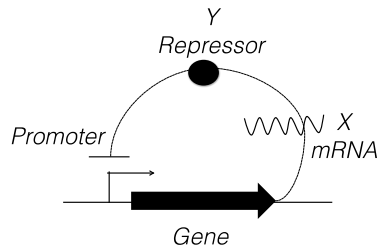


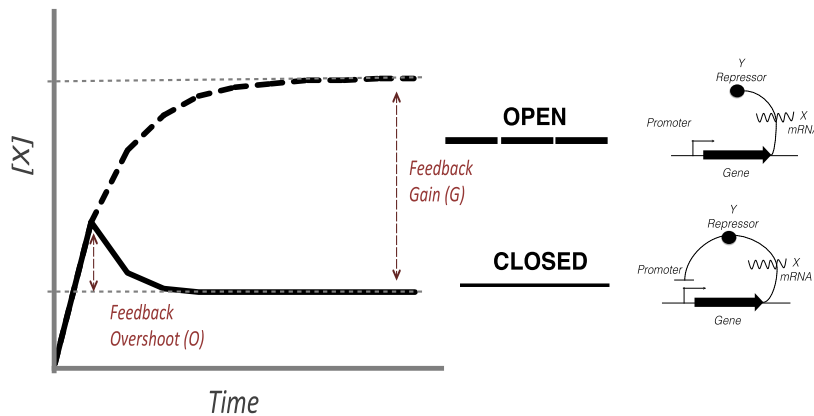
Supporting Text S1- Calculations for the Feedback Gain & Overshoot.

Feedback Gain

Suppose a simple feedback system consisting of an mRNA molecule (X) that encodes a transcriptional repressor (Y), able to repress transcription from its own promoter.



Let G be the feedback gain, defined as the ratio between the steady-states of the negative feedback (X_{fb}) and the open loop (X_0).



The dynamics of the negative feedback follow

$$\begin{cases} \frac{dx}{dt} = \frac{\lambda_1 k^n}{k^n + (y_t)^n} - \beta_1 x_t \\ \frac{dy}{dt} = \lambda_2 x_t - \beta_2 y_t \end{cases}$$

Eq 1.

Where x is the RNA concentration, Y is the protein concentration, λ stands for production rates, β represents degradation/dilution rates, k is the feedback constant, and n is the cooperativity of the system (non-linearity of the feedback). In these condition the steady-state of the system is

$$\begin{cases} \frac{dx}{dt} = \frac{\lambda_1 k^n}{k^n + (y_t)^n} - \beta_1 x_t = 0 \\ \frac{dy}{dt} = \lambda_2 x_t - \beta_2 y_t = 0 \end{cases}$$

In order to simplify the calculations we replace $k^n = K$ and the steady-state for strong repression ($K + y_{ss} \approx y_{ss}$) for X follows

$$X_{fb} = \left(\frac{\lambda_1 K}{\beta_1} \right)^{\frac{1}{n+1}} \left(\frac{\beta_2}{\lambda_2} \right)^{\frac{n}{n+1}}$$

Eq 2.

Similarly the equations for the open loop

$$\begin{cases} \frac{dx}{dt} = \lambda_1 - \beta_1 x_t \\ \frac{dy}{dt} = \lambda_2 x_t - \beta_2 y_t \end{cases}$$

Eq 3.

yield in steady-state

$$X_0 = \frac{\lambda_1}{\beta_1}$$

Therefore the feedback gain equals

$$\begin{aligned} G &= \frac{X_o}{X_{fb}} = \left(\frac{\lambda_1 \lambda_2}{\beta_1 \beta_2} \right)^{\frac{n}{n+1}} \left(\frac{1}{K} \right)^{\frac{1}{n+1}} = \left(\frac{\lambda_1 \lambda_2}{\beta_1 \beta_2 k} \right)^{\frac{n}{n+1}} \\ G &= \left(\frac{\lambda_1 \lambda_2}{\beta_1 \beta_2 k} \right)^{\frac{n}{n+1}} \end{aligned}$$

Eq 4.

This expressions yields the following limits:

$$\text{Lim}_{k \rightarrow 0} \left(\frac{X_o}{X_{fb}} = \left(\frac{\lambda_1 \lambda_2}{\beta_1 \beta_2} \right)^{\frac{n}{n+1}} \left(\frac{1}{K} \right)^{\frac{1}{n+1}} \right) = \text{Lim}_{k \rightarrow 0} \left(\frac{X_o}{X_{fb}} = \left(\frac{\lambda_1 \lambda_2}{\beta_1 \beta_2} \right)^{\frac{n}{n+1}} \left(\frac{1}{k^n} \right)^{\frac{1}{n+1}} \right) = \text{Lim}_{k \rightarrow 0} \left(\frac{X_o}{X_{fb}} = \left(\frac{\lambda_1 \lambda_2}{\beta_1 \beta_2 k} \right)^{\frac{n}{n+1}} \right) = \infty$$

