles (origami:gold = 1:2). Lane 4 contained DNA origami with three binding sites and the DNA-modified gold nanoparticles (origami:gold = 1:3). Lane 5 contains DNA origami with one binding site and the DNA-modified gold nanoparticle, same as lane 2. The selected bands were excised and purified for analysis using Freeze-squeeze column (Bio-Rad) at 4°C. 4 μ l NiCl₂ (10 mM) was dropped on freshly cleaved mica. After 20 minutes, the surface was dried by nitrogen gas. 4 µl of the sample with DNA origami and gold nanoparticles was dropped on the pretreated substrate. Then the samples were scanned in TAE-Mg²⁺ (1X) buffer on AFM (Veeco Multimode with NanoScope V) in tapping mode with a SNL-10 tip (Bruker corporation). Scale: 100 nm x 200 nm.

16 DNA sequence of staple strands.

Sequence (5'-3') of staples strands used in the experiments is shown below. Gold nanoparticles embedded to DNA origami structures were prepared by substituting original staple strands (HA856, 901, 902, 851, 896, 897, 861, 906, and 907) with hook staple strands (HA1057-1065).

HA0795	GGTCATAGAATTCCACACATAATTGGGCG	HA0877	GAAAAGGTCATAAAGCTAAATCGGATCGATGA	HA0959	ΤΑΔΑΓΑΘΓΤΤΑΓΘΑΘΓΑΤΘΤΑΘΑΑΘΑΑΤΓΘΓΓ
HA0796	CCCCGGGTAAGTGTAAAGCCTGGGCGGCCAAC	HA0878	TAGCATTAATTAGCAAAAATTAAGCTCAATCAT	HA0960	TAAGAAACCTGAACAAGAAAAATTTTAGGC
HA0797	CTTGCATCTAACTCACATTAATGAAACCTG	HA0879	TATTTGCATTTTCAGGTTTAACGTTATTTTAG	HA0961	GAAAATAGGAACGCGCCTGTTTATAGAGAATA
HA0798	CACGACGTTGTAAAACGACGGCCAGTGCCAAG	HA0880	ATGGAAGAACAGTACCTTTTACGACAAAGA	HA0962	TAAAAACACAGGGAGTTAAAGGCCCGGTCGCT
HA0799	TTAAGTTGGGCTGCGCAACTGTTGCAGGAAGA	HA0881	AATCCTGAACGGATTCGCCTGATTATATGTAA	HA0963	GGGATCGATGAACGGTGTACAGGAGTAATC
HA0800	TTACGCCAGCTGGCGCGGGCCTCTTCGCTA	HA0882	TGATTATCTTACAAAATCGCGCAGTAACCTCC	HA0964	ATCGGAACGAACCGAACTGACCAAACCCAAAT
HA0801	ATTGTTATCCGCTCACCTGTTTCCTGTGTGAA	HA0883	ACCAGAATCAATTACCTGAGCATCAAAATC	HA0965	CTTTGAGGCGGAACGAGGCGCAGAAGTGAATA
HA0802	GAAGCATAACCGAGCTCGAATTCGTAATCAT	HA0884	GTAACATTCAAACATCAAGAAAACTAAGACGC	HA0966	TTTCCATGAAATCCGCGACCTGAGAACGAG
HA0803	TGAGTGAGGCCTGCAGGTCGACTCTAGAGGAT	HA0885	TGCCCGAATAACAATTTCATTTGAGAATCCTT	HA0967	ACTACGAAGAGATTTGTATCATCGTTAATTTC
HA0804	GCTCACTGGGAAACCAGGCAAAGCCACCGCTT	HA0886	CAAACAAGAAACAGTACATAAAATCGT	HA0968	GCAAAAGAGATTATACCAAGCGCGTTATGCGA