Eq 5.

$$\text{Lim}_{n \rightarrow \infty} \left(\frac{X_o}{X_{fb}} = \left(\frac{\lambda_1 \lambda_2}{\beta_1 \beta_2} \right)^{\frac{n}{n+1}} \left(\frac{1}{K} \right)^{\frac{1}{n+1}} \right) = \text{Lim}_{n \rightarrow \infty} \left(\frac{\lambda_1 \lambda_2}{\beta_1 \beta_2} \right)^{\frac{n}{n+1}} \left(\frac{1}{k^n} \right)^{\frac{1}{n+1}} = \text{Lim}_{n \rightarrow \infty} \left(\frac{\lambda_1 \lambda_2}{\beta_1 \beta_2 k} \right)^{\frac{n}{n+1}} = \left(\frac{\lambda_1 \lambda_2}{\beta_1 \beta_2 k} \right)^1 = \frac{\lambda_1 \lambda_2}{\beta_1 \beta_2 k}$$

Eq 6.

This indicates that while decreasing k (increasing the affinity of the repressor for its cognate site) increases indefinitely the feedback gain, increasing n reaches a limit gain that equals the intrinsic promoter strength $\left(\frac{\lambda_1 \lambda_2}{\beta_1 \beta_2} \right)$ times the inverse of the half-repression constant (k).

The gain in y is calculated in the same way, yielding

$$G = \frac{y_o}{y_{fb}} = \left(\frac{\lambda_1 \lambda_2}{\beta_1 \beta_2} \right)^{\frac{n}{n+1}} \left(\frac{1}{K} \right)^{\frac{1}{n+1}} = \left(\frac{\lambda_1 \lambda_2}{\beta_1 \beta_2 k} \right)^{\frac{n}{n+1}}$$

$$G = \frac{y_o}{y_{fb}} = \left(\frac{\lambda_1 \lambda_2}{\beta_1 \beta_2 k} \right)^{\frac{n}{n+1}}$$

Which indicates that the feedback gain is equivalent for values of x and y

Feedback Overshoot existence

System of Ec. 1 produces a transient overshoot whenever x and y reach a maximum that is higher than the steady state value. A max. in x is reached iif

$$x' = \frac{dx}{dt} = 0 \text{ and } x'' = \frac{d^2x}{dt^2} < 0$$

$$\frac{dx}{dt} = \frac{\lambda_1 K}{K + (y_i)^n} - \beta_1 x_{\max} = 0$$

$$x_{\max} = \frac{\lambda_1 K}{\beta_1 (K + (y_i)^n)} - \frac{x'}{\beta_1} = \frac{\lambda_1 K}{\beta_1 (K + (y_i)^n)}$$

$$x'' = \lambda_1 K \frac{0 - n y^{n-1} y'}{(K + y^n)^2} = \lambda_1 K \frac{-n y^{n-1} y'}{(K + y^n)^2}$$

$$x'' = \lambda_1 K \frac{-n}{y^{n+1}} y' < 0$$

$-n < 0$ since there cannot be negative cooperativity

$y^{n+1} > 0$ since y cannot take negative values

$\lambda_1 K$ are always positive

$$\text{then } x'' < 0 \iff y' > 0$$

From this follows that y at $x = x_{\max}$ y is always smaller than its steady state value

$$y' = \lambda_2 x - \beta_2 y$$

$$y' = \lambda_2 x - \beta_2 y_{x_{\max}}$$

$$\frac{\lambda_1 \lambda_2 K}{\beta_1 \beta} > y_{x_{\max}}^{n+1}$$

$$\text{Since } y_{ss} = \left(\frac{\lambda_1 \lambda_2 K}{\beta_1 \beta} \right)^{\frac{1}{n+1}}$$

$$\left(\frac{\lambda_1 \lambda_2 K}{\beta_1 \beta} \right)^{\frac{1}{n+1}} > y_{x_{\max}}$$

$$y_{ss} > y_{x_{\max}}$$

Equivalent reasoning yields that $x' < 0$ at $y = y_{\max}$ and $x_{ss} < x_{y_{\max}}$

Gain-Overshoot relationship

The overshoot (O) is the ratio between the maximal value of X or Y and its steady-state value. In the case of an RNA

$$O = \frac{X_{\max}}{X_{ss}} = \frac{X_{\max}}{\left(\frac{\lambda_1 K}{\beta_1} \right)^{\frac{1}{n+1}} \left(\frac{\beta_2}{\lambda_2} \right)^{\frac{n}{n+1}}} = \frac{X_{\max}}{\left(\frac{\lambda_1}{\beta_1} \right)^{\frac{1}{n+1}} \left(\frac{\beta_2}{\lambda_2} k \right)^{\frac{n}{n+1}}} \quad \text{Eq.7}$$