HA0805		HAU887		HA0969	
HA0800	CARGETECTEATTECCCTTCACCETCCACTA	1140888		HA0970	GCCGAACATAAGTTTATTTGTCACAATCAA
HA0807	GCGCGGGGGAGTTGCAGCAAGCGGTGGGTTGAG	HA0889	TAGAGAGTATTCATTGAATCCCCCAATACCAC	HA0972	CGAAGCCCTCATATGGTTTACCAGCGCCAAAG
HA0809	TCGTGCCCAGCAGGCGAAAATCCCCTTATA	HA0891	AGACCGGAAGTTCAGAAAACGAGAAGGTAGAA	HA0973	AGAAACAGCGACATTCAACCGATTGAGGGA
HA0810	CTEGTECCCCCCCTTTCCAGTCGGTGCGTGC	HA0892	ATCGCGTTAATCAGGTCTTTACCATAAAAC	HA0974	CAAGAATTAAATATTGACGGAAATGTTTGCCT
HA0811	TCGCACTCGATAGGTCACGTTGGTTTTCATCA	HA0893	CATCAAAAAGATTAAGGAAGCAAAGCGGATTG	HA0975	AATTGAGCAATTATCACCGTCACCGCAGCACC
HA0812	CAGTTTGAGGGGACGTAACCGTGCATCTGC	HA0894	AAGAAATTGCGTAGACGTAAAACAGAAATA	HA0976	TAACTGAGAATTAGAGCCAGCAGCCGGAAA
HA0813	GTGAGACGGGCAACAGGTTTTTCTTTTCACCA	HA0895	TATACAGTGGTTAGAACCTACCATAAAACAGA	HA0977	GAGGCTTGGGGAAGCGCATTAGACGAATAACA
HA0814	CCTGAGAGAGAGGCGGTTTGCGTCGAGCCG	HA0896	AAACAATATTGTTTGGATTATACTCGCCTGCA	HA0978	CGCCCACGACTGAGTTTCGTCACCCCTCAGAA
HA0815	GTTTGCCCAGCTGCATTAATGAATGTGCCTAA	HA0897	ATACCAAGAGATGATGGCAATTCGCAAATG	HA0979	CCGATAGTCCTGTAGCATTCCACAGACAGCC
HA0816	TGGTGGTTGTGGGAACAAACGGCGACCCGTCG	HA0898	TATTCATTGGAGCGGAATTATCATGAACCTCA	HA0980	TTTCGAGGTAGCGTAACGATCTAAAGTTTTGT
HA0817	GTAATGGCAGCCAGCTTTCCGGGCCATTCG	HA0899	TGATGAAAATCATTTTGCGGAACACTGGTCAG	HA0981	AGCCTTTACCAGACGTTAGTAAATGAATTTTC
HA0818	GCGCATCGACGACAGTATCGGCCTGGAAGGGC	HA0900	ATTACATTCGTTATTAATTTTAAATTGAGG	HA0982	TTGAAAATATTTTGCTAAACAACTTTCAACA
HA0819	CCCGCCGCTGGTTGCTTTGACGAGCGCGAACT	HA0901	TTTTAATGTTCGACAACTCGTATTAGCACTAA	HA0983	GGAACAACTAAAGGAAGGAGTGAGAATAGAAA
HA0820	TGTAGCGTCCTCGTTAGAATCAAATATTTT	HA0902	TGTGAGTGAGCGAGAGGGCTTTTGCCGATAAAA	HA0984	ACGCAGTATGTTAGCTTAAGACTCCTTATT
HA0821	GCGAAAGGGGAGGCCGATTAAAGGGACCTGAA	HA0903		HA0985	GGIGGCAATAATAACGGAATACCCCCTCCCGA
HA0822	GGLGAALGLGGTALGLLAGAATLLALATTLIG	HA0904	AGACIGGATTTTGCGGGATGGCTTTTCACCA	HA0986	
HAU823		HA0905		HAU987	
HA0824	TGTIGTICCTICTTIGATTAGTAAGCTCATGG	HA0900		HA0988	
HA0825	ΔΑΤΓΑΔΔΔΑΓΤΑGΔΔGΔΔCΤΓΔΔΤΑΤΤΑΓΓG	HA0908	TATAGTCAAGGAAGCCCGAAAGACAATAGTAG	HA0990	TAAAGGTGGCTAATATCAGAGAGATCCAAA
HA0827	GATTCTCCCCGAAATCGGCAAAATCTGTTTGA	HA0909	TTAATTTCTACCGACCGTGTGATAGCAAGCAA	HA0991	CCATTTGGACACCCTGAACAAAGTTCAAAAAAT
HA0828	ACATTAAATGATATTCAACCGTTCAAATGCAA	HA0910	ACGCGAGAGAATAAACACCGGATTCATCGT	HA0992	AGTAGCACGCAAGCCCAATAGGAACTCATTTT
HA0829	GCGTCTGGGCCGGAGAGGGTAGCGATAAAA	HA0911	ATGCTGATAAAGCCTGTTTAGTATCACTCATC	HA0993	CCGTAACCATAACCGATATATTGCTTTTGC
HA0830	TAACCAATACAAAGGCTATCAGGTTTTTGCGG	HA0912	GGCTTAGGAATTCTTACCAGTATAATTCCAAG	HA0994	CTACAACGTGCGCCGACAATGACAAAGACAGC
HA0831	CATTAAATTGGAGCAAACAAGAGATTGTACCA	HA0913	ATAGGTCGTAGGGCTTAATTGAACCAATCA	HA0995	CTCATAGTTGAATTTCTTAAACAGTACAGAGG
HA0832	AATTGTAACGTAAAACTAGCATGAATAAAG	HA0914	TGAGAAGACAACGCCAACATGTAAAATATCCC	HA0996	CGTCTTTATTGTATCGGTTTATTGAGGAAG
HA0833	AAGCCCCAAAAACAGGCGGTTGATAATCAGAA	HA0915	GAAAACATTTTCGAGCCAGTAATACAACAATA	HA0997	TGTATGGGCTCCAAAAAAAGGCTGTAATGCC
HA0834	ACAGGGCGCGTACTAGCTTAATGCGCCGCT	HA0916	CGCTATTCGACAAAAGGTAAAGTGTTCAGC	HA0998	GTTTCAGCTTGCGAATAATAATTTCGAAAGAG
HA0835	ACGTGCTTGTCACGCTGCGCGTAACCACCACA	HA0917	ACCAAAATAATAACCTTGCTTCTGTCAATATA	HA0999	TTAGCGTCTCATAGCCCCCTTATTAGGAGGTT
HA0836	GCTAAACAAGCGGGCGCTAGGGCGCTGGCAAG	HA0918	CATAACCCGAACCGGATATTCATTCTTTGAAA	HA1000	GTAATCAGTTCATAATCAAAATCAAACCACCA
HA0837	GACAGGAATGGCGAGAAAGGAAGGGAAGAAA	HA0919	GGAATTACCAAAGCTGCTCATTCCGGTCAA	HA1001	CGTCACCCACCGGAACCGCCTCTCAGAGCC
HA0838	GTTTTTATGTCTATCACTTGACGGGGAAAGCC	HA0920	ATTCAACTCCTGACGAGAAACACCCCTCCATGT	HA1002	CAGGGATACATTACCATTAGCAAGAAATCACC
HA0839	AGAGICIGCGIGGACICCAACGICAAAGGGCG	HA0921	AGATTCATTTGGGCTTGAGATGGTCCTGATAA	HA1003	CCGCCACCGGTTGATATAAGTATAGAGGCTGA
HA0840		HA0922		HA1004	GGTTTAGTACCGCCATCACCGTACTCAGGA
HAU641		HA0925		HA1005	CCATCHTAGCGACAGAATCAATATTCAT
HA0842		HA0924		HA1000	
HA0844		HA0925		HA1008	
HA0845	AGAGATCTAGGAACGCCATCAAAAATAATTC	HA0927	GTTATACATIGGGTTATATAACTGCTTTGA	HA1009	TCGAGAGCTCAGAGCCACCACCCCCATGTA
HA0846	GAGAGTCTTTTGTTAAATCAGCTCATTTTT	HA0928	GCTCAACATGAGAGACTACCTTTTAGGCGAAT	HA1010	TAGGTGTACCCTCAGAACCGCCACAGTACAAA
HA0847	ACGGTAATACGTTAATATTTTGTTAAAATTCG	HA0929	ATATTTAAGTCAATAGTGAATTTAAAAGAAGA	HA1011	GAGGCAGGTAAATCCTCATTAAAGCCAGAAT
HA0848	ATGTACCCAAGATTGTATAAGCAAATATTTA	HA0930	AGAGGCATAGCGATAGCTTAGATAAAATTA	HA1012	CCAGAGCCCAGTCTCTGAATTTACCGTTCCAG
HA0849	GATAGCCCACCAGCAGAAGATATCAAAAT	HA0931	TAAAGTACAATTAATTTTCCCTTAATTACCTT	HA1013	ACCACCCATACATGGCTTTTGATGATACAG
HA0850	TGAATGGGGTCAGTATTAACACTCTGAATA	HA0932	TCCAGACGGGCTGACCTTCATCAAACCAGGCG	HA1014	GGTTTTGCCTCAGAACCGCCACCCCCTCAGAG
HA0851	AGCGTAAGACGCTGAGAGCCAGCAATCAATAT	HA0933	TTGACAATCGTTTACCAGACGAAAAAGAAG	HA1015	GACTCCTCGAGTAACAGTGCCCGTATAAACAG