The highly non-linear nature of the ODE system prevents the calculation of X_{\max} , but in the case of strong self-repression ($k+y \approx y$) and high cooperativity we can linearize the system, approximating X_{\max} to the equivalent

value for the open loop when $t = t_{x_{\max}}$

$$\frac{dx}{dt} = \lambda_1 - \beta_1 x_t \text{ from } t=0 \rightarrow t = t_{x=x_{\max}}$$

$$\frac{dx}{dt} = \frac{\lambda_1 K}{K + (y_t)^n} - \beta_1 x_t \text{ from } t = t_{x=x_{\max}} \rightarrow t = \infty$$

This allows direct integration of X_{\max}

$$\int \frac{dx}{dt} dt = \int_0^{t=t_{x=x_{\max}}} (\lambda_1 - \beta_1 x_t) dt = \frac{\lambda_1}{\beta_1} (1 - e^{-\beta_1 t_{x=x_{\max}}})$$

This approximation holds for highly-nonlinear systems, where the high cooperativity index (n) acts as an effective delay between the accumulation of the repressor (y) and the onset of repression. Therefore

$$O_x = \frac{X_{\max}}{X_{SS}} \approx \frac{\frac{\lambda_1}{\beta_1} (1 - e^{-\beta_1 t_{x=x_{\max}}})}{\left(\frac{\lambda_1 K}{\beta_1}\right)^{\frac{1}{n+1}} \left(\frac{\beta_2}{\lambda_2}\right)^{\frac{n}{n+1}}} = \left(\frac{\lambda_1 \lambda_2}{\beta_1 \beta_2}\right)^{\frac{n}{n+1}} \left(\frac{1}{K}\right)^{\frac{1}{n+1}} (1 - e^{-\beta_1 t_{x=x_{\max}}})$$

$$O_x \approx (1 - e^{-\beta_1 t_{x=x_{\max}}}) G$$

To calculate the overshoot for y we follow the same reasoning. Linearizing x until the onset of the negative feedback, we can approximate the value of Y_{\max}

$$O_x = \frac{Y_{\max}}{Y_{SS}}$$

$$\frac{dy}{dt} = \lambda_2 x_t - \beta_2 y_t \text{ and } x_t \approx \frac{\lambda_1}{\beta_1} (1 - e^{-\beta_1 t})$$

$$\frac{dy}{dt} \approx \frac{\lambda_1 \lambda_2}{\beta_1} (1 - e^{-\beta_1 t_{x=x_{\max}}}) - \beta_2 y_t$$

$$O_y \approx \left(\left(\frac{\lambda_1 \lambda_2}{\beta_1 \beta_2}\right)^{\frac{n}{n+1}} \left(\frac{1}{K}\right)^{\frac{1}{n+1}} \right) \left(\frac{\beta_1 (1 - e^{-\beta_1 t}) - \beta_2 (1 - e^{-\beta_2 t})}{\beta_1 - \beta_2} \right)$$

$$O_y \approx \left(\frac{\beta_1 (1 - e^{-\beta_1 t}) - \beta_2 (1 - e^{-\beta_2 t})}{\beta_1 - \beta_2} \right) G$$

This indicates that the $O_y \neq O_x$, and

$$O_y = O_x \left(\frac{\beta_1 - \beta_2 \frac{(1 - e^{-\beta_2 t})}{(1 - e^{-\beta_1 t})}}{\beta_1 - \beta_2} \right)$$

Simulations indicate that these approximation holds for highly-nonlinear systems (Figure 4, main text). This condition can be met by systems where the repressor exhibits high cooperativity to its cognate binding site or where the repressor dimer/multimerization is required for binding.

Effect of multimerization

The following system includes a step of repressor dimerization

$$(k^n = K)$$

$$\frac{dx}{dt} = \frac{\lambda_1 K}{K + (z_t)^n} - \beta_1 x_t$$

$$\frac{dy}{dt} = \lambda_2 x_t - \beta_2 y_t$$

$$\frac{dz}{dt} = c_a y - c_d z$$

And in steady-state

$$\frac{dz}{dt} = c_a y - c_d z$$

$$z = \frac{c_a}{c_d} y$$

Therefore

$$\frac{dx}{dt} = \frac{\lambda_1 K}{K + (z_{ss})^n} - \beta_1 x_{ss} = \frac{\lambda_1 K}{K + \left(\frac{c_a}{c_d} y_{ss}\right)^n} - \beta_1 x_{ss} = 0$$

This indicates that at steady state the dimer system is formally identical to the monomeric system with the only difference of c_a/c_d multiplying y , which reflects the steady-state of the dimerization dynamics. Similarly, the gain in the dimer system can be expressed as

$$G = \frac{X_o}{X_{fb}} = \left(\frac{\lambda_1 \lambda_2 \frac{c_a}{c_d}}{\beta_1 \beta_2 k} \right)^{\frac{n}{n+1}}$$