HA0852	GCCAACAGAAAGCATCACCTTGCTCATATTCC	HA0934	CAACGTAAGAGGCATAGTAAGAGCAAATGTTT	HA1016	AACCTATTATTCTGACCCTGCCTATTTCGG
HA0853	TCACACGACCCTCAATCAATATAAGAAACC	HA0935	AGGCTTGCAATGCAGATACATAACCGGAATCG	HA1017	GATATTCACAAACAAATCAGACGATTGGCCTT
HA0854	AAATGGATTCAACAGTTGAAAGGAAAGTTTGA	HA0936	TAGTAAACAGTTGAGATTTAGGTCAAATGC	HA1018	GGAAAGCGGCCGCCAGCATTGACAGCGTTT
HA0855	AAATACCTCTAAAATATCTTTAGGAAATCCTT	HA0937	AACTTTAAGGAACAACATTATTACATGACCAT	HA1019	TAAGCGTCTCAGAGCCGCCACCAGCCGGAACC
HA0856	CCAGCCAAGATTAGAGCCGTCAAGACTTTA	HA0938	TTTTAAGAAGAAAAATCTACGTTACTGACTAT	HA1020	GAGTGTACTGGTAATAAGTTTTAACGGGGTCA
HA0857	GGGTGAGAGTAATATCCAGAACAAACTATCGG	HA0939	ATCAGATAGAGGCGTTTTAGCGAAAAAAGAAC	HA1021	GTGCCTTAAGAGAAGGATTAGGAAGTGCCG
HA0858		HA0940	AGGAAICAGGIIIIGAAGCCIIACCGAGGA	HA1022	
HA0859		HA0941		HA1056	
HA0860		HA0942		141057	
HAU601		HA0945		HA1057	
HA0863		HA0945	GATAAGTCGATTTTTGTTTAACGCAGAGGGGT	HA1058	
HA0864	AAAAATACCGAACGATAAAAACATCGCCATT	HA0946	TAATGCACAGCCTTTACAGAGAGGGAGAAT	1011050	AGTGAGCGAGAGGCTTTTGCCGATAAAA
HA0865	GGTGAGGCCTATTAGTCTTTAATGCACGTATA	HA0947	CATAGGCTACGACAATAAACAACATAATTCTG	HA1060	ΑΑΑΑΑΑΑΑΑΑΑΑΑΑΑΑΑΑΑΑΑΑΑΑΑΑΑΑΑΑ
HA0866	ACAGTGCCAATACGTGGCACAGACGAGCGGGA	HA0948	GAGGACAGTCACCCTCAGCAGCGAACAACCAT		TAAGACGCTGAGAGCCAGCAATCAATAT
HA0867	AAAAATCTAGATAGAACCCTTCTGATTTTA	HA0949	TCATAAGGGAGGGTAGCAACGGCCTTGATA	HA1061	ΑΑΑΑΑΑΑΑΑΑΑΑΑΑΑΑΑΑΑΑΑΑΑΑΑΑΑΑΑΑ
HA0868	AATATCAAACCAGTAATAAAAGGGTGAGAAGT	HA0950	TACTTAGCACTAAAGACTTTTTCACAGCTTGC		AATATTGTTTGGATTATACTCGCCTGCA
HA0869	TTGGCAAATATTTACATTGGCAGACGAGTAAA	HA0951	ATTGTGTCTAAACGGGTAAAATACCCAAAAGG	HA1062	ΑΑΑΑΑΑΑΑΑΑΑΑΑΑΑΑΑΑΑΑΑΑΑΑΑΑΑΑΑΑΑΑΑΑΑΑΑΑΑ
HA0870	AAGGTTATACATTTTGACGCTCAACCGTTG	HA0952	GTACAACGGGCACCAACCTAAAATTTCACG		CAAGAGATGATGGCAATTCGCAAATG
HA0871	CAACTAATTTGCAACAGGAAAAACTAACATCA	HA0953	ATCTTTGACCCCCAGCATACACTAAAACACTC	HA1063	ΑΑΑΑΑΑΑΑΑΑΑΑΑΑΑΑΑΑΑΑΑΑΑΑΑΑΑΑΑΑΑΑΑΑ
HA0872	TACATTTGATGCAACTAAAGTACGTCAACATG	HA0954	GTATTCTAAGAACGCTAGAAGGCTTATCCG		CATTATATTTCATTTGGGGAGCGAACC
HA0873	AAGTTTCTAATGTGTAGGTAAAGAAATCACC	HA0955	CTTGCGGGATTACCGCGCCCAATAAATAAGGC	HA1064	
HAU8/4		HA0956		HA1065	
HAU8/5				LAT002	
11AU670	THAGCIATGACCETGTAATACCATTGCCT	11AU936	CITICLAGGUIGICITICUTATCAAGULAAU		CAAATTAATTCGAGCTTCAACGCGAGCT

